



Challenges for Solar Distribution Planning and Operations Workshop

AGENT-BASED COORDINATION SCHEME FOR PV INTEGRATION (ABC4PV)

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Overview

- ABC4PV main idea and objectives
- Focusing on Consensus+Innovation (C+I) framework
- What was the case for C+I before ABC4PV
- What was achieved for C+I through the ABC4PV



NRECA

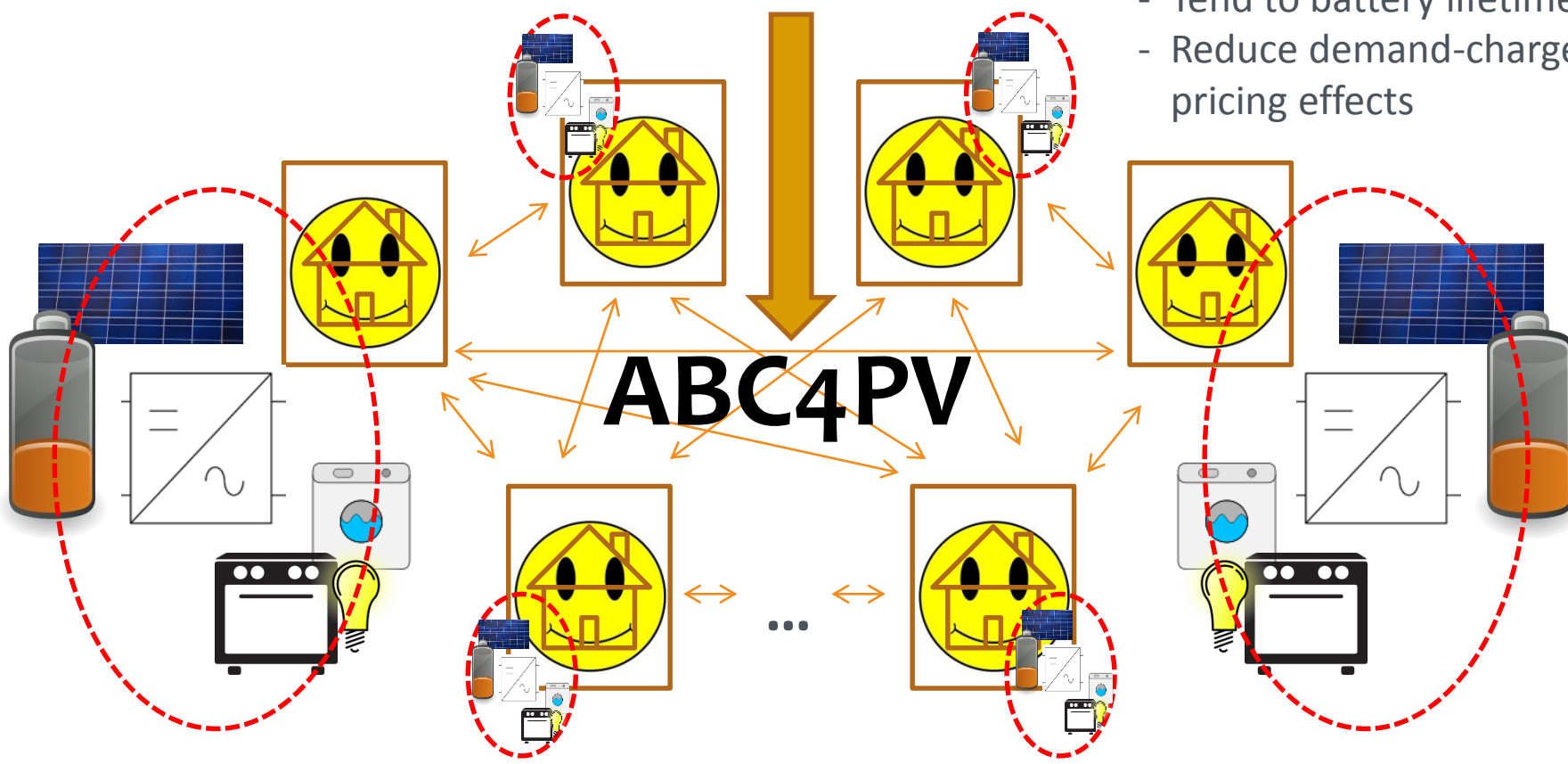
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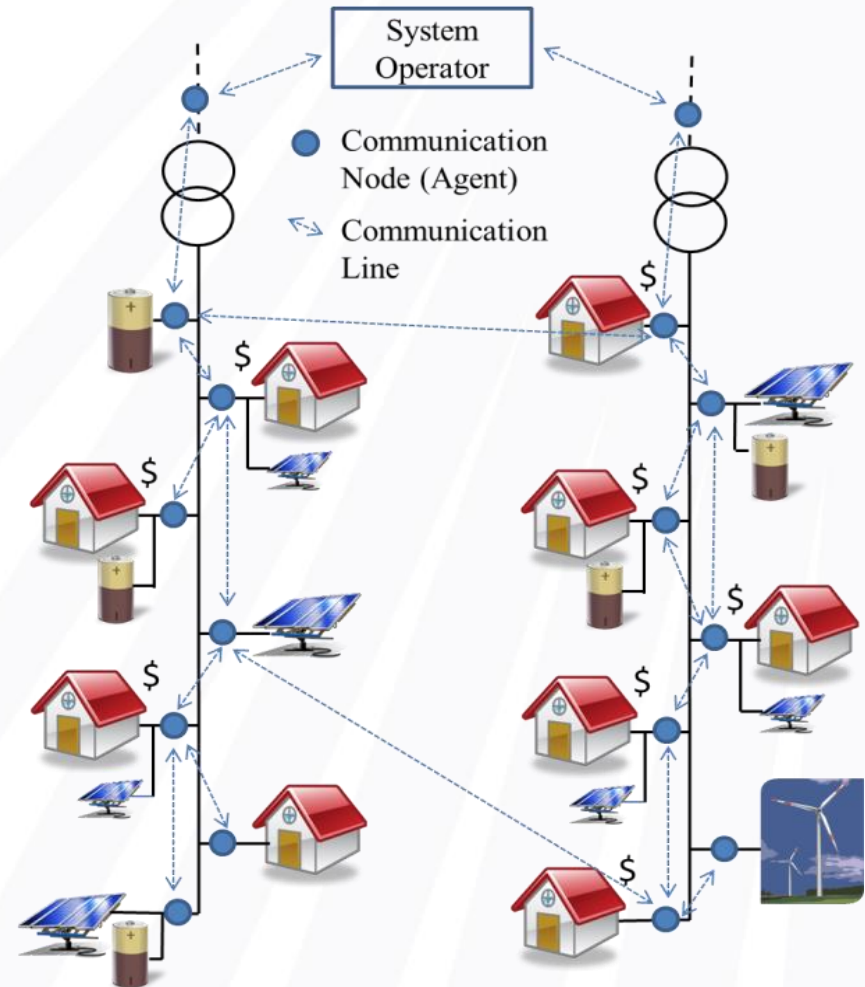
Roadmap Approach:

