Appendix T Section 106 Geophysical Survey Review

# Section 106 Geophysical Survey Review for Icebreaker Wind

Prepared for:

# Icebreaker Windpower Inc.

Icebreaker Windpower Inc. 1938 Euclid Avenue, Suite 200 Cleveland, Ohio 44115



Lead Agency: Department of Energy (DOE)

Submitted by: David M. VanZandt, MMA RPA VanZandt Engineering 1226 Lakeland Avenue Lakewood, Ohio 44107 216-956-2338 <u>dvanzandt@sbcglobal.net</u>

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#### 1.0 EXECUTIVE SUMMARY

A geophysical survey of a portion of the Lake Erie lakebed was conducted for the Icebreaker Wind project by Canadian Seabed Research Ltd. (CSR) from mid- August to early September 2016 on behalf of Icebreaker Windpower Inc. Icebreaker Wind is a six turbine 20.7 megawatt offshore wind demonstration project 8 to 10 miles off the shore of Cleveland, Ohio. The data from this survey was evaluated according to Section 106 of the National Historic Preservation Act of 1966 (NHPA) requirements. Three (3) areas of potential effects (APE) were assessed:

- Turbine area 4.7 km (2.9 miles) x 0.3 km (0.2 miles). Beginning about 12.9 km (8 miles) from the mouth of the Cuyahoga River, Cleveland, Ohio, Cuyahoga County, at a depth of 17-18 m (56 59 feet). Within this area six (6) wind turbines will be constructed and interconnected with trenched and buried cables at a depth of about 1.5 m (5 feet).
- Export cable area 13.2 km (8.2 miles) x 0.36 km (0.2 miles). Beginning 1.7 km (1.1 miles) west of the end of the east breakwater offshore of Cleveland, Ohio, Cuyahoga County, and running 13.2 km (8.2 miles) to the Turbine area at a water depth of 10-17 m (33 56 feet). Within this area the export cable from the wind turbines to east breakwater will be trenched and buried at a depth of about 1.5 m (5 feet).
- 3. Inner harbor area 0.85 km (0.53 miles) x 0.36 km (0.22 miles). Beginning 1.7 km (1.1 miles) west of the end of the east breakwater offshore of Cleveland, Ohio, Cuyahoga County, and running 0.85 km (0.53 miles) to shore at the CPP power plant at a water depth of 4-10 m (13 33 feet). Note: The export cable route will be horizontally drilled beginning 1.7 km (1.1 miles) west of the end of the east breakwater on the north side, south to the CPP power plant at a minimum depth of 4 m (12 feet) below the foundation of the breakwater.

The geophysical survey was designed to be in compliance with the guidelines developed by the Bureau of Ocean Energy Management (BOEM) set forth in "Guidelines for Providing Archaeological and Historic Property Information Pursuant to 30 CFR Part 585," compliance with which are directed by the Ohio State Historic Preservation Office (SHPO). Results from the geophysical survey confirmed that there were no artifacts or properties of historical significance identified at the Icebreaker Wind's APE that would impact the construction of the Project. Nor was there any evidence from the literature search that any artifacts or properties exist at the proposed sites.

VanZandt Engineering recommends that no further archaeological investigation is warranted for the Icebreaker Wind project areas at this time and that clearance for construction be granted.

This report will be submitted to the Ohio SHPO by the U.S. Department of Energy for Section 106 review.

#### 2.0 INTRODUCTION

David M. VanZandt of VanZandt Engineering carried out the Section 106 assessment of the geophysical survey data collected by Canadian Seabed Research from mid- August to early September 2016 for Icebreaker Wind. The following technical report presents the results of this archaeological assessment undertaken to comply with the Section 106 guidelines and the guidelines established by the Ohio State Historic Preservation Office (SHPO) and the U.S. Department of Energy (DOE).

David M. VanZandt, MMA, RPA was responsible for background research, data analysis and interpretation, and report preparation. Mr. VanZandt is qualified as a professional archaeologist by the Register of Professional Archaeologists (RPA), is on the Ohio SHPO historic archaeologists' consultants list, and a member of the Ohio Archaeology Council.

This report details the Section 106 archaeological assessment of the data acquired during the geophysical underwater remote sensing survey conducted by Canadian Seabed Research Ltd. (CSR) for the Icebreaker Wind demonstration project proposed by Icebreaker Windpower Inc. Icebreaker Wind will be the first freshwater offshore wind project in the Great Lakes and in all of North America. The project has three (3) areas of potential effects. The first APE is the Turbine area. The area is 4.7 km (2.9 miles) long by 0.3 km (0.6 miles) wide, bbeginning about 14 km (8.7 miles) offshore of Cleveland, Ohio, Cuyahoga County, at a depth of 17-18 m (56 - 59 feet). Within this area six 3.45 MW wind turbine generators (WTGs) will be located and interconnected with trenched and buried interconnect cables. The interconnect cables will be buried in an excavated trench 1.5 m (5 feet) wide by 1.5 m (5 feet) deep. Each of the WTGs will be supported by a mono-pole substructure atop a suction bucket foundation (mono-bucket). The Mono Bucket (MB), Figure 1, combines the benefits of a gravity base, a monopile, and a suction bucket. It is a Suction Installed Caisson (SICA) or "all-in-one" steel foundation system to support offshore wind turbines. The interface with the lakebed is accomplished by means of a steel skirt that penetrates the seabed. This steel skirt (or bucket) is welded to an upper steel tube and transition piece that resembles the elements above the mudline of a standard offshore wind monopile. The MB skirt for the Icebreaker Wind project will be approximately 17.5 m (57 feet) in diameter and a maximum of 10 m (33 feet) deep.

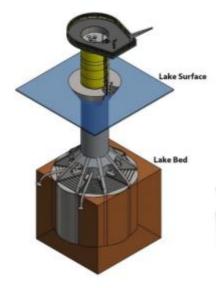


Figure 1 Mono Bucket (MB) Design

The Mono Bucket is installed (Figure 2) by means of both gravity and suction. When the steel bucket is placed on the lakebed, it initially self-penetrates by gravity about 1-2 m (3-6 feet). Suction is then applied and water is pumped from the bucket causing the foundation to penetrate into the lakebed. Once the bucket has achieved the specified penetration, the pump is stopped.

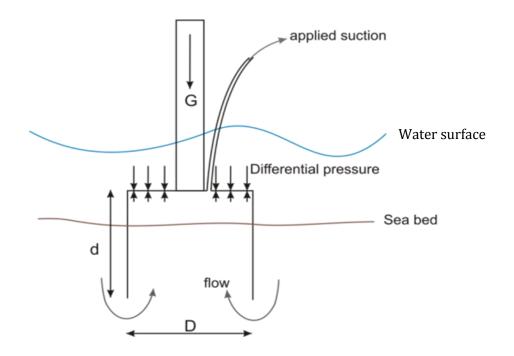


Figure 2 Mono Bucket (MB) Installation

The second APE is the Export cable area. The energy generated from the WTGs will be transmitted through an export cable from the offshore project area to shore. This area is 13.2 km (8.2 miles) x 0.36 km (0.2 miles). Beginning 1.7 km (1.1 miles) west of the end of the east breakwater offshore of Cleveland, Ohio, Cuyahoga County, and running 13.2 km (8.2 miles) to the Turbine area at a water depth of 10-17 m (33 - 56 feet). The export cables will be buried in an excavated trench 1.5 m (5 feet) wide by 1.5 m (5 feet) deep.

The third APE is the Inner harbor area. The export cable will be run in horizontal bore holes generated from Horizontal Directional Drilling (HDD) to allow the cables to pass beneath the Cleveland harbor breakwater and the commercial navigation channel east of Burke Lakefront Airport. The cable will come ashore at the Cleveland Public Power (CPP) Lake Road substation. This area is 0.85 km (0.53 miles) x 0.36 km (0.22 miles). Beginning 1.7 km (1.1 miles) west of

the end of the east breakwater offshore of Cleveland, Ohio, Cuyahoga County, and running 0.85 km (0.53 miles) to shore at the CPP substation at a water depth of 4-10 m (13 - 33 feet). The HDD borehole depth will be a minimum of 4 m (12 feet) below the foundation of the breakwater.

The scope of work includes installing six WTGs assemblies, WTGs interconnect cabling, and export cabling to shore. This work would take 6 months to complete.

#### 3.0 BACKGROUND RESEARCH

#### 3.1 Environmental Context

#### 3.1.1 Bathymetry

The Icebreaker Wind site lies in Lake Erie, the southernmost of the five Great Lakes in North America. The Great Lakes are shown in Figure 3, along with their profiles and surface elevations as the flow of fresh water is traced from Lake Superior to the lower lakes and eventually out into the Atlantic Ocean through the St. Lawrence River (Michigan Sea Grant, 2014).

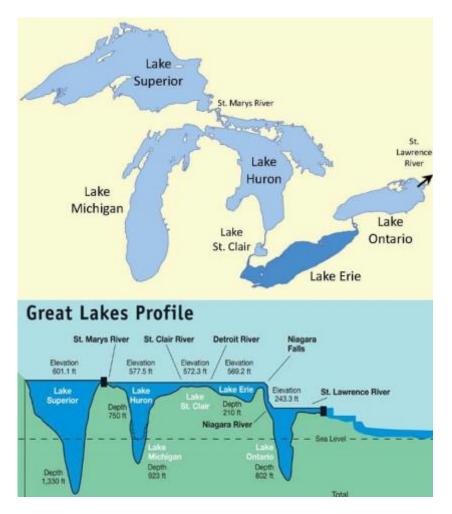


Figure 3 North American Great Lakes (Michigan Sea Grant)

Lake Erie is the shallowest of the Great Lakes with an average depth of 19 m (62 feet) and a maximum depth of 64 m (210 feet) (NOAA, 2014a). It is also the smallest of the Great Lakes by volume (116 cubic miles, or 483 cubic km), although it is only the fourth smallest by surface area (9,910 square miles, or 25,655 square km) (NOAA, 2014a). The water retention or replacement time is 2.7 years, which is short compared to the 6 to 173 years of the other Great Lakes (NOAA, 2014a). An overall bathymetric view of Lake Erie is shown in Figure 4 (NOAA, 2014c).

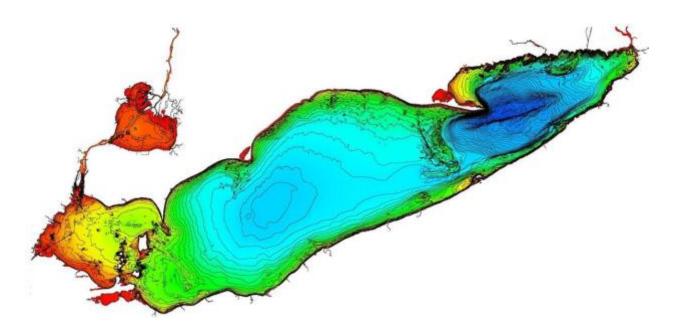
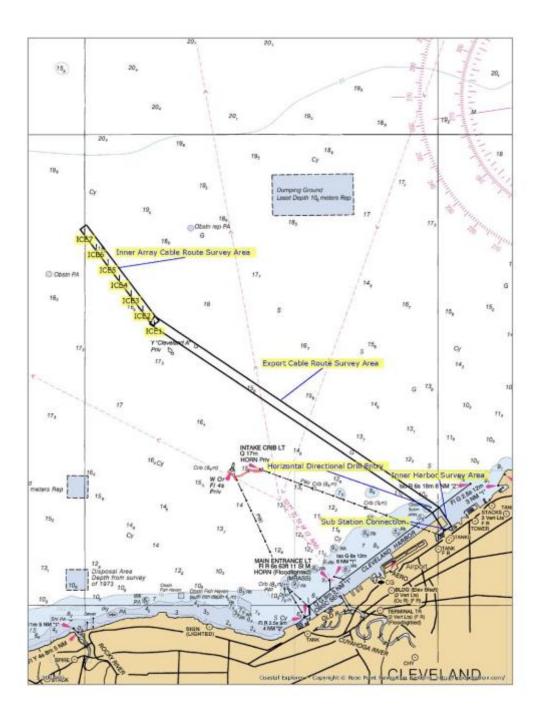


Figure 4 Bathymetric Map of Lake Erie (NOAA)

Lake Erie consists of three distinct regions: the western, central, and eastern basins. Each region has significantly different bathymetric characteristics. The western basin is the shallowest with an average depth of 7 m (21 feet) and features rocky outcrops, shoals, and islands (Waterkeeper, 2014). The central basin has a large flat bottom with an average depth of 20 m (65 feet) and a maximum depth of 24 m (80 feet) in a broad depression in the middle of the Lake (Waterkeeper, 2014)(NOAA, 2014d). In contrast, the eastern basin contains a sharp, deep gouge with several escarpments, an average depth of 24 m (80 feet), and the deepest depths of the Lake off the tip of a long sandy peninsula (Waterkeeper, 2014).

