



Self-Healing & Re-Adhering Cements with Improved Toughness at Casing and Formation Interfaces for Geothermal Wells

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Track Name

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Relevance to Industry Needs and GTO Objectives

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Challenges/Barriers

- Damage of underground cement and other structures is challenging not only to repair but often to even locate
- Major factors causing failure are:
 - 1. Cement-well incompatibility, i.e., lack of chemical bonding to metal casing and clays/rocks
 - 2. Undesirable phase transitions in cement at the interfaces
 - 3. Mechanical, thermal, and chemical stress
- Thermally/chemically stable cements with self-healing properties and improved adhesion at casing and formation interfaces are yet to be developed

Project Objectives

- To develop advanced cement composites with the following features:
 - 1. Self-repairing capability of cracked cement matrix
 - 3. Resilience to high T environment (including thermal shock)

- 2. Re-adhering ability to casing and formation
- 4. Improved chemical stability
- All resulting in lifetime cost reduction leading to a reduction of the LCOE on geothermal power generation via:
 - A. Enhancing wellbore integrity and operational safety
 - B. Reducing frequency of wellbore intervention, associated repair costs, and temporarily production shutdown

Project Supports the following GTO Goal(s)

- 1. Improving processes of identifying, accessing, and developing geothermal resources
- 2. Identifying and accelerating near term conventional and/or blind hydrothermal resource growth
- 3. Accelerating a commercial pathway to and securing the future of Enhanced Geothermal Systems
- 4. Overcoming deployment barriers 5. Collaborating on solutions to subsurface energy challenges
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Methods/Approach



Summary of 3y-project plan (so far, no deviation from original plan):

- *FY16:* a. Screening novel polymer-cement and inorganic-cement composites that outperform conventional wellbore cement by retaining +90% mechanical strength when subjected to different EGS-representative thermal and chemical environments.
 - b. Demonstrate self-repairing capability.
- FY17: a. Down-select polymer-cement and inorganic-cement composites based on re-adhering capability to casing after mechanical (shear) separation
 - b. Demonstrate multiple re-adhesion to casing after materials weathering under different thermal and chemical EGS-representative conditions.
- *FY18:* Synthesis of a hybrid inorganic-polymer cement composite(s) that synergistically combine the properties of the best-performing (organic and inorganic) composites towards amplifying the range of EGS fields at which these advanced materials can be deployed at followed by:
 - a. Long-term (one month) high temperature (up to 300C) performance evaluation including self-healing capability
 - b. Evaluation of cement-rock interface bond strength and re-adherence after exposure to different EGS's thermal & chemical conditions
 - c. Evaluation of slurry pumpability following API standards

Tasks performed at EGS-representative conditions

1. Additives-cement slurry compatibility (FY16)

a. Slurry homogeneity b. Slurry density c. Slurry viscosity and consistency at 85C

2. Bulk mechanical properties (FY16)

- a. Compressive strength b. Fracture toughness
- d. Before and after 1-month exposure of material to:
 - i. 6 cycles of 25C-300C
 - ii. H2SO4 pH 1-2 brine at 90C
 - iii. 15,000 ppm CO2 in brine at 90C for 1 month

3. Self-repairing capability (FY16)

- a. After shear fracture
- b. Compressive strength before and after heal event
- c. Permeability before and after heal event

c. Young Modulus



X-ray Microtomography of a fracture before and after healing in an inorganic-cement composite



HP/HT reactors for cement weathering at different EGS-representative conditions

Methods/Approach

Tasks performed at EGS-representative conditions (cont.)

- 4. Cement-casing interface mechanical properties (FY17)
 - a. Shear bond strength at cement-steel interface before material's weathering (lap-shear and/or pipe-shear)
 - b. Shear bond strength at cement-steel interface after material's exposure (1 week) to:
 - i. 6 cycles of 25C-300C
 - ii. H2SO4 pH 1-2 in 1wt% NaCl brine at 90C
 - iii. 15,000 ppm CO2 in 1wt% NaCl brine at 90C
 - c. Re-adhesion (healing) capability at cement-steel interface after shear separation before material's weathering
 - d. Re-adhesion (healing) capability at cement-steel interface after shear separation after material's exposure (1 week) to:
 - i. Identical conditions as in b.