- Explore exchanges potential
- Coordinate at scales
- Tend to battery lifetime
- Reduce demand-charge pricing effects



Approach: Inter-unit collaboration

- Agent-based distributed algorithm:
 - Units communicate and share information
 - Communication with system operator possible, not required
 - Computations carried out locally



Approach: Distributed optimization framework

- Form of updates (based on the Lagrangian multipliers and slack vars)
 - Mathematical formulation based on consensus + innovation approach:

$$\lambda_j^{(i+1)} = \lambda_j^{(i)} - \underbrace{\beta_i \sum_{l \in \omega_j} (\lambda_j^{(i)} - \lambda_l^{(i)})}_{\text{consensus}} - \underbrace{\alpha_i \hat{d}_j^{(i)}}_{\text{innovation}}$$

where λ is the consensus variable and innovation term ensures

$$\sum_{j=1}^J \hat{d}_j(\lambda_j) = 0,$$

Considered Application:

- Consensus ensures cost optimality
- Innovation fulfills power balance & equipment constraints

➡ Low computational effort required

What is Consensus?

- Think of Gossip, but reliable...
- Gossip = exchange of info at small scale of interaction
- Reliable = minimum info exchange
- Required to agree on a common value across stakeholders, e.g. marginal price of generation

Example:

20 players are dealt each one card from a 21-cards deck.
Which card wasn't dealt to any of the players?

Why do we need Innovation?