The survey areas (Figure 5) lie between 0 and 20 km (0 and 12.4 miles) offshore of Cleveland, Ohio in the central basin. Corresponding water depths are 5 to 19 m (15-60 feet) relative to the Lake Erie Chart Datum of +173.5 m (NOAA Chart 14829).



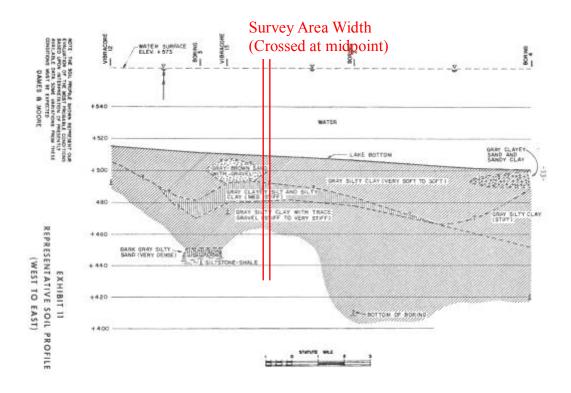
# Figure 5 Icebreaker Demonstration Wind Project Site and Bathymetry (VanZandt, NOAA Chart 14829)

# 3.1.2 Geology

The Great Lakes were formed predominantly by glacial processes. After repeated carving by glaciers during the Pleistocene epoch, only Paleozoic sedimentary rocks remain under

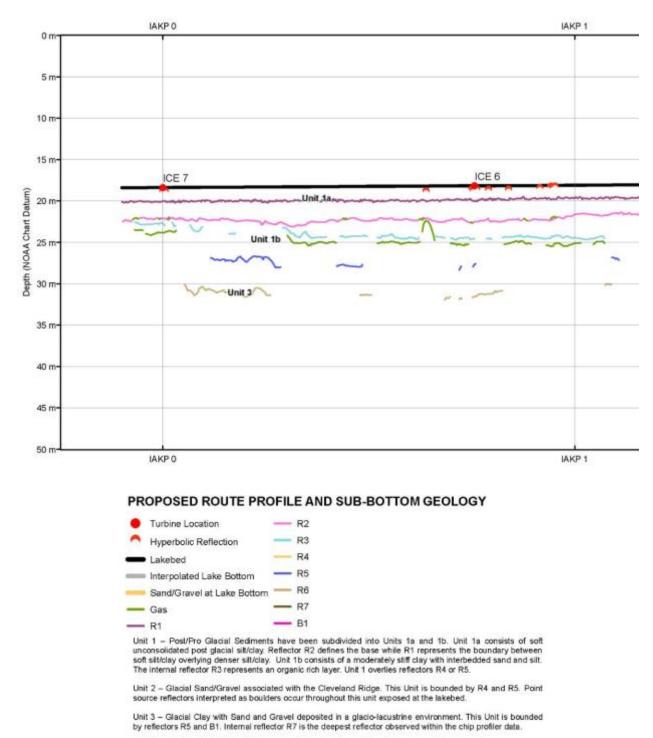
northern Ohio (Dames, 1974). The Paleozoic bedrock exposed under Cleveland is from the Upper Devonian period and roughly dates to between 360 and 380 million years ago (Dames, 1974). This rock is mostly shale and is exposed in cliffs along Lake Erie's shoreline both to the east and west of the City (Carter, 1982). The basin containing Lake Erie itself was carved into this bedrock by repeated Pleistocene glaciations (Dames, 1974). During the last period of Wisconsinan glaciations, the ice moved from the northeast to the southwest to create the lake basin known today (NOAA, 2014d). During the Wisconsinan ice sheet's retreat starting 14,000 years ago and ending 12,600 years ago, glacial till deposits were left behind (Carter, 1982). These deposits are generally unstratified hard clay and gravel called basal till (Carter, 1982). They were created in a deep prehistoric lake that existed until the ice sheet fully retreated (Carter, 1982).

After the start of the Holocene 12,600 years ago, fine-grained lake sediments were deposited above the Pleistocene till layer (Carter, 1982). These post-glacial sedimentary deposits consist of either soft silt or sand in various mixtures. A cross section of Lake Erie water, silt, till, and bedrock is shown in Figure 6 running west to east, through the midpoint of the turbine area, showing the typical subbottom conditions that exist in that area. It should be noted both the bedrock and till layer thicknesses are fairly constant within the boundaries of the 300 meter (1000 foot) width of the survey area.



# Figure 6 West to East Geologic Cross Section, Lake Erie off Cleveland, Ohio (Dames & Moore)

The geology along the 4.7 km (2.9 miles) length of the turbine area varied slightly from southeast to northwest. Isopach data for soft clay sediment from the Dames & Moore survey vary from 3 m (10 feet) at the southeastern end to 7.6 m (25 feet) at the northwestern end of the survey area (Dames, 1974). This is comparable with CSR's higher resolution multi-beam subbottom geology survey results of 3 to 7 m (10 to 23 feet) clay sediment layer (Unit 1) from southeastern to the northwestern end (Figure 7) (CSR, 2016, Enclosure 1).



Unit 4 - Undifferentiated Glacial Sediments. This unit is bounded by B1 and acoustic basement.

#### Figure 7 Typical Sub-bottom Geology Turbine Area (CSR)

The geology along the 13.2 km (8.2 miles) length of the export cable area varied slightly from southeast to northwest. The soft clay sediments (Unit 1) vary from 0 m at the southeastern end to 3 m (9 feet) at the northwestern end of the export cable area (CSR, 2016, Enclosure 2-4).

The glacial sand/gravel sediments (Unit 2) average about 5 m (15 feet) for the export cable area (CSR, 2016, Enclosure 2-4). These sediment layers are much deeper than the trench depth of the export cable of 1.5 m (5 feet).

#### 3.1.3 Flora and Fauna

Lake Erie is the most biologically productive of all of the Great Lakes and contains a large, active freshwater fishery (Waterkeeper, 2014). The lake's productivity is due mostly to the large abundance of phytoplankton, small plants in the water column which form the basis of the food chain (NOAA, 2014b). The warm lake water temperatures due to the relatively shallow depths and an abundance of nutrients from rivers help the phytoplankton thrive. Green alga, a single celled plant, is the most important and the basis of the summer food web (NOAA, 2014b). Diatoms, flagellates, and blue-green algae (cyanobacteria) are also present, especially in the early spring or late summer months (NOAA, 2014b). An overabundance of both phosphoric nutrients combined with rain events, and summer sunlight can lead to algae blooms. These have posed significant environmental problems during recent years.

The phytoplankton serves as food for a variety of creatures in the Lake, including zooplankton and macroinvertebrates (NOAA, 2014b). Zooplankton, small animals in the water column, feed on both the phytoplankton and each other (NOAA, 2014b). Macroinvertebrates (larval insects, worms, amphipods, or mollusks) feed on the phytoplankton or detritus on the bottom (NOAA, 2014b). Foraging fish (perch, shad, drum, catfish, carp, and gobies) eat both the zooplankton and macroinvertebrates (NOAA, 2014b). These fish are then eaten by the piscivores, or the top predatory fish, such as walleye, bass, and trout (NOAA, 2014b).

Figure 8 illustrates the food web of Lake Erie (NOAA, 2014b). At the bottom of the web are the phytoplankton colored in green. The next level is comprised of the zooplankton and macroinvertebrates colored in light blue and orange, respectively. The third level is made up of the foraging fish shown in dark blue, and the top level includes the piscivores colored in purple.

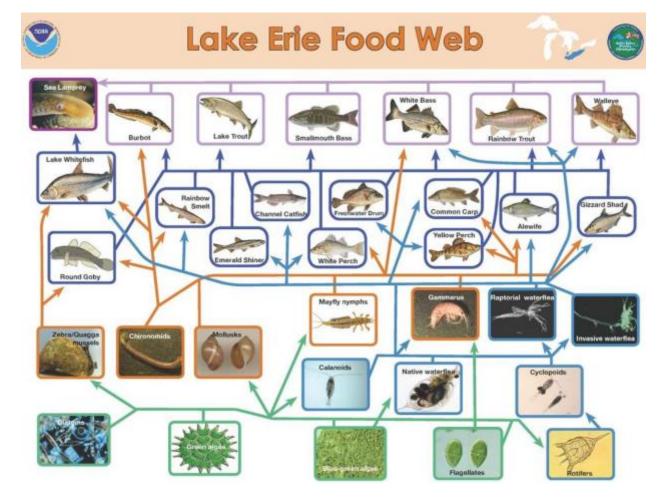


Figure 8 Lake Erie Food Web (NOAA Great Lakes Environmental Research Laboratory)

#### **3.2 Prehistoric Context**

Any prehistoric artifacts or structures predating the Holocene Epoch were either destroyed or scattered during glaciations that occurred during that time. The last of the glacial ice sheets, the Wisconsinan's, began retreating during the Pleistocene Epoch ~14,000 years before present (YBP) and ended ~12,600 YBP with glacial till deposits being left behind (Carter, 1982). These deposits generally consist of unstratified hard clay and gravel that are called basal till (Carter, 1982). Additional deposits are stratified and clay-rich, and these are called flow till (Carter, 1982). These deposits were deposited over the Lake Erie basin's shale layer. The thicknesses of the glacial till in the survey area have a range of 55 to 93 feet (Dames, 1974) and 53 to 85 feet (Alpine, 2010).

After the start of the Holocene ~12,600 YBP, fine-grained lake sediments were deposited above the Pleistocene till layer (Carter, 1982). These post-glacial sedimentary deposits consist of either soft silt or sand in various mixtures. The thickness of these soft silt and clay deposits in the survey area vary from 10 to 25 feet (Dames, 1974) and 10 to 16 feet (Alpine, 2010).

During the period from ~12,000 YBP to ~5,400 YBP the lake level was below the turbine APE, which has an elevation at the glacial till layer of +492 feet, thus exposing the land for possible human habitation or use. The lake level during that period varied from +394 feet during the post glaciations Early Lake Erie stage to +476 feet during the Middle Lake Erie stage, ~7,500 YBP (Herdendorf, 2013). At the start of the Middle Lake Erie stage, ~5,400 YBP, the lake level had risen to +525 feet, which inundated the turbine APE, placing any possible prehistoric occupation site underwater (Herdendorf, 2013). After the Middle Lake Erie stage the lake level continued to rise to its present day level of +569 feet (Herdendorf, 2013).

Paleoindian occupation of Northern Ohio was believed to have occurred between 13,000 to 11,000 YBP (Herdendorf, Klarer, Herdendorf, 2006). The earliest evidence in Ohio of occupation is at the Paleo Crossing site (33ME274) in Medina County, Ohio, which has been dated between 10,000 to 11,500 YBP (Brose, 1994).

It is possible that artifacts from early occupation could exist buried at the proposed site, but to date Lake Erie has not been a focus of archaeological research on Paleoindian culture (Stothers, Abel, 2001).

> "Paleoindian sites present a very low archaeological profile across the landscape and are representative of areas where small groups of people would perform specific tasks of short duration. Additionally in northern Ohio, Stothers and Pratt (1980) note that Early and Middle Archaic sites are usually of two types: "those in which a single or a few points are included in a collection of material from other cultural periods, and those in which Early or Middle Archaic materials predominate." The later, mixed sites, would not be represented in the areas examined. The potential for locating Early and Middle Archaic sites beneath Holocene lake sediments with today's remote sensing technologies is a factor of sedimentation depths and relict landscapes. Features such as hidden outcrops that may indicate cultural use areas, have been covered by natural lake sedimentation processes. Therefore, it would be difficult or impossible to locate sites if they existed (Gray & Pape, 2014)."

#### **3.3 Historic Context**

Lake Erie has been instrumental in historical shipping and transportation in the Great Lakes. The permanent settlement of the Ohio shores of Lake Erie occurred at a slower pace than that of the Ohio or Mississippi valleys due to the control of the lake by Great Britain (Mansfield, 1899). It wasn't until 1796 that the British relinquished control of their post commanding Lake trade (Mansfield, 1899). Since the opening of the Erie Canal in 1826 from the Hudson River to Buffalo, New York, Lake Erie has served as the crucial nexus for shipping into the upper Great Lakes region and eventually points further west. Immigrants and goods moving westwards would start in New York City; move up the Hudson River by ship, travel along the Erie Canal by boat, and then board yet another ship in Buffalo for transportation down the length of the Lake. At first, Lake Erie was the earliest of the Great Lakes' destination as immigrants from Europe and the Northern States began to settle along its shores. Eventually, however, passengers and goods continued on to the other lakes and, ultimately, Chicago, which then served as the starting point for further western expansion (Mansfield, 1899). It was estimated in 1832 that more than half of the immigrants arrived in the West by water (Mansfield, 1899).