5. Chemical analysis including atomistic simulations (FY16- FY17)

- a. SEM/EDX, X-ray diffraction spectroscopy (XRD), CT scan, FTIR, synchrotron high-resolution XMT,
- b. X-ray fluorescence spectroscopy (XAS), X-ray absorption near edge structure spectroscopy (XANES),
- c. Surface area analysis and pore size distribution analysis

5. Will the advanced cements last? Long-term thermal stability and healing ability (FY18)

- a. One month curing followed by compressive strength, permeability, and adhesion to casing analysis
- b. Shear fractures followed by permeability analysis and healing materials at 200-300C temperatures
- c. Perform post-healing tests (cement matrix and cement-casing interface) including:
 - I. Compressive strength (recovery)
 - II. Permeability reduction
 - III. Re-adhesion (adhesive strength recovery)
- 6. Cement-formation interface mechanical properties (FY18): Identical approach to item 4 replacing steel with granite
- 7. Rheological and placement tests (thickening time) (FY18):
 - a. Under typical simulated pressure and Bottom Hole Circulating Temperature (BHCT) according to API standards



Lap-shear testing





New pipe-shear testing



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Concept Summary

Combine a self-healing polymer w the cement to create a self-healing polymer-cement composite material







- Polymer molecules anchored to cement matrix and \geq interfaces via coordination bonds, covalent bonds, Hbonding, and/or van der Waals interactions
- Introduce self-healing properties in bulk cement and \geq self-re-adhesion at cement-formation and cementcasing interfaces

confirmed healing due to reversible and dynamic polymercement and polymerpolymer debonding-



Current state of the art: **Microcapsules**

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Rheological, thermal, chemical and spectroscopic analysis

FY16 M1 met: identify at least 2 organic-based and 2 inorganic-based cement composites for initial screening **FY16 M2 met**: Identify at least 1 organic and 1 inorganic slurry with flowability (3 hours at 85° C) similar to OPC slurries.



Slurry consistency

- Polymer cement slurries show similar rheological properties to traditional well cements
- 2. Use of a retarder might not be required



Polymer homogeneously

distributed in cement

matrix (XMT)

Two main phases, xonolite and

quartz when curing at 85C

Cement 10 wt% Polymer

1 200

1 000

TG suggests high thermal stability (250-430 C !)

SEM/EDX: Areas rich in C & S due to polymer presence



Polymer





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Cement composites resistance to EGS environments

FY16~M3~met: At least one cement composite with structural fracture toughness ${>}0.006~MN/m^{3/2}$

FY16 M4 met: Cement composite(s) with structural toughness ≥90% with respect to unexposed cement after weathering

Note: PNNL/NETL was limited to 250C for curing or thermal weathering (instead of originally proposed 300C

Geothermal well criteria: Compressive strength >1000psi Fracture toughness > 0.006 MN m^{-3/2}

Compressive strength **BEFORE** weathering



Fracture toughness before weathering: Polymer-cement = 0.007 MN m^{-3/2} Base cement = 0.011 MN m^{-3/2}

Young Modulus before weathering: Polymer-cement = 7.0 GPa Base cement = 11.3 GPa



Compressive strength after weathering

Polymer-cement

- Remained unchanged when exposed to:
 - ✓ Six thermal shock cycles
 - High temperature mineral acid
- Decreased by 30% when exposed to:
 - High HP/HT CO₂ / brine

Conventional cement

- Only 7% decrease after thermal shock and 13% decrease after mineral acid exposure.
- Doubled by carbonation



FY17 M1 met: Cement composites with shear bond strength @ carbon steel (CS) /cement joint +30%> OPC **FY17 M2 and Go/No-go met**: At least one cement formulation with \geq 30% higher resistance to shear debonding at steel interfaces with respect to OPC after weathering

Note: Large variance in shear tests values using lap-shear method made these tests very challenging

Cement composites adhesion to steel casing





15% Poly(elhylene.co-acrylic acid) Zn salt

10% BPAIPEOIEDIN N-ED

Unaged Thermal Shock

250

200

150

100





Before Weathering:

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 Polymer-cements outperform (by nearly 3X) conventional cement's adhesive strength to SS casing

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After weathering:

- Thermally-shocked samples:
 polymer-cements outperform by 6X
 base cement
- Sulfuric acid attack: polymer-cements outperform by 40X base cement
- CO₂ brines: Polymer-cements have statistically similar adhesion to base cement.