- Innovation terms are the derivatives of the Lagrangian with respect to the updated variable
- Unless they become constant, there is no convergence
- All updates include innovation terms, but not all include consensus term

ABC4PV problem formulation

$$\text{minimize } \sum_{i \in g} C(P_{g,i})$$

$$\text{s.t. } P_{g,i} - P_{l,i} = \sum_{j \in NBi} (g_{ij} - b_{ij}) \cdot (\theta_i - \theta_j)$$

$$Q_{g,i} - Q_{l,i} = \sum_{j \in NBi} \left[(\theta_i - \theta_j) \cdot \left(\frac{g_{ij}^2}{b_{ij}} - g_{ij} \right) + \frac{|v_i|}{b_{ij}} (-g_{ij}^2 - b_{ij}^2) + \frac{|v_j|}{b_{ij}} \cdot (g_{ij}^2 + b_{ij}^2) \right]$$

$$P_{g,i,m} \leq P_{g,i} \leq P_{g,i,M} \quad \& \quad Q_{g,i,m} \leq Q_{g,i} \leq Q_{g,i,M}$$

$$|v_{i,m}| \leq |v_i| \leq |v_{i,M}|$$

$$(g_{ij} - b_{ij})^2 \cdot (\theta_i - \theta_j)^2 + \left[(\theta_i - \theta_j) \cdot \left(\frac{g_{ij}^2}{b_{ij}} - g_{ij} \right) + \frac{|v_i|}{b_{ij}} (-g_{ij}^2 - b_{ij}^2) + \frac{|v_j|}{b_{ij}} \cdot (g_{ij}^2 + b_{ij}^2) \right]^2 \leq S_{ij,M}^2 *$$

*can be easily expressed linearly

COPF approximation formulation in the C+I f/w (1/2)

$$\begin{aligned}
 L = & \sum_{i \in g} C(P_{g,i}) + \sum_{i \in B} \lambda_i \cdot \left[-P_{g,i} + P_{l,i} + \sum_{j \in NBi} (g_{ij} - b_{ij}) \cdot (\theta_i - \theta_j) \right] + \\
 & + \sum_{i \in g} \mu_i \cdot \left\{ -Q_{g,i} + Q_{l,i} + \sum_{j \in NBi} \left[(\theta_i - \theta_j) \cdot \left(\frac{g_{ij}^2}{b_{ij}} - g_{ij} \right) + \frac{|v_i|}{b_{ij}} (-g_{ij}^2 - b_{ij}^2) + \frac{|v_j|}{b_{ij}} (g_{ij}^2 + b_{ij}^2) \right] \right\} + \\
 & + \sum_{i \in g} u_{P,i} \cdot (P_{g,i} - P_{g,i,M} + T_{P,i}^2) + \sum_{i \in g} l_{P,i} \cdot (-P_{g,i} + P_{g,i,m} + K_{P,i}^2) + \\
 & + \sum_{i \in g} u_{Q,i} \cdot (Q_{g,i} - Q_{g,i,M} + T_{Q,i}^2) + \sum_{i \in g} l_{Q,i} \cdot (-Q_{g,i} + Q_{g,i,m} + K_{Q,i}^2) + \\
 & + \sum_{i \in B} u_{V,i} \cdot (V_i - V_{i,M} + T_{V,i}^2) + \sum_{i \in B} l_{V,i} \cdot (-V_i + V_{i,m} + K_{V,i}^2) + \\
 & + \sum_{i \in B} \sum_{j \in NBi} u_{ln,ij} \left\{ (g_{ij} - b_{ij})^2 \cdot (\theta_i - \theta_j)^2 + \right. \\
 & \left. + \left[(\theta_i - \theta_j) \cdot \left(\frac{g_{ij}^2}{b_{ij}} - g_{ij} \right) + \frac{|v_i|}{b_{ij}} (-g_{ij}^2 - b_{ij}^2) + \frac{|v_j|}{b_{ij}} (g_{ij}^2 + b_{ij}^2) \right]^2 - S_{ij,M}^2 + T_{l,ij}^2 \right\}
 \end{aligned}$$