As settlers grew crops, harvested timber, and mined copper and iron ores, these products flowed eastwards back down the lakes and across Lake Erie to be delivered to the east coast. Meanwhile, coal from Pennsylvania, new immigrants, and finished manufactured goods continued to travel westward across Lake Erie from Buffalo. In order to deliver these people and goods, many hundreds of ships operated on the Great Lakes every season in the 19th century (Mansfield, 1899). These ships were frequently made of wood and lacked radio, radar, or modern electronic navigational aids. Furthermore, there was a general lack of accurate weather forecasting, detailed bathymetric information, and other useful aids to safety. As a result, many unfortunate vessels collided with each other, ran aground, sprang leaks, caught fire, or foundered in storms. Lake Erie is the shallowest of all the Great Lakes and is known to have especially severe waves due to its lack of depth and prevailing winds, which blow along the length of the Lake and have caused many ships to succumb to its depths. The end result is a high number of shipwrecks, possibly numbering in the thousands, in Lake Erie (Frew, 2014).

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The exact number and location of these shipwrecks is unknown because of the lack of accurate records for these events. There is no central governmental repository that records sinkings. In many cases the only record of a shipwreck may be a story in a local town or city newspaper. Official records are split among two national governments (United States and Canada) and multiple governmental agencies and archives, making an accurate accounting nearly impossible. This is further exacerbated by the fact that many ships were raised and put back into service without as much publicity as surrounded their sinking events, making the total number of shipwrecks in Lake Erie and more are found regularly (ODNR, 2009). Estimates put the total number of shipwrecks in Lake Erie at between 500 and 3,000 (Frew, 2014) (ODNR, 2009).

Historic shipwrecks consist of both wooden and metal ships, sailing vessels, sidewheel steamers, and propeller steamers. The cold fresh water of the Great Lakes tends to serve as an excellent preservative for these wrecks. There are no wood-eating organisms, such as the Teredo worm found in warm ocean environments. Cold water greatly inhibits bacterial decay, allowing wooden timbers and grain cargos to survive. The fresh water is also much less corrosive on metal artifacts, unlike the salty oceans, and the inland seas do not have storms as destructive as ocean-borne hurricanes and typhoons. Thus, many of the shipwrecks in the Great Lakes serve are well preserved archaeological sites that provide significant information about 19th century shipbuilding, shipboard life, and the associated maritime landscape associated with these wrecks.

#### **3.4 Literature Review**

VanZandt Engineering consulted the Ohio Historic Preservation Office (OHPO) online mapping system in an effort to locate any inventoried cultural resources identified within the survey area. The archival study included a review of the Ohio Archaeological Inventory (OAI), Ohio Historic Inventory (OHI), the National Register of Historic Places (NRHP), Ohio Sea Grant Shipwreck map, the Cleveland Underwater Explorers shipwreck data base, and the Cleveland Underwater Explorers historical Lake Erie nautical chart collection. Four previously-inventoried cultural resources (shipwrecks) have been identified within 3.5 nm of the survey area. These shipwrecks were the *Admiral* and *Dundee* (3.0 and 3.3 nm, respectively, from the northwest survey corner point), and the CSU wreck and East Breakwall Barge (0.5 and 1.6 nm,

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respectively, from the export cable area). None of these wrecks were detected within the survey area.

Results of the literature review are described below:

#### **Ohio Archaeology Inventory:**

No properties listed on the Ohio Archaeology Inventory are present within the survey area.

#### **Ohio Historic Inventory:**

No properties listed on the Ohio Historic Inventory are present within the survey area.

#### **National Register of Historic Places:**

No individual properties or districts listed on or determined eligible for listing on the NRHP are present within the survey area.

#### **Ohio Sea Grant Shipwreck Map:**

No shipwrecks on the Ohio Sea Grant Shipwreck map are present within the survey area. Four shipwrecks are located within 3.5 nm of the survey area. These shipwrecks were the *Admiral* and *Dundee* (3.0 and 3.3 nm, respectively, from the northwest survey corner point), and the CSU wreck and east breakwall barge (0.5 and 1.6 nm, respectively, from the export cable area). The shipwreck map shows the possibility of the *Dreadnaugt* (probably *Dreadnaught*) and the *Mackinaw* being close to the survey area, but these locations are unconfirmed and based off of shipwreck maps that were for sale to the public. Most of the locations derived from these maps are not verified, and therefore the ODNR did not base their offshore wind farm siting analysis on them. See, Wind Turbine Placement Favorability Analysis Map Methodology (ODNR, 2009).

Further historical research on both shipwrecks show that the *Dreadnaugt* came ashore and was abandoned and the *Mackinaw* was farther from the project APEs than the shipwreck map indicated. Thus, neither would be close to project APEs. The Cleveland Underwater Explorers (CLUE) has recently discovered what they believe are the remains of the *Mackinaw*, and it is its located 4.4 nm east of the project site.

#### **Cleveland Underwater Explorers Shipwreck Data Base:**

No shipwrecks in the Cleveland Underwater Explorers shipwreck data base are present within the survey area.

#### **Cleveland Underwater Explorers Historical Lake Erie Nautical Chart Collection:**

No shipwrecks were found charted on any chart in the Cleveland Underwater Explorers historical Lake Erie nautical chart collection within the survey area or within 3.5 nm of the survey area.

#### 4.0 METHODS

#### 4.1 Survey Design

The main objectives of the survey were to identify and map surficial geology, lakebed features and sub-bottom conditions within the WTG area and the proposed submarine cable routes.

The objectives of the geophysical survey were accomplished by the collection, interpretation and subsequent reporting of geophysical data. The following types of data were collected during the marine geophysical survey (CSR, 2016):

- Differential GPS navigation was constantly recorded to provide real-time georeferencing for all data sets acquired during the survey.
- Sidescan sonar data were acquired to identify potential hazards exposed on the surface of the lakebed (shipwrecks, pipelines, boulders, debris, ice gouging) and to categorize surficial sediment types.
- High-resolution chirp profiler data were acquired throughout the geophysical program to identify the sub-bottom geology to a depth of at least 5 m (15 feet).
- Lakebed bathymetry data was continuously logged throughout the geophysical program using a multibeam echosounder in order to determine water depths (lakebed elevations) along the route.
- Marine magnetometer data were collected to identify surface and buried ferrous targets.
- Grab samples were collected to ground truth the surficial geology interpretation.
- High resolution 50 kHz profiler data was collected over the proposed turbine locations to aid the interpretation of the near surface unconsolidated sediments.
- High-resolution single channel seismic (mid penetration "boomer") data were acquired within the Harbor and near shore areas to aid the interpretation over the HDD location.
- Sidescan sonar and magnetometer data were not collected in the harbor since the cable will be installed at depth within a HDD casing and therefore there was no requirement for archaeological clearance.

#### 4.2 Overall Survey Layout

#### 4.2.1 Turbine Area

Survey coverage over the Turbine Area included a 240 m (720 feet) corridor centered on the proposed route extending from WTGs ICE1 to ICE7. Overall, 22 lines were surveyed totaling 47 line km. Tie line spacing was 375 m (1,125 feet) along the Turbine Area. Figure 9 illustrates the geophysical survey track lines in the Turbine Area (CSR, 2016).

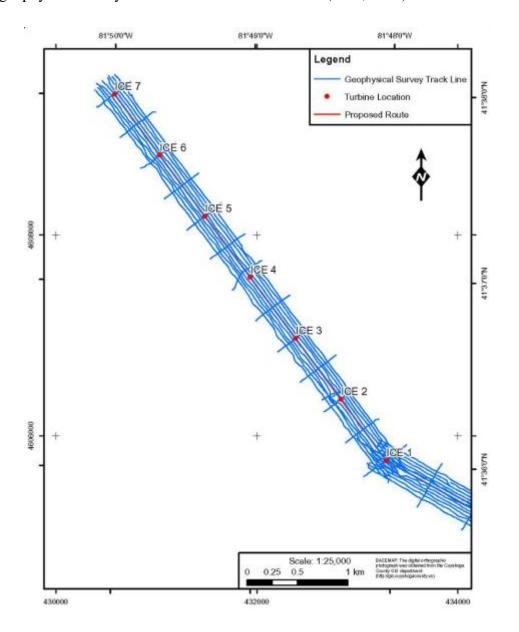
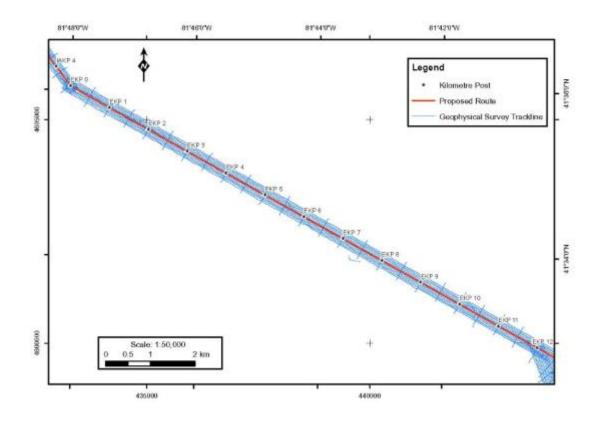


Figure 9 Geophysical survey track lines over the Turbine Area. (CSR)

#### 4.2.2 Export Cable Area

Survey Coverage over the Export Cable Area included a 300 m (990 feet) corridor centered on the proposed route. The Export Cable Area extends from the proposed HDD exit location to WTG ICE1. The survey area was expanded north of the breakwater to TP1 and TP2 to ensure that enough data was acquired to accommodate alternative HDD exit locations. Additional lines were surveyed parallel to the breakwater to gain more information in the HDD exit area, and to map the toe of the breakwater slope. Overall, 73 geophysical survey lines were run totaling 206 line km. Figure 10 illustrates the geophysical survey track lines along the Export Cable Area (CSR, 2016).

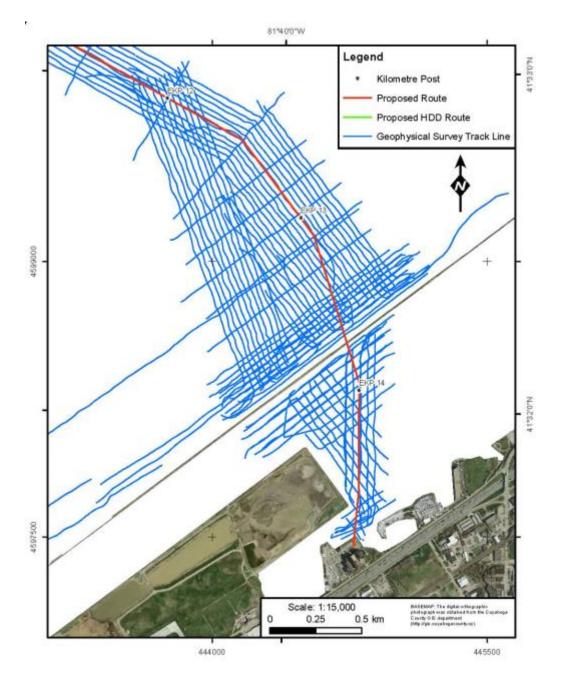


# Figure 10 Geophysical survey track lines along the Export Cable Area. (CSR)

#### 4.2.3 Inner Harbor Area

The geophysical survey lines were designed for the collection of multibeam sonar and sub-bottom profiler data along potential HDD routes between the Cleveland breakwater and the landfall. A total of 26 lines were surveyed, totaling 18 line km. Figure 11 illustrates the geophysical survey track lines within the harbor area (CSR, 2016).

Sidescan sonar and magnetometer data were not collected in the harbor since the cable will be installed at depth within a HDD casing, and therefore there was no requirement for archaeological clearance (CSR, 2016).



# Figure 11 Geophysical survey track lines within the Harbor and over the near shore HDD exit Location. (CSR)

### 4.2.4 Locational Data:

Note: Locational data in decimal degrees, WGS84 geodetic and UTM, NAD27, Zone 17, M

#### Table 1 Wind Turbine Generator Locations:

- ICE1 N41.60072 W81.80055 433273.438E 4605537.801N
- ICE2 N41.60616 W81.80602 432823.244E 4606146.037N
- ICE3 N41.61159 W81.81150 432372.284E 4606753.200N
- ICE4 N41.61702 W81.81697 431922.235E 4607360.384N
- ICE5 N41.62246 W81.82245 431471.440E 4607968.716N
- ICE6 N41.62789 W81.82793 431020.712E 4608575.966N
- ICE7 N41.63333 W81.83340 (Backup site) 430570.906E 4609184.348N

#### 4.3 Field Methods (CSR, 2016)

The following section describes the methodologies and equipment used to perform the data collection task required for the survey. Survey design and control was based on the guide-lines developed by the Bureau of Ocean Energy Management (BOEM) set forth in NTL No. 2005-G07.

