Appendix T-1 Section 106 Geophysical Survey Review

Section 106 Geophysical Survey Review for Icebreaker Wind

Prepared for:

Icebreaker Windpower Inc.

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1.0 EXECUTIVE SUMMARY

A geophysical survey of a portion of the Lake Erie lakebed was conducted for the Icebreaker Wind project by Canadian Seabed Research Ltd. (CSR) from mid- August to early September 2016 on behalf of Icebreaker Windpower Inc. Icebreaker Wind is a six turbine 20.7 megawatt offshore wind demonstration project 8 to 10 miles off the shore of Cleveland, Ohio. The data from this survey was evaluated according to Section 106 of the National Historic Preservation Act of 1966 (NHPA) requirements. Three (3) areas of potential effects (APE) were assessed:

- Turbine area 4.7 km (2.9 miles) x 0.3 km (0.2 miles). Beginning about 12.9 km (8 miles) from the mouth of the Cuyahoga River, Cleveland, Ohio, Cuyahoga County, at a depth of 17-18 m (56 59 feet). Within this area six (6) wind turbines will be constructed and interconnected with trenched and buried cables at a depth of about 1.5 m (5 feet).
- Export cable area 13.2 km (8.2 miles) x 0.36 km (0.2 miles). Beginning 1.7 km (1.1 miles) west of the end of the east breakwater offshore of Cleveland, Ohio, Cuyahoga County, and running 13.2 km (8.2 miles) to the Turbine area at a water depth of 10-17 m (33 56 feet). Within this area the export cable from the wind turbines to east breakwater will be trenched and buried at a depth of about 1.5 m (5 feet).
- 3. Inner harbor area 0.85 km (0.53 miles) x 0.36 km (0.22 miles). Beginning 1.7 km (1.1 miles) west of the end of the east breakwater offshore of Cleveland, Ohio, Cuyahoga County, and running 0.85 km (0.53 miles) to shore at the CPP power plant at a water depth of 4-10 m (13 33 feet). Note: The export cable route will be horizontally drilled beginning 1.7 km (1.1 miles) west of the end of the east breakwater on the north side, south to the CPP power plant at a minimum depth of 4 m (12 feet) below the foundation of the breakwater.

The geophysical survey was designed to be in compliance with the guidelines developed by the Bureau of Ocean Energy Management (BOEM) set forth in "Guidelines for Providing Archaeological and Historic Property Information Pursuant to 30 CFR Part 585," compliance with which are directed by the Ohio State Historic Preservation Office (SHPO). Results from the geophysical survey confirmed that there were no artifacts or properties of historical significance identified at the Icebreaker Wind's APE that would impact the construction of the Project. Nor was there any evidence from the literature search that any artifacts or properties exist at the proposed sites.

VanZandt Engineering recommends that no further archaeological investigation is warranted for the Icebreaker Wind project areas at this time and that clearance for construction be granted.

This report will be submitted to the Ohio SHPO by the U.S. Department of Energy for Section 106 review.

2.0 INTRODUCTION

David M. VanZandt of VanZandt Engineering carried out the Section 106 assessment of the geophysical survey data collected by Canadian Seabed Research from mid- August to early September 2016 for Icebreaker Wind. The following technical report presents the results of this archaeological assessment undertaken to comply with the Section 106 guidelines and the guidelines established by the Ohio State Historic Preservation Office (SHPO) and the U.S. Department of Energy (DOE).

David M. VanZandt, MMA, RPA was responsible for background research, data analysis and interpretation, and report preparation. Mr. VanZandt is qualified as a professional archaeologist by the Register of Professional Archaeologists (RPA), is on the Ohio SHPO historic archaeologists' consultants list, and a member of the Ohio Archaeology Council.

This report details the Section 106 archaeological assessment of the data acquired during the geophysical underwater remote sensing survey conducted by Canadian Seabed Research Ltd. (CSR) for the Icebreaker Wind demonstration project proposed by Icebreaker Windpower Inc. Icebreaker Wind will be the first freshwater offshore wind project in the Great Lakes and in all of North America. The project has three (3) areas of potential effects. The first APE is the Turbine area. The area is 4.7 km (2.9 miles) long by 0.3 km (0.6 miles) wide, bbeginning about 14 km (8.7 miles) offshore of Cleveland, Ohio, Cuyahoga County, at a depth of 17-18 m (56 - 59 feet). Within this area six 3.45 MW wind turbine generators (WTGs) will be located and interconnected with trenched and buried interconnect cables. The interconnect cables will be buried in an excavated trench 1.5 m (5 feet) wide by 1.5 m (5 feet) deep. Each of the WTGs will be supported by a mono-pole substructure atop a suction bucket foundation (mono-bucket). The Mono Bucket (MB), Figure 1, combines the benefits of a gravity base, a monopile, and a suction bucket. It is a Suction Installed Caisson (SICA) or "all-in-one" steel foundation system to support offshore wind turbines. The interface with the lakebed is accomplished by means of a steel skirt that penetrates the seabed. This steel skirt (or bucket) is welded to an upper steel tube and transition piece that resembles the elements above the mudline of a standard offshore wind monopile. The MB skirt for the Icebreaker Wind project will be approximately 17.5 m (57 feet) in diameter and a maximum of 10 m (33 feet) deep.



Figure 1 Mono Bucket (MB) Design

The Mono Bucket is installed (Figure 2) by means of both gravity and suction. When the steel bucket is placed on the lakebed, it initially self-penetrates by gravity about 1-2 m (3-6 feet). Suction is then applied and water is pumped from the bucket causing the foundation to penetrate into the lakebed. Once the bucket has achieved the specified penetration, the pump is stopped.



Figure 2 Mono Bucket (MB) Installation

The second APE is the Export cable area. The energy generated from the WTGs will be transmitted through an export cable from the offshore project area to shore. This area is 13.2 km (8.2 miles) x 0.36 km (0.2 miles). Beginning 1.7 km (1.1 miles) west of the end of the east breakwater offshore of Cleveland, Ohio, Cuyahoga County, and running 13.2 km (8.2 miles) to the Turbine area at a water depth of 10-17 m (33 - 56 feet). The export cables will be buried in an excavated trench 1.5 m (5 feet) wide by 1.5 m (5 feet) deep.

The third APE is the Inner harbor area. The export cable will be run in horizontal bore holes generated from Horizontal Directional Drilling (HDD) to allow the cables to pass beneath the Cleveland harbor breakwater and the commercial navigation channel east of Burke Lakefront Airport. The cable will come ashore at the Cleveland Public Power (CPP) Lake Road substation. This area is 0.85 km (0.53 miles) x 0.36 km (0.22 miles). Beginning 1.7 km (1.1 miles) west of

the end of the east breakwater offshore of Cleveland, Ohio, Cuyahoga County, and running 0.85 km (0.53 miles) to shore at the CPP substation at a water depth of 4-10 m (13 - 33 feet). The HDD borehole depth will be a minimum of 4 m (12 feet) below the foundation of the breakwater.

The scope of work includes installing six WTGs assemblies, WTGs interconnect cabling, and export cabling to shore. This work would take 6 months to complete.

3.0 BACKGROUND RESEARCH

3.1 Environmental Context

3.1.1 Bathymetry

The Icebreaker Wind site lies in Lake Erie, the southernmost of the five Great Lakes in North America. The Great Lakes are shown in Figure 3, along with their profiles and surface elevations as the flow of fresh water is traced from Lake Superior to the lower lakes and eventually out into the Atlantic Ocean through the St. Lawrence River (Michigan Sea Grant, 2014).



Figure 3 North American Great Lakes (Michigan Sea Grant)

Lake Erie is the shallowest of the Great Lakes with an average depth of 19 m (62 feet) and a maximum depth of 64 m (210 feet) (NOAA, 2014a). It is also the smallest of the Great Lakes by volume (116 cubic miles, or 483 cubic km), although it is only the fourth smallest by surface area (9,910 square miles, or 25,655 square km) (NOAA, 2014a). The water retention or replacement time is 2.7 years, which is short compared to the 6 to 173 years of the other Great Lakes (NOAA, 2014a). An overall bathymetric view of Lake Erie is shown in Figure 4 (NOAA, 2014c).



Figure 4 Bathymetric Map of Lake Erie (NOAA)

Lake Erie consists of three distinct regions: the western, central, and eastern basins. Each region has significantly different bathymetric characteristics. The western basin is the shallowest with an average depth of 7 m (21 feet) and features rocky outcrops, shoals, and islands (Waterkeeper, 2014). The central basin has a large flat bottom with an average depth of 20 m (65 feet) and a maximum depth of 24 m (80 feet) in a broad depression in the middle of the Lake (Waterkeeper, 2014)(NOAA, 2014d). In contrast, the eastern basin contains a sharp, deep gouge with several escarpments, an average depth of 24 m (80 feet), and the deepest depths of the Lake off the tip of a long sandy peninsula (Waterkeeper, 2014).

The survey areas (Figure 5) lie between 0 and 20 km (0 and 12.4 miles) offshore of Cleveland, Ohio in the central basin. Corresponding water depths are 5 to 19 m (15-60 feet) relative to the Lake Erie Chart Datum of +173.5 m (NOAA Chart 14829).



Figure 5 Icebreaker Demonstration Wind Project Site and Bathymetry (VanZandt, NOAA Chart 14829)

3.1.2 Geology

The Great Lakes were formed predominantly by glacial processes. After repeated carving by glaciers during the Pleistocene epoch, only Paleozoic sedimentary rocks remain under

northern Ohio (Dames, 1974). The Paleozoic bedrock exposed under Cleveland is from the Upper Devonian period and roughly dates to between 360 and 380 million years ago (Dames, 1974). This rock is mostly shale and is exposed in cliffs along Lake Erie's shoreline both to the east and west of the City (Carter, 1982). The basin containing Lake Erie itself was carved into this bedrock by repeated Pleistocene glaciations (Dames, 1974). During the last period of Wisconsinan glaciations, the ice moved from the northeast to the southwest to create the lake basin known today (NOAA, 2014d). During the Wisconsinan ice sheet's retreat starting 14,000 years ago and ending 12,600 years ago, glacial till deposits were left behind (Carter, 1982). These deposits are generally unstratified hard clay and gravel called basal till (Carter, 1982). They were created in a deep prehistoric lake that existed until the ice sheet fully retreated (Carter, 1982).

After the start of the Holocene 12,600 years ago, fine-grained lake sediments were deposited above the Pleistocene till layer (Carter, 1982). These post-glacial sedimentary deposits consist of either soft silt or sand in various mixtures. A cross section of Lake Erie water, silt, till, and bedrock is shown in Figure 6 running west to east, through the midpoint of the turbine area, showing the typical subbottom conditions that exist in that area. It should be noted both the bedrock and till layer thicknesses are fairly constant within the boundaries of the 300 meter (1000 foot) width of the survey area.



Figure 6 West to East Geologic Cross Section, Lake Erie off Cleveland, Ohio (Dames & Moore)

The geology along the 4.7 km (2.9 miles) length of the turbine area varied slightly from southeast to northwest. Isopach data for soft clay sediment from the Dames & Moore survey vary from 3 m (10 feet) at the southeastern end to 7.6 m (25 feet) at the northwestern end of the survey area (Dames, 1974). This is comparable with CSR's higher resolution multi-beam subbottom geology survey results of 3 to 7 m (10 to 23 feet) clay sediment layer (Unit 1) from southeastern to the northwestern end (Figure 7) (CSR, 2016, Enclosure 1).



Unit 4 - Undifferentiated Glacial Sediments. This unit is bounded by B1 and acoustic basement.

Figure 7 Typical Sub-bottom Geology Turbine Area (CSR)

The geology along the 13.2 km (8.2 miles) length of the export cable area varied slightly from southeast to northwest. The soft clay sediments (Unit 1) vary from 0 m at the southeastern end to 3 m (9 feet) at the northwestern end of the export cable area (CSR, 2016, Enclosure 2-4).

The glacial sand/gravel sediments (Unit 2) average about 5 m (15 feet) for the export cable area (CSR, 2016, Enclosure 2-4). These sediment layers are much deeper than the trench depth of the export cable of 1.5 m (5 feet).

3.1.3 Flora and Fauna

Lake Erie is the most biologically productive of all of the Great Lakes and contains a large, active freshwater fishery (Waterkeeper, 2014). The lake's productivity is due mostly to the large abundance of phytoplankton, small plants in the water column which form the basis of the food chain (NOAA, 2014b). The warm lake water temperatures due to the relatively shallow depths and an abundance of nutrients from rivers help the phytoplankton thrive. Green alga, a single celled plant, is the most important and the basis of the summer food web (NOAA, 2014b). Diatoms, flagellates, and blue-green algae (cyanobacteria) are also present, especially in the early spring or late summer months (NOAA, 2014b). An overabundance of both phosphoric nutrients combined with rain events, and summer sunlight can lead to algae blooms. These have posed significant environmental problems during recent years.

The phytoplankton serves as food for a variety of creatures in the Lake, including zooplankton and macroinvertebrates (NOAA, 2014b). Zooplankton, small animals in the water column, feed on both the phytoplankton and each other (NOAA, 2014b). Macroinvertebrates (larval insects, worms, amphipods, or mollusks) feed on the phytoplankton or detritus on the bottom (NOAA, 2014b). Foraging fish (perch, shad, drum, catfish, carp, and gobies) eat both the zooplankton and macroinvertebrates (NOAA, 2014b). These fish are then eaten by the piscivores, or the top predatory fish, such as walleye, bass, and trout (NOAA, 2014b).

Figure 8 illustrates the food web of Lake Erie (NOAA, 2014b). At the bottom of the web are the phytoplankton colored in green. The next level is comprised of the zooplankton and macroinvertebrates colored in light blue and orange, respectively. The third level is made up of the foraging fish shown in dark blue, and the top level includes the piscivores colored in purple.



Figure 8 Lake Erie Food Web (NOAA Great Lakes Environmental Research Laboratory)

3.2 Prehistoric Context

Any prehistoric artifacts or structures predating the Holocene Epoch were either destroyed or scattered during glaciations that occurred during that time. The last of the glacial ice sheets, the Wisconsinan's, began retreating during the Pleistocene Epoch ~14,000 years before present (YBP) and ended ~12,600 YBP with glacial till deposits being left behind (Carter, 1982). These deposits generally consist of unstratified hard clay and gravel that are called basal till (Carter, 1982). Additional deposits are stratified and clay-rich, and these are called flow till (Carter, 1982). These deposits were deposited over the Lake Erie basin's shale layer. The thicknesses of the glacial till in the survey area have a range of 55 to 93 feet (Dames, 1974) and 53 to 85 feet (Alpine, 2010).

After the start of the Holocene ~12,600 YBP, fine-grained lake sediments were deposited above the Pleistocene till layer (Carter, 1982). These post-glacial sedimentary deposits consist of either soft silt or sand in various mixtures. The thickness of these soft silt and clay deposits in the survey area vary from 10 to 25 feet (Dames, 1974) and 10 to 16 feet (Alpine, 2010).

During the period from ~12,000 YBP to ~5,400 YBP the lake level was below the turbine APE, which has an elevation at the glacial till layer of +492 feet, thus exposing the land for possible human habitation or use. The lake level during that period varied from +394 feet during the post glaciations Early Lake Erie stage to +476 feet during the Middle Lake Erie stage, ~7,500 YBP (Herdendorf, 2013). At the start of the Middle Lake Erie stage, ~5,400 YBP, the lake level had risen to +525 feet, which inundated the turbine APE, placing any possible prehistoric occupation site underwater (Herdendorf, 2013). After the Middle Lake Erie stage the lake level continued to rise to its present day level of +569 feet (Herdendorf, 2013).

Paleoindian occupation of Northern Ohio was believed to have occurred between 13,000 to 11,000 YBP (Herdendorf, Klarer, Herdendorf, 2006). The earliest evidence in Ohio of occupation is at the Paleo Crossing site (33ME274) in Medina County, Ohio, which has been dated between 10,000 to 11,500 YBP (Brose, 1994).

It is possible that artifacts from early occupation could exist buried at the proposed site, but to date Lake Erie has not been a focus of archaeological research on Paleoindian culture (Stothers, Abel, 2001).

> "Paleoindian sites present a very low archaeological profile across the landscape and are representative of areas where small groups of people would perform specific tasks of short duration. Additionally in northern Ohio, Stothers and Pratt (1980) note that Early and Middle Archaic sites are usually of two types: "those in which a single or a few points are included in a collection of material from other cultural periods, and those in which Early or Middle Archaic materials predominate." The later, mixed sites, would not be represented in the areas examined. The potential for locating Early and Middle Archaic sites beneath Holocene lake sediments with today's remote sensing technologies is a factor of sedimentation depths and relict landscapes. Features such as hidden outcrops that may indicate cultural use areas, have been covered by natural lake sedimentation processes. Therefore, it would be difficult or impossible to locate sites if they existed (Gray & Pape, 2014)."

3.3 Historic Context

Lake Erie has been instrumental in historical shipping and transportation in the Great Lakes. The permanent settlement of the Ohio shores of Lake Erie occurred at a slower pace than that of the Ohio or Mississippi valleys due to the control of the lake by Great Britain (Mansfield, 1899). It wasn't until 1796 that the British relinquished control of their post commanding Lake trade (Mansfield, 1899). Since the opening of the Erie Canal in 1826 from the Hudson River to Buffalo, New York, Lake Erie has served as the crucial nexus for shipping into the upper Great Lakes region and eventually points further west. Immigrants and goods moving westwards would start in New York City; move up the Hudson River by ship, travel along the Erie Canal by boat, and then board yet another ship in Buffalo for transportation down the length of the Lake. At first, Lake Erie was the earliest of the Great Lakes' destination as immigrants from Europe and the Northern States began to settle along its shores. Eventually, however, passengers and goods continued on to the other lakes and, ultimately, Chicago, which then served as the starting point for further western expansion (Mansfield, 1899). It was estimated in 1832 that more than half of the immigrants arrived in the West by water (Mansfield, 1899).

As settlers grew crops, harvested timber, and mined copper and iron ores, these products flowed eastwards back down the lakes and across Lake Erie to be delivered to the east coast. Meanwhile, coal from Pennsylvania, new immigrants, and finished manufactured goods continued to travel westward across Lake Erie from Buffalo. In order to deliver these people and goods, many hundreds of ships operated on the Great Lakes every season in the 19th century (Mansfield, 1899). These ships were frequently made of wood and lacked radio, radar, or modern electronic navigational aids. Furthermore, there was a general lack of accurate weather forecasting, detailed bathymetric information, and other useful aids to safety. As a result, many unfortunate vessels collided with each other, ran aground, sprang leaks, caught fire, or foundered in storms. Lake Erie is the shallowest of all the Great Lakes and is known to have especially severe waves due to its lack of depth and prevailing winds, which blow along the length of the Lake and have caused many ships to succumb to its depths. The end result is a high number of shipwrecks, possibly numbering in the thousands, in Lake Erie (Frew, 2014).