COPF approximation formulation in the C+I f/w (2/2)

$$\lambda_i(k+1) = \lambda_i(k) - \beta_\lambda \frac{\partial L}{\partial \theta_i} - \alpha_\lambda \frac{\partial L}{\partial \lambda_i}$$

$$\mu_i(k+1) = \mu_i(k) - \beta_\mu \frac{\partial L}{\partial |v_i|} - \alpha_\mu \frac{\partial L}{\partial \mu_i}$$

$$\theta_i(k+1) = \theta_i(k) + \beta_\theta \frac{\partial L}{\partial \lambda_i}$$

$$|v_i(k+1)| = \text{P} \left(|v_i(k)| + \beta_V \frac{\partial L}{\partial \mu_i} \right)$$

$$P_{g,i}(k+1) = \text{P} \left(P_{g,i}(k) - \alpha_P \cdot \left(\frac{\partial C(P_{g,i})}{\partial P_{g,i}} - \lambda_i(k+1) \right) \right) = \text{P} \left(P_{g,i}(k) - \alpha_P \cdot (2 \cdot a_g \cdot P_{g,i} + b_g - \lambda_i(k+1)) \right)$$

$$Q_{g,i}(k+1) = \text{P} (Q_{g,i}(k) + \alpha_Q \cdot \mu_i(k+1))$$

$$u_{|v|,i}(k+1) = \text{P} \left(u_{|v|,i}(k) + \beta_{|v|} (|v_i| - |v_{i,M}|) \right) \quad l_{|v|,i}(k+1) = \text{P} \left(l_{|v|,i}(k) + \beta_{|v|} (-|v_i| + |v_{i,m}|) \right)$$

$$u_{\ln,ij}(k+1) = \text{P} \left(u_{\ln,ij}(k) + \beta_{\ln} \frac{\partial L}{\partial u_{\ln,ij}} \right)$$

Proof of convergence of the C+I – Why?

- Ensures that a control set-point exists under ALL operating conditions
- If the control set-point is fixed, there is insight about the nature of the fixed point => Optimal in our case
- Convergence affects the cyber-security assessment of the tool
- Before the ABC4PV, convergence was proved only for the unconstrained DC OPF formulation... The one at hand is an “alternative” of the decoupled OPF

Proof of convergence of the ABC4PV C+I (1/2)

- Iteration Matrix (excl. ineq. constr.) $G_{itr} = \begin{bmatrix} \lambda_1 & \lambda_2 & 0 & \lambda_3 & \lambda_4 & 0 \\ 0 & \mu_1 & \mu_2 & \mu_3 & 0 & \mu_4 \\ 0 & 0 & v_1 & v_2 & 0 & v_3 \\ 0 & 0 & 0 & \theta_1 & \theta_2 & 0 \\ p_1 & 0 & 0 & 0 & p_2 & 0 \\ 0 & q_1 & 0 & 0 & 0 & q_2 \end{bmatrix}$
- P and Q are monotonic sequences $\Rightarrow \begin{bmatrix} \lambda_1 & \lambda_2 & 0 & 0 \\ 0 & \mu_1 & \mu_2 & \mu_3 \\ 0 & 0 & v_1 & v_2 \\ 0 & 0 & 0 & \theta_1 \end{bmatrix}$
- Convergence conditions ($\rho < 1$) properly met
- Updates of the power quality & line limit constraints

$$u_{|v|,i}(k+1) = \mathbb{P}\left(u_{|v|,i}(k) + \beta_{|v|}(|v_i| - |v_{i,M}|)\right)$$

i.e. persistent unitary eigenvalues (non-convergent in this context)

Proof of convergence of the ABC4PV C+I (2/2)

- Rewriting the updates in the lagrangian form

$$u_{|v|,i}(k+1) = \mathbb{P} \left(u_{|v|,i}(k) + \beta_{|v|} \frac{\partial L}{\partial u_{|v|,i}} \right)$$

- Of the gradient descent form
- Convergent to a fixed point if properly bounded

QED.

Improving Rate of ABC4PV COPF Convergence - Heuristic

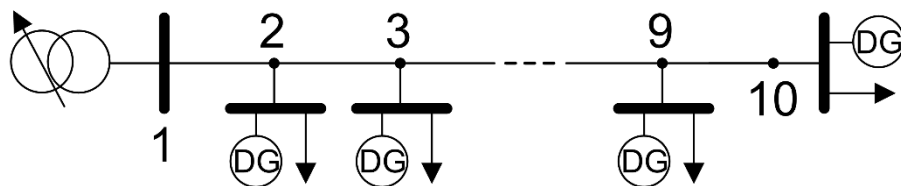
- Algorithm:

(for the part of the iteration matrix with non-unitary eigenvalues)