#### 4.3.1 Vessel

The Survey operations were conducted from Underwater Marine Contractors Inc. vessel *Salvage Chief* (Figure 12). The *Salvage Chief* is steel constructed, with an overall length of 49ft. The *Salvage Chief* had ample deck space with a knuckle boom and an extendable hydraulic A-frame, ideal for mounting winches and the deployment/recovery of geophysical equipment. CSR installed over-the-side mounts for dual frequency single beam and multibeam transducers on the starboard side of the Salvage Chief. Electronic equipment and data collection workstations were set up in the vessel's wheelhouse (CSR, 2016).



Figure 12 Salvage Chief (CSR)

### 4.3.2 Survey Reference

Horizontal positioning was calculated using Differential Global Positioning System (DGPS). The primary Coast Guard differential corrections were acquired from the Detroit, MI reference station. The geodetic parameters for the survey were as follows (CSR, 2016):

- Vertical Datum: Lake Erie Chart Datum (173.5 m or 569.2 ft. above IGLD 1985)
- Horizontal Datum: NAD83
- Projection: Universal Transverse Mercator, Zone 17
- Central Meridian 81°W

- False Easting: 500000.00
- False Northing: 0.000000
- Scale Factor: 0.999600
- Latitude of Origin: 0.0
- Linear Unit: Meter

#### 4.3.3 Navigation Control

A real-time DGPS system was utilized during the geophysical survey. CSR's integrated navigation system consisted of a Hemisphere VS-330 DGPS system and the Hypack survey navigation package. The integrated navigation system included real time digital data logging of positional data, a left/right steering monitor for the helmsman, and an interface to the geophysical equipment so that all data was correctly geo-referenced (CSR, 2016).

#### Hemisphere VS-330 GNSS Receiver & Heading System

The Hemisphere VS-330 is a dual antenna DGPS system with a horizontal accuracy of 0.3 m (1 foot) under ideal conditions. The secondary antenna (forward) is used to calculate heading to an accuracy of 0.09° RMS. The system was configured to receive Coast Guard differential corrections from Detroit, MI, which operates on a transmission frequency 319 kHz. Positions for the multibeam bathymetry were calculated based on the offset from the primary Hemisphere DGPS antenna, to the multibeam transducer (CSR, 2016).

#### • Hemisphere R110 DGPS

The Hemisphere R100 DGPS system was used in tandem with the Hemisphere VS-330 during the geophysical survey operations. The system was configured to receive Coast Guard differential corrections from Detroit, MI. The Hemisphere R100 is a single antenna GPS system with a horizontal accuracy of 0.6 m (2 feet) under ideal conditions (CSR, 2016).

Positions for the single beam bathymetry were calculated based on the offset from the Hemisphere R110 DGPS antenna to the transducer. Hemisphere R110 DGPS positioning combined with vessel heading and offset measurements were also used to georeference the sidescan sonar, chirp, and magnetometer data collected during the survey. Cable out measurements were recorded by the operator during the survey for each line with layback corrections applied during processing and interpretation (CSR, 2016).

#### • Hypack/Hysweep Survey Acquisition Software

Hypack is a complete hydrographic survey navigation software package that includes: survey preparation, data collection, data editing, cross-section display, geodesy and exporting capabilities. In operational survey mode, the system supports a helmsman display with survey line indicator, to assure survey lines are followed as accurately as possible. In addition to planned survey grid lines, the survey screen also displays bathymetric contours, coastline, navigational hazards, and target/sample locations. During survey operations all navigation information was logged in Hypack to ensure simultaneous geo-referencing of all datasets (CSR, 2016).

#### 4.3.4 Survey Equipment

#### • SURVEY NAVIGATION

- Hemisphere VS-330 GNSS Receiver & Heading System
- Hemisphere R110 DGPS Receiver
- o HYPACK Survey Navigation Software

#### • MULTIBEAM ECHOSOUNDER

- Teledyne-Odom ES3 Multibeam Echosounder (240 kHz)
- Teledyne-TSS DMS-05 Motion Sensor
- o Teledyne-Odom DigiBar-Pro Velocimeter
- Applied Microsystems SVPlus
- HYSWEEP Multibeam Acquisition System

#### • SINGLE BEAM ECHOSOUNDER

• Odom CV3 Dual Frequency Echosounder (50/200 kHz)

#### • SIDESCAN SONAR

- o Klein 3000 (100/500 kHz) Sidescan Sonar System
- o SonarPro Sidescan Acquisition Software

#### • MAGNETOMETER

o Marine Magnetics SeaSPY Marine Magnetometer

#### • SUB-BOTTOM PROFILER

• Klein 3000 Chirp Profiler (2-8 kHz)

#### • SEISMIC REFLECTION

- EG&G 240 Low Frequency (400-14,000 Hz) Shallow Seismic System (Boomer)
- Applied Acoustics CSP-300 Power Supply
- o Ministreamer with GeoSpectrum M5 Hydrophones
- SonarWiz SBP Acquisition & Processing Software

#### • TIDE GAUGE

- o HOBOware U20 Titanium Water Level Data Logger
- SAMPLING
- Van Veen Grab Sampler

#### 4.3.5 Side Scan Sonar Survey

A Klein 3000 dual frequency sidescan system was used to complete the seabed imaging component of the Icebreaker Wind cable route assessment. The Klein 3000 consisted of a sonar instrumented towfish, a transceiver and processing unit (TPU) and an acquisition computer running Klein's proprietary Sonar Pro software. Capable of simultaneous dual frequency operation (100/500 kHz) and constructed with advanced electronics and transducers, the Klein 3000 produced superior high resolution imagery of the seafloor. High frequency (500 kHz) ranges of between 75 and 100 m on both the port and starboard channels allowed for wide area swath coverage and target detection over the route.

Frequency: 500 kHz
Range Setting: 75 m and 100 m range
Target Resolution: 10-20 cm in ideal conditions
Lane Size: 27 m
Tow Height: 5 to 6 m above the lake bottom
Rationale: 100% seafloor coverage; target detection & surficial geology mapping

During the 2016 geophysical survey, the sidescan system was integrated with the Klein 3000 chirp profiler and marine magnetometer. When the sidescan system is integrated with the chirp profiler only one frequency can be recorded. For this survey the higher 500 kHz frequency was acquired.

Calculated layback measurements were used to position the sidescan sonar system during interpretation and mapping of the data. Layback is calculated using the offset between the DGPS antenna and tow point, the height of the tow above the water line, the depth of the system below the surface, and the length of cable deployed. Where possible, feature matching between the sidescan, sub-bottom profiler and multibeam data was used to confirm layback calculations.

SonarPro was used to operate the Klein 3000 sidescan sonar and chirp systems. The system provides navigational recording, target management, and real-time display of the sidescan data. SonarPro also provides the options to adjust the towfish sensors during data acquisition, including range and transmit power, which is directly recorded with the raw data. The target management feature enabled the selection of seabed targets in both real-time and during playback following collection. The sidescan and chirp data were recorded to XTF format (CSR, 2016).

#### 4.3.6 Magnetic Survey

A Marine Magnetics SeaSpy Magnetometer was used for the survey. The SeaSpy is a digital marine magnetometer that operates using an advanced Overhauser sensor. Measuring the ambient magnetic field, using a specialized branch of magnetic resonance technology, the SeaSpy has an absolute accuracy of 0.2 Nanotesla (nT). The sensor is capable of measuring a range of 18,000 nT to 120,000 nT in all directions, resulting in no dead zones and reliable data.

29

During the 2016 geophysical survey, the marine magnetometer was integrated with the Klein 3000 system (CSR, 2016).

#### 4.3.7 Sub-bottom Mapping System

Sub-bottom geophysical data was acquired using two systems, a chirp profiler and a single channel seismic system (CSR, 2016).

The Klein system uses two Chirp transmit transducers with a single linear hydrophone. The Mills Cross configuration achieves higher resolution and deeper bottom penetration than comparable systems. The Klein 3000 chirp sub-bottom profiler (SBP) integrates with the Klein 3000 sidescan system. It mounts directly to the Klein 3000 tow vehicle and uses the existing physical connections and electrical communications. This option takes advantage of the existing Klein 3000 sidescan hardware by using the same tow cable, transceiver processor unit (TPU), workstation and towing systems. The chirp sub-bottom profiler consists of a subsea assembly used to contain the transmit projectors, receive hydrophone and SBP electronics. These components are enclosed in a fiberglass shroud with an integrated support structure to allow for combined transducer/electronics mounting and towing. The Klein 3000 tow vehicle installs into the rear portion of the shroud assembly where it interconnects with the SBP electronics. The amplifier modulates both amplitude and phase of the transmit waveform for pulse lengths up to 40 msec.

#### **Specifications:**

Chirp Frequency: 2-8 kHz Beam Angle: 20° along track; 40° cross track @ 5 kHz Resolution: 12.5 cm or better Power: 1 kwatt Source Level: 204 db @ 1 m

CSR has achieved penetration of up to 100 m (330 feet) with this system in fine grained sediments. During this survey the maximum penetration achieved was 15 to 20 m (49 to 66 feet) within post glacial and glacial fine grained sediments. The chirp signal was impeded in areas where shallow gas and coarse grained glacial sediments occurred.

Additional survey data were collected using a single channel seismic (Boomer) system. This system provides low frequency energy in the range of 400-10,000 Hz and includes four main components (boomer plate, power supply, hydrophone, and acquisition computer). The energy source for the system was the Applied Acoustics CSP-300 which has output settings ranging from 50-300 joules. The CSP supplied power to the boomer plate, which was towed in conjunction with a low frequency hydrophone streamer. The boomer plate was responsible for transmitting the sound energy through the water column and lakebed sediments. The hydrophone streamer received the reflected sound energy, transmitting the signal to the topside recording computer.

The raw and processed acoustic signal was recorded on a topside computer running SonarWiz acquisition software. DGPS positioning information was integrated with the data in real-time and recorded by SonarWiz in seismic data SEG-Y format. Acoustic frequency filters applied to the data in real time using SonarWiz were not recorded to the raw data. The frequency filters essentially "cleaned" the data allowing for better visualization and interpretation of the sub-surface sediments. Low- Cut (400 Hz) and High-Cut (4000 Hz) frequency filters were applied to the data in real time using the SPA-3 processing unit. This data was recorded to a second channel within the SGY file. In addition to filter processing, the SPA-3 unit (IKB Technologies Ltd) also controlled the firing rate of the boomer system.

During this survey the energy source was operated at an output level of 100, 200, and 300 joules with a firing rate of 1/4 second (100 joules) and 3/8 second (200 & 300 joules). The record length was synced to the firing rate within SonarWiz.

CSR has achieved penetration of greater than 100 m (330 feet) with this system in fine to coarse grained sediments. During this survey the maximum penetration achieved was 50 to 60 m (165 to 198 feet) within post glacial and glacial sediments over the HDD survey area. The boomer signal was impeded in areas where shallow gas and acoustic basement (interpreted to be bedrock) occurred.

# 4.3.8 Personnel

Party Chief	Colin Toole, CSR
Hydrographic Surveyor	Luke Melanson, CSR
Electronics Technician	Jon MacDonald, CSR
Vessel Captain	Joel Frazer, Underwater Marine

# 5.0 DATA ANALYSIS

# 5.1 Sidescan Sonar Data Analysis

A review of 271 line km of sidescan data showed no historic structures (such as shipwrecks) or artifacts were present within the turbine (Figure 13) and export cable (Figure 14) survey areas. (Note: For full size images see appendices)



Figure 13 Turbine Survey Area Sidescan Mosaic. (CSR)

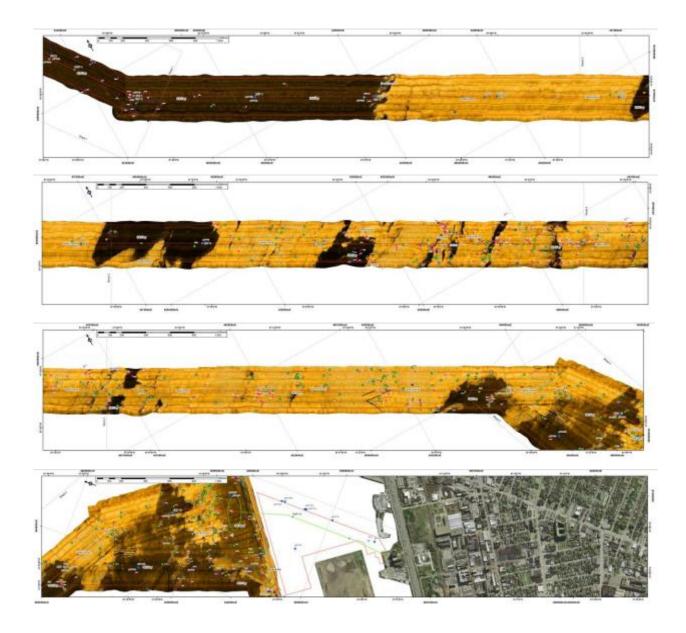


Figure 14 Export Cable Survey Area Sidescan Mosaic (CSR)

The Side Scan Sonar showed a generally uniform and smooth lake bottom. Some evidence of ripples or other sedimentary features were observed along the survey route (Figure 15) and some areas of the bottom revealed enhanced reflectivity denoting a change in geological structure (Figure 16). These locations were assigned a target number, and corresponding imagery and information can be found in Appendix A.