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The exact number and location of these shipwrecks is unknown because of the lack of accurate records for these events. There is no central governmental repository that records sinkings. In many cases the only record of a shipwreck may be a story in a local town or city newspaper. Official records are split among two national governments (United States and Canada) and multiple governmental agencies and archives, making an accurate accounting nearly impossible. This is further exacerbated by the fact that many ships were raised and put back into service without as much publicity as surrounded their sinking events, making the total number of shipwrecks in Lake Erie and more are found regularly (ODNR, 2009). Estimates put the total number of shipwrecks in Lake Erie at between 500 and 3,000 (Frew, 2014) (ODNR, 2009).

Historic shipwrecks consist of both wooden and metal ships, sailing vessels, sidewheel steamers, and propeller steamers. The cold fresh water of the Great Lakes tends to serve as an excellent preservative for these wrecks. There are no wood-eating organisms, such as the Teredo worm found in warm ocean environments. Cold water greatly inhibits bacterial decay, allowing wooden timbers and grain cargos to survive. The fresh water is also much less corrosive on metal artifacts, unlike the salty oceans, and the inland seas do not have storms as destructive as ocean-borne hurricanes and typhoons. Thus, many of the shipwrecks in the Great Lakes serve are well preserved archaeological sites that provide significant information about 19th century shipbuilding, shipboard life, and the associated maritime landscape associated with these wrecks.

3.4 Literature Review

VanZandt Engineering consulted the Ohio Historic Preservation Office (OHPO) online mapping system in an effort to locate any inventoried cultural resources identified within the survey area. The archival study included a review of the Ohio Archaeological Inventory (OAI), Ohio Historic Inventory (OHI), the National Register of Historic Places (NRHP), Ohio Sea Grant Shipwreck map, the Cleveland Underwater Explorers shipwreck data base, and the Cleveland Underwater Explorers historical Lake Erie nautical chart collection. Four previously-inventoried cultural resources (shipwrecks) have been identified within 3.5 nm of the survey area. These shipwrecks were the *Admiral* and *Dundee* (3.0 and 3.3 nm, respectively, from the northwest survey corner point), and the CSU wreck and East Breakwall Barge (0.5 and 1.6 nm,

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respectively, from the export cable area). None of these wrecks were detected within the survey area.

Results of the literature review are described below:

Ohio Archaeology Inventory:

No properties listed on the Ohio Archaeology Inventory are present within the survey area.

Ohio Historic Inventory:

No properties listed on the Ohio Historic Inventory are present within the survey area.

National Register of Historic Places:

No individual properties or districts listed on or determined eligible for listing on the NRHP are present within the survey area.

Ohio Sea Grant Shipwreck Map:

No shipwrecks on the Ohio Sea Grant Shipwreck map are present within the survey area. Four shipwrecks are located within 3.5 nm of the survey area. These shipwrecks were the *Admiral* and *Dundee* (3.0 and 3.3 nm, respectively, from the northwest survey corner point), and the CSU wreck and east breakwall barge (0.5 and 1.6 nm, respectively, from the export cable area). The shipwreck map shows the possibility of the *Dreadnaugt* (probably *Dreadnaught*) and the *Mackinaw* being close to the survey area, but these locations are unconfirmed and based off of shipwreck maps that were for sale to the public. Most of the locations derived from these maps are not verified, and therefore the ODNR did not base their offshore wind farm siting analysis on them. See, Wind Turbine Placement Favorability Analysis Map Methodology (ODNR, 2009).

Further historical research on both shipwrecks show that the *Dreadnaugt* came ashore and was abandoned and the *Mackinaw* was farther from the project APEs than the shipwreck map indicated. Thus, neither would be close to project APEs. The Cleveland Underwater Explorers (CLUE) has recently discovered what they believe are the remains of the *Mackinaw*, and it is its located 4.4 nm east of the project site.

Cleveland Underwater Explorers Shipwreck Data Base:

No shipwrecks in the Cleveland Underwater Explorers shipwreck data base are present within the survey area.

Cleveland Underwater Explorers Historical Lake Erie Nautical Chart Collection:

No shipwrecks were found charted on any chart in the Cleveland Underwater Explorers historical Lake Erie nautical chart collection within the survey area or within 3.5 nm of the survey area.

4.0 METHODS

4.1 Survey Design

The main objectives of the survey were to identify and map surficial geology, lakebed features and sub-bottom conditions within the WTG area and the proposed submarine cable routes.

The objectives of the geophysical survey were accomplished by the collection, interpretation and subsequent reporting of geophysical data. The following types of data were collected during the marine geophysical survey (CSR, 2016):

- Differential GPS navigation was constantly recorded to provide real-time georeferencing for all data sets acquired during the survey.
- Sidescan sonar data were acquired to identify potential hazards exposed on the surface of the lakebed (shipwrecks, pipelines, boulders, debris, ice gouging) and to categorize surficial sediment types.
- High-resolution chirp profiler data were acquired throughout the geophysical program to identify the sub-bottom geology to a depth of at least 5 m (15 feet).
- Lakebed bathymetry data was continuously logged throughout the geophysical program using a multibeam echosounder in order to determine water depths (lakebed elevations) along the route.
- Marine magnetometer data were collected to identify surface and buried ferrous targets.
- Grab samples were collected to ground truth the surficial geology interpretation.
- High resolution 50 kHz profiler data was collected over the proposed turbine locations to aid the interpretation of the near surface unconsolidated sediments.
- High-resolution single channel seismic (mid penetration "boomer") data were acquired within the Harbor and near shore areas to aid the interpretation over the HDD location.
- Sidescan sonar and magnetometer data were not collected in the harbor since the cable will be installed at depth within a HDD casing and therefore there was no requirement for archaeological clearance.

4.2 Overall Survey Layout

4.2.1 Turbine Area

Survey coverage over the Turbine Area included a 240 m (720 feet) corridor centered on the proposed route extending from WTGs ICE1 to ICE7. Overall, 22 lines were surveyed totaling 47 line km. Tie line spacing was 375 m (1,125 feet) along the Turbine Area. Figure 9 illustrates the geophysical survey track lines in the Turbine Area (CSR, 2016).



Figure 9 Geophysical survey track lines over the Turbine Area. (CSR)

4.2.2 Export Cable Area

Survey Coverage over the Export Cable Area included a 300 m (990 feet) corridor centered on the proposed route. The Export Cable Area extends from the proposed HDD exit location to WTG ICE1. The survey area was expanded north of the breakwater to TP1 and TP2 to ensure that enough data was acquired to accommodate alternative HDD exit locations. Additional lines were surveyed parallel to the breakwater to gain more information in the HDD exit area, and to map the toe of the breakwater slope. Overall, 73 geophysical survey lines were run totaling 206 line km. Figure 10 illustrates the geophysical survey track lines along the Export Cable Area (CSR, 2016).



Figure 10 Geophysical survey track lines along the Export Cable Area. (CSR)

4.2.3 Inner Harbor Area

The geophysical survey lines were designed for the collection of multibeam sonar and sub-bottom profiler data along potential HDD routes between the Cleveland breakwater and the landfall. A total of 26 lines were surveyed, totaling 18 line km. Figure 11 illustrates the geophysical survey track lines within the harbor area (CSR, 2016).

Sidescan sonar and magnetometer data were not collected in the harbor since the cable will be installed at depth within a HDD casing, and therefore there was no requirement for archaeological clearance (CSR, 2016).



Figure 11 Geophysical survey track lines within the Harbor and over the near shore HDD exit Location. (CSR)

4.2.4 Locational Data:

Note: Locational data in decimal degrees, WGS84 geodetic and UTM, NAD27, Zone 17, M

Table 1 Wind Turbine Generator Locations:

- ICE1 N41.60072 W81.80055 433273.438E 4605537.801N
- ICE2 N41.60616 W81.80602 432823.244E 4606146.037N
- ICE3 N41.61159 W81.81150 432372.284E 4606753.200N
- ICE4 N41.61702 W81.81697 431922.235E 4607360.384N
- ICE5 N41.62246 W81.82245 431471.440E 4607968.716N
- ICE6 N41.62789 W81.82793 431020.712E 4608575.966N
- ICE7 N41.63333 W81.83340 (Backup site) 430570.906E 4609184.348N

4.3 Field Methods (CSR, 2016)

The following section describes the methodologies and equipment used to perform the data collection task required for the survey. Survey design and control was based on the guide-lines developed by the Bureau of Ocean Energy Management (BOEM) set forth in NTL No. 2005-G07.

4.3.1 Vessel

The Survey operations were conducted from Underwater Marine Contractors Inc. vessel *Salvage Chief* (Figure 12). The *Salvage Chief* is steel constructed, with an overall length of 49ft. The *Salvage Chief* had ample deck space with a knuckle boom and an extendable hydraulic A-frame, ideal for mounting winches and the deployment/recovery of geophysical equipment. CSR installed over-the-side mounts for dual frequency single beam and multibeam transducers on the starboard side of the Salvage Chief. Electronic equipment and data collection workstations were set up in the vessel's wheelhouse (CSR, 2016).



Figure 12 Salvage Chief (CSR)

4.3.2 Survey Reference

Horizontal positioning was calculated using Differential Global Positioning System (DGPS). The primary Coast Guard differential corrections were acquired from the Detroit, MI reference station. The geodetic parameters for the survey were as follows (CSR, 2016):

- Vertical Datum: Lake Erie Chart Datum (173.5 m or 569.2 ft. above IGLD 1985)
- Horizontal Datum: NAD83
- Projection: Universal Transverse Mercator, Zone 17
- Central Meridian 81°W

- False Easting: 500000.00
- False Northing: 0.000000
- Scale Factor: 0.999600
- Latitude of Origin: 0.0
- Linear Unit: Meter

4.3.3 Navigation Control

A real-time DGPS system was utilized during the geophysical survey. CSR's integrated navigation system consisted of a Hemisphere VS-330 DGPS system and the Hypack survey navigation package. The integrated navigation system included real time digital data logging of positional data, a left/right steering monitor for the helmsman, and an interface to the geophysical equipment so that all data was correctly geo-referenced (CSR, 2016).

Hemisphere VS-330 GNSS Receiver & Heading System

The Hemisphere VS-330 is a dual antenna DGPS system with a horizontal accuracy of 0.3 m (1 foot) under ideal conditions. The secondary antenna (forward) is used to calculate heading to an accuracy of 0.09° RMS. The system was configured to receive Coast Guard differential corrections from Detroit, MI, which operates on a transmission frequency 319 kHz. Positions for the multibeam bathymetry were calculated based on the offset from the primary Hemisphere DGPS antenna, to the multibeam transducer (CSR, 2016).

• Hemisphere R110 DGPS

The Hemisphere R100 DGPS system was used in tandem with the Hemisphere VS-330 during the geophysical survey operations. The system was configured to receive Coast Guard differential corrections from Detroit, MI. The Hemisphere R100 is a single antenna GPS system with a horizontal accuracy of 0.6 m (2 feet) under ideal conditions (CSR, 2016).

Positions for the single beam bathymetry were calculated based on the offset from the Hemisphere R110 DGPS antenna to the transducer. Hemisphere R110 DGPS positioning combined with vessel heading and offset measurements were also used to georeference the sidescan sonar, chirp, and magnetometer data collected during the survey. Cable out measurements were recorded by the operator during the survey for each line with layback corrections applied during processing and interpretation (CSR, 2016).

• Hypack/Hysweep Survey Acquisition Software

Hypack is a complete hydrographic survey navigation software package that includes: survey preparation, data collection, data editing, cross-section display, geodesy and exporting capabilities. In operational survey mode, the system supports a helmsman display with survey line indicator, to assure survey lines are followed as accurately as possible. In addition to planned survey grid lines, the survey screen also displays bathymetric contours, coastline, navigational hazards, and target/sample locations. During survey operations all navigation information was logged in Hypack to ensure simultaneous geo-referencing of all datasets (CSR, 2016).

4.3.4 Survey Equipment

• SURVEY NAVIGATION

- Hemisphere VS-330 GNSS Receiver & Heading System
- Hemisphere R110 DGPS Receiver
- o HYPACK Survey Navigation Software

• MULTIBEAM ECHOSOUNDER

- Teledyne-Odom ES3 Multibeam Echosounder (240 kHz)
- Teledyne-TSS DMS-05 Motion Sensor
- o Teledyne-Odom DigiBar-Pro Velocimeter
- Applied Microsystems SVPlus
- HYSWEEP Multibeam Acquisition System

• SINGLE BEAM ECHOSOUNDER

• Odom CV3 Dual Frequency Echosounder (50/200 kHz)

• SIDESCAN SONAR

- o Klein 3000 (100/500 kHz) Sidescan Sonar System
- o SonarPro Sidescan Acquisition Software

• MAGNETOMETER

o Marine Magnetics SeaSPY Marine Magnetometer

• SUB-BOTTOM PROFILER

• Klein 3000 Chirp Profiler (2-8 kHz)

• SEISMIC REFLECTION

- EG&G 240 Low Frequency (400-14,000 Hz) Shallow Seismic System (Boomer)
- Applied Acoustics CSP-300 Power Supply
- o Ministreamer with GeoSpectrum M5 Hydrophones
- SonarWiz SBP Acquisition & Processing Software

• TIDE GAUGE

- o HOBOware U20 Titanium Water Level Data Logger
- SAMPLING
- Van Veen Grab Sampler

4.3.5 Side Scan Sonar Survey

A Klein 3000 dual frequency sidescan system was used to complete the seabed imaging component of the Icebreaker Wind cable route assessment. The Klein 3000 consisted of a sonar instrumented towfish, a transceiver and processing unit (TPU) and an acquisition computer running Klein's proprietary Sonar Pro software. Capable of simultaneous dual frequency operation (100/500 kHz) and constructed with advanced electronics and transducers, the Klein 3000 produced superior high resolution imagery of the seafloor. High frequency (500 kHz) ranges of between 75 and 100 m on both the port and starboard channels allowed for wide area swath coverage and target detection over the route.

Frequency: 500 kHz
Range Setting: 75 m and 100 m range
Target Resolution: 10-20 cm in ideal conditions
Lane Size: 27 m
Tow Height: 5 to 6 m above the lake bottom
Rationale: 100% seafloor coverage; target detection & surficial geology mapping

During the 2016 geophysical survey, the sidescan system was integrated with the Klein 3000 chirp profiler and marine magnetometer. When the sidescan system is integrated with the chirp profiler only one frequency can be recorded. For this survey the higher 500 kHz frequency was acquired.

Calculated layback measurements were used to position the sidescan sonar system during interpretation and mapping of the data. Layback is calculated using the offset between the DGPS antenna and tow point, the height of the tow above the water line, the depth of the system below the surface, and the length of cable deployed. Where possible, feature matching between the sidescan, sub-bottom profiler and multibeam data was used to confirm layback calculations.

SonarPro was used to operate the Klein 3000 sidescan sonar and chirp systems. The system provides navigational recording, target management, and real-time display of the sidescan data. SonarPro also provides the options to adjust the towfish sensors during data acquisition, including range and transmit power, which is directly recorded with the raw data. The target management feature enabled the selection of seabed targets in both real-time and during playback following collection. The sidescan and chirp data were recorded to XTF format (CSR, 2016).

4.3.6 Magnetic Survey

A Marine Magnetics SeaSpy Magnetometer was used for the survey. The SeaSpy is a digital marine magnetometer that operates using an advanced Overhauser sensor. Measuring the ambient magnetic field, using a specialized branch of magnetic resonance technology, the SeaSpy has an absolute accuracy of 0.2 Nanotesla (nT). The sensor is capable of measuring a range of 18,000 nT to 120,000 nT in all directions, resulting in no dead zones and reliable data.

29

During the 2016 geophysical survey, the marine magnetometer was integrated with the Klein 3000 system (CSR, 2016).

4.3.7 Sub-bottom Mapping System

Sub-bottom geophysical data was acquired using two systems, a chirp profiler and a single channel seismic system (CSR, 2016).

The Klein system uses two Chirp transmit transducers with a single linear hydrophone. The Mills Cross configuration achieves higher resolution and deeper bottom penetration than comparable systems. The Klein 3000 chirp sub-bottom profiler (SBP) integrates with the Klein 3000 sidescan system. It mounts directly to the Klein 3000 tow vehicle and uses the existing physical connections and electrical communications. This option takes advantage of the existing Klein 3000 sidescan hardware by using the same tow cable, transceiver processor unit (TPU), workstation and towing systems. The chirp sub-bottom profiler consists of a subsea assembly used to contain the transmit projectors, receive hydrophone and SBP electronics. These components are enclosed in a fiberglass shroud with an integrated support structure to allow for combined transducer/electronics mounting and towing. The Klein 3000 tow vehicle installs into the rear portion of the shroud assembly where it interconnects with the SBP electronics. The amplifier modulates both amplitude and phase of the transmit waveform for pulse lengths up to 40 msec.

Specifications:

Chirp Frequency: 2-8 kHz Beam Angle: 20° along track; 40° cross track @ 5 kHz Resolution: 12.5 cm or better Power: 1 kwatt Source Level: 204 db @ 1 m

CSR has achieved penetration of up to 100 m (330 feet) with this system in fine grained sediments. During this survey the maximum penetration achieved was 15 to 20 m (49 to 66 feet) within post glacial and glacial fine grained sediments. The chirp signal was impeded in areas where shallow gas and coarse grained glacial sediments occurred.

Additional survey data were collected using a single channel seismic (Boomer) system. This system provides low frequency energy in the range of 400-10,000 Hz and includes four main components (boomer plate, power supply, hydrophone, and acquisition computer). The energy source for the system was the Applied Acoustics CSP-300 which has output settings ranging from 50-300 joules. The CSP supplied power to the boomer plate, which was towed in conjunction with a low frequency hydrophone streamer. The boomer plate was responsible for transmitting the sound energy through the water column and lakebed sediments. The hydrophone streamer received the reflected sound energy, transmitting the signal to the topside recording computer.

The raw and processed acoustic signal was recorded on a topside computer running SonarWiz acquisition software. DGPS positioning information was integrated with the data in real-time and recorded by SonarWiz in seismic data SEG-Y format. Acoustic frequency filters applied to the data in real time using SonarWiz were not recorded to the raw data. The frequency filters essentially "cleaned" the data allowing for better visualization and interpretation of the sub-surface sediments. Low- Cut (400 Hz) and High-Cut (4000 Hz) frequency filters were applied to the data in real time using the SPA-3 processing unit. This data was recorded to a second channel within the SGY file. In addition to filter processing, the SPA-3 unit (IKB Technologies Ltd) also controlled the firing rate of the boomer system.

During this survey the energy source was operated at an output level of 100, 200, and 300 joules with a firing rate of 1/4 second (100 joules) and 3/8 second (200 & 300 joules). The record length was synced to the firing rate within SonarWiz.

CSR has achieved penetration of greater than 100 m (330 feet) with this system in fine to coarse grained sediments. During this survey the maximum penetration achieved was 50 to 60 m (165 to 198 feet) within post glacial and glacial sediments over the HDD survey area. The boomer signal was impeded in areas where shallow gas and acoustic basement (interpreted to be bedrock) occurred.