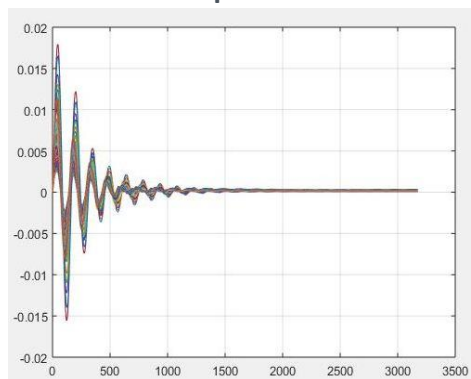
$$G_{itop} = \begin{bmatrix} \lambda_1 & \lambda_2 & 0 & \lambda_3 & \lambda_4 \\ 0 & \mu_1 & \mu_2 & \mu_3 & 0 \\ 0 & 0 & \nu_1 & \nu_2 & 0 \\ 0 & 0 & 0 & \theta_1 & \theta_2 \\ p_1 & 0 & 0 & 0 & p_2 \end{bmatrix}$$

- Step 1: for all α_x & β_x determine min/max value for convergence
- Step 2: for all α_x β_x exhaustively explore between min/max values of convergence
- Step 3: for all α_x β_x not in G_{itop} , set minimum α_x β_x from Step 2

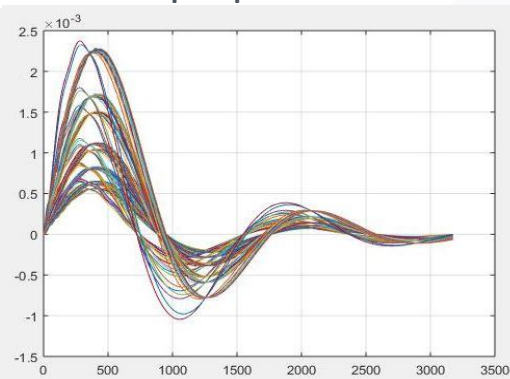
Rate of Convergence Assessment (10-bus system)



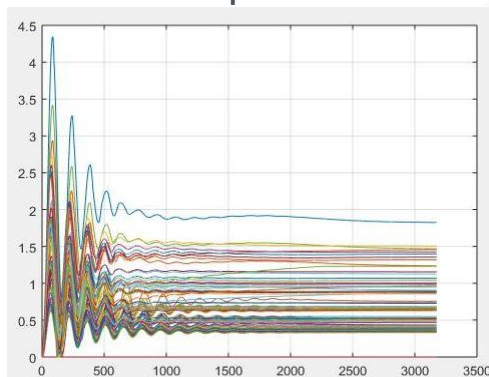
λ updates



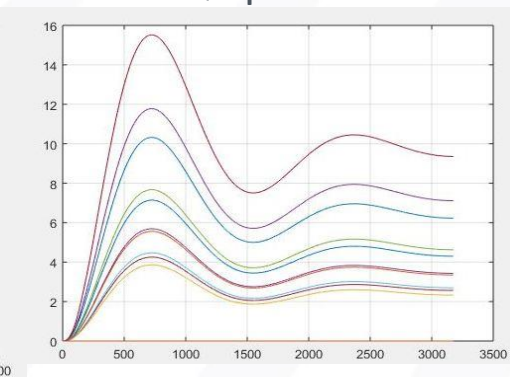
μ updates



P updates



Q updates



Bus	$P_{load,n}$ (kW)	$P_{DG,n}$ (kW)	BusK	BusL	Type	Length (m)
2	500	130	1	2	ACSR-95	1000
3	200	50	2	3	ACSR-95	5000
4	500	130	3	4	ACSR-95	1000
5	300	75	4	5	ACSR-95	500
6	100	25	5	6	ACSR-95	1000
7	200	50	6	7	ACSR-95	500
8	300	75	7	8	ACSR-95	1000
9	500	130	8	9	ACSR-95	500
10	200	50	9	10	ACSR-95	1000

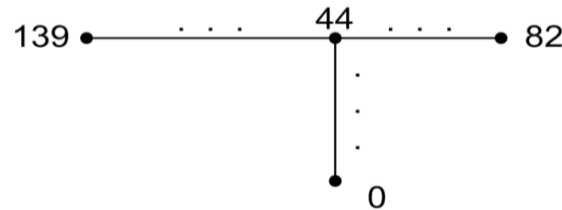
DG f/c Error Intl	Convergence time (s)
$\pm 10\%$	0.9688 ± 0.9588
$\pm 20\%$	0.8954 ± 0.4638
$\pm 30\%$	1.2313 ± 0.5601
$\pm 40\%$	1.3811 ± 0.4382
$\pm 50\%$	1.5283 ± 0.5044