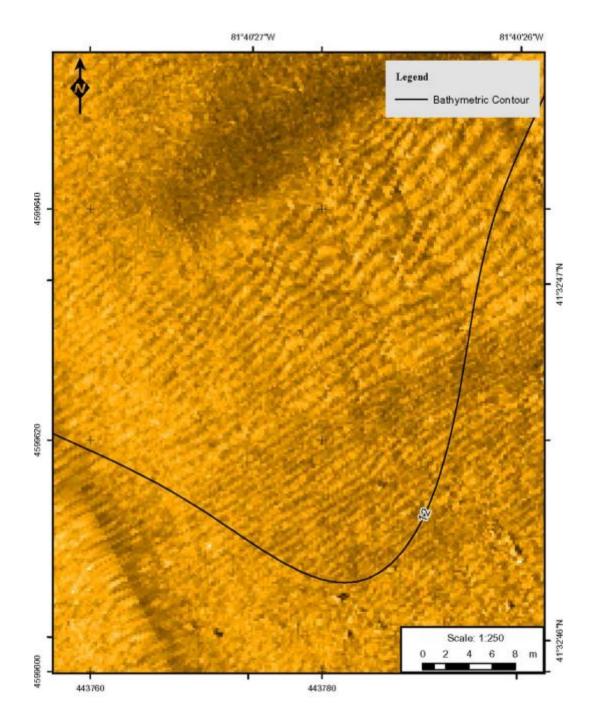
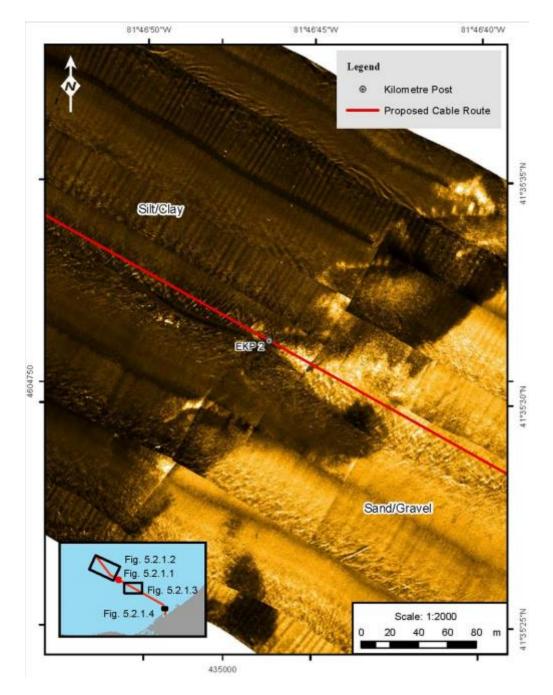


Figure 15 Sediment Rippling along Export Cable Route (CSR)





The only targets identified were geological or the result of old trash dumpings (rectangular, circular, and linear contacts) and dredge spoil (circular contacts) in the survey areas (Figure 17). A total of 455 identified targets were analyzed and the detailed description of the targets can be found in Table 2 (Locational data in NAD83 Geographic, NAD83, Zone 17, M, and NAD83, Ohio State Plane North, US Survey Feet). See Appendix A for complete target data with images. There are a number of targets that may indicate the presence of a linear ferrous feature perpendicular to the proposed route. This feature could not be identified from the sidescan or sub-bottom profiler data acquired over this area. An analysis of the magnetic data shows that these targets are most likely buried steel or iron buoy blocks or anchors.

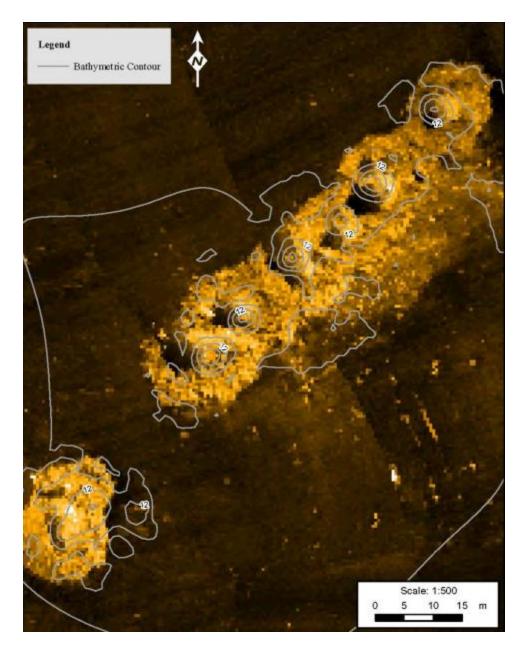


Figure 17 Sidescan Sonar Record of Dredge Spoil. Center of Data Example is Located 150 m E of EKP 12. (CSR)

	MADES 0	leographic .	MADES U	TM Zene 17	MADES Ohio S	tate Plane North	ican Senar Con	and the second second second			000000		harren ar an an a
ID	Latitude	Longitude	East(m)	North (m)	East (US survey feet)	North (US survey feet)	Bathymetry (m)	Distance from Proposed Route (m)	(m)	Width (m)	Height (m)	Description	Associated Ma Associated Ma
a		-81.8181120		4607646.7	2154951.3	711527.0	17.8	35.5	2.6	0.5	0.2	Linear Contact	-
0	41.6170757	-81.8170325	491990.9	4607584.3	2155248.0	711327.6	27.7	0.9	30.0	0.2		Linear Contact	1 (#) 1
G	41.8127124	-81.0118483	432358.2	4607095.8	2156678.1	709748.8	17.6	51.6	2.5	1.0	- 88	Point Source (Probable Buoy Mooning)	
64	41.6114662	-81.8115284	432383.6	4606957.2	2156769.2	709295.5	17.5	10.6	7.4	7.0	- 42	Circular Contact (Probable	
25	41.6051141	-81.8060026	432838 A	4606358.7	2158295.7	707357.3	17.3	1.6	3.9	35		Beoy Mooring) Greuler Contact	
65	41.6044110	-81.8026013	433120.1	4506167.0	2159230.9	705744.1	17.2	110.5	2.2	12	0.6	Point Source	M84
0	41.6043767	-81.9035480	433124.5	4606163.1	2159245.5	705731.8	17.2	111.8	1.8	0.8	0.6	Paint Source	2
CE	41.5006765	-81.8006100	433262.2	4605750.0	2159706.4	705367.6	17.1	7.2	5.5	5.5	÷.1	Groular Contact (Probable Buoy Mooning)	M49, N50
CB	41.6002432	-81.8004522	433291.6	4605702.6	2159619.9	705250.1	17.1	44.5	1.0	1.5	0.1	Rectangular Contact	
C10	41.5975261		453806.4	4605374.0	2161527.9	704180.5	16.9	79.4	3.0	1.8		Linear Contact	
C11 C12	41.5882561		434570.8 435588.1	4604611.5 4604351.2	2165392.0 2167268.2	700923.0	16.0	175.5 125.3	3.2	0.3	0.2	Linear Contact Rectangular Contact	
C13	41.5838214	-81.7591219		4603848.3	2171185.5	699340.0	15.8	15.1	\$.7	0.9	0.2	Linear Contact	с эк
C14	41.50331114	-01.7552133	437048.2	4603766.6	2172256.9	699090.4	36.4	102.8	19.5	8.6	10	Circular Contact (Possible Dredge Spoil)	
C15	41 5801031	-81.7460653	437807.9	4603426.2	2174769.0	698016.5		177.1	3.9	2.4		Low Reflectivity Patch (Possible	
LIS	41 5001051	-01.74606555	+37607.9	40034.20.2	21/4/09/0	609010-3	- 73	117.1	2.9	2.4	100	Slag)	- 13 -
C16	41.5785477	-81.7451360	437883.9	4608252.6	2175028.2	697451.9	15.9	62.8	8.1	14	D.6	Loss Reflectivity Patch (Possible Slag)	1.00
617	41.5794293	-81.7450774	437889.6	4603850.5	2175041.4	697772.6	15.9	150.9	11.0	0.4	0.0	Linear Contact	5 (8
CLE	41.5782767	-81.7449797	437896.6	4603222.2	2175071.8	697352.2	15.8	42.5	6.7	1.5	0.5	Low Reflectivity Patch (Possible	÷
C19	41 5780199	-81.7445240	437934.4	4603193.6	2175197.3	697260.4	15.8	36.0	4.3	0.5	-	Slag  Linear Contact	1
C20	41.5761775	-81.7444257	437940,0	4602909.0	2175230.0	696589.3	15.7	139.4	1.2	0.2	- 430	Linear Contact	12
C21	41.5753894	-81.7432666	438036.7	4602900.7	2175549.6	696304.9	0.0	169.8	0.8	0.5	0.1	Orcular Contact (Probable Tine)	- 1e
C22	41.5749766		438144.3	4602853.5	2175905.2	696157.6	15.7	157.8	2.7	0.7	0.5	Point Source	
C23	41.5763451	-81.7416041	438176.2	4603005.6	2176001.5	696687.1	15.8	9.9	3.9	0.5	+	Livear Contact	
C24	41.5767962	-81.7412561		4603048.7	2176095.4	696800.4	15.8	42.1	9.2	0.2	0.1	Linear Costact	<ul> <li>(#)</li> </ul>
C25		-85.7410623		4603169-4	2176145.6	697131.6	15.7	138.2	2.6	0.5	0.1	Linear Contact Low Reflectivity Patch (Possible	
26	41.5764126	-81.7407087	458250.9	4605012.4	2176246.2	696683.8	15.0	32.6	2.0	0.0	0.4	Slagi	(m)
C27		-81.7405391		4605067.6	2175291.0	595065.8	15.8	87.9	8.1	0.4	+02	Linear Contact	2 (H)
C28 C29	41.5748367	-81.7404957 -81.7402303	438267.2 438291.5	4602837.3 4603097.4	2176309.5	696110.1 696565.1	15.7	112.2	2.8	0.6	0.1	Linear Contact Linear Contact	
(30		-81.7387384		4603067.4	2176788.0	696531.5	15.7	69.9	3,4	0.8		Linear Contact	
C91		-81.7382432		4.903017.5	2176920.9	696712.2	15.7	137.6	11.1	0.3	0.1	Linear Contact	
- 12	41.5756655	-81.7376941	430501.5	4601927.3	2177073.4	696410.0	15.7	80.6	2.2	1.1	- 49	Low Reflectivity Patch (Possible	2 12
C33	41.5726019	-01.7357009	439557.A	4602585.9	2177604.4	693307.1	15.4	140.0	4.9	1.4	- 40.0	Slag) Circular Contact	
034	41.5727777	-81.7355758	and the second second second	4602605.2	2177662.2	695371.7	15.4	115.2	2.4	2.2	0.7	Circular Contact (Probable	1.1
											- 0.7	Oredge Spoil)	
C35	41.5781219	-81.7352714	0211011101020	4602643.1	2177744.4	695497.5	15.4	69.6	6.0	3.4		Rectangular Contact Loss Reflectivity Patch (Possible	
Call	41.5746357	-91.7351299	438714.3	4602811.2	2177778.2	696049.7	15.6	83.5	1.9	11	- 13,	Slag)	191
C97	41.5742500	-81.7351027	438716.2	4602708.3	3177786.9	695009.3	15.6	47.1	2.1	1.5	- K/-	Circular Contact	6 - 38 -
C38	41.5745852	-61.7350109	438724.2	4602805.5	2177813.0	696031.0	15.6	83,4	4.5	2.9	*	Low Reflectivity Patch (Possible Slag)	1 (A)
			-				15.4		4.5	31	- 20	Low Reflectivity Patch (Possible	0.00
C39	41.5732856	-81.7349705	438726,3	4602661.2	2177826.2	693558.2	15.4	41.5	4.5	- 24	- 100	Slag	
648	41.5720940	-81,7341911	438790.2	4601528.3	2178043.2	695125.9	15.3	126.2	7.0	5.6	- 83	Low Reflectivity Patch (Possible Slag)	(H)
041	41.5748022	-91.7341269	438798.1	4602928.9	2178052.1	696112.0	15.6	140.0	2.6	1.5	D.B	Point Source (Probable	1.2
_												Bouider] Low Reflectivity Patch (Possible)	2
D42	41.5717875	-81.7540750	458799.7	4602494.2	2178076.5	695014.5	15.2	151.1	7.3	3.4	- 80	Slag]	1.0
643	41.5719499	-81.7940639	438800.7	4602511.8	2178078.5	695072.2	15.3	135.5	3.7	31	- 63	Low Reflectivity Patch (Possible	1.12
	TAUTACTOR			TYPECALT		Propriate .						Sing	<u> </u>
644	41,5721798	-81,7336485	438835.5	4602537.5	2178193.4	695158.5	18.3	96.8	17.9	17,4	- 43	Low Reflectivity Patch (Possible Slag)	2 13
C45	41 5722820	-81.7332410	438869.6	4602548.5	2178302.6	695196.7	15.2	69.7	4.0	0.4	D.1	Linear Contact	1.12
D46	41.5729978	-81.7850702	430004.5	4002627.9	2178947.0	\$95457.£	15.4	6.0	2.0	0.4	0.5	Point Source (Probable	1 18
-												Bouiderj Potrt Source (Probeble	
D47	41.5727938	61.7330514	438885.9	4602605.4	2178552.0	695384.3	15,5	12.1	1.3	1.0	0,5	Boulderj	
648	41.5726638	-81.7321062	438964.4	4602590.1	2178611.3	695338.5	35.8	12.9	1.2	0.9	0.7	Point Source (Probable	1.00
									-	1000		Bouider) Low Reflectivity Patch (Possible	
C49	41.5726909	-81.7312521	439035.8	4602592.5	2178945.5	695350.5	15.3	49.9	2.8	1.2	0.3	Slag	3 88
C50	41.5719909	-01.7311054	439040.7	4602514,7	2170865.0	695093.0	15.2	15.6	4.4	2.2	- +:	Loss Reflectivity Patch (Possible	
C51	10.0263555	-81.7305695	439091.8	4602488.8	2179035.2	695013.4	15.2	13.2	19	0.5	0.3	Stag  Lineer Contact	
C52	41.5702956	-81.7505075	439095.6	4602326.1	2179056.9	594479.6	15.5	155.5	3.6	0.5	0.0	Linear Contact	
C53		-81.7300963		4602327.5	2179169.4	694486.3	15.3	135.3	3.6	0.6	+ ·	Linear Contact	+
C54		-81.7300183	10000000000	4602270.4	2179173.2	694298.9		185.0	13.8	6.7	+	Unknown Contact Low Reflectivity Patch (Possible	+
CSS	41.5711445	-81.7291570	439209.0	4602419.4	2179423.7	694792.1	15.3	16.5	4.0	1.7	- #0)	Shag)	15
C56	41.5711069	-61.7291492	439209.6	4602415.2	2179426.0	694776.4	15.5	19.9	2.5	1.6	+.8	Low Reflectivity Patch (Possible	(+)
-												Slag) Low Reflectivity Patch (Possible	1 CS 7 CS
57	41.5711870	-81.7291295	439211.3	4802424.1	2179433.2	894807.6	15.5	11.3	1.7	2.5		Slag)	12
CSE	41.5710575	-81.7290973	439213.9	4602409.6	2179640.3	694760.5	15.3	32.6	2.1	1.7		Low Reflectivity Patch (Possible	
-									-	-	003	Slag) Line Reflectivity Patch (Rossible)	0.5
C59	41.5712076	-81.7290676	439216.5	4603426.3	2170448.0	694815.3	15.3	6.8	6.1	3.6	- 595	Loss Reflectivity Patch (Possible) Slag	(3)
090	41.5711559			4602420.3	2179524.7	694796.8	15,8	0.7	3.1	0.6	B.2	Linear Contact	1.1
061	41.5696265	and the second se		4603272.5	2179630.8	694513.0	15.2	115.0	4.1	0.4	0.1	Linear Contact	
C62	41.5706782		439271.0	4602367.1	2179630.5 2179657.8	694624.0 694122.8	15.2	31.8	4.2	1.2	D.4 D.3	Lineer Contact Linear Contact	6.692
064				4602255.4	2179657.0	694258.0	15.2	125.6	1.5	0.5	0.1	Linear Contact	+
065	110000000	-81.7282603		4603359.8	2179670.8	694600.9	15.2	32.3	3.4	1.0	1.5	Low Reflectivity Patch (Possible	e 😳
CGS		2010 A. 10		4602270.8	2179679.9	694302.7	15.2	109.4	1.9	0.5		Slagi Linear Contact	-
C65	41.5696118	-81.7282402 -01.7202310	439294.2	4602370.8	2179678.9 2179676.7	694308.7 694012.6	15.2	109.4	1.9	0.0	- 0.4	Linear Contact Linear Contact	
Cót	41.5707368			4602373.4	2179696.6	694645.0	15.2	17.9	5.2	1.5		Loss Reflectivity Patch (Possible	
	12.0101000	-21//202010	-222.00.3	Housana.4	**************************************	0.04040.0	12.2	17.9	312	1.5		Slagi	
		-81.7281394	439293.8	4602360.1	2179703.8	694602.4	15.2	27.0	8.5	3.5	+	Low Reflectivity Patch (Possible Slag)	9 SQ