4.3.8 Personnel

Party Chief	Colin Toole, CSR
Hydrographic Surveyor	Luke Melanson, CSR
Electronics Technician	Jon MacDonald, CSR
Vessel Captain	Joel Frazer, Underwater Marine

5.0 DATA ANALYSIS

5.1 Sidescan Sonar Data Analysis

A review of 271 line km of sidescan data showed no historic structures (such as shipwrecks) or artifacts were present within the turbine (Figure 13) and export cable (Figure 14) survey areas. (Note: For full size images see appendices)



Figure 13 Turbine Survey Area Sidescan Mosaic. (CSR)



Figure 14 Export Cable Survey Area Sidescan Mosaic (CSR)

The Side Scan Sonar showed a generally uniform and smooth lake bottom. Some evidence of ripples or other sedimentary features were observed along the survey route (Figure 15) and some areas of the bottom revealed enhanced reflectivity denoting a change in geological structure (Figure 16). These locations were assigned a target number, and corresponding imagery and information can be found in Appendix A.



Figure 15 Sediment Rippling along Export Cable Route (CSR)





The only targets identified were geological or the result of old trash dumpings (rectangular, circular, and linear contacts) and dredge spoil (circular contacts) in the survey areas (Figure 17). A total of 455 identified targets were analyzed and the detailed description of the targets can be found in Table 2 (Locational data in NAD83 Geographic, NAD83, Zone 17, M, and NAD83, Ohio State Plane North, US Survey Feet). See Appendix A for complete target data with images. There are a number of targets that may indicate the presence of a linear ferrous feature perpendicular to the proposed route. This feature could not be identified from the sidescan or sub-bottom profiler data acquired over this area. An analysis of the magnetic data shows that these targets are most likely buried steel or iron buoy blocks or anchors.



Figure 17 Sidescan Sonar Record of Dredge Spoil. Center of Data Example is Located 150 m E of EKP 12. (CSR)

Table 2 Sides	scan Sonar	Contacts	List
---------------	------------	----------	------

-	MADES	econ arthur	MADRS U	TM Zene 17	MADES Chie S	Side Jate Plane North	ican Sonar Con	tacts	-				-
ID		and a second	Andrea o		East (US	North (US	Bathymetry	Distance from Proposed	Length	Width	Height	Description	Associated Mag
	Latitude	Longitude	East (m)	North (m)	survey feet}	survey feet)	(m)	Boute (m)	(440)	(m)	0m3		Anomaly ID
a	41.6176299	-81.8581120	431841.5	4607646.7	2154951.3	711527.0	17.8	35.5	2.6	0.5	0.2	Linear Contact	-
<i>a</i>	41.6170757	-81.8170325	491990.9	4607584.3	2155248.0	711827.6	17.7	0.9	30.0	0.2		Linear Contact Point Source (Probable Buoy	
a	41.6127124	-81.0118483	432358.2	4607095.8	2156678.1	709748.8	17.6	51.6	2.5	1.0	- 683	Mooningi	
64	41.6114662	-81.8115284	432383.6	4606057.2	2156769.2	709295.5	17.5	10.6	7.4	7.0	100	Circular Contact (Probable Barry Monrine)	1.25
<5	41.6051141	-81.8060026	432838 A	4606358.7	2158295.7	707357.3	17.3	1.6	3.9	3.5	+	Orcular Contact	+
66	41.6044110	-81.8026013	433120.1	4506167.0	2159230.9	705744.1	17.2	110.5	2.2	12	0.6	Point Source	1/84
10	41 8006348		499349.3	4404780.8	2120204.5	708782.4	17.1					Orcular Contact (Probable	
	41.0000765	-01.0006100	*33202.2	4000/30.8	2139/00.4	705307.8	17.1	14	3.3	23	200	Baby Mooring)	1849, NDU
C10	41.5975261	-81.7942784	433291.6	4605374.0	2159019.9	704180.5	16.9	79.4	3.0	1.8		Linear Confact	
C11	41.5905543	-81.7802254	434570.8	4604611.5	2165392.0	701744.9		175.5	3.2	0.3	0.2	Linear Contact	· · · · ·
C12 C13	41.5882561 41.58882561	-81.7753918 -81.7591319	435558.1	4603848.3	2167268.2	700923.0 699340.0	15.8	125,3	3.5	0.9	0.2	Reclangular Contact Linear Contact	-
C14	41 5031114	-81.7552133	437048.2	4603766.6	2172256.9	699090.4	36.4	102.6	19.5	2.6		Circular Contact (Possible	
							0.000				222	Dredge Spoil) Loss Reflectivity Patch (Possible)	
C15	41.5801051	-81.7460655	437807.9	4603426.2	2174769.0	698016.5	- 12	177.1	5.9	2.4	- 5.3	Slag)	1. C.
C16	41.5785477	-81.7451360	437883.9	4608252.6	2175028.2	697451.3	15.9	62.8	8.1	1.4	D.6	Low Reflectivity Patch (Possible	
C17	41.5794293	-81.7450774	437889.6	4603850.5	2175041.4	697772.6	15.9	150.9	11.0	0.4	0.0	Linear Contact	6 (8)
C18	41.5782767	-81.7449797	437896.6	4603222.2	2175071.8	697352.2	15.8	42.5	6.7	1.5	0.5	Low Reflectivity Patch (Possible	(
C19	41 5780199	-81.7645240	437934.4	4603193.6	2175197.3	697260.4	15.8	36.0	6.3	0.5	100	Linear Contact	
C20	41.5761775	-81.7444257	437940,0	4602989.0	3175290.0	696589.1	15.7	130.4	1.2	0.2	- 430	Linear Contact	- (+) X
C21	41.5753894	81.7432666	438036.7	4602900.7	2175549.6	696304.9	0.0	169.8	0.8	0.5	0.1	Orcular Contact (Probable Tine)	
C22	41.5749766	-81,7419717	438144,3	4602853.9	2175905.2	696157.6	15.7	157.8	2.7	0.7	0.5	Point Source	
C23	41.5763451	-81.7416041	438176.2	4603005.8	2176001.5	696657.1	15.8	9.9	3.9	0.5	+	Linear Contact	
C25	41.5776437	-81.7410623	438222.6	4603149.4	2176145.6	697131.6	15.7	138.2	2.6	0.5	0.1	Linear Contact	
626	41.5764126	-81.7407087	456250.9	4605012.4	2176246.2	696683.8	15.0	32.6	2.0	0.0	0.4	Loss Reflectivity Patch (Possible	1 i i i i i i i i i i i i i i i i i i i
C27	41.5769110	-81.7403391	435265.5	4605067.6	2176291.0	596065.0	15.8	87.9	8.1	0.4	+	Singi Linear Contact	
C28	41.5748367	-81.7404957	438267.2	4602837.3	2176909.5	696110.1	15.7	112.2	2.8	0.6	0.1	Linear Contact	
C25 C30	41.5771813 41.5759815	-81.7402303	438291.5	4603097.A 4603953.2	2176374.7 2176788.0	696565.1 696531.5	15.7	125.6	9.4	0.4	0.2	Linear Contact	
-C91	41.5764743	-81.7382422	438456.6	4603017.5	2176920.9	696712.2	15.7	137.6	11.1	0.3	0.1	Linear Contact	+
C32	41.5756655	-81.7376941	430501.5	4601927.3	2177075.4	696410.0	15.7	80.6	2.2	1.1	- 43	Low Reflectivity Patch (Possible Class	-
C33	41.5726019	-01.7357009	439557.A	4602585.9	2177604.4	693307.1	15.4	140.0	4.9	1.4	- 20	Circular Contact	
C34	41.5727777	-81.7355758	438675.A	4602605.2	2177662.2	695371.7	15.4	115.2	2.4	2.2	0.7	Circular Contact (Probable	1.1
035	41.5781210	-81.7352714	438701.1	4602643.1	2177744.4	695497.5	15.4	69.6	6.0	84		Dredge Spoil) Rectangular Contact	
Cal	41 5746357	-01 7251 200	438714.3	4603911.7	2177778.3	696049.7	15.6	85.5	1.9	1.1	- 20	Los Reflectivity Patch (Possible	1 12
(37	41 6343600	.01 7351.027	436716.3	4601768.3	2177204.0	605000.3	15.6	47.1	2.0	15	-	Slag) Conduc Contact	
C	41 8348885	#1 7180100	100730.2	44220018-8		EDEDUCE.	10.0			20	100	Low Reflectivity Patch (Possible	
Car.	41.5/45052	-01./200209	430/24.2	4000003.5	21/2011.0	596531.6	10.0	52,4	.4.2	- 4.9	*	Slag	
C39	41.5732856	-81.7349705	438726.3	4802661.2	2177826.2	693558.2	15.4	41.5	4.5	31	- 833	Lou Neffectivity Patch (Possible Slac)	
1040	41.5720940	-81 7341911	438790.2	4603528.3	2178043.2	695125.9	15.8	126.2	7.0	5.6	4.5	Low Reflectivity Patch (Possible	12
-									-	-		Slag) Point Source (Probable	
041	41.5748022	-91.7341269	438798.1	4602928.9	2178052.1	696112.0	15.8	140.0	2.6	1.8	D.8	Bouider)	,
042	41.5717875	-81.7940750	438799.7	4602494.2	2178076.5	695014.5	15.2	151.1	7.3	3.4	1.0	Loss Reflectivity Patch (Possible Stavi	
642	41 8218448	.01 7540630	490000.7	4603511.8	2170028.6	685022.2	16.8	198.62	3.7	3.1		Low Reflectivity Patch (Possible	
043	41.0(19438	-91.7940509	439000/17	+0025110	\$1/90/19/2	00091212	45.2	135/2	- 217	57		Sing)	
644	41.5721798	-81.7336485	438835.5	4602537.5	2178191.4	695158.5	15.3	96.8	17.9	17,4	- 18	Low Reflectivity Patch (Possible Slag)	
C45	41.5722820	-81.7332410	438869.6	4602548.5	2178302.6	695196.7	15.2	69.7	4.0	0.4	D.1	Linear Costact	<u> </u>
646	41.5729978	-81.7850702	430004.5	4603627.9	2178947.0	\$95457.£	15.4	6.0	2.0	0.4	0.5	Point Source (Probable Boulder)	1 18
197	41.5727938	81 7330514	438805.0	4602605.4	2178952.8	605324.3	15.5	12.1	18	1.0	0.5	Point Source (Probable	1
						00000000		5309802.0	1.000	-		Pourider) Point Scence (Probable	
648	41.5726638	-81.7321082	438964,4	4902590.1	2170611.3	695338.5	35.3	12.9	1.2	0.9	0.7	Bouider)	1
C49	41.5726909	-81.7312521	439035.8	4602592.5	2178945.5	695350.5	15.3	49.9	2.8	1.2	0.3	Low Reflectivity Patch (Possible Start	1.14
1000	41 5710000		439040 7	4003014.7	DITION C	603001.4	16.5	15.6	44	22	. 3	Low Reflectivity Patch (Possible	-
	41 571 9909	at the co	435561.7	4002304.7	2170000.0	1003003.0	12.2	10.0				Slag	. <u> </u>
031	41.5702956	-81.7305695	439095,6	4002408.8	2179035.2	894479.6	15.5	15.3	3.6	0.5	0.5	Linear Contact	-
C53	41.5703116	-81.7300963	439129.9	4602327.5	2179169.4	694486.3	15.3	135.3	3.6	0.6	+ .	Linear Contact	+
634	41.5697973	-81.7500883	439130.1	4002270.4	2179173.2	694298.9		185.0	15.8	6.7	+	Low Reflectivity Patch (Roscible)	*
CSS	41.5711445	-81.7291570	439209.0	4602419.4	2179623.7	694792.1	15.3	16.5	4.0	1.7	- 56	Shagj	15
C55	41.5711069	-61.7291492	439209.6	4602415.2	2179426.0	694776.4	15.5	19.9	2.5	1.6	*/8	Low Reflectivity Patch (Possible Star)	1
C87	41 571 18**	-81.7201.104	439211.3	4803474.7	2179433.7	894807.A	15.5	11.5	17	2.5		Low Reflectivity Patch (Possible	
		50.000000		Terratid	and a state of the	and an a						Sing) Low Reflectivity Date: Character	
CSE	41.5710575	-81.7290973	439213.9	4603409.6	2179640.8	694760.5	15.3	32.6	2,1	1.7	7.15	Slagi	
C59	41.5712076	-81.7290676	439216.5	4603426.3	2179448.0	694915.3	15.3	6.8	6.1	3.6		Low Reflectivity Patch (Possible	
090	41.5711550	-01.7297679	439239.0	4602420.3	2179524.7	694796.8	15.8	0.7	3.1	0.6	0.2	Hagi Linear Contact	
C61	41.5696265	-61.7204156	439269.6	4603272.5	2179630.8	694313.0	15.2	115.0	4.1	0.4	D.1	Linear Contact	-
C62	41.5706782	-61.7284075	439271.0	4602367.1	2179630.3	694624.0	15.2	31.0	4.2	1.2	0.4	Lineer Contect	1007
C64	41.5696733	-81.7283218	439277.2	4602255.4	2179657.0	694258.0	15.2	125.6	1.5	0.5	0.1	Linear Contact	+
C65	41.5706138	-81.7282603	439283.3	4603359.8	2179670.8	6.0038603	15.2	32.2	3.4	1.0	- 23)	Low Reflectivity Patch (Possible	· · · ·
C65	41.5696118	-81.7282402	439294.2	4602270.8	2179678.9	694302.7	15.2	109.4	1.9	0.5	- 20	Linear Contact	-
C67	41.5711946	-01.7202310	439296.2	4603424.3	2179676.7	696012.6	15.3	25.5	3.3	0.0	0.4	Lineer Contact	-
C68	41.5707968	-81.7282010	439288,3	4602373.4	2179686.6	694645.0	15.Z	17.9	5.2	1.5	10	Low Reflectivity Patch (Possible Stagi	<u> </u>
059	41.5706172	-81.7281394	439293.8	4602360.3	2179703.8	694602.4	15.2	27.0	8.5	35		Los Reflectivity Patch (Possible	6 3
						and the second s						Singi	