Cement composites multiple readhesion (healing) to steel casing



for re-adhesion

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Re-adhesion BEFORE weathering (top plot):

One polymer-cement show 167% casing adhesive strength recovery

AFTER weathering (left plots):

- Thermally-shocked samples: polymercements outperform by 20-40% conventional cement with recovery rates of up to 150%
- Sulfuric acid attack: polymer-cements show significantly lower adhesive strength recovery in the 1st healing event and higher adhesive strength recovery in the 2nd healing event compared to conventional cement
- **CO2** brines: similar to sulfuric acid attack

FY17 M3 met:

- shear bond strength recovery rate >80% for debonded cement/carbon steel (CS) joint samples, compared with that before re-adhering.
- identify at least one cement technology that self-adhere • to the CS casing and base cement when cured at 300C after mechanical/chemical and/or thermal stresses
- Note: base cement showed surprisingly high shear bond strength with this pipe shear method





Thermal shock

Base cemer Polymer-cement





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- Mechanical properties: Three composites met the wellbore requirements. The composites seem to be more ductile than conventional cement (40% lower Young Modulus). FY16 Milestones Q1 and Q3 met
- Rheological properties: Could be deployed in the same way conventional cement is. FY16 Milestone Q2 met
- Thermal stability: Could, in principle, be applied in T ranges between 60C-300C
- Self-repairing: Demonstrated bulk cement reduction in fracture permeability between 62% and 87% (apertures as large as 0.5mm). Mechanism: dynamic & reversible bonding at cement-polymer and polymer-polymer.
- Bulk cement resistance to EGS environments: Resistance to all extremely harsh geothermal environments (thermal and chemical stresses). FY16 Milestone Q4 met
- · Adhesion strength to (stainless) steel casing: Outperform (by up to 300%) conventional cement. FY17 Milestone Q1 met
- Casing adhesion resistance to EGS environments: Either match (CO₂/brine) or outperform by 6X (thermal shock) and by 40X (mineral acid) conventional cement. FY17 Milestone Q2 and Go/No-go met
- · Cement-casing re-adhesion (healing): FY17 Milestone Q3 met
 - Before weathering: Two cement composites recovered 71% and 167% of original adhesive strength
 - After thermal shock: Outperforms conventional cement in multiple healing events after thermal shock (150% recovery rate).
 - After chemical stress: Shows significantly lower % of adhesive strength recovery after the 1st self-repairing event but higher % recovery after the 2nd repairing event respect to conventional cement
- Cost: estimated in \$0.40/lb, 8X of base cement (Cement H/SiO₂). Working to reduce it to the proposed 3X of base cement.
- One publication, three pending / One patent application / Six Presentations / One press release / Data uploaded to GDR

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Establishing Mechanism of healing

- XRD
- FTIR/TGA
- SEM+µEDX and µEDX mapping
- Raman
- CT scan
- 3D Optical Microscope

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Examples of Matrix strength recovery: A+>100%; A 80-99%; B 60-79%; C<60%

Cement system	Curing Environment (270°C and 350°C)				
	Water	Alkali Carbonate	Geothermal brine	Thermal shock	
Class G/SiO ₂	С	В	В	А	
CAC (#80)/FAF (TSRC)	Α	Α	Α	A+	
CAC(#80)/Zeolite 1	А	А	A+	A+	
Class G/SiO ₂ /Zeolite 1	С	A	C	N/A	
OPC/Zeolite 2/SiO ₂ (FlexCem)	A+	А	С	A+	
CAP/FAF	С	С	А	A+	
GBFS/FAC	В	В	В	А	
GBFS/FAC/Zeolite 1	А	А	А	А	
FAC/FAF	С	В	С	А	

Formulations with Micro Glass Fibers (MGF)						
	Water	Alkali Carbonate	Geothermal brine			
Class G/SiO ₂ /MGF	А	А	A			
CAC (#80)/FAF/MGF	A+	A+	A+			
CAC(Fondu)/FAF/MGF	A+	A+	A+			
CaP/FAF	С	В	A			
FAC/FAF/MGF	С	С	В			
GBFS/SiO ₂ /MGF	А	A+	В			

Example TSRC/MGF healing in water at 300°C :



Example of cracks sealing after healing at 300°C :





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Examples of Interface strength recovery, corrosion protection of Carbon Steel (CS)



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Bond durability



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Results

- 1) Various cement chemistries, including 4 cement binders, 8 pozzolanic materials and 3 healing aid additives are tested (635 cement matrix and cement-metal interface samples prepared and evaluated);
- 2) Matrix strength recoveries of more than 100% and cracks sealing achieved for several cements in water, carbonate and geobrine after repeated damage tests and healing at 300°C;
- 3) Bond recoveries of more than 60%, more than 5 times lower corrosion rate than for common well cement, more than 2-times lower corrosion rate after 5-day healing compared to that before healing (decreased permeability).