	MADES C	ieographic	NADER U	TM Zona 17	NADER ONLY S	tate Plane North	scan Sonar Con			-	-	-	1.1
10	Latitude	Longitude	East(m)	North (m)	East(US servey feet)	North (US	Bathyreetry (m)	Distance from Proposed Route (m)	Length (m)	Wildth (m)	Height (m)	Description	Associated M Anomaly B
670	41.5705225	-81.7280796	439298.3	4602349.5	2179730.5	694.568.0	15.2	33.8	3.0	0.7		Low Reflectivity Patch (Possible	
671	41.5701074	-81 7280731	439302.6	4602303.4	2179737.3	694416.9	15.2	72.0	42	2.8	0.1	Sleg  Groular Costact	
672	41.5705831	-41.7280016	439304.8	4603356.2	2179797.3	6944993	15.2	24.8	2.6	21		Low Reflectivity Patch (Possiale	
173	41.5701562	-01.7279966	439304.8	4602308.3	2179744.4	694-134.8	15.2	66.1	4.2	1.8		Slag) Orcular Contact	-
674	41,5702992	-81.7279554	439310.0	4502324.7	2179760.7	694-457.0	15.2	49.8	2.5	1.6	-	Low Reflectivity Patch (Possible	-
-												Slagj Low Reflectivity Patch (Possible	
175	41.5705050	-81.7278572	455525.6	4602525.2	2179782.1	694499.3	15.2	45.1	5.0	1.5	1.8	Slag)	
C76	41.5702668	-81.7278261	4999399.1	4602323.0	2175750.7	694475.5	15.2	45.5	4.2	1.		Low Reflectivity Patch (Possible Sleg)	
(77	41,5723950	-81.7277941	439323.8	4602557.2	2179792.6	695251.0	15.2	159.9	2.8	1.6	14	Low Reflectivity Patch (Possible Short	
(78	41.5691421	-81.7270113	439386.0	4602255.5	2180017.3	694067.7	15.1	125-3	3.3	0.4	0.0	Slag) Linear Contact	+
C79 C80	41.5694292 41.5719450	-81.7267636 -81.7264907	439407.0 439432.0	4602233.9 4602506.4	2180063.9 2180150.7	695090.2	15.1	31.6	1.8	1.1		Groular Contact Groular Contact	
C81		-81 7263764	430441.5	4603498.4	2180382.2	695064.7	15.3	166.1	7.2	41		Low Reflectivity Patch (Possible	
C82		-01.7263525	439442.7	4603430.9	2180391.3	694777.5	15.3	90.3	3.0	0.6	0.1	Stag Linear Contact	M213. M2
(85	41.5717858		439451.2	4602408.5	2180214.5	695032.7	15.5	162.2	9.1	1.5		Low Reflectivity Patch (Possible	M82
						1011173 3					24	Sing Point Source (Probable	
C84	41.5707443	-81.7261001	435463.5	4602372.8	2180261.4	694653.7	15.2	67.2	2.8	1.8	0.6	Boulder)	
(85	41.5714122	-81.7260088	489471.7	4602446.9	2180284.3	694897.2	15.2	135.9	13.6	4.2	24	Low Reflectivity Patch (Possible Slag)	M215
CB6	41.5714945	-81.7259543	429475.5	4602456.0	2180298.9	694927.4	15.2	146.1	6.7	4.9	1.5	Low Reflectivity Patch (Possiale Slag)	N216
CR7	41.5709615	-81.7259081	639679.7	4602396.8	2180313.3	694733.3	15.2	95.1	10.1	0.5	0.1	Linear Contact	N/112
C80	41.5705741	-41.7254051	438521.3	4902353.4	2380452.2	694593.3	15.2	78.5	9.5	0.5	0.2	Lineer Contact Low Reflectivity Patch (Possible	
C89	41.5702816	41.7252589	439533.2	4602320.8	2180493.1	694487.1	15.1	55.0	11.2	4.0	1.00	Slag	
C90	41.5704508	-81.7251787	439540.0	4602339.5	2180514.5	694 549.0	15.1	75.6	15.0	5.1	- 14	Low Reflectivity Patch (Possible Slag)	1.4
(91	41.5703843	-81.7251217	499544.7	4602332.1	2180530.3	694524.9	15.1	71.5	4.9	11		Low Reflectivity Petch (Possible	1.245
C92	41.5701708	-81.7245087	439595.6	4602307.9	2180696.7	696468.4	15.0	75.2	13.4	2.5	1	Slag Low Reflectivity Patch (Possible	1.12.1
			ing and a second second			10	2 	2	-	-		Slag Low Beflectivity Patch (Possible	
C93	41.5697446	-81.7244667	439598.7	4602260.5	2180711.6	694293.4	16.P	35.5	6.1	2.5	0.6	Slag	્ર
C94	41.5695610	-81.7244551	439599.5	4002240.3	2180715.4	694226.5	14.9	18.1	6.2	2.8	94	Low Reflectivity Patch (Possible Slag)	1.1
(95	41,5692934	-81 7244120	439601.7	4602077.3	2180731.9	603691.9	13.1	125.0	15	14	0.6	Point Source (Probable	1.445
0.96		-81 7243582	439606.1	4602063.5	2180747.0	693647.0	15.1	132.9	5.4	0.5	0.1	Boulder) Linear Contact	
697		41,7242984	439611.1	4602059.6	2180768.5	693634.5	15.1	133.8	4.9	0.5	0.2	Linear Contect	
C98	41.5691417	-81.7240365 -81.7239699	439632.9	4602064.3 4602193.4	2180835.0 2180845.5	693651.1 694074.9	15.1	3.3	2.2	0.4	0.1	Linear Contact Linear Contact	
C100 C101	41.5676910	-81.7270113	439386.0	4602185.5	2180017.8	694067.7 693546.9	15.1	125.3	8.5	0.9	0.4	Linear Cantact	-
CLOD	41.5694327	-81.7287905	439659.6	4602225.5	2180914.2	694181.5	15.0	34.6	2.6	2.5	0.3	Linear Contact Low Reflectivity Patch (Possible	MISS
CLOB	41.5679436	-81.7296402	439666.0	4602059.8	2100943.6	693638.1	15.0	106.9	4.2	0.3		Slag  Linear Contact	
CLD4	41,5691001	-81 7235985	439570.6	4602197.4	2180951.0	694089.8	14.9	15.4	4.9	3.2	14	Low Reflectivity Patch (Possible)	
-						Second and						Slag  Point Source (Probable	
cité	41,069,2913	-81.7235862	439671.7	4602209.7	2180954,0	694130.3	14.9	26.7	2.8	0.9	0.7	Soulder)	
C106	41.5692118	-81.7284997	439678.9	4602200.8	2180977.9	694101.6	14.9	22.5	1.8	1.0	0.5	Point Source (Probable Boulder)	1.00
CL87	41.5691907	-81.7234616	439682.0	4602185.1	2180988.5	694083.1	14.9	19.0	8.8	21	0.3	Low Reflectivity Patch (Possible Stud	(e)
CLDB	41.5688718	-81.72333951	499992.2	4602163.0	2181023-8	693978.1	15.0	4.1	4.0	0.5	0.1	Stag! Linear Cantaut	
C1.09	41.5694729	-41.7252421	439700.6	4602229.6	2181047.6	694197.4	14.9	58.2	2.1	1.0	0.2	Point Source (Probable Boulder)	
C1 10	41.5684564	-81.7231098	499700.7	4602136.7	2101007.3	693827.3	15.0	35.4	3.1	0.7	0.1	Linear Contact	- (+)
CL 13	41.5689415	-01.7234.011	439715.8	4602170.5	2183087.9	694036.1	15.0	12.1	2.3	0.4	0.3	Linear Contact Low Reflectivity Patch (Possible	-
CI 12	41.5675506	-81.7224855	433762.0	4602036.6	2181261.4	693501.7	14.8	97.6	4.6	8.0	12	Slag)	
CL13	41.5685835	-81.7224107	439769.2	4602141.4	2181277.6	693911.8	15.0	14.8	5.8	17	- *	Low Reflectivity Patch (Possible Slag)	
C134	41.5687263	-81.7223625	489773.2	4602146.1	2181290.7	698927.5	15.0	20.9	3.8	11		Low Reflectivity Petch (Possisle	1.042
CL 15		-81.7222909	439778.6	4483877.0	2181312.3	600301.0		25.0		0.7	1.0	Steg Point Source (Prohable	
			Sec. Hills	4602077.0	101516-5	693701.0	14.8	35.8	2.8	47		Boukler) Low Reflectivity Patch (Possible)	
CL 16	41.5685281	-81.7222826	639779.7	4602134.1	2181313.2	693855.4	14.9	4.0	4.6	1.9	8	Slag]	1 - AN
CL 17	41.5667006	41.7222544	439782.2	4602343.2	2183330.3	693918.4	14.9	22.7	7.4	1.5	0.2	Low Reflectivity Patch (Possible Slag)	1.2
CL 18	41.5682772	-81 7222051	439785.9	4602096.2	2181335.2	693764.2	14.8	16.5	3.6	1.5	0.3	Low Reflectivity Patch (Possible	
							1000	14000	0.00		-	Slag  Low Reflectivity Patch (Possible	-
CL 19	1.C. A. (2015)	-81.7221252 -81.7220727	499792.7	4602105.0	2181356.8	693793.5	14.9	5.6	9.1	3.4		Slag]	-
CL28		-81.7220727	439797.0	4602185.1	2181371.5 2181370.5	693761.5 693894.0	14.8	23.4	4.0	2.5	0.2	Linear Contact Low Reflectivity Patch (Possible	M156
C121							1000				10	Slag) Low Reflectivity Patch (Possible	WT90
C1 22	41.5696837	-81.7219585	439907.0	4602253.6	2101390.1	694276.2	14.9	129.9	12.2	10.8	10	Slagj	1
C1 23	41.5603559	-01.7219340	439838.5	4002305.0	2101400.9	693797.2	14.8	3.0	1.2	1.1	10	Low Reflectivity Patch (Possible Slag)	3 to 2
C125	42.5654571	-61.7217073	433527.6	4662136.2	2181470.8	693832.4	14.8	21.5	1.7	1.0	1.0	Point Source (Probable	M211
CL25		41.7215501	419038.9	4001856.2	2181520.2	693117.8		163.3	2.8	1.2	11	Boulder) Rectangular Contact	mart
CL 27	1-01-01-01-01-01-01-01-01-01-01-01-01-01	-81 7215392		4602137.9	2181536.8	693838.T	14.8	29.7	1.5	1.5	0.5	Point Source (Probable	-
							2,802				1000	Boulder) Point Source (Probable	-
C128	41.5678129	-81.7215361	439841.3	4602044.1	2181519.8	693396.7	14.7	34.9	1.6	1.0	0.5	Boulder)	-
C129	41.5682537	-81.7212608	439964.6	4602092.9	2181599.7	693758.0	14.8	19.1	1.3	0.4	0.5	Point Source (Probable Boulder)	M157
C1.34	41.5677509	-81.7207627	439905.7	4602096.7	2181731.6	693576.0	14.8	9.8	3.7	0.5	0.1	Linear Contact	
		-01.7201661	439953.9	4801854.9	2181900.2	692982.1	14.8	144.9	8.4	2.0		Low Reflectivity Patch (Possible)	