93	MADER O	ieographic	NADER U	ITM Zone 17	NADER ONLY S	tata Plane North	scari Sonar Con	tacts	-	-	-		
10	Latitude	Longitude	East(m)	Sorth (m)	East(US	North (US	Bathymetry	Distance from Proposed	Length	Wildth (m)	Height (m)	Description	Associated Ma Anomaly ID
					servey feet)	sarvey feet0		Route (m)				Low Reflectivity Patch (Possible	8
670	41.5705225	-81.7280796	438298.2	4902349.5	2179720.5	694562.0	15.2	33.8	3.8	0.7		Skigl Grandha Ganthart	25
672	41.5705831	-41.7280016	439304.0	4603356.2	2178741.7	694 590 3	15.2	24.8	2.6	2.1	0.4	Low Reflectivity Patch (Possible	1
672	41.5701562	-81.7279966	439304.8	4602308.8	2179744.4	694-134.8	15.2	66.1	4.2	1.8		Slag) Orcular Contact	
674	41.5702992	-61.7279554	439310.0	4802524.7	2179760.7	694-487.0	15.2	49.8	2.5	1.6	-	Low Reflectivity Patch (Possible	·
-							16.7					Steg) Low Reflectivity Patch (Possible)	
LIS	41.5703030	1-92-7210572	420310.0	4992325.2	21/9/62.1	609492.5	15.4	=0.1	2.0	1.5		Sing) Loss Reflectivity Datch (Describe	
C76	41.5702668	-81.7276261	499319.1	4602323.0	2175750.7	694475.5	15.2	45.5	4.2	1.1		Sing)	
(77	41.6723950	-81.7277941	439323.8	4602567.2	2179792.6	695251.0	15.2	159,9	2.8	1.6	1	Low Reflectivity Patch (Possible Slag)	1.141
(78	41.5691421	-81.7270113	439386.0	4602195.5	2180017.3	694057.7	15.1	125.3	3.3	0.4	0.0	Linear Contact	+
C80	41.5719450	-81.7264907	439432.0	4602506.4	2180150.7	695090.2		168.4	3.1	1.0	1.4	Groular Contact	+
C81	41.5718742	-81.7263764	430441.5	4603498.4	2180382.2	695064.7	15.3	166.1	7.2	4.1		Low Reflectivity Patch (Possible Starl	1. 20.00
C82	41.5710858	-81 7263525	439442.7	4602430.9	2180191.3	694777.5	15.3	90.3	3.0	0.6	0.1	Linear Contact	M115, M214
C85	41.5717858	81.7262595	499451.2	4603488.5	2180214.5	695032.7	15.5	162.2	9.1	I.5	1.8	Low Reflectivity Patch (Possible Slag)	M82
(84	41.5707449	-81.7261001	499463.5	4602372.8	2180261.4	694653.7	15.2	67.2	2.8	1.8	0.6	Point Source (Probable	1.124
085	41.5214123	-41 7260088	49947177	0603446.9	3180394.3	604.997.2	15.2	135.9	13.6	4.2	12	Low Reflectivity Patch (Possible	MH15
		41.1444444	4494040		11010413	apress 2		1000			-	Slag Low Reflectivity Patch (Possible	
(16)	41.5714945	-81.7259543	439475.5	4602456.0	2180206.9	694927.4	15.2	146.1	6.7	4.9	-	Slag	N216
C87	41.5709615	41.7254051	438521.3	4602356.8	2180313.5	694593.3	15.2	96.1 78.5	9.5	0.5	0.2	Linear Contact	N0112
C89	41.5702816	-81.7252589	439533.2	4602320.8	2180493.1	694487.1	15.1	55.0	11.2	4.0	12	Low Reflectivity Patch (Possible	1 2.5
C90	41.5704549	41.7261787	439549.0	4607335.5	2182514.5	694549.0	15.1	25.6	184	184	1.4	Low Reflectivity Patch (Possible)	1 840
- 30	-2.0104908	-910/201/67	-33340.0	4942339.3	1100343	004.040.0	131	73.0	- 50	2.7	-	Slag Low Beflectivity Patch (Possible)	
(91	45.5703843	-81.7251217	498544.7	4602332.1	2180530.9	694524.9	15.1	71.5	4.9	11	1.1	Sleg	(*) ·
C92	41.5701709	-81.7245087	439595.6	4602307.9	2180696.7	696468.4	15.0	75.2	13.4	7.5		Lew Reflectivity Patch (Possible Slag)	
C93	41.5697446	-81.7244667	439598.7	4602260.6	2180711.6	694293.4	16.P	35.5	6.1	2.5	0.6	Low Reflectivity Patch (Possible	1
C 94	41 5505614		433555 K	44977347.3	3180715.4	604756.6	14.5	20.1	4.5		142	Low Reflectivity Patch (Possible	1.241
	11.3093020	-88.7499.224	438389.3	1002240.3	2180712/4	004.529.5	10.9	10.1	0.4			Slag! Point Source (Probable	
C95	41.5650934	-81.7244120	439601.7	4602077.3	2180731.9	603691.9	15.1	125.0	15	14	0.6	Boulderi	(14)
C96	41.5679893	-81 7243582	439606.1	4602063.5	2180747.0 2180768.5	603647.0 603634.5	15.1	132.9	3.4	0.5	0.1	Linear Contact Linear Contact	
696	41.5679791	-81 7240565	439632.9	4602064.3	2180635.0	693651.1	15.1	119.1	2.2	0.4	0.1	Lineer Contact	S
C100	41.5691417 41.5691421	-81.7259699	439539.6	4602153.4	2180845.5	694074.9 694067.7	14.5	3,3	8.5	5.9	0.4	Linear Contact Linear Contact	
C181	41.5679910	-81.7287505	499656.5	4602092.1	2180914.2	693546.9	15.0	135.6	2.5	0.4	-	Linear Contact	-
CE 02	41.5694327	-81.7237330	439659.6	4602225.5	2180913.4	694181.5	14.D	34.6	2.8	2.5	0.3	Slag	N155
CLOB	41.5679406	-81.7296402	439996.0	8.9802099	2180943.6	690538.1	15.D	106.9	4.2	0.3	-	Linear Contact Low Reflectivity Parch (Dominia	0 v.+
CI D4	41.5691001	-01.7235905	439570.6	4602197.A	2180951.0	694089.8	14.9	15.4	4.9	3.2	1.0	Slag	
CL 15	41.5692913	-81.7235862	439671.7	4602209.7	2180954.0	694130.3	14.9	26.7	2.8	0.9	0.7	Point Source (Probable Boulder)	(1.183)
C1.06	41.5692118	-81 7284997	439678.9	4602200.8	2180977.9	694101.6	14.9	22.5	1.8	1.0	0.5	Point Source (Probable	1.000
~	41 16916/1		A reserve	44011851	110102015	404/003.1	16.0	15.0			0.3	Low Reflectivity Patch (Possible	1.200
CLDR	41.5698718	-81 7253361	499992.3	4602163.0	2181033.8	693978.1	15.0	41	4.0	0.5	0.1	Slag! Linux Cantast	
C1.09	41.5694729	41.7252421	439700.6	4602229.6	2183047.6	694197.4	14.9	58.2	2.1	1.0	0.2	Point Source (Probable	1.0
C1 10	41.5684564	-81.7291098	499750.7	4602136.7	2181087.3	693827.3	15.0	35.4	3.0	0.7	0.1	Soulder) Linear Contact	
CLIN	41.5689415	-41.7234011	439711.8	4602170.5	2181087.9	694006.1	15.0	12.1	2.3	0.4	0.3	Livear Contact	-
C1 12	41.5675506	-81.7224855	433762.0	4602036.6	2181261.4	693501.7	14.8	97.6	4.6	5.0	14	Slag	0.00
CL13	41.5686835	-81.7224107	439769.2	4602141.4	2181277.6	693911.8	15.0	14.8	3.8	1.7	1.0	Low Reflectivity Patch (Possible Stard	1.00
c134	41.5687269	-81.7223625	489773.2	4602146.1	2181290.7	698927.5	15.0	20.9	3.8	11	1.4	Low Reflectivity Patch (Possible	1.042
			1446-1974	0000000		Contention of						Steg) Point Source (Probable	1000
cras	41.5681043	-81.7222909	439778.6	4603033.0	2181812.3	698.701.0	16.8	39.2	2.8	0.7	1.0	Boukler)	1.145
CLIE	41.5685281	-81.7222826	639779.7	4602124.1	2101313.2	693855.4	14.9	4.0	4.6	1.9	8	Slag	1.243
C\$ 37	41.5687008	-41.7222544	439782.2	4602343.2	2103320.3	693918.4	14.9	22.7	7.4	1.5	0.2	Low Reflectivity Patch (Possible Shart	1.00
C1.18	41 5082772	41 7222051	439285.5	4602056.7	2181335.7	693264.2	14.8	16.5	3.6	15	0.3	Low Reflectivity Patch (Possible	
												Slag Low Reflectivity Patch (Pomible)	1 200
CL19	41.5683570	-81.7221.252	439792.7	4602305.0	2181356.8	693793.5	14.9	5.6	9.1	3.4	2	Slegj	
CL 28	41.5682688	-81 7220727	499797.0	4602085.1	2181371.5	693761.5	14.8	12.0	41	0.6	0.2	Linear Contact Low Reflectivity Patch (Possible)	
un	41.9609524	-81-7220719	439/9/.4	4402135-5	1103/0.5	PAISBAC11	Ie'a	25.4	4.0	1.5	2	Slag)	M156
C1 22	41.5696007	-81.7219585	439907.0	4602253.0	2181398.1	694276.2	14.9	139.9	12.2	10.8	10	Slag]	1.53
C1.23	41.5683659	-01.7219340	439908.5	4002305.0	2181408.9	693797.2	14.8	3.0	1.2	1.1	10	Low Reflectivity Patch (Possible Skyl	3. the set
(125	41,5654471	-61.7717079	439577.6	4602134-2	2181470.0	625837.4	14.5	21.5	17	1.0	1.0	Point Source (Probable	M211
C124	41,5664187	41.7215501	419035.9	4001858.2	2181520.2	693117.8		363.3	2.8	12	11	Boulder) Rectanguler Contact	
C1 27	41.5684775	-81.7215392	435841.6	4602117.9	2181536.8	693838 T	14.8	29.7	1.5	1.5	0.5	Point Source (Probable	
	A1 8419417	at minut	-	ABRIDGE	1100000	600 mar 2						Point Source (Probable	1.1.51
1.18	+1.0678129	41.7215961	435641.5	4992044.5	2383539.8	695398.7	14.7	34.9	2.0	1.0	0.9	Boulders Bount Science (Bachable	- net
C129	41.5682537	-81.7212608	439964.6	4602092.9	2383599.7	693758.0	14.8	19.1	1.8	0.4	0.5	Boulder:	M157
CF 30	41.9677909	-81.7207627	439905.7	4602096.7	2181731.6	693/576.0	14.8	9.8	3.7	0.5	0.1	Linear Contact Line Reflectivity Patch (Poscilida	
CE 81	41.5661109	-81.7201661	439953.9	4801854.9	2181900.2	692982.1	14.8	144.9	4.4	2.0		Slag!	

_						Side	ican Senar Ceel	tacts					
1.16	NADES G	eographic	MADES U	TM Zone 17	NADER ONLY S	tate Plane North	Barbana atras	Distance from	Innit	MUM	Harte	1 conserver 1	Annacistand Mars
10	tattade	Longitude	Eastint	North Inc.	East(US	North (US	ini	Proposed	dan)	(m)	(m)	Description	Anomaly ID
10		engrana.	second.	researched.	servey feet)	sarvey feet)	6.9	Route (m)			414	3	Sector Sector
12	41.5659769	-81.7201452	439955.5	4603839.3	2181906.4	692931.1	14.6	157.7	8.2	5.7	1.0	Low Reflectisity Patch (Possible	1 1.190
33	41.5686979	-81 7201278	439959.5	4602343.4	2183902.3	693922.6	14.8	107.8	2.4	1.2	1.0	Reitangular Covitact	
134	41.5676314	-41 7200550	433954.6	4803023.0	2183935.6	6935347	14.8	7.0	2.0	0.8	0.5	Point Source (Probable	8
_												Soulder) Low Reflectivity Datch (Describing	
CLBS	41.5676987	-81.7197246	419992.2	4602030.2	2182015.8	693559.5	14.9	25.8	1.7	21		Slag	1.00
C138	41.5675313	-81.7196271	440000.2	4602011.5	2152543.1	603-895.7	14.8	14.4	2.1	1.1	0.6	Point Source (Probable	2 2 2 2
(137	41 5652810	41 7156278	440000.0	4601878.5	2182647.2	693226.1	14.6	58.2	37	0.0		Soutier)	M192
CA.PC.				********	ALCONT. A	0001101	10.0				-	Low Reflectivity Patch (Possible	61152
CT 28	41.3678191	41.7195825	440004.0	4602021.3	2182055.9	695593.8	14.8	24.7	0.5	4.5		Sleg)	M156
C199	41.9674205	-81.7195334	440007.9	4601599.2	2182869.1	698458.6	14.8	7,4	2.5	1.7	1.1	Low Reflectivity Patch (Possible) Stari	
CL40	41.5689559	-81.7194864	440013.2	4602169.6	2182076.9	694018.2	14.8	158.7	3.6	2.4	0.5	Linear Contact	+
C141	41.5668873	-81 7193049	440026.4	4601899.8	2182133.3	693264.9	14.7	35.4	2.6	0.4	1.0	Linear Contact	
C142	41.3684296	-81.7191049	440344.5	4602130.9	2122183.0	699827.8	14.9	122.8	3.5	0.4	-	Linear Contact	
C149	41.5673790	-81.7189203	0.920046	4601996.0	2162237.0	693454.6	14.8	27.8	3.4	0.6	0.1	Linear Contact	
CL45	41.5665241	-01.7161643	440112.9	4601598.8	2182419.3	693135.1	14.0	28.9	3.0	0.3	0.3	Linear Contact	
C1.48	41.5665197	-81 7181509	441172.5	4651858.7	2162450.3	693133.8	14.8	74.8	1.0	0.8	0.6	Point Source (Probable	
	21 56 595 72	.01 2121000	445334.5	2621668.6	1181715.6	601251.0		185.4	4.7		0.1	Boulder)	
CL48	41.5665584	-81.7147141	440200.5	4601575.9	2162720.6	695083.4	14.5	97.5	3.7	0.5		Linear Contact	
C1.45	41,5668368	-81 7139193	440475.0	4601874.9	2183608.8	699077.4	14.4	127.2	6.8	0.2		Linear Contact	C 040 0
CL50	41.5642624	-81.7135349	440905.1	4601644.4	2183720.0	692322.6	14.2	59.1	4.0	0.9	0.3	Point Source (Proitable	1.253
(14)	41.5654104	-81 7120571	680529.2	4601771.6	2183763.1	692741.6	16.1	62.7	2.0	0.6	0.1	(soutiler) Linear Contact	1.1.1.1.1.1.1
10.00	11.00000000	31.7104371	444469.0	488477378	1104100	000.001.0	10.0	1000	100		W.3	Low Reflectivity Patch (Possible)	1 255
c152	41.3654432	-41.7120650	440528.8	4001775.2	2184119.2	002758.7	16.4	115.4	10.6	3.1		Slag	2 ⁽¹⁴⁾ 3
C1.53	41.5652723	-81.7120203	440632.3	4601735.5	2184132.0	692094.4	14.4	100.0	1.6	1.5	0.9	Point Source (Probable	2.0
	1		Table Contract	They be property	10120-0020-001	000000000	10000	1.400.00	1.000	20.025	1000	Point Source (Prohable	1.
C154	41.5652956	-81.7119548	440637.6	4601735.8	2184150.5	692630.1	14.4	85.4	1.4	0.8	0.7	(Soulder)	1 St#12
C155	41.5622040	-81 7113199	440587.9	4603434.4	2164333.8	691578.1		170.5	2.4	0.5	0.2	Linear Contact	
C156	41.5636074	-81.7112257	440697.1	4601570.1	2184354.9	692099.7	14.5	30.1	3.8	0.3		Linear Contact	
C157	45.5645572	-81.7111407	440705.0	4601675.5	2184375.0	692435.0	14.5	65.7	8.0	0.5	0.1	Unsar Contect	
C158	41.9621915	-81.7108191	441729.9	4601412/8	21844/3//	691574.7	16.4	151.5	1/8	0.4	0.5	Linear Contact	-
C160	41.5632394	-81.7103922	440774.6	4601529.6	2184611.6	691957.9	16.4	28.5	5.2	0.4	0.1	Linear Contact	-
C161	41.5632090	-81.7101770	440788.2	0601525.2	2184643.2	691947.1	34.4	26.8	2.0	0.4	· •	Linear Contact	
C162	41.5641429	-01.7101760	440785.1	4001529.0	2104640.4	692287.4	14.5	64.1	8.3	4.0	0.5	Low Reflectivity Patch (Possible	-
			for some of									Sing Point Source (Dephable	-
C183	41,5636117	-81.7101548	440785.4	4003589.8	2184646.0	692095.9	14.4	18.5	1.2	11	0.6	Boulder)	1.00
(164	41.564818	31,7101038	440291.3	4601655.3	2184656.4	692324.6	14.5	91.8	824	64	1.	Low Reflectnoty Patch (Possible	1 640
					Addresseet	Accession of	10.0			and.	-	(Slag)	
C1.65	41.5645768	-81.7100824	440793.8	4601676.9	2184664.6	692445.6	14.5	110.1	4.8	2.8	38	Low Heflectivity Patch (Possible) Slavi	
		-21-000					0.000	in and the second	1000		-	Low Ballectivity Patch (Possible)	
1196	43.3547833	-31.7099927	44080170	4963106.9	2384688.4	690324.5	14.5	134.6	10.4	8.5	. ¹⁰	Sbg	
C167	41.5620329	-81.7098601	440909-5	4001304.4	2184783.8	691519.4	16.4	128.5	1.8	1.6	0.4	Point Source (Probable	N144
1145	41 5435547	.41 7005.054	440033.1	4651567.6	31647661	6020201	14.4	23.7	3.5	0.5	0.1	Boulder)	
CLEE	41.5630641	-01.7095612	440651.9	4601530.7	2104066.3	691903.6	14.4	6.3	3.0	0.5	0.6	Linear Contact	
C170	41.5625297	-81 7090747	440875.4	4003449.0	2154947.1	691702.4	14.4	45.6	7.2	0.4		Linear Contect	(a) (a) (b)
C171	41.5617026	-81.7050549	440575.5	4601557.1	2104955.2	691401.0	14.5	128.3	7.2	1.0		Linear Contect	17 S.#77 St
C172	41.5627621	-81,7087721	440900.9	4603474.6	2185025.1	691787.8	14.4	13.9	7.5	0.6	0.2	Linear Contact	1.1.8.1.1
CL73	41.5628201	-81.7052814	440941.9	4603463.8	2165165.2	691812.3	14.4	22.1	7.3	0.6	0.1	Lineer Contect	
CL 75	41.5609433	-81.7065854	441081.6	4601271.2	2185633.6	691130.5	14.1	108.0	4.4	0.5	0.2	Linear Contact	-
C1.72	41 5607366	41 1061521	441117.6	4401354.6	2105751.4	691/778 1	14.1	99.9		0.0	0.5	Point Source (Probable	1
												Bou klert	1. 1950
CL 77	41.5610523	-81 7052342	0411033.0	4601283.7	2185841.2	6911224	16.0	02.E	1.8	0.4	0.1	Linear Contact	
		- and the second	-TREESE A			destra.4				0.5		Point Source (Probable	
C179	41.5615467	-81.7055942	641104.4	4601283.1	2185904.1	691207.1	14.0	63.6	2.5	0.7	0.0	Riculder)	1.135
C1.85	41.5605036	-81.7047237	441238.4	4601221.1	2188344.5	690975.0	14.0	71.0	1.4	0.9	0.6	Point Source (Probable	0.400
						4000000	45.0					Point Source (Probable	
ci fi	41.5604539	-81,7046716	441240.7	4603215.5	2188158.9	690957.0	13.9	75.8	2.2	1.1	0.4	Bouldert	(1.1.1) (1.1.1)
C1 82	41.5600491	-81.7045812	441247.9	4601170.5	2186185.0	690809.7	13.0	109.5	1.1	0.7	0.5	Point Source (Probable	1.040
					Sections.	(Assessed)	1.0000	and the second s	-	1000		Boulders Point Source (Postankia	1.001
C1 83	41.5597743	-\$1.7044097	441261.9	4001139.9	2186332.9	690710.0	13.9	129.4	0.9	0.6	0.5	Boukler)	
C1.04	41 5608955	41 7016 724	441724.4	4601364.0	2166430.0	601120.7	13.0		10			Point Source (Probable	21
	11.3031933	-46.7006729	1915-121.1	4963294.0	2320120.9	691120.7	11.9	**	10	0.9	0.6	Boulder)	1.1
CLES	41.5618126	-41.7036052	441330.9	4001365.6	2186446.2	691454.7	13.9	101.3	10	0.7	0.0	Lineer Contact	
CLBS	41.5617893	-81.7035322	441336.9	4601363.0	2186466.3	691445.4	13.9	101.9	1.8	0.5	0.5	Souther!	1.20
eres.		.41 7023-014	APTROP 1	4631971.6	HIRESPE E	AND DOM: N	12.0	93.8		87	0.6	Point Source (Probable	1.000
C197	41.0014015	41-1050313	447345.1	4003322.0	1100300/0	0013143	13.5				4.5	Boulder)	1.12.0
C1.88	41.5614252	-81.7033161	441354.6	4601322.4	2186536.6	691314.3	13.8	75.2	1.6	0.9	0.6	Point Source (Probable Boulder)	1.8*8
				-		400000	140					Point Seurce (Probable	1
C189	41.5592663	-91.7032146	441352.8	4601082.7	2186534.2	690527.6	13.6	184.8	11	0.7	0.6	Boulder)	1.1
CL90	41.5608771	-81.7006744	441574.4	4601259.8	2187251.4	691121.2	13.3	137.9	2.3	0.4	0.2	Linear Contact	+
C191	41.5583372	-\$1.7005013	441903.2	4600977.6	2187362.0	690196.7	13.2	104.2	6.D	0.5		Linear Contact	(*)
C192	41.5590858	-81.6991500	441099.9	4003039.9	2187674.6	690472.3	11.2	14.9	0.7	0.4	0.6	Boalderi	1.8%
-	41 88 84 1		441714.5			4000004	10.0					Point Source (Probable	
as and	- 1 NO.001 NO.	-61.5969471	441/15.5	4001003.8	2187730.5	690446.6	13.5	10.0	12	0.7	U.B	6oulder)	
C193	41.20001.20		1000 C		COLOR SCALS		13.4	52.0	1.4	0.9	0.6	Point Source (Probable	9 Dec 8
CL93	41.5591477	-81.6505757	441764.5	4603066.2	2187888.5	000490.0	4,017					the same behavior	
C195	41.5591477	-81.6685757	441764.5	4603066.2	2187888.5	600496.0					7.5.5	Boulder) Point Source (Probable	
C195 C194 C195	41.55836477	-81.6905757 -81.6979033	441764.5	4603066.2 4600567,4	2187888.5	690174.7	13.5	15.4	1.9	0.7	0.5	Boulder) Point Source (Probable Boulder)	
C193 C194 C195 C196	41.5591477 41.5582904 41.5563200	-81.6985757 -81.6979033 -81.6971195	441764.3 441803.1 441865.7	4603066.2 4600567.4 4600753.5	2187888.3 2188018.5 2188239.5	690174.7 689469.7	13.5	15.4	1.9	0.7	0.5	Boulder) Point Source (Probable Boulder) Linear Contact	-
C193 C194 C195 C195 C195	41.5582804 41.5582804 41.5563200 41.5564578	-81.6979033 -81.6979033 -81.6971195 -81.6971195	041764.3 041803.1 041865.7 041919.6	4603066.2 4600567.4 4600753.5 4600756.3	2187888.5 2188018.5 2188236.5 2188413.1	690174.7 699469.7 689469.7	18.5	15.4 172.7 113.9	1.0 2.5 2.1	0.7 0.7 1.4	0.5	Boalder) Point Source (Probable Boalder) Linear Cantact Point Source (Probable	- M143
C195 C194 C195 C196 C197	41.5591477 41.5582934 41.5563200 41.5564578	-81.6979033 -81.6971033 -81.6971195 -81.6964873	441764.5 441803.1 441865.7 441919.6	4603066.2 4600567.4 4600753.5 4600766.3	2187898.5 2189018.5 2188230.5 2188413.1	690174.7 689469.7 689521.5	18.5 18.2	15.4 172.7 113.9	1.9 2.5 2.1	0.7 0.7 1.4	0.5 0.2 0.6	Souther) Point Source (Probable Souther) Linear Cantact Point Source (Probable Boulder) Point Source (Probable	- N143