Major Healing Factors

- 1) Moderate Young's modulus (YM), ranging from 1×10^5 to 3×10^5 psi, to avoid brittle fractures
- 2) Crack-plugging by new crystalline and amorphous reaction products in matrix and at interfaces formed by the cement surfaces and reactants from different thermochemical environments,
- 3) Utilization of alkali metals-incorporated CaO-Al₂O₃-SiO₂ type of pozzolanic additives as healing aides to accelerate healing in water, CO₂, and brine environments,
- 4) Attractive-physical and chemical bonds at interfaces between cement-derived hydration products and CS.
- 5) Void-free (low permeability) coverage of CS surfaces by specific amorphous and crystalline phases, and extension of this coverage by prolonged cement's hydration time
- 6) Great re-adhering properties of broken cement to cement remaining on CS (as for matrix recovery).

Cost

Current cost of the best performing formulation is \sim 7.2x(common well cement) (OPC/SiO₂); more economical options are under evaluation (if successful the cost of the advanced cement would be \sim 3x(common well cement))

Data Sharing and Collaboration

Published 4 peer-reviewed papers and 6 talks (4 invited talks); GRC-2016 best presentation award

Research Collaboration and Technology Transfer

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- PNNL signed an NAA with Halliburton where the later performed rheological studies on polymer-cement composite slurries. Halliburton showed special interest in the polymer-cement technology.
- Lafarge Holcim has also shown interest on our polymer-cement composites and we will begin conversations during FY18 towards potential opportunities for licensing and commercialization
- BNL collaborated with Trabits group on evaluation of new cement-zeolite composites developed with support of EERE office of DOE.

Future Directions

- Synthesis of a hybrid inorganic-polymer cement composite that synergistically combine the properties of the best-performing (organic- and inorganic-) cement composites to amplify the range of EGS fields at which these advanced materials can be deployed at*
- Evaluate long-term stability at EGS temperatures (one month) and slurry pumpability following API standards.
- A comprehensive technical report will be generated with all material's info including material's cost together with identifying potential stakeholders for technology licensing and field deployment.

Milestone or Go/No-Go	Status /Expected Completion Date
FY17-M4: At least one cement composite with +90% reduction in permeability and/or +90% recovery of compressive strength after self-repairing from mechanically induced radial cracks (tensile failure)	Predicted by October 30th
FY18-M1: At least one cement composite thermally-stable at 200C for 5days for further evaluation. At least one cement composite thermally-stable at 250C for 5days for further evaluation. At least one cement composite thermally-stable at 300C for 5days for further evaluation.	
FY18-M2: Fit-for-purpose cement composites: A. cement composite with self-healing capability and re-adhering (to casing) capability with thermal stability in the 200-250C range for up to one month; B. cement composite with self-healing capability and re-adhering (to casing) capability with thermal stability in the 250-300C range for up to one month	
FY18-M3: At least 2 cement composites that meet field requirements based on API procedures w/ controlled thickening times of at least 90min @ 85°C. - (Minimum) one cement composite with shear strength at formation (granite or other representative lithology) interfaces equal to or no lower than 70% with respect to the same material before re-adhering. - (Minimum) one cement composite that self-re-adhere to the formation with a +70% recovery after exposed to thermal and/or chemical stresses.	
FY18-M4: A technical report on (minimum) two fit-for-purpose formulation(s). Identification of at least one stake holder for technology transfer. Two per- reviewed publications. Determine if additional lab-scale tests specific to a geothermal site are required with the identified stakeholder.	

Summary Slide

- **ENERGY** Energy Efficiency & Renewable Energy
- This project demonstrated the synthesis of advanced inorganic-cement and (patent-pending) organic (polymer)-cement composites with enhanced tolerance to extreme thermal and chemical environments found in EGS (maintaining near-original mechanical properties)
- Both, inorganic-cement and organic-cement composites posses self-repairing capability w/ strength recoveries after damage of more than 90% and/or permeability reduction of up to 87% (fractures as large as 500μm).
- Both, inorganic-cement and organic-cement composites posses strong adhesion to steel casing (up to 300% higher than conventional cement) and re-adhering capability w/ strength recoveries after damage of 70-167%
- Re-adhesion capability is, for most cases, maintained after exposure to EGS thermal and chemical environments
- Work is ongoing to determine:
 - a. Long-term stability at EGS temperatures
 - b. Adhesion and re-adhesion capability to formation
 - c. Slurry pumpability



- · Goal is to:
 - 1. Generate **fit-for-purpose cement composites** that can be deployed in a **wide (and complementary) range of EGS fields**, *outperforming conventional wellbore cement in terms of durability and reliability*.
 - 2. Approach potential stake holders for **technology licensing and field deployment**. Once identified, additional work specific to a geothermal field might be required
- Milestones/deliverables met on time and budget (no deviation from plan). Cost as of FY17-Q3: \$ 1,557,222