Load f/c Error Intl	Convergence time (s)
$\pm 10\%$	0.9792 ± 0.4318
$\pm 20\%$	1.5562 ± 0.6775

No DG units w/ random	Convergence time (s)
3	0.0245 ± 0.0134
6	0.0456 ± 0.0228
12	0.0300 ± 0.0156
24	0.0048 ± 0.0077
48	0.3344 ± 0.3068
96	1.1879 ± 0.4956
192	2.0577 ± 1.0573

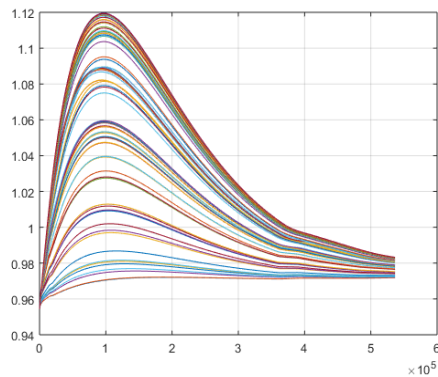
No of loads w/ random	Convergence time (s)
3	0.4234 ± 0.0760
6	0.6920 ± 0.0641
12	1.0727 ± 0.0510
24	1.5146 ± 0.0855
48	2.3048 ± 0.5754

Rate of Convergence Assessment (Ikaria R-21 feeder)

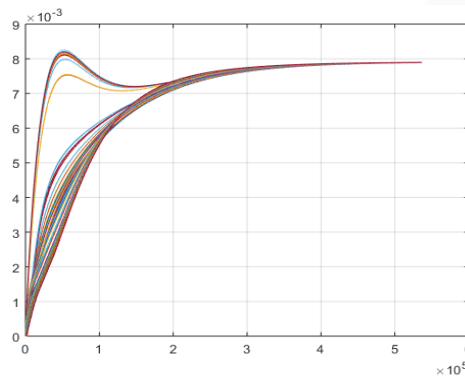


55 load/DG buses

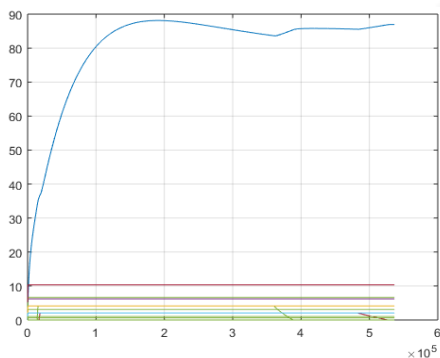
λ updates



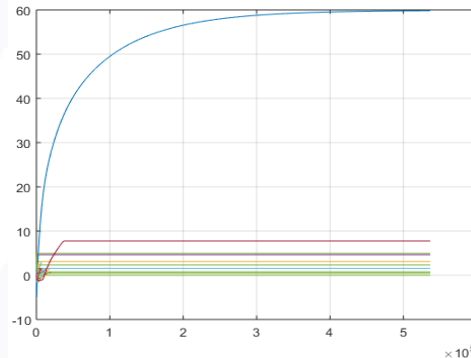
μ updates



P updates



Q updates



DG f/c Error Intl	Convergence time (s)	Load f/c Error Intl	Convergence time (s)
$\pm 10\%$	0.1203 ± 0.0015	$\pm 10\%$	3.3830 ± 7.5155
$\pm 20\%$	2.1362 ± 6.0266		

No DG units w/ random	Convergence time (s)	No of loads w/ random	Convergence time (s)
		3	0.0791 ± 0.1035
3	0.0808 ± 0.0007	6	0.0755 ± 0.0802
6	0.0945 ± 0.0005	12	0.0904 ± 0.0881
12	0.1040 ± 0.0002	24	0.2444 ± 0.5699
24	0.1084 ± 0.0002	48	0.7432 ± 1.9187
48	0.1115 ± 0.0007		
96	0.1620 ± 0.0640		
192	0.7121 ± 1.3419		

Concerns for Path forward

- C+I for convexified formulations?
- Explicit method optimizing acceleration parameters?
- Any concern/thought you would like to add?

Questions?