						Side	scan Sonar Con	tacts					
	MADER C	eographic	MADER U	TM Zone 37	NADER Office S	tate Plane North		Distance from				The second second	S
10	damash.	Include	Cont line	man fait	East(US	North (US	Badtyreetry	Proposed	Length	wikes.	Height	Description	Associated Mag
	Pictures.	torgade.	case(na)	second (set	servey feet)	narvey feet)	6.0	Houte (m)	444	444	040	ST CONTRACTOR	second in
-		-	100000			4000463 B	5.54	22.2				Point Source (Probable	C 8
C138	42.9979488	-81.0900171	941333.0	0806830.8	5166920.8	690095.2	19.4	47.4	**	0.0	0.6	Bou klert	225.00
C200	41.5595616	-81,6659293	441968.1	4603030.6	2186557.4	690325.9	13.5	108.0	3.6	0.7	0.3	Linear Contact	
C225	41.3369938	-81.69080124	441978.7	44630333	188392-1	696327.7	18.2	108.3	5.4	0.6	0.4	Low Reflectivity Patch (Possible)	
C205	41.5568203	-01.6949755	442346.0	4600605.6	2188824.6	609657.4	13.1	37.9	7.2	1.7	0.2	Slagj	
C200	41.5570300	-01.6847107	442068.2	4600629.3	2100096.4	609735.6	13.2	6.2	4.6	0.4	1.34	Linear Contact	1 - 1 a - 1
C204	41.5558011	-81.6946811	442059.6	4600682.2	2188906.6	689285.B	13.2	125.2	1.0	0.7	0.5	Point Source (Probable	2 a 1
					hopping h	200,223,0	14.4					Goulder)	
C206	41.5592301	-01.004-00L0	442345.0	4000/41.9	2100906.2	A294272.8	13.5	141.7	41	0.4	0.2	Linear Contact	
		AL COLLARS				100100						Point Source (Probable	
C187	41.3039597	-81.69(1853	442277.5	4600660.8	2388592.6	689195.7	18.1	30.9	11	0.8	0.5	Soulder)	(
C208	45.5571185	-81.6921.246	442284.0	4600836.4	2189603.9	689772.0	13.8	105.3	3.0	0.3		Linear Contact	
C218	41,8969012	-81.6919940	442294.8	4600768.1	2189641.7	689508.7	18.2	50.9	6.6	0.4		Linear Contact	+
C230	41.5572323	-91.6919918	442301.3	4600625.0	2109645.0.9	609215.2	13.2	115.0	8.1	0.5		Linear Contact	
C212	41.5562366	-81.6919059	662301.4	4600738.5	2189666.7	689451.7	12.2	28.5	4.1	0.5	0.2	Linear Contact	
C213	43.5570168	-01.6910770	442304.5	4600625.3	2109672.0	609736.8	13.2	105.7	2.6	0.5	0.5	Lineer Contect	+
C234	41.5572423	-01.6017529	442315.1	4600650.3	2189705.2	609819.3	13.2	132.7	4.1	0.5	0.1	Linear Contact	
C215	41.3555306	-81.6899.598	442464.8	4600659.0	2190207.2	609200.2	12.0	39.0	2.5	1.0	0.5	Lineer Contact	
(235	41.3003161	-91.0090.221	0.8/14280	4000037.3	2190239.4	669195.0	12.9	42.5	12.5	2.4		Linear Contact Line Ballartosty Patrik (Possible)	
(217	41.5552677	-81.6897695	442478.7	4600625.7	2190254.6	689104.9	12.9	20.2	14.5	2.4	0.7	Sing)	1.191
1210		41 (2007.000)	443,491.7	4636438.5	3186364 7	6007171	10.0	124.5		0.5	0.5	Point Source (Probable	2550
1438	*1.3358495	41.9690.992	042015	4900448.3	5190806.7	688312.1	17.8	151.8	51	17.2	0.5	Soulder)	2
\$219	41.5562301	-81.6895567	462497.8	4606736.4	2190309.5	689456.1	12.9	\$22.4	7.8	0.8	0.1	Linear Contain	
1222	41.9543942	-81.6690621	442536.9	4646532.3	2190451.2	648788.4	12.8	36.3	2.6	0.4		Linear Contact	
	AL ADDRESS	-41.0601.010	082398.7	**********	a tangata a	003313-1	10000	109.7	6.2	12.4	4.8	Point Source (Prohable	
C222	41.5532781	-61.6685019	442599.4	4606407.8	2190663.1	688353.7	12.6	114.4	1.0	0.7	0.6	Boulder)	
C223	41.3526391	-51.6867105	442731.5	4000335.0	2191100.6	600154.9	12.5	112.6	E.9	0.7	0,2	Linear Contact	0 0+10 b
C224	41,5541710	-81 6666219	442740.2	4800505.9	2391119.8	660713.3	12.7	40.0	7.4	0.4	0.1	Linear Contact	
\$225	41.5554069	-81.6864658	442752.6	4600420.9	2191165.1	688435.5	12.6	28.1	1.1	0.7	0.5	Point Source (Probable	
					And and a second se							Boulder)	
C228	41,0005000	-61.6665724	992792.1	4800603.5	2191164.1	009140.0	11.7	150.0	19.0	0.9	0.2	Desiret Science (Peering ble	Mrs
C227	41.5517972	-81.6859713	442792.4	4600235.2	2191306.2	687828.2		170.6	1.8	0.9	0.5	Boukler)	
C228			447303.7		2101206.2	400313.4	15.2	47.5	1.1			Point Source (Probable	1 2237
C228	43.3041970	-91.09209.949	.0047/97.1	0000005.0	2191306.3	085714.6	12.5	97.6	1.5		0.6	Boukler)	
C229	41.5541516	-01.6058827	442001.9	4600503.2	2191332.2	688708.1	12.7	67.B	1.5	1.5	0.6	Point Source (Probable	243
				1000010 5		1001051	15.0					Boulder)	
1290	41.392/3/3	-91 BEDEUKU	4922017.0	4005046.2	2161948-8	0001533-1	12.0	99.5	- 0.U	0.3		Unear Contact Oniet Source (Drohable	-
C251	41.5539001	-81.6657192	442825.3	4600475.2	2151367.8	602616.9	12.7	43.5	2.1	0.8	0.7	Boulderi	1.00
	and standards	as recents	1000000	22222222	Accession of		100.07	10.0				Point Source (Probable	1 0000
1232	41.000000	10000000	440027.7	90004/3/5	21910/5/0	600012.5	107	50.0	- 1-2	0.0	.0.5	Bouker)	
C238	41.5540599	-81.6855265	442831.5	4600492.8	2153420.0	688675.6	12.7	73.2	3.6	0.2	0.1	Lineer Contect	S
234	41.5540713	-81.6854649	442836.6	4900484.0	2153436.8	688679.9	12.7	76.8	2.4	0.5	0.1	Linear Conflact	-
(234	41.3349087	-81.68583978	442898.0	4600566.7	2191554-8	688565.0	12.6	73.8	2.6	0.5	0.2	Linear Contact	-
C237	41.5533787	-41.6846558	442903.5	4600416.6	2193660.6	688429.6	12.6	41.9	2.9	0.5	0.1	Linear Contact	
C238	41.5532757	-81.6845677	442910.8	4600405.1	2191685.1	6493992.3	12.5	35.4	4.5	0.5	0.2	Linear Contact	<pre>0 + 0 2</pre>
C239	41.5539354	-01.6045295	442934.5	4600478.3	2193699.3	609632.R	12.6	101.2	2.3	0.5	0.1	Lineer Contact	(*) (*) (*
C240	41.5545156	-81.6843472	442930.5	4600544.0	2191741.1	600852.0		366.9	2.5	0.5	0.1	Linear Contact	
C241	41.3540052	-81.6043075	4429333.1	4000465.9	2191753.6	0000358.8	12.6	116.9	4.0	0.4		Linear Contact	
	44.00000010	-92.0042712			1101/04/0	00004120	11.0	440.7		0.0		Circular Contact (Probable	
C243	41.5508531	-81.6838111	442971.7	4600135-8	2191900.4	687511.6		169.8	13.2	11.9	13	Oredge Spoil)	M(102
1244	41 8521990	-91 6857997	442979.9	201003847	2101006.2	687998 4	354	29.4	24	0.0	0.5	Point Source (Probable	1 200
	41.000.0000		seener and		essieres.		1664	जरूर .				Boukler)	1.000
245	41.5564578	-81.6964873	641919.6	4600796.3	2188412.1	689521.5	13.2	133.9	36.7	1.0	1.0	Crouter Contact (Probable	8.42
(246	41 5531469	-81 6010530	442995.2	0600325.7	2101967 9	688365.2	12.4	62.5	24	0.5	0.3	Linear Contact	5 97a. 1
C247	41.5536321	-41.6834705	449332.6	4600443.9	2191904.2	688525.0	12.5	114.2	4.5	0.8	0.2	Linear Contact	+
C248	41.5539318	-01 6053425	443013.5	4600477.1	2102018.2	600634.5	12.5	140.5	2.0	0.4	0.1	Linear Contact	-
C245	41.5541202	-81 6855277	449015.4	4600505.6	2192022.8	608721.4	1.20	172.5	1.5	11	0.5	Point Source (Probable	1.047
		-			1163555.5		17.4				-	Boulder)	
(250	41.5524949	-81.6651299	449021.6	4000317.5	2152055.9	600111.3	12.4	13.2	5.0	0.2	-	Linear Contact	
		41.00000000		ACREATED.I'	2462240	1000000		2012	10	4.7		Ortular Contact (Probable	
08	41.5514445	-81.6829157	443046.9	4606200.7	2192148.5	687729.4	12.2	76.3	5.6	8.3	0.5	Credge Spoil	ML2
210	41.5514725	-81.6819723	443050.6	4600003.2	2102155.3	687739.7	12.1	71.8	6.6	51	0.5	Groular Contact (Probable	1 B
	-and press	an order of the		- second d	ensema	Constant.		199		1940	4.8	Credge Spoil)	U KEN
C254	41.5504814	-81.6827315	443051.4	4600053.7	2192197.2	687378.9	12.5	162.6	14.5	15.8	LD	Creater Contact (Probable	1.523
				100.000							-	Point Source (Probable	
C255	41.5539100	-01.6026490	443071.3	4600474.9	2192206.0	600630.5	13	174.8	1.0	0.9	0.5	Goulder)	12.2
(255	41 35471 64	-	403032	4855118.4	2182247.5	ARTIST I	17.4	1919	191	14.1	11	Orcular Contact (Probable	MILLIO
-1.20		31.00(23690		40000129.0	111120-112	00.1404.0		132.3	2.712	14.2		Oredge Spoil)	H-140
C257	41.5510998	-81.6823615	443092.8	4600157.6	2192296.5	687590.6	12.5	91.5	15.9	14.6	0.8	Orcular Contact (Probable	ML3
-			Sec. 7856	2010000114	100000000		1 3 25	200	-		-	Credge Sport	0.56
(256	41.5511747	-81.6823186	443036.5	4600170.4	2192307.8	687632.6	12.4	78.6	\$4.0	13.7	0.8	Credge Spoill	3.*2
	as personal			against a	3103327.4	Apparent A	int	157				Condex Contract Contract	1 8
-128	41.3924078	-41.8622663	004101.9	4606907.2	2192317.9	6490382.0	124	43.5	+5	1.5	0.1	Circalar Contact (Probable Tire)	852
C260	41.5501032	-81.6818890	443131.5	4600051.1	2182419.4	687243.3	1 (P)	564.9	3.8	1.6	0.3	Linear Contact	1.1.1
C251	41.5571021	-01.6010519	441116.2	4606273.0	2193482.4	687971.7	12.5	30.4	1.9	0.7	0.6	Point Source (Probable	1 1.42
1342	AL REAL PLACE		465744.7	4800000	3163833.7	A205404 T	5023	187.6		0.7	0.5	Goulder)	
(243	41.55405434	-81.66114695	443583.4	4606434.9	2193563.1	607189.5	17.4	197.8	77	0.7	0.0	Linesr Contact	8/105
		00 001100P		seconda.r	********	war spills		1000				Point Source (Probable	masid
C264	41.3536304	-81.6809926	995207.5	4800220.1	2152665.2	667802.0	12.5	19.0	1.4	0.7	0.8	Boulder)	1.5
(265	41.5516517	\$1.6805545	443244.0	4600222.2	2192789.0	687810.9	12.6	33.7	3.7	0.5	0.1	Lineer Contact	
(265	41.5524868	-81.6799997	443291.0	4600534.5	2152538.0	688116.6	12.5	142.3	3.5	0.5	0.4	Lineer Contact	
(26)	41.5493883	31.6798299	443302.5	4399930,4	2192995.1	686388.1	12.4	152.8	2.0	1.5		nectangular Confact	20 S. # C. 3
C268	41.5509326	-81.6796207	443321.3	4600041.7	2399647.1	687551.3	12.4	6.3	1.6	0.7	0.6	Boulder)	1.00
C265	41.5516782	-81 6795035	443331.7	4600224.4	2159076.6	687823.3	12.4	83.5	3.2	0.3	0.1	Linear Contact	
(2.15	41 5571845	.016794339	441738.0	4800380.7	2153051.0	600004.5	12.5	125.0	12	12	0.7	Point Source (Probable	8
					erested.	Construction of						(Goulder)	1 1 1 1 1