7.8	NADER G	ieographic	NADER U	TM Zona 17	NADER ONLY S	tate Plane North	scan Senar Cen	Distance from	·				÷
10	Latitude	Longitude	East(m)	North (m)	East (US servey feet)	North (US sarvey feet)	Bathynetry (m)	Proposed Route (m)	(m)	(m)	(vn)	Description	Associated Ma Anomaly ID
C132	41.5659769	-81.7201452	439955.5	4603839.3	2181906.4	692931.1	14.6	157.7	8.2	5.7		Low Reflectivity Patch (Possible Slag)	0 1. 28% (
CL33	41.5686979	-81.7201278	439959.5	4602343.4	2183902.3	693922.6	14.8	107.8	2.4	1.2	1.0	Reitangalar Contact Point Source (Prolable	() ()#1) ()
C134	41.5676314	-41.7200550	439954.6	4602023.0	2183935.6	693534.2	14.8	7.0	2.0	0.6	0.5	Boulder)	
CL35	41.5675987	-81.7197246	419992.2	4602030.2	2182015.8	693559.5	14.9	25.8	17	2.1		Low Reflectivity Patch (Possible Sbg]	1 . C.
C136	41.5675313	-81.7196271	440000.2	4602011.5	2182043-1	603-898.7	14.8	14.4	2.1	1.1	0.6	Point Source (Probable Soulder)	
CL37	41.5667830	-81 7196 209	440000.0	4601528.5	2182647.2	693226.1	14.8	58.2	3.7	0.9		Linear Contact	M152
CLSE	41.5676191	-81.7195825	440004.0	4602021.8	2382055.0	693530.8	14.8	24.7	6.5	4.5		Low Reflectivity Patch (Possible Sleg)	M158
C139	41.9674205	-81.7195334	440007.9	4601599.2	2182869.1	693458.6	14.8	7.4	2.5	1.7	-	Low Reflectivity Patch (Possible Slag)	1.1
	41,5689559	-81.7194864	440013.2	4602169.6	2182076.9	694018.2 693264.9	14.8	158.7	3.6	2.4	0.5	Linear Contact Linear Contact	+
C142	41.3684296	-81.7191049	440344.5	4602130.9	2182183.0	693827.8	14.9	122.8	3.5	0.4		Linear Contact	+
C143 C144	41.5673790 43.5660761	-41.7189203	640059.0 440506.5	4601996.0	2152237.0	693454.6 692971.7	14.0 14.0	27.8	3.4	0.6	0.1	Linear Contact Linear Contact	
	41.5665241	-01.7181643	440112.9	4601595.5	2182419.3	693135.1	\$4.0	28.9	3.0	0.3	0.3	Linear Contact	
C2.46	41.5665197	-81.7181509	440122.5	4603858.2	2182450.3	653133.8	14.8	24.8	1.0	0.8	0.6	Point Source (Probable Boulder)	1.4
CL47 CL48	41.5643573	-81.7171889	440200.5 440408.7	4601658.6	2162720.6	692351.9	14.5	195.6	5.7	0.8	0.1	Linear Contect	
CL48 CL49	41.5663368	-81.7147141 -81.7159193	440405.0	4601877.9 4601874.9	2183391.3 2183608.8	693083.4 693077.4	14.5	97.5	5.7	0.5		Linear Contact Linear Contact	
CL 50	41.5642624	-81.7135349	440905.1	4603646.4	2189720.8	692322.6	14.2	59.1	4.0	0.9	0.3	Point Source (Prohable Boulder)	1.55
CL 54	41.5654100	-81.7132571	440529.3	4901771.6	2183799.1	692741.5	14.3	63.7	2.9	0.6	0.1	Linear Contact	S - 194 1
C152	41.5654492	-81.7120650	440528.0	4601775.2	2184119.2	602758.7	14.4	115.4	10.6	3.1	14	Low Reflectivity Patch (Possible Slag)	1.04
C153	41.5652728	-81.7120203	440632.3	4601755.5	2184152.0	692994.4	14.4	100.0	1.6	1.5	0.9	Point Source (Probable	1.00
C154		-81.7119548	440637.6	4601735.8	2184150.5	692630.1	14.4	85.4	14	0.8	0.7	Soulder) Point Source (Probable	1.240
C155	41.5622040	-81 7115199	440687.9	4503434.4	2164333.8	691578.1	14.4	170.5	2.4	0.6	0.2	(Soulder) Linear Contact	
C156	41.5636074	-81.7112257	440697.1	4601570.1	2384354.9	692099.7	14.5	90.1	3.8	0.3		Linear Contact	
C1.58	41.5645572 41.5621913	-81.7111407	440725.0	4603675.5 4603412.6	2184375.0 2184471.7	692436.0 691574.7	14.5	65.7 151.5	8.0 17.8	0.5	0.1	Linear Contact Linear Contact	
	41.5633610	-81.7104062	440765.2	4601542.2	2184580.0	692001.9	14.4	21.2	4.9	0.5	0.1	Linear Contact	
C160 C161	41.5632394		440774.6	4601528.6	2184611.6 2184643.2	691957.9	16.4	28.5	5.2	0.4	0.1	Linear Contact Linear Contact	
C162		-81.7101760	440785.1	4601529.0	2104640.4	692287.4	14.5	64.1	13	4.0	0.5	Low Reflectivity Patch (Possible)	
					-	-			-			Slag Point Source (Probable	-
C1.63		-61.7101548	440785.4	4003565.8	2184646.0	692093.9	14.4	15.5	12	11	0.6	Soulder) Low Reflectnoty Patch (Possible	
C1.64		-81.7101038	440791.3	4601855.3	2184655.4	692374.6	14.5	90.8	12.4	6.4	1.4	Sing) Low Reflectivity Patch (Possible)	
CL 65	41.5645763	-81.7100824	440793.3	4603676.9	2184664.6	692445.6	14.5	110.1	4.8	2.8	100	Sing) Low Bellectivity Patch (Possible	
C1 66	41.5647895	-81.7099927	440801.0	4601700.5	2184668.4	692523.5	14.5	134.6	10.4	4.3	10	Shgl	5. e 1
C167	41.5620329	and the second second		4603394.4	2104783.8	691519.4	14.4	128.5	1.8	1.6	0.4	Point Source (Probable Boulder)	N144
	41.5635947 41.5630941	manhana amandalah ara-	440832.1	4601567.6	2104066.3	692029.1 691903.6	14.4	33.7 6.3	2.7 3.0	0.5	0.1	Linear Contact Linear Contact	5 100
	41.5625297		440875.4	4003449.0	2154947.1	691702.4	14.4	40.6	7.2	0.4		Linear Contact	
	41.5617026		440575.3	4601557.1	2164555.2	691401.0	14.5	128.3	7.2	1.0		Linear Contact	0.000
	41.5627621 41.5628261		440900.9	4603474.6 4603483.8	2185025.1 2185365.2	691787.8 691812.3	14.4	13.9	7.5	0.6	0.2	Linear Contect Linear Contect	
C1,74	41.5634166	-81.7078989	440974.3	4601546.6	2185265.9	692028.4	14.4	84.9	4.0	0.6	10	Linear Contect	(e)
	41,5609433	10.000	441081.6	4601271.2	2185633.6	691130.5	14.1	108.0	4.4	0.5	0.2	Linear Contact Point Source (Probable	
C175	41.5607966		441117.6	4401254.6	2185753.6	691078.1	16.1	99.9	11	0.8	0.5	Boukler)	190
22.2.2	41.5610431	-81.7058256	441152.6	4603283.7	2185841.2 2185866.0	691168.9 691172.4	14.0	62.8 58.3	1.R 4.D	0.4	0.1	Linear Contact Linear Contact	-
C1.79	41.3611467	-81.7055942	441164.4	4601283.1	2185904.1	691207.1	14.0	43.4	2.5	0.7	0.0	Point Source (Probable Soulder)	1.000
C1.85	41.5605036	-81.7047237	441236.4	4601221.1	2188344.5	690975.0	14.0	71.0	1.4	0.9	0.6	Point Source (Probable	
							100000	1445				Boulderi Point Source (Probable	1.050
1005		-81,7046716	Contraction of the	4603215.5	2186158.9	690857.0	13.9	75.8	2.2	11	0.4	Bouldert Point Source (Profeable	1.1252
C7.85	41.5600491	-81.7045812	441247.9	4601170.5	2186185.0	690809.7	13.9	109.5	1.1	0.7	0.5	Boulders	1.253
CLES	41.5597743	-81.7044097	441261.9	4901139.9	2186332.9	690710.0	13.9	129.4	0.9	0.6	0.5	Point Sounce (Proloable Boulder)	1.20
CL 04	41.5692965	-61.7036724	441324.4	4601264.0	2156430.9	691120.7	13.9	9.4	1.0	0.6	0.6	Point Source (Probable Boulder)	1.000
C1 85	41.5618126	-41.7036052	441330.9	4001365.6	2106446.2	691434.7	13.9	101.3	1.0	0.7	0.8	Lineer Contact	+
CL 86	41.5617893	-81.7035322	441335.9	4601363.0	2186466.3	691446.4	13.9	101.9	1.8	0.5	0.5	Point Source (Probable Soulder)	1.200
CL 87	41.5614265	-81 7088929	441348.2	4601322.6	2186505.6	691314.5	13.9	72.2	2.2	0.7	0.5	Point Source (Probable Soulder)	1.195
C1.88	41.5614252	-81.7033161	441354.6	4601322.4	2186536.6	691314.3	13.8	75.2	1.6	0.9	0.6	Point Source (Probable Boulder)	2.42
C1 89	41.5592953	-81.7033146	441352.8	4601082.7	2186534.2	690527.6	13.6	134.8	1.1	0.7	0.6	Point Seurce (Probable Boukler)	0.000
		-81 7006744		4601259.8	2187251.4	691121.2	13.3	137.9	2.3	0.4	0.1	Linear Contact	
		-41 7006013		4600977.6	2387362.0	690196.7	13.2	104.2	6.D	0.5		Linear Contact Point Source (Probable	S 0.43
		-81.6991500		4803059.9	2187674.6	690472.3	13.2	14.9	0.7	0.4	0.6	Boulder) Point Source (Probable	15.5
		-81.6969471		4601051.8	2187750.5	690446.6	15.5	16.0	1.2	0.7	0.6	Boulder) Point Source (Probable	1.5
		-81.6985757		4603066.2	2187888.5	690496.8	13.4	52.0	1.4	0.9	0.6	(Soulder)	1.51
1.347		-81.6979033 -81.6971195		4600567,4 4600753,5	2188038.5	690174.7 689499.7	13.5	15.4	1.0	0.7	0.5	Point Source (Probable Bouilder)	
1011		-81.6971195	1000 C	4600753.5	2188255.5	689499.7	19.2	132.7	2.5	1.4	0.2	Linear Contact Point Source (Prolatile	M143
1000												Boukler)	
												Point Source (Probable	