_						Side	can Senar Cen	tects			-		
1	MADES G	eographic	ILADER U	TM Zone 37	NADEL ONLY S	tate Plane North	Bathymetry	Distance from	Length	Width	Height	1 1201200	Associated Mag
10	Latitude	Longitude	East(m)	North (m)	East(US servey feet)	North (US sarvey feet)	(m)	Proposed Route (m)	(m)	(m)	(m)	Description	Anomaly ID
73	41,5510600	-81.6787136	443397.0	4600155.3	2199294.9	687600.1	12.6	85.1	1.7	0.6	0.6	Point Source (Probable Boalder)	0 1980 - 1
72	41.5515349	-81.6763774	643433.0	4600207.7	2189412.7	687778.2	12.5	118.9	1.7	0.6	0.6	Point Source (Probable Boalder)	1. e 1
273	41.5510539	-81.6781199	9.206620	4600154.2	2193458.5	687599.4	12.6	78.6	12.2	0.9	0.2	Linear Contact	() - () + () - ().
2274	41.5500291	-81.6779915	443455.4	4600040.3	2103406.1	687225.3	12.4	16.1	4.1	0,7	0.6	Linear Contact	<u>(</u> (4) (
275	41.3511723	-81.5779343	445462.1	4500157.2	2193507.8	687643.0	12.6	97.4	1.0	0.7	0.6	Boulder)	1 (4) 1
278	41.3518535	-81.6776264	445455.4	4600243.8	2155589.7	667695.6		177.0	1.5	1.0	0.7	Point Source (Probable Boulder)	5 500
277	41.5519197	\$1.6775816	443492.2	4600250.0	2159601.4	687916.2	. (*	184,3	14	1.2	0.6	Point Source (Probable Boulder)	
278	41.5507812	-81.6770972	443531.6	4600123.2	2158738.3	687502.6	12.5	93.0	3.3	0.2	0.1	Lineer Contect	
12.80	41.5510285	-81.6768499	043552.8	4600150.5	2193806.2	687593.4	12.6	127.1	3.3	0.2	0.5	Linear Contact	
281	41.5682126	-81.6766111	663509.9	4589637.8	2100880.2	686568.0	11.9	137,6	16.4	15.9	0.6	Groulay Costact (Probable Oradire Sociili	161
2331	41.5462126	-41.6766111	662569.9	4599637.8	2193860.2	6065551.0	12.3	100.7	5.6	1.0	1.0	Linear Contact	1.4
282	41.5404095	-81.6763690	445590.5	4599068.4	2150545.5	600993.6	11.0	95.9	13.0	15,1	0.4	Orcular Contact (Probable Oredge Spoil)	1.141
285	41.5484909	41.6765290	443593.7	4599668.5	2199956.4	686670.1	12.5	107.0	19.6	17.3	1.5	Orcular Contact (Probable Oracles Spoil)	1.1.1
284	41,5508066	-81.6763271	443595.7	4600103.4	2198545.7	687441.0	12.5	91.8	4.2	0.5	0.2	Lineer Contect	
285	41.5485524	-81.6762871	443597.2	4599675.3	2199967.7	686692.7	12.5	136.0	11.9	15.9	0.6	Circular Contact (Probable Dredge Spoil)	M34, M39
286	41.5508125	-81.6760986	443634.9	4600126.1	2194011.5	687516.6	11.9	70.4	5.7	0,3	+	Linear Contact Conular Contact (Probable	
287	41.5486795	-81.6760787	443415.1	4599629.2	2104035.4	686739.5	11.5	60.5	14.4	96.9	0.7	Oredge Spoil)	MIRS
280	41.5487472	-81.6759931	443621.9	4599696.7	2194947.5	606764.4	11.6	43.6	\$7.3	18.4	11	Oredge Spoil)	M200
280	41.5489584	41.6758657	443632.6	4595030.1	2154061.9	686838.9	12.0	245.8	14.7	10.0	0.7	Oradga Spollj	2.00
290	41.5463369	-81.6747615	443722.5	4599628.3	2154392.9	685889.4	12.4	155.2	0.9	0.7	0.7	Point Source (Probable Soulder)	243
291	41.5504215	-81 6746781	443733.0	4600061.7	2154401.7	687377.8	11.5	216.3	4.4	0.3		Linear Contact	
292	41.5465075	-81.6744406	445749.5	4599647.0	2154480.2	6859352.4	12.1	229.3	15.3	1.1	0.4	Lineer Contect Point Source (Probable	
	11 10 10 10 10 10 10 10 10 10 10 10 10 1		separat.	A239864.3	2194804.5	003939.1	10.4	100.0				Soukler) Point Source (Probable	
294	41 5497804	-81 6736/843	442815.4	4600009.9	2100675.9	687146.0	15.3	544.0	1.0	0.0	8.0	Boukler) Dojat Source	
276	41,5462036	-81.6735-062	445527.0	4599612.7	2154736.4	605844.0	12.0	224.8	1.5	11	0.9	Point Source (Probable	
267	415456141	41 6724721	449917.9	4100446.6	2154013.1	APSATE D	17.0	216.7	15	0.0	0.1	Boulder) Linear Contact	
256	41.5455854	-81.6724516	443924.5	4599543.4	2155017.8	685621.5	12.2	111.3	3.0	0.6	0.2	Linear Contact	1.1.4.5.5
295	41,5466707	-81.6722098	443935.7	4555663.7	2155090.2	686017.6	12.2	10.8	1.4	0.8	0.4	Lineer Contect	
300	41.5478349	-81.6719941	443954.6	4599792.8	2195145.2	686442,4	12.2	128.5	1.3	0.8	0.6	Boulder)	
100	41.5469226	-81.6719892	44393993.7	4599528.7	2155342.4 2165276.2	686381.9	12.2	59.0 69.1	2.9	1.0	0.5	Linear Contact Linear Contact	
303	41.5466524	-81.6711224	4440326.3	4599661.6	2195387.9	686016.0	11.2	\$33.2	1.0	0.0	0.5	Point Source (Prolitable	
D4	41.5403643	-81.6710955	4440223.1	4596962.8	2105417.1	681722.7	11.3	385.6	2.6	4.1	0.9	Point Source	de la enclarita
105	41.5421899	-81.6707211	4440355.0	4599365.3	2195513.2	604328.9	12.1	32.3	3.5	1.9	-	Linear Contact Point Source (Probable	
300	41.34/32/3	-91.6/0/04/	000001.9	4599/57.3	2190499.2	600333./	141	255		0.9	0.5	Boulderj Point Source (Probable	
307	41.5469167	-81 6705619	444065.0	4599690.0	2199515.1 2104676.7	686111.3	17.0	711.7	1.9	0.6	0.6	Boulder) Linear Contart	
309	41.5467378	-81.6701856	444104.5	4599669.9	2195644.0	686047.3	11.5	435.5	2.5	0.4	0.2	Lineer Contect	
(319	41.5408811	-\$1.6701475	444102.7	4599005.6	2195674.8	688913.5	11.7	184.0	2.7	0.7	0.7	Linear Contact	5 141 2
311	41.5445263	-81.6700519	444113.8	4599434.2	2105668.3	685241,9	12.1	71.7	21.8	14.2	1.7	Loss Reflectivity Patch (Possible Slag)	1.849
312	41.58611.50	-81.6699625	444122.1	4599600.6	2195705.6	685821.0	10.6	541.4	2.6	0.8		Linear Contact Low Reflectivity Patch (Possible	
-113	41.5580676	-01.0690703	494122.7	4566707.1	2195750.5	667889.1	12.0	1.00	5.0	8.2	2	Slug	1.550
C314	41.5477103	-01.6690294	444125.1	4599777,6	2155788.2	605957.2	12.1	32.7	4.5	0.4	0.2	Linear Contact Linear Contact	
328	41.5464516	-81.8697290	444142.5	4599637.8	2155770.3	605944.2	10.5	565.0	3.1	0.3	0.1	Linear Contact	
(317	41.5368635	-81.6697192	444134.9	4998573.3	2195806.0	682450.8	10.6	528,1	33.1	14.8		Low Reflectivity Patch (Pomible Sleg)	1. (89)
1016	41.5589069	-81.6696/052	444138.8	4596700.2	2199811.3	682867.5	10.0	854.7 532.9	5.0	1.8	0.2	Grouler Contact Ornder Contact	M71
320	41.5375090	-81.6695359	4441.90.8	4998844.5	2195853.9	682685.3	11.5	414.2	10.8	21	-	Linear Contact	+
C323	41.5405298	-81.6694702	444159.9	4596900.2	2195861.4	683787.3	11.5	415.4	2.8	0.5	0.3	Linear Contact	M139
322	41,5404999	-81.6694588	444159.8	4598576-3	2105864.6 2105864.6	683776.4	12.0	473.0	2.9	3.0	0.3	Linear Contact Linear Contact	
C324	41.5462797	-41 6690122	444177.0	4599618.4	2195884.7	605282.7	9.8	634.5	11.9	3.9	-	Linear Contact	+
325	41.5336501	-81.6693049	444165.7	4598237.2	2195930.5	601203.9	12.0	133.0	1.0	0.8	-	Ortular Contact Point Source (Probable	
328	41.5479957	-\$1.6695047	444179.1	4595007.9	2155880.8	606504.7	11.5	506.6	11	0.7	0.8	Boulder)	
328	41.5477931	-81.6689345	444209.8	4599786.2	2195966.4	686435.1	12.0	16.3	3.3	0.9	0.7	Linear Contact	
325	41.54.590.50	-81.6689218	444209.2	4599576.6	2155992/9	685747.2	11.9	127.1	9.7	0.8		Linear Contect	
990	41.5477590	-81.6688946	444213.1	4599782.3	2195993.9	686422.4	11.9	137.4	1.5	1.0	0.8	Boulder)	1.052
282	41.5343228	-81 6683087	464250.4	4596290.3	2196300.9	681528.7	9.9	541.8	3.2	0.3	01	Linear Contact Point Source (Probable	+
103	41.5097820	-91.0681.239	499270.5	4598295.9	2196213.5	600320.5	11.4	194.3	24	1.5	0.E	Goulder) Point Source (Probable	1.54
134	42.5595448	-51.6680857	444273.2	4556625.5	2196245.2	603286.0	11.1	362.8	1.6	1.2	0.6	Goulder)	
357	41.5394141	-51.6679282	444286.5	4596855.3	2156267.4	6655584.8	11.2	341.3	12.9	0.5	0.2	Linear Contact	
338	41.5552459	81.6678937	444285.8	4598392.5	2156811.3	681365.9	5.7	477.9	7.1	0.5	. 1	Linear Contact	
338	41.5465290	-81.6678419	444299.7	4595622.6	2196267.0	605903.4	11.9	83.7	31	0.4	0.1	Lineer Contact Point Source (Probable	
	1.0549490	of a section /d	500,003.0		climiter.4	101.355.9		408.4	+1			Boukler) Point Source (Probable	1 252
41	41.5888749	-81.6676224	444222.5	4598795.5	2196373.0	695038.0	11.1	116.9	15	0.9	0.5	Bouker) Linear Contact	
341	41.5434978	-01.6673347	444129.5	4599908.3	2106435.7	604974.2	11.5	72.8	1.5	0.8	0.5	Lineer Contact	-

_						Side	scan Senar Cen	tacts					
10	Latitude	longitude	East(m)	North (m)	East (US servey feet)	North (US sarvey feat)	Bathyreetry (m)	Distance from Proposed Route (m)	Length (m)	Wildth (m)	Height (m)	Description	Associated Ma Anomaly ID
(344	41.5433712	-81.6673183	444340.8	4599294.2	2196440.6	684828.2	11.5	80.3	2.2	1.8	0.6	Point Source (Probable Broaklast	
C345	41.5428351	-81.6672239	444348.2	4599234.7	2106468.3	68(633.1	11.4	110.0	2.0	1.5	0.6	Point Source (Prohable	
(346	41.5390907	-81.6670194	444362.0	4596215.5	2196537.4	683258.4	11.1	260.9	6.9	0.8		Linear Contact	
C347	41.5400290	-81 6669459	666377.3	4596934.1	2196581.5	603615.6	11.5	214.2	4.6	1.1		Orcular Contact	
C548	41.5448288	-51.5567617	444388.5	4599455.7	2156587.9	605360.7	11.5	54.7	14	0.6	0.6	Boulder)	
C345	41.5564545	-01.0000075	444359.1	4596523.7	2196642.9	602302.3	10.0	540.6	4.5	0.5	0.1	Lineer Contect	+
C350	41.5555920	-51.5554224	444405.9	4596430.0	2196695.1	651996.1	10.5	349.3	3.9	LS	- 0.1	Circular Contact	
353	41.5357122	-81 6664035	444410.5	4596443.3	2196717.7	682039.9	10.1	348.1	3.1	2.4	0.4	Rectangular Contact	
052	41.5354592	-81.6661312	444433.0	4596424.5	2196722.9	681978.5	10.1	345.8	6.9	0.4	0.5	Linear Contact	M94
(355	41.5359835	-81.6660122	444443.4	4598473.2	2196823.9	682139.8	t0.0	308.6	2.0	2.0	0.4	Rectangular Contact	+
C156	41.5606358	-81.6659965	44448.5	4596967.5	2196812.6	683762.1	11.3	153.5	17	1.0	0.5	Boukler)	1.000
C357	41.5668531	-41 6659764	666158.0	4599457.9	2106802.8	685371.6	11.5	108.4	2.2	0.4	0.1	Linear Contact	
C359	41.5393036	-81.6659024	444455.5	4596850.3	2196842.1	603377.9	11.1	182,5	3.0	0.4	0.1	Linear Contact	
C360	41.5555404	-81.6656774	444454.3	4598423.9	2156862.5	601978.7	10.1	\$07.6	10.6	1.1		Lineer Contect	+
C362 C363	41.5594764	-81.6657848	444465.2	4586843.0	2196874.5	683354.4	11.0	174.1	9.1	0.5	0.1	Linear Contact Linear Contact	M164
(364	41.5405681	-81.6653921	444499.1	4598581.8	2196977.6	683811.9	11.5	100.9	1.7	0.9	0.6	Point Source (Probable	
365	41.5383879	-81.6653599	444499.9	4596739.7	2186894.1	683017.6	10.4	171.9	3.8	0.4	+	Boulder) Linear Cantait	M166
C3 66	41.5413167	-81.6653200	- 444505.7	4599064.9	2196994.8	684084.8	11.4	70.2	6.1	0.5	-	Linear Contact	
C367	41.5366580	-41.6652979	444503.6	4598548.7	2107017.0	682391.1	10.0	223.0	10.7	2.8	1.0	Roulders	-
C358	41.5412080	-41.6652677	444510.0	4599052.0	2197000.5	601045.3	11.4	69.7	6.D	.0.3	0.1	Lineer Contact	+
C389 C370	41.5405385	-01.6651522	444510.0	4596009.5	2197015.7	601037.9	11.5	85.5	3.4	2.4	0.2	Linear Contact Ortular Contact	+
C371	41.5429487	-81.6649.808	444535.4	4599245.8	2107061.9	684690.3	11.3	40.5	2.8	0.9		Linear Contact	
C372	41.5565556	-51.6648749	444535.5	4598544.9	2357352.9	602393.4	10.0	191.3	2.7	2.2		Rectangular Contact	
0374	41.5441247	-81.6645217	444591,4	45999376.0	2197258.2	685110.5	11.5	169.3	5.5	0.5		Linear Contact	
675	41.5398762	-81.6641478	464593.9	4596904.2	2197293.4	683562.8	10.9	33.0	5.0	0.4	0.1	Unsar Contect	
0.78	43.940.25.09	31.0042573	444737.1	4998945.8	219/294.9	665992.7	11-0	20.5	3.5	0.4		Low Reflectivity Patch (Possible	
C477	41.06/99/9	-81.066/185	0043399.8	03899037.4	210/287.5	442,622,000	11.5	104.9	10.4	8.4		Stag	-
Ca/IE	41.5399078	-81 6641158	004396.5	4286696.6	2107302.3	623537.9	10.9	32.8	9.5	0.6	100	Point Source (Probable	
ca79	41.541.9479	-81.6639784	499617.6	4599067.5	2197361.9	604039.7	11.5	37.6	12	1.0	0.6	Boulder)	1.00
CIE	41.5419127	-01.6639231	444622.7	4599132.4	2197375.0	604112.9	11.5	61.5	5.8	0.7	0.1	Lineer Contact Point Source (Probable	-
CIL	41.5416010	-81.6637215	444639.5	4599095.4	2197451.3	684192.6	11.2	66.5	2.9	2.7	0.8	Boulder)	0.00
38	41.5407071 41.5867471	-\$1,6635943	444649.1	4598598.1	2197469.3	683967.2 683434.4	9.8	46.T 84.0	4.9	2.5	0.1	Linear Contact Rectangular Contact	
314	41.5376005	-81.6654348	444659.8	4598853.1	2157523.8	682735.7	10.1	44.5	3.1	2.1		Rectangular Contact	5
GIS	41.5411380	-81.6634188	444954.1	4599043.8	2197515.8	684024.7	11.2	43.3	11.0	0.5	0.1	Linear Centact	M29
GB7	41.5612526	-81 6633317	444671.5	4599056.4	2197530.3	681065.6	11.2	85.8	6.9	0.4	0.1	Linear Cantact	-
1963	41.5426937	-81 6631525	444697.7	4599236.3	2197563.3	604.992.2	11.5	151.9	19.3	0.6	0.4	Linear Contact Point Source (Probable	+
C389	41.5409948	-01.6631201	444688.3	4599027.7	2197505.9	603973.3	11.1	93.4	13	0.7	0.6	Boulder)	
C350	41.5572015	-81.6629816	444697.2	4596606.5	2197649.3	682591.5	10.0	21.8	1.7	1.0	14	Soulder)	
C391	41.5412820	-81.6629508	444704.9	4599057.3	2157649.0	684071.2	11.1	118.0	16.5	0.5	0.2	Lineer Contect	
C392 C393	41.5412085	-81.6619304	444704.9	4599051.3	2197849.3 2197711.4	684051.7	11.1	116.3	6.9	0.7	0.0	Lineer Contect Lineer Contect	
(354	41.5401107	-81.6625952	444732.0	4598929.2	2157744.9	683652.5	10.5	106.2	5.0	0.4		Linear Contact	- 1 e -
C395	41.5410408	-81.6625764	444733.5	4596993.7	2197748.9	681099.8	10.6	108.5	5.0	0.8		Linear Contact	*
C387	41.5402982	-81 6624951	444740,5	4598950.0	2187771.6	683721.1	10.6	120.5	4.4	0.3		Linear Contact	-
Case	41.5421236	-41.6623073	444795.0	4599152.5	2167844.0	604387.0	11.1	204.4	7.0	0.5		Linear Contact Doint Source (Doobable	-
C3 59	41.5378287	-81.6621331	444768.6	4586875.6	2107079.4	602022.5	10.2	65.7	2.5	3.7	11	Goulder)	
C400.	41.5378276	-81.6621031	4997711	4596875.A	2157887.6	682822.0	10.2	69.1	1.8	1.2	0.6	Point Source (Probable	0.400
6400	41.5415157	-81.6620963	444774.6	4599062.7	2197877.2	684092.9	11.0	186.2	15.8	0.5		Linear Contact	
6462	41.5879908	-81.6620264	444777.5	4598686.8	2197908.2	682859.8	10.2	78.6	2.0	1.5	1.2	Point Source (Probable Boulder)	1.47
cain	41 541946	11 12 12 12 12	444792-2	4596121.0	2162867.0	6043075	11.7	210.2	1.5	0.7	0.F	Point Source (Probable	
CAPA	41 540050	41.66101/4	444749.0	10000000	0.167617.7	6000000	10.5	100.5		0.5	4.5	Boukler)	-
C4104	41.5611253	-81.6612759	444792.8	4599043.4	2197936.2	694024.1	10.9	197.4	9.2	0.4		Linear Contact	-
CADE	41.5419295	-01.6610404	444795.0	4599128.5	2197943.0	664310.0	11.1	225.8	1.5	0.8	3.0	Point Source (Probable	
C407	41.5409961	41.6616459	444905.6	4599026.9	2197990.7	663977.5	10.8	208.2	5.6	0.5	0.1	Linear Contact	
C408	41.5580128	-51.6616176	000011.7	4555555.7	2150015.8	681890.7	10.1	115.9	1.9	0.5	0.8	Point Source (Probable	1
C408	41.5412277	-81.6614278	444530.3	4599052.5	2150060.5	684062.6	10.8	256.4	5.7	0.4	0.1	Boulder) Lineer Contect	
6410	41.5383226	-81.6611910	444839.2	4598729.9	2196106.2	683034.5	10.2	150.2	2.7	1.6	0.7	Point Source (Probable	1.45
							1 - 2024 A	1 2020	10.00			Boulder) Point Saurce (Probable	1.1
C4111	41.5383523	-41.6611642	0.426240	4596733.1	2196142.6	683015.6	10.1	161.3	+5	1.0	as	Bowkler)	1
6812	41.5383755	-81 6611077	444854.6	4596735.6	2100150.2	663024.3	10.2	166.6	3.1	1.2	0.9	Point Source (Probable Boulder)	1.07:0
6413	41.5354757	-81.6610147	444852.4	4598746.7	2190183.3	683061.0	10.3	177.3	12	0.7	0.4	Poliet Source (Probable	
											-	Boulder) Point Source (Probable	-
6454	41.3385863	-81.8606008	444897.0	4596758,7	2196296.2	683102.4	10.5	213.9	3.1	1.0	1.0	Boulder)	
6415	41.5585604	-81.6605-811	444898.7	4598766.9	2156300.5	683129.4	10.5	218.0	2.2	1.5	0.7	Point Source (Probable Soulder)	1000
6416	41.5587020	-81.6605745	444999.1	4588771.5	2199302.4	683144.6	10.5	218.7	2.5	1.2	0.7	Point Source (Probable	-
97												Soulders Point Source (Prohable	-
¢417	41.5386709	-81.6605-802	444902.1	4598768.1	2196332.5	683133.4	10.6	221.6	2.5	0.7	0.7	Boulder)	
6438	41.5391259	-81.6604032	444914.0	4598818.5	2196348.4	683299.5	10.5	247.7	3.4	1.8	0.6	Rectangular Contact Rolet Source (Rechards	N106
C419	41.5367776	-01.6604102	444913.1	4598779.8	2150347.7	683172.6	10.5	235.5	2.6	1.1	0.7	Boulderi	

Sidescar Sanar Centracts													
1.15	MADES Geographic		MADEL UTM Zone 17		NADER Ohio State Plane Rorth			Distance from	Sec. 1	anas	man	the second	
10	Latitude	Longitude	East (m)	North (m)	East(US servey feet)	North (US servey feet)	Eachyra etry (m)	Proposed Route (m)	(m)	(m)	(m)	Description	Anomaly ID
G420	41.5385383	-81.6603481	444918,1	4598753.2	2196365.5	683085.5	10.5	232.4	1.7	0.7	0.5	Point Source (Probable Boulder)	1000
6421	41.5387309	-\$1.6602.029	444923.2	4598774.6	2100303.1	623155.9	10.7	243.6	4.0	2.2	0.7	Point Source (Probable Boalder)	100
C422	41.5590100	-61.6602/672	444923.4	4590704.3	2150581.2	605187.9	10.5	246.6	1.9	2.2	0.6	Point Source (Probable Boulder)	
CA23	41.5599555	-\$1.6601601	444934.9	4596511.7	2196412.0	663606.5	10.4	298.1	6.D	0.7	0.2	Lineer Contect	
6424	41.5386927	-81.6601.584	444934.0	4598770.2	2156435.9	683142.3	10.6	252.7	2.3	1.1	0.8	Point Source (Probable Soulder)	
6425	41.5389034	-81.6601138	444937.9	4588793.6	2156428.4	683219.3	10.5	263.3	1.9	1.0	0.7	Point Source (Probable Boulder)	
6428	43.5407736	-81.6600747	444942.8	4599001.2	2398432.5	683900.7	10.5	338.9	2.1	1.7	0.6	Orcular Contact Oxist Counce (Deshable	M26
G127	41.5189287	-81.6600659	444941.9	4598296.4	2100441.4	689728.5	10.5	267.9	1.6	1.0	0.9	Boukler)	-
0123	41.58994999	-01.60494.45	006352.7	4595874.9	2358472.4	662-625-8	10.5	801.8	.2.2	2.0	0.6	Rectangular Contact	-
C429	41.5589773	-81.6599405	444952.4	4596803.7	2190475.5	603246.6	10.6	279.5	2.9	11	0.4	Boulderj	
0430	41.5390395	-81.6599005	444955.0	4596808.6	2196468.3	683269.3	10.5	264.8	3.0	1.2	0.7	Linear Contact :	
6431	41.5591901	-81.6595928	444981.6	4598825.1	2198570.0	688325.0	10.4	314.3	2.2	2.3	0.7	Boulder)	M52
6432	41,5395059	-81.6594679	444992.3	4598860.1	2198603.1	683440.4	10.6	334.8	2.1	1.6	-	Rectangular Contect	M96
6434	41.5412463	-81.6591813	449017.7	4599053.1	2159675.4	684075.3	0.0	415.7	2.2	1.6	1.2	Point Source (Probable Soulder)	1.00
Ç435	41.5393496	-41.6591395	485019.6	4596942.4	2196693.5	623354.0	3.01	155.6	2.2	1.0	1.3	Poliet Source (Probable Bouider)	
C458	41.5394000	-61.6590536	445026.8	4596849.0	2156716.0	605406.1	10.6	564.5	2.5	1.4	0.7	Point Source (Probable Boulder)	1.00
C457	41.5394521	-\$1.6590459	445027.5	4556853.8	2156718.8	655421.9	10.6	366.5	2.7	1.0	0.9	Poiet Source (Probable Boulder)	1.00
6438	41.5597920	-61.6550282	445029.2	4596691.0	2156722.5	653543.8	10.7	\$79,3	5.2	2.3	0.5	Rectangular Contact	
C439	41.5394321	-81.6590259	449029.1	4586851.6	2158734.3	685414.7	10.6	367.5	2.2	0.9	0.6	Point Source (Probable Boulder)	
C640	41.5394747	-81.6589939	449331.8	4596856.3	2199733.0	683430.3	10.6	371.4	2.7	1.2	12	Point Source (Probable Boulder)	
(44)	41.5398344	-81.6590029	445031.3	4596892.9	2196726.3	683550.4		343.2	2.0	2.4		Rectangular Contact	
C442	41.5395829	-01.6589004	445039.0	4556868.3	2150756.0	603470.0	10.7	101.0	1.5	0.5	1.0	Point Source (Probable Boulder)	1.1
C443	41.5594981	41.6587317	445053.6	4596848.5	2156805.0	603-405.0	10.7	390.0	1.5	1.4	0.7	Point Source (Probable Boulder)	
G444	42.5398521	411.6586279	445062.7	4596856.0	2196831.6	683.568.II		413.2	3.5	1.6	0.6	Rectangular Contact	
\$445	41.5595778	41.6586050	445064.3	4596659.7	2156885.3	683443,4	- 34	403.5	2.8	0.8	0.6	Point Source (Probable Boulder)	
C446	41.5396563	41.6585672	449067.5	4596876.2	2196849.1	689497.6	194 - C	411.4	1.4	1.0	0.5	Point Source (Probable Boulder)	0.00
6447	41.5990272	-81.6581060	445031.1	4586295.1	2356892.7	643 563.3		430.0	1.6	0.0	1.0	Point Source (Probable Boulder)	1.00
C448	41.5397896	-01.6505021	445303.1	4596690.4	2106890.1	603546.3	3.4	430.6	2.5	1.0	0.6	Polet Source (Probable Boulder)	
0445	41.5599923	-\$1.6582954	445290.5	4596513.3	2356522.4	665620.7	141	444.3	2.5	2.5	0.7	Point Source (Probable Boulder)	
6450	41.5398635	-\$1.6581472	445794.4	4596898.9	2156936.0	683573.8	200	443.8	2.4	2.2	0.8	Point Source (Probable Boulder)	
(45)	41.5399502	-81.6582051	445098.0	4596508.6	2156547,2	688905.6	199	450.1	1.8	0.7	0.9	Point Source (Probable Boulder)	1.000
C452	41.5600100	-81.6581874	485099.5	4598915.2	2199951.9	683627.5		453.5	2,1	1.0	1.0	Point Source (Probable Boulder)	(+)
C453	41.5402440	-01.6577455	445135.6	4598540.9	2199072.0	663713.9	39	496.5	2.1	17	0.9	Point Source (Probable Boulder)	
6454	41.5402700	-01.6575067	445156.5	4596543.7	2199137.3	683724.0		516.3	1.7	0.8	0.6	Point Source (Probable Boulder)	1.384
GISS	41.5402653	-\$1.6573468	445178.2	4596543.0	2199206.4	683723.0		536.8	3.2	1.4	-	Gittular Contact	-

5.2 Magnetometer Results

A review of 271 line km of magnetometer data showed no historic structures (such as shipwrecks) present within the turbine and export cable survey areas.

A total of 178 magnetic anomalies were identified and mapped from the magnetometer data acquired over the Icebreaker Wind survey area. The anomaly location, type, magnitude and observations from the sidescan sonar in the area of each anomaly are listed in Table 3. Profiles of the magnetic anomalies within a 150 m (495 feet) corridor centered on the proposed route. Profiles of those outside the corridor can be found in Appendix A.

Table 3 Magnetic Anomalies Contact List

Marine Magnetometer Anomalies											
1	NAD83 G	eographic	NAD83 UT	M Zone 17	NAD83 Ohio S	tate Plane North	Bathymetry	Distance		Amplitude	Associated
in	Latitude	Longitude	Easting (m)	Northing (m)	East (US survey	feetil	(m)	Present	Potarity	(11)	Sidescan Contact ID
MI	41.5960349	-81,7914838	434038.0	4605228.5	2162296.1	703716.7	16.9	93.1	Monopole	66.9	Contact for
M12	41.5727049	-81.7348227	438738.1	4602596.6	2177868.5	695347.0	15.4	92.1	Dipole	63.9	
M3	41.5707487	-81.7299932	439138.9	4602376.0	2179196.2	6/34645.8	15.3	88.6	Monopole	43.4	
544	41.5684997	-81.7245598	439589.8	4602122.5	2180690.2	693839.5	15.0	89.4	Monopole	78.5	
MIS	41.5649288	-81.7160063	440299.5	4601720.1	2183041.8	692559.4	14.3	91.6	Dipole	37.0	
M15	41.5629714	-81.71123.59	440695.8	4601499.5	2184354.8	691857.9	14.5	92.4	Dipole	23.3	-
648	41 5568402	-81.7090409	441930.9	4600808.7	2189446.9	6995611	12.0	92.8	Monorola	68.6	-
M19	41.5567475	-81.6961940	441944.3	4600798.3	2158491.4	889627.8	13.2	93.9	Dipole	25.7	-
M10	41.5540823	-81.6897585	442478.6	4600498.1	2190261.7	688673.0	12.8	94.6	Monopole	59.6	
M11	41.5522990	-81.6853676	442843.2	4600297.2	2191469.5	688034.4	12.5	.91.7	Monopole	30.7	
M12	41.5513733	-81.6830568	443035.1	4600192.9	2192105.1	687703.0	12.4	88.9	Dipole	21.5	£252
M13	41.5510943	-81.6824088	443088.9	4600161.5	2192283.4	687603.1	12.4	90.0	Dipole	52.6	C257
M14	41.5485383	-81.6762752	443598.2	4599873.7	2193971.0	686687.5	11.9	92.2	Monopole	187.5	C285
M15	41.5397510	-81.6714625	443992.0	4598895.0	2195318.7	683498.3	11.1	598.8	Monopole	10.8	-
M18	41.5436196	-81.6763341	443601.7	4599882.7	21999990.0	686717.3	11.0	398.0	Disole	107.7	(285
M20	41 5404086	-81.6720712	443941.8	4508968.4	2195149.8	683736.3	11.3	594.9	Dipole	29.2	6403
M24	41.5369037	-81.6576089	444311.0	4598576.4	2196383.5	682470.9	10.1	399.8	Monopole	26.3	
M25	41.5315404	-81.6747700	443709.0	4597985.6	2194441.6	680498.1	0.0	1091.5	Dipole	145.1	
M26	41.5407863	-81.6600479	444945.0	4599002.6	2198439.8	683905.4	10.5	331.4	Dipole	108.9	C426
M27	41.5389450	-81.6635191	444653.9	4598800.4	2197496.0	683225.4	10.3	6.2	Monopole	32.5	
M28	41.5348691	-81.6682138	444258.8	4598350.9	2196225.0	681728.0	9.7	515.9	Monopole	54.7	2
M29	41.5376216	-81.6634084	444662.0	4558653,4	2197531.0	682743.5	10.1	41.7	Dipole	27.6	C384
M30	41.5394153	-81.5600664	444942.3	4508850.4	2198419.6	683405.8	30.4	284.1	Monopole	23.8	
M32	41.5410904	-81.6590152	445031.4	4599035.7	2198721.5	684018.9	0.0	423.7	Manopale	57.5	-
M33	41.5408670	-81.6593186	445005.9	4599011.1	2198639.2	683936.7	0.0	392.1	Dipole	136.6	(263
M34	41.53535832	-81.6651043	444510.4	4508505.3	2190726.0	682249.4	10.0	345.0	Dipole	68.7	1352
M36	41.5395686	-81.6594085	444997.5	4598867.0	2198610.1	683463.4	10.6	341.6	Monopole	38.6	C437
M40	41.5394539	-81.6502418	444927.7	4598854.8	2198391.4	683419.4	10.4	271.5	Monopole	42.6	- Car
1/141	41.5604476	-81.6996252	441661.5	4601211.4	2187540.0	690967.1	13.1	128.3	Monopole	15.0	· · · · · · · · · · · · · · · · · · ·
M42	41 5631635	-81.7063681	441101.7	4601517.5	2185685.7	691940.0	14.2	121.7	Dipole	23.9	
M43	41.5660867	-81.7134617	440512.9	4601846.9	2183734.9	692987.5	14.3	121.3	Dipole	18.4	
M44	41.5676671	-81.7172859	440195.5	4602025.0	2182683.3	693554.0	14.9	121.6	Dipole	69.5	
M45	41.5682266	-81.7187086	440077.4	4602088.1	2182292.1	693754.3	14.9	118.9	Dipole	24.7	<u></u>
M46	41.5690275	-81.7205561	439924.1	4602178.3	2181784.0	694041.6	14.9	122.7	Monopole	88.5	
M47	41.5713855	-81.7263001	439447.4	4602444.1	2180204.6	694886.8	15.3	121.6	Monopole	122.2	-
M148	41.6028184	-81.8025381	433115.4	4605990.2	2159225.4	705153.8	17.2	1.5	Monopole	10.1	20
845/0	41.6006515	-B1.6006007	433273.0	4605768.1	2159764.4	705418.0	12.1	156	Monopole	49.1	68
M51	41.6001685	-81,7991386	433404.3	4605693.3	2160190.3	705205.9	17.1	2.7	Monopole	17.0	
M52	41.5984615	-81.7950101	433746.6	4605500.6	2161324.5	704593.0	17.0	1.8	Monopole	30.2	-
M53	41 5733222	-81.7339397	438812.3	4602664.5	2178108.1	695574.0	15.5	3.5	Monopole	98.0	1
M54	41.5710419	-81.7284984	439263.8	4602407.5	2179604.2	694756.3	15.3	0.1	Manapole	16.4	0.0
M55	41.5705945	-81.7274535	439350.5	4602357.1	2179891.6	694595.8	15.2	1.7	Dipole	28.8	
M56	41.5679312	-81.7210021	439885.9	4602056.9	2181665.5	693641.1	14.7	1.9	Dipole	16.6	
M57	41.5651370	-81.7166729	440245.2	4601854.7	2182856.0	6/92998.0	14.8	2.7	Dipole	155.3	
M58	41.5658578	-81.7159728	440303.3	4601821.0	2183048.6	692890.7	14.6	3.7	Dipole	84.8	
M159	41.5636580	-81.7154803	440344.2	46/0899.5	2183183.9	689960.8	18.9	2.4	Monopole	294.0	
M61	41.5512857	-81.6806541	441235.4	4600181.7	2192763.0	687677.7	12.6	0.8	Monopole	9.7	
M62	41.5391598	-81.6595351	444986.4	4598821.7	2198585.9	685314.1	20.4	317.9	Monopole	41.5	6431
M65	41.5410308	-81.6583996	445082.7	4599028,7	2198890.2	683998.8	0.0	470.7	Monopole	125.3	
M66	41.5409427	-81.6585305	445071.7	4599019.0	2198854.7	683966.4	0.0	457.4	Monopole	233.1	
M67	41.5335442	-81.6689649	444195.0	4598204.3	2196024.0	681243.3	9.6	606.2	Monopole	25,0	1
M69	41.5479070	-81.5751860	443688.5	4599802.9	2194271.3	686460.3	12.1	109.8	Monopole	29.1	-
M70	41.5407007	-81.6/14029	443997.8	4599000.4	2195331,7	683844.5	11.3	530.9	Dipole	60.0	47.17
M/1	41.5378505	-81.0696039	449195.4	45598582.8	21958134.1	682810.7	30.5	326.1	Michopole	33.2	CITH
M74	41.5551000	-01.0015700	4432724.4	4600616.5	3101216.6	689078.3	12.7	155.4	Monorale	25.2	(226
M76	41.5629892	-81,7051321	441204.6	4601492 3	2186024 5	691879.6	341	154.4	Monopole	16.4	1.000
M77	41.5634985	-81.7063778	441301.2	4601554.7	2185681.9	692062.1	14.2	151.9	Monopole	47.1	
M78	41.5649951	-81.7102511	440779.6	4601723.5	2184617.0	692597.7	14.5	344.0	Monopole	15.9	0
M79	41.5671708	-81.7152571	440364.2	4601968.5	2183240.0	693378.1	34.7	154.7	Monopole	13.3	
MBO	41.5675736	-81.7162534	440281.5	4602013.9	2182966.1	693522.4	14.8	153.9	Monopole	18.0	2
M81	41.5695702	-81.7210491	439883.5	4602238.9	2181647.3	694238.2	15.0	155.7	Monopole	27.9	S. Andrews
M82	41.5717140	-81.7261910	439456.8	4602480.5	2180233.4	695006.8	15.3	157.9	manopole	19.3	C83
M83	41.5797575	-81.7457494	437833.9	4603387,4	2174856.6	697890.6	16.0	155.9	Monopole	13.3	-
M84	41.6044681	-81.8025638	433123.3	4606173.3	2159241.0	706765.0	1/2	116.9	Monopole	123.9	6.6
M80	41.6028804	-81.8045865	432353.1	4606591.4	2138692.4	706182.1	17.4	31.5	Monopole	150.4	-
M80	41.6010727	-81.8010084	433366.0	4605795.0	2159405 5	705529.1	17.1	77.8	Dirode	50.7	-
M90	41,5994800	-81.8012672	433226.2	4605618.5	2159610.1	704950.4	17.1	149.6	Monopole	26.3	-
M91	41.5723577	-81.7353154	438695.7	4602558.4	2177734.8	695219.1	15.4	345.6	Monopole	142.0	· · · · · ·
M92	41 5694135	-81.7283386	439275.6	4602226.6	2179653.2	694163.3	15.2	152.1	Dipole	79.6	C63
M93	41.5681926	-81.7252617	439531.0	4602088.9	2180499.1	693725.9	15.0	147.4	Dipole	17.1	
M94	41.5677188	-81.7242741	439612.9	4602035.6	2180770.9	693555.7	15.1	153.9	Dipole	16.7	10
M95	41.5658153	-81.7197241	439990.5	4601821.1	2182022.1	692873.3	14.6	156.5	Dipole	33.5	
M196	41.5654690	-81.7187908	440068.0	4601782.0	2182278.6	692749.4	14.8	152.7	Dipole	18.5	-
M97	41.5649433	-81.7177223	440156.6	4601722.9	2182572.7	692560.4	14,7	161.0	Monopole	44.1	
M98	41.5646518	-81.7170716	440210.6	4601691.2	2182751.7	692459.5	14.5	162.3	Dipole	20.2	-
M99	41.5644116	-81.7160350	440296.8	4601662.7	2183036.2	692370.9	14.3	145.0	Monopole	79,4	-
M100	41.5598377	-81.7048125	441228.4	4601147.2	2186122.4	690732.1	13.9	139.4	Monopole	22.4	-
M101	41.3583784	-81.0028964	441387.4	4001050.5	2186649.8	690425.8	12.4	146.0	Disale	45.4	(243
W1107	41-3310702	-01.083004/	447.484.1	40.0134.8	\$747939.9	087373.1	P. 54	247.7	Pribone	14.9	6.243

Marine Magnetometer Anomalies											
	NADB3 Geographic NADB3 UTM Zone 17 NADB3 Ohio State Plane North Bethemater Distance Asset										Associated
ID	fastlands.	Annual States	Frankland (m)	Marshi Inc. Inc.	East (US survey	North (US survey	bathymetry	from	Polarity	Ampiroude	Sidescan
	Landende	conficence	Easting (m)	Northing (m)	feet)	feet)	field	Proposed		hul	Contact ID
M103	41.5500740	-81.6813081	443179.8	4600047.5	2192588.2	687234.1	12.5	145.0	Dipole	65.3	C263
M106	41.5391328	-81.6603260	444920.4	4598819.2	2198369.5	683302.2	10.5	254.0	Monopole	17.8	C418
M107	41.5540152	-81.6850092	442874.6	4600487.5	2191561.7	688660.6	12.6	89.7	Dipole	10.2	
M108	41.5676584	-81.7179539	440139.8	4602024.5	2182500.5	693549.1	14.9	98.9	Dipole	75.2	3
M109	41.5691766	+81.7217620	439823.7	4602195.7	2181453.5	694093.0	15.0	88.8	monopole	85.5	
M111	41.5700593	-81,7239224	439644.4	4602295.2	2180859.5	694409.4	14.9	88.0	Dipole	20.9	-
M112	41.5708789	-81.7259358	439477.3	4602387.6	2180306.0	694703.1	15.2	86.9	Dipole	20.4	C87
M113	41.5710823	-81,7263759	439440.8	4602410,5	2180184.9	694776.1	15.3	89.0	Dipole	25.6	C82
M115	41.5739316	-81.7332821	438867.7	4602731.7	2178286.1	695797.6	15.6	89.2	Monopole	23.9	
M116	41.5744240	-81.7344668	438769.4	4602787.2	2177960.4	695974.2	15.6	89.5	Dipole	14.8	1
M117	41.5872063	-81.7656452	436182.7	4604228.9	2169390.5	700558.3	15.7	83.0	Monopole	11.8	
M118	41.5960000	-81.7867306	434434.1	4605221.0	2163596.3	703714.5	16.9	93.9	Monopole	21.9	
M120	41.6024963	-B1.8010345	433248.7	4605953.2	2159665.0	706049.9	17.1	86.5	Monopole	20.2	
M121	41.6053231	-81.8038295	433018.7	4606269.2	2158892.3	707073.8	17.3	89.9	Monopole	22.5	
M122	41.5736267	-81.7333638	438860.6	4602697.9	2178264.7	695686.3	15.5	56.2	Monopole	74.9	
M123	41.5669524	-81,7170705	440212.8	4601945.5	2182744.5	693294.1	24.9	60.7	Dipole	26.2	
M124	41.5657431	-81.7141164	440458.0	4601809.2	2183556.9	692860.7	14.3	61.6	Monopole	58.1	
M127	41.5364138	-81.66619817	444362.9	4558521.6	2196556.9	687294.1	10.0	366.3	Monopole	20.1	
M128	41.5354060	-61.6674209	444325.4	4598410.0	2196440.2	681925.7	9.8	434.9	Dipole	35.6	-
M129	41.5360893	-81.6579494	444281.9	4598486.2	2196293.2	682173.3	9.9	454.1	Monopole	37.5	
M151	41.53/3/26	-81.668538/	444233.8	4598623.5	2196127.5	682621.1	10.3	459.8	monopole	39.5	
M133	41.5400208	-61.0699850	444115.6	4598924.0	2195722.0	683600.5	11.4	482.5	Monopole	21.6	-
M134	41.5374646	-61.008/921	444215.7	4009016.3	2190045.9	685909.0	11.5	34/.0	Manapole	31.0	
M133	41 5380067	-81.6696015	444333.2	4508000 4	2196304.5	688220.0	51.0	409.9	Monopole	20.2	
M130	41 5405007	-81.6694349	444563.7	4508087.0	2195623.6	683812.0	31.6	406.0	Directe	5.0	C121
M140	41.5508763	-81.6822508	443085.2	4600122.3	21930/3.0	687523.4	12.5	312.0	Monorola	15.2	1366
M141	41 5512089	-81 6836089	443989.0	4600185.0	2191954 3	687624.5	12.4	118.3	Monanole	14.2	0,00
M142	41 5524452	-81,6853745	442250.4	4600314.2	2191103 5	688085.1	12.6	117.0	Dipole	72.3	
M143	41.5565323	-81.6963428	441931.7	4600774.5	2188451.4	689549.0	18.2	120.8	Monopole	17.2	C197
M144	41 5620845	-81,7098618	440809.4	4601400 1	2184733.2	691538.2	14.4	173.5	Monopole	10.6	C167
M147	41.5653679	-81.7178134	440149.4	4601770.1	2182546.4	692714.9	14.8	123.3	Dipole	128.2	
M148	41.5725375	-81,7352346	438203.6	4602578.3	2177756.3	695285.0	15.4	124.9	Dipole	256.8	
M149	41.5990424	-81.7993035	433389.4	4605568.4	2160148.5	704795.2	17.1	111.6	Manapole	19.0	
M150	41.5999644	-81.8015504	433203.1	4605672.5	2159531.2	705126.2	17.1	118.5	Monopole	30.2	
M151	41.6010881	-81.8005671	433286.2	4605796.5	2159796.9	705537.8	17.1	23.4	Monopole	23.5	-
M153	41.6006404	-81.7995452	433370.9	4605746.0	2160077.7	705377.0	17.1	32.3	Monopole	18.5	1
M154	41.5735256	-81.7336781	438834.3	4602686.9	2178179.0	695648.7	15.5	33.7	Monopole	101.9	S
M155	41.5693697	-81.7237252	439660.2	4602218.5	2180915.7	694158.6	14.9	28.8	Monopole	13.7	C102
M156	41.5686945	-81.7219413	439808.3	4602142.3	2181406.0	693916.9	14.9	34.7	Dipole	36.7	C121
M157	41.5683751	-81.7213093	439860.7	4602106.4	2181580.0	693802.1	14.8	29.0	Monopole	11.5	C129
M158	41,5675903	-81.7194811	440012.4	4602018.0	2182082.8	693520.6	14.8	26.0	Monopole	25.1	C138
M159	41.5663746	-81.7165652	440254.4	4601881.0	2182884.7	693084.8	14.8	24.7	Dipole	58.7	
M161	41.5653242	-81.7139834	440468.7	4601762.6	2183594.6	692708.4	14.2	26.2	Dipole	28.0	
M163	41.5652091	-81.7135192	440507.3	4601749.5	2183722.0	692667.6	14.2	33.6	Dipole	91.4	Summer
M164	41.5396470	-81.6654948	444489.7	4598879.6	2196952.7	683476.0	11.0	139.9	Dipole	8.9	C363
M165	41.5487229	-81.6761189	443611.4	4599894.1	2194013.1	686755.2	12.3	67.9	Dipole	108.8	C287
M166	41.5382546	-81.6654769	444490.0	4598725.0	2196962.5	682968.7	10.4	185.0	Dipole	25.8	C365
M167	41.5384707	-B1.6661133	444437.1	4598749.4	2196787.5	683045.8	10.6	228.4	Dipole	144,4	
M169	41.5526855	-81.6847601	442894.2	4600339.7	2191634.4	688176.8	12.5	29.7	Monopole	11.0	-
M170	41.5529418	-81.6852665	442852.2	4600368.5	2191495.0	688268.9	12.6	25.1	Dipole	26.6	
M1/1	41.5569863	-81.6951401	442032.4	4600824,1	2188779.0	689717.4	13.1	28.3	Monopole	52.0	-
M1/2	41.5572905	-81.6960727	441954.9	4600858.5	2188522.8	689825.9	15.2	36.2	Monopole	21.4	-
M1/3	41.5573/35	-81.000.019	441064.2	40/000/3	2100407.1	690835.8	12.3	33.3	Disala	7.4	
M179	41.3572903	-81.0903000	441045.7	4000638.4	21883333.0	620707.0	12.2	34.7	Magazzala	12.9	-
M176	41 5563030	81.6921451	441791.0	4600061.3	2187953 5	690151.7	124	30.7	Mananale	17.5	-
M173	41 5647372	-81 7140546	440462.2	4601682.5	2183577.0	692494.4	14.2	32.9	Dinde	52.7	-
M129	41.5718504	-81 7312475	439035.4	4602499.2	2178849.6	695044.2	15.2	11.2	Dipole	32.0	(50
M181	41 5758412	-81.7415576	438179.5	4602949.6	2176015.8	696473.6	15.7	57.1	Monopole	93	
M182	41.5920046	-81.7800926	434983.3	4604772.4	2165423.9	702273.7	16.8	29.0	Monopole	11.3	-
M184	41.6004022	-81.8011538	433236.6	4605720.8	2159638.4	705286.6	17.1	61.6	Manapale	15.8	-
M185	41.5992251	-81.7985377	433453.4	4605588.1	2160357.4	704863.5	17.0	65.1	Monopole	19.8	
M186	41.5772457	-81.7451496	437881.5	4603108.1	2175028.6	696976.8	15.6	64.5	Monopole	11.1	3
M187	41.5729492	-81.7345112	438764.3	4602623.5	2177952.9	695436.7	15.4	55.8	Monopole	11.6	C
M188	41.5716811	-81.7313903	439023.3	4602480.5	2178810.9	694982.2	15.2	53.9	Dipole	9.7	2
M189	41.5703497	-81.7282867	439280.8	4602330.5	2179664.4	694504.6	15.2	59.0	Dipole	11.2	
M190	41.5685808	-81.7239886	439637.5	4602131.1	2180646.2	693870.5	15.0	58.6	Monopole	8.7	
M191	41.5679971	-81.7225513	439756.8	4602065.3	2181241.4	693661.3	14.9	57.7	Dipole	9.5	
M192	41.5668192	-81.7197856	439986.3	4601932.6	2182002.0	693238.9	14.6	61.3	Dipole	24.8	C137
M193	41.5594978	-81.7020637	441457.3	4601107.6	2186875.8	690615.1	13.3	62.1	Dipole	20.6	0.000
M194	41.5594349	-81.7018892	441471.8	4601100.5	2186923.8	690592.6	13.3	61.2	Monopole	13.9	
M195	41.5579714	-81.6983177	441768.3	4600935.6	2187906.1	690068.4	18.5	60.1	Monopole	8.2	
M196	41.5571836	-81.6964709	441921.6	4600846.9	2188414.1	689786.0	13.3	62.6	Monopole	6.7	
M197	41.5566534	-81.6950753	442037.5	4600787.1	2188797.9	689596.3	13.1	58.1	Monopole	16.8	
M198	41.5526142	-81.6852246	442855.4	4600332.1	2191507.6	688149.6	12.5	55.3	Dipole	50.7	
M199	41.5506155	-81.6805272	443245.4	4600107.1	2192800.1	687433.4	12.5	61.0	Dipole	85.2	Section 2
M200	41.5487343	-81.6760171	443619.9	4599895.3	2194041.0	686759.6	11.9	62.7	Dipole	163.8	C288
M201	41.5516852	-81.6790551	443369.1	4600224.9	2193199.3	687827.0	12.4	102.2	Dipole	27.6	_
M202	41.5518646	-81.6788879	443383.2	4600244.7	2193244.5	687892.8	12.4	126.4	Monopole	7.9	
M203	41.5599115	-81.7003941	441595.9	4601152.4	2187331.3	690770.0	13.1	45.2	Manopole	8.4	-
M204	41.5604475	-81.7068565	441058.5	4601216.3	2185561.0	690949.2	14.1	162.2	Monopole	4.8	-
M205	41.3654662	-81.7100979	440/92.8	4601775.7	2184657.4	692769.8	0.0	196.0	Dipole	61.2	
M200	41.5649531	-81.7105442	440771.8	4001718.9	2164591.7	692382.2	24.5	196.2	Depote	00.4	-
M208	41.5200845	-81.7302442	4300411	4603365.6	21029/28	694435.3	24.7	30.8	Monopole	21.2	-
11/2/07	14-3103003	-04/12030///			L.0+01040.3	1.044120.7	9.0	432.3	THE REAL PROPERTY AND ADDREED	14.1	

Marine Magnetometer Anomalies													
	NAD83 G	eographic	NAD83 UTM Zone 17		NAD83 Ohio State Plane North		Real and the second second	Distance		American	Associated		
ID	Latitude	Longitude	Easting (m)	Northing (m)	East (US survey feet)	North (US survey feet)	(m)	from Proposed	Polarity	(nT)	Sidescan Contact ID		
M211	41.5683874	-81.7216561	439831.8	4602108.0	2181485.1	693805.7	14.8	16.2	Monopole	22.7	C125		
M214	41.5711257	-81.7263560	439442.5	4602415.3	2180190.2	694792.0	15.3	94.1	Monopole	14.1	C82		
M215	41.5713403	-81.7261749	439457.8	4602439.0	2180239.0	694870.6	15.3	122.2	Monopole	61.7	C85		
M216	41.5715103	-81.7260724	439466.5	4602457.8	2180266.5	694932.8	15.3	142.9	Monopole	14.0	C86		
M217	41.6001150	-81.8016471	433195.2	4605689.3	2159504.4	705180.9	17.1	113.6	Monopole	32.9			
M218	41.6028241	-81,8045222	432958.4	4605992.3	2158710.1	706161.7	17.2	123.4	Dipole	79,7			

Some of the magnetic anomalies were correlated to known sidescan contacts (targets). The remaining magnetic anomalies were not correlated to a sidescan contact or known lakebed installation such as a pipe or cable. There are a number of anomalies mapped on adjacent survey lines that may indicate the presence of a linear ferrous feature perpendicular to the proposed route at EKP 6.3 (Figure 18). This feature could not be identified from the sidescan or subbottom profiler data acquired over this area. An analysis of the magnetic data shows that the feature is most likely a buried steel or iron buoy block or anchor at the southwest contact with associated cable running to the northeast.



Figure 18 Location of linearly-aligned magnetic anomalies between EKP 6 and EKP 6.5. (CSR)

Past magnetic surveys in this area of the lake have also shown no correlation between the magnetic data and sidescan sonar imagery, with most of the magnetic hits having very small pole-to-pole distances indicating small or thin objects (Alpine, 2010)(VanZandt, 2015). This is primarily due to the proximity of the area being close to shore and used as a dumping ground for the past 200 years. Even today there are 5 dumping grounds identified on the latest Moss Point to Vermilion NOAA chart 14826 (Figure 19).



Figure 19 Current Dump Sites in Survey Areas (NOAA, VanZandt Engineering)

It is possible that some of the more magnetically intense anomalies are manmade but have no archaeological context, thus do not represent potentially significant resources. The less magnetically intense objects are most likely a function of geology, perhaps representing small pockets of glacial till or other magnetic rocks/sediment near the surface. In both cases, the Sidescan sonar imagery did not show any objects that would correlate with the anomalies. The lack of correlation is likely due to the magnetic objects being masked by overlying sediment.

5.3 Sub-bottom Data Analysis

A review of 271 line km of sub-bottom data showed no historic structures (such as shipwrecks) or artifacts were present within the turbine, export cable, and inner harbor areas.

The presence of gas charged sediments within the Icebreaker survey area was interpreted from chirp sub-bottom profiler and boomer seismic data. The presence of gas charged sediments can accentuate sub-bottom reflectors causing "bright spots" as well as prevent the penetration of the acoustic energy from the profiling system, thereby masking the acoustic signal.

The origin of the near surface gas in the survey area cannot be determined from the data collected from this survey. This gas may originate from shallow decomposed organic material (biogenic) or from deep underlying bedrock formations (petrogenic). In this area the biogenic source is plausible since vegetation has been buried during the numerous lake transgressions. This burial and subsequent decomposition could account for the presence of sub-surface gas.

Small localized erosional depressions or channels have been identified near the proposed WTG ICE1 turbine location (Figure 20) and over the near shore survey area. These features are infilled and were likely formed by glacial fluvial processes.



Figure 20 ICE 1 Erosional Depression or Channel (CSR)

6.0 SECTION 106 REVIEW RESULTS

The purpose of this review was to determine if any prehistoric/historically significant artifacts, such as shipwrecks or human occupation sites, might be present in the three APEs in the construction area of the Icebreaker Wind project.

6.1 Prehistoric Results

During the period from ~12,000 YBP to ~5,400 YBP the lake level was below the survey site so the possibility of prehistoric occupation sites does exist. A review of the Dames & Moore and Alpine geological data does not indicate the existence of any potential river systems or water sources that may have provided occupation sites for Paleoindians. A further literature review did not identify any past or ongoing research for the identification of prehistoric Lake Erie river systems.

Several small localized erosional depressions or channels were identified near the proposed ICE1 turbine location and over the nearshore survey area. These features are infilled and were likely formed by glacial fluvial processes. It is highly unlikely that these features contain prehistoric artifacts because erosional and sedimentation processes would have affected any prehistoric sites. This erosion would have mixed -- and destroyed -- the context of any site (Gray & Pape, 2014).

The impact of the project's construction to any prehistoric archaeological sites in the area would be negligible due to the small footprint that the foundation will occupy. Even though the mono bucket will be approximately 17.5 m (57 feet) in diameter and penetrate a maximum of 10 m (33 feet) deep into the lake bed and also into the glacial till layer, the disturbance area is small. This is due to the fact that the portion penetrating the lake bottom is only a cylindrical shell, like a biscuit cutter, not a solid object. The skirt thickness of the mono bucket is 3.175 cm (1.25 inches). The estimated surface area of disturbance for each WTG site is only 3.5 square meters (38 square feet). This coupled with the fact that the sub-bottom geology does not indicate any riverine structures leads to the conclusion that it is very unlikely that any prehistoric sites existed

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in the turbine APE or that its installation would impact such a site if it were to penetrate one at a thickness of 3.175 cm (1.25 inches.)

The interconnect cables in the turbine APE are buried at a depth of 1.5 m (4.5 feet) which is above these glacial till deposits. Their installation would not impact any potential prehistoric site.

The export cable, running to shore, is buried at a depth of 1.5 m (4.5 feet) and disturbance width of 1.5 m (4.5 feet). Several possible paleo-depressions/channels have been interpreted from the sub-bottom geology data and these are below the burial depth of the export cable. Any disturbance to any possible prehistoric site due to the small disturbance area seem unlikely.

The borehole for the HDD export cable will be well below any potential prehistoric site. The 0.6 m (18 inch) borehole will run from the breakwater, through the inner harbor, and exit at the CPP substation at a total depth of 18 - 27 m (60 - 90 feet) bottom level and a minimum of 4 m (12 feet) below the foundation of the breakwater.

6.2 Historic Results

No properties of historical significance were identified by the survey at the Icebreaker Wind APEs.

7.0 CONCLUSIONS AND RECOMMENDATIONS

Results from the Section 106 review have confirmed that there were no artifacts or properties of historical significance identified within the Icebreaker Wind APEs. Moreover, the literature search produced no evidence of the existence of any artifacts or properties within the project's proposed APEs.

Based on this review, VanZandt Engineering concludes that the Icebreaker Wind project will have no impact on historic properties. VanZandt Engineering believes that no further archaeological investigation is required for this project and that project construction be approved. However, while the research and survey work for this project were thorough, no survey technique is completely adequate to identify all cultural resources in a given area. In the unlikely event any historic or prehistoric remains are discovered during project construction, the SHPO and/or VanZandt Engineering should be contacted to investigate and evaluate the significance of any such finds.

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Exhibit BB

Section 106 Geophysical Survey Review for Icebreaker Wind

Appendix A

Icebreaker Offshore Wind Demonstration Project 2016 Marine Geophysical Survey Results

CONFIDENTIAL FILED UNDER SEAL

Icebreaker Windpower Incorporated has requested confidential treatment of Appendix A to this document in accordance with OAC Rule 4906-2-21.

Appendix A to Exhibit BB contains critical infrastructure information, confidential research and development information, or commercial information, trade secrets, and/or proprietary information and, as such, is entitled to confidential treatment under state and/or federal statutes and regulations.

An unredacted version of Appendix A has been submitted to the Docketing Division of the OPSB in accordance with OAC Rule 4906-2-21(D)(2).