42	MADES 6	ieographic	MADER U	TM Zone 37	NADER ONE S	tate Plane North	scan Senar Cen	Distance from				<i>1</i>	18
10	Lattade	Longitude	East(m)	North (m)	East(US servey firet)	North (US sarvey feet)	Bathyreetry (m)	Proposed Route (m)	(m)	(m)	Height (m)	Description	Associated Ma Anomaly ID
C1 59	41.5579418	-81.6960717	441955.6	4600930.8	2186530.8	690363.2	13.4	27.2	1.2	0.6	0.6	Point Source (Probable Bouilder)	
(200	41.5596616	-81.6959293	441968.1	4403230.6	2188557.4	690325.9	13.5	108.0	3.6	0.7	0.7	Linear Contact	
C214	45.5586658	-81.6958023	441978.7	8601011.0	2188592.1	690327.7	13.5	108.5	8.4	0.6	0.4	Linear Contain	
C202	41.5566203	-01.6049755	482046.0	4800805.6	2188824.6	609657.4	13.1	37.9	7.2	1.7	0.2	Low Reflectivity Patch (Possible) Slag)	1.00
C200	41.5570100	-01.6947107	442068.2	4600629.3	2100096.4	609736.6	13.2	6.2	4.6	0.4		Linear Contact	
C284	41.5558011	-81.6946811	442059.6	4600682.2	2188908.6	689285.B	13.2	125.2	1.0	0.7	0.5	Point Source (Probable Soulder)	
C215	41.5562501	-81.8945018	442085.0	4600741.9	2188956.2	689450.8	13.1	74.3	6.6	0.4	0.2	Linear Contact	
C206	41,5578692	-81.6925614	442248.0	4600058.2	2385482.4	609972.8	13.5	141.7	4.1	0.4	0.1	Linear Contect	
C257	41.5555337	-81.6921.853	442277.5	4600660.8	2189592.6	689195.7	13.1	50.9	1.1	0.6	0.5	Point Source (Probable Soulder)	
208	45.5571151	-81.6921246	442284.0	4600836.4	2189603.9	689772.0 689508.7	13.8	105.3 50.9	3.9	0.3	. *	Linear Contact	
C218	41.5569012 41.5569952	-81.6919940 -81.6919808	442294.8 442295.9	4600768.1 4600623.0	2189643.7 2189643.6	689728.7	18.2	99.5	4.6	0.4		Linear Contact Linear Contact	
C211	41.5572323	-81.6919185	642301.3	4600645.3	2129650.9	689815.2	13.2	125.0	8.2	0.2	1.	Linear Contact	+
C212	41.5562366	-81 6919059	662305.4	4600738.5	2169666.7	689451.7	13.2	28.5	4.1	0.5	0.2	Linear Contact	1.4
C213	41.3570168	-81.6918770	442304.5	4600625.3	2169672.0	609736.8	13.2	105.7	2.6	0.5	0.5	Linear Contact	+
C214 C215	41.5572423 41.5555906	-81.6917529 -81.6890398	442315.1 442464.0	4600650.3	2160705.2 2190207.2	609019.3 609200.2	13.3	132.7	4.1	0.5	0.1	Linear Contact Linear Contact	
C215	41.5555181	-81.6698221	442474.6	4600657.5	2190230.4	689196.0	12.9	42.5	13.5	9.4		Linear Contact	
(217	41.5552677	-81.6897696	443478.7	4600625.7	2190254.6	689104.9	12.9	20.2	14.5	. 2.4	0.7	Low Reflectivity Petch (Possible Slag)	1.20
C218	41.5536396	-81.6895995	442491.5	4600448.8	2150306.7	688512.1	12.8	131.3	1.1	0.5	0.5	Point Source (Probable Bouider)	1
C219	41.5562301	-81.6895567	462497.8	4606736.4	2190309.5	689456.1	12.9	\$22.4	7.8	0.8	0.1	Linear Contain	S-10431-
(222	41.5543942	-81.6890621	442536.9	4600532.3	2190451.2	688788.4	12.8	36.3	2.6	0.4	-	Linear Contact	
C221					2190536.4	689515.7	1000	1.0.0.0	4.5	0.4	0.3	Linear Contact Point Source (Probable	-
C222	41.5532781	-81.6685019	442599.4	4606407.8	2190663.1	600353.7	12.6	114.4	1.0	0.7	0.6	Boulder)	
C223	41.5526391	-\$1.6867105	442731.5	4000535.0	2191100.6	600154.9	12.5	112.6	IL9	0.7	0,2	Linear Contact	0.00
C224	41,5541710	-81.6866219	442740.2	4800505.9	2101110.8	660713.3	12.7	40.0	7.4	0.4	0.1	Linear Contact	
C225	41.5554069	-81.6864658	442752.6	4600420.9	2151165.1	688435.5	12.6	28.1	1.1	0.7	0.5	Poiet Source (Probable Boulder)	
\$226	41,35555586	-81.6865724	442762.1	4600637.5	2151184.1	689146.6	12.7	165.6	19.6	0.9	0.2	Linear Contact	M75
can	45.5517972	-81.6859713	442792.4	4600235.2	2191306.2	687828.2		170.6	1.8	0.9	0.5	Poriet Source (Probable	1 2 2
	AL MALIAN	-91.00091123	anti-base		1191900-2			87.579			4.5	Boukler)	
C228	41.5541570	-81.6859333	642797.7	4600505.0	2191308.3	689713.6	12.7	67.3	1.5	1.7	0.6	Point Source (Protable Boukler)	(*).
C229	41.5541516	-01.6050827	442901.9	4600503.2	2191332.2	688708.1	12.7	67.8	1.5	1.5	0.6	Point Source (Probable Boulder)	140
C230	41.5527375	-01 6050030	442007.3	4000346.2	2101348.6	6001931	12.6	66.5	6.0	0.3		Linear Contact	-
C251	41.5539001	41.6857192	442815.3	4800475.2	2151367.8	608616.9	12.7	43.5	2.1	0.8	0.7	Point Source (Probable	
									-			Boulder) Point Source (Probable	
(232	41.5538888	-81.6856907 -81.6855265	442817.7	4600473.9	2151875.6	688612.9 688675.6	12.7	50.0 73.2	15	0.8	0.6	Baulder)	1.45
0234	41.5540718	-81.66000.000	442836.6	4800492.8	2151420.0 2151436.8	688679.9	12.7	76.8	3.6	0.2	0.1	Lineer Contect Linear Contact	-
(235	41.5549087	-81.6850973	442968.0	4600586.7	2191534.6	688985.0		178.0	4.8	0.5	0.2	Linear Contact	-
G36	41.5537789	-81.6848326	442889.1	4600461.1	2191610.9	688575.0	12.6	73.8	2.6	0.5	0.1	Linear Contact	5 S.+ S
C237	41.5588787	-91.6846559	442903.5	4600416.6	2193660.6	688429.6	12.6	41.9	2.9	0.5	0.1	Linear Contact	
(238	41.5539354	-81.6045677 -01.6045295	442930.8	4600405.1	2193695.5	689392.3 689632.8	12.5	35.4	4.5	0.5	0.2	Linear Contact Linear Contact	
C240	41.5545156	-01.6043472	442930.3	4000544.0	2191741.1	600052.0		366.9	2.5	0.5	0.1	Linear Contact	-
C241	41.5540052		442333.1	4600485.9	2191753.6	600658.R	12.8	116.9	4.0	0.4		Linear Contact	
C242	41.3539578	-51.6841979	442942.2	4500480.6	2151784.0	658641.B	12.5	116.7	2.3	0.5	0.0	Linear Contact	0 0.401
C243	41.5508531	-81.6838111	442971.7	4600135-6	2191900.4	687511.6		169.8	13.2	11.9	1.8	Circular Contact (Probable	M102
(244	41.5521890	-81.6837990	442973.9	4600284.0	2191899-2	687998.4	12.4	39.4	2.4	0.9	0.5	Dredge Spoil) Point Source (Probable Boukler)	
(245	41 5564578	-81.6964873	441919.8	4600766.3	2188412.1	669521.5	13.2	133.9	16.7		1.4	Groular Contact (Probable	1.042
1244	41 5531969	-01 6016536	442995.3	4400985.7	2101963.9	600365.2	12.4	62.5	2.4	0.5	0.3	Oredge Spoil)	
	41.5534321	-81.6834705	449002.6	4600443.9	2101904.2	600525.0	12.5	114.2	4.5	0.8	0.8	Linear Contact Linear Contact	-
C248	41.5539318	and a local device the second second	663013.5	4600477.1	2102018.2	600534.5	12.5	140.5	2.8	0.4	0.1	Linear Contact	-
C245	41,5541702	-81.6855227	449015.4	4600505.6	2153832.8	608721.4		172.5	1.5	11	0.5	Point Source (Probable	1.00
		5.18.205		10000000				1. 20000			**C	Boulder)	
C250 C251	41.5524949	-81.6851299 -81.6851028	449021.6	4600317.5 4600465.7	2192058.9 2192064.1	600111.3 600598.2	12.4	15.2	6.D 3.D	0.2	-	Linear Contect Linear Contect	-
		-81.6829157		4606208.7							0.5	Circular Contact (Probable	444.3
0.82		1000000000	100000000	-044944444	2192343.5	687729.4	12.2	76.3	5.6	5.3	0.5	Oredge Spoil) Groular Contact (Probable	ML2
(253	41.5514725	-81.6828723	443050.6	4600203.8	2192155.3	687739.7	12.3	71.8	4.6	51	0.5	Ovedge Spoil)	1.45
	41 5504014	-81.6827315	449051.4	4600093.7	2192197.2	687378.9	12.5	162.6	14.5	15.8	LD	Groular Contact (Probable Oredge Spoil)	12:45
C254				4600474.9	2192206.0	600630.5	100	174.8	1.0	0.9	0.5	Point Source (Probable Boulder)	1.25
C254		-01.6026490	441071.5	4000474.3	100000000000	2010/01/01/07						Orcular Contect (Probable	M140
	41.5539100	-81.6825490 -81.6825446	100000	4600119-0	2352247.5	687464.8	12.4	132.3	17.1	14.3	11	Oredge Spoil)	
C255	43.5539140 43.5597157		443077.2		2352247.5 2152256.5	687464.8 687590.6	12.4 12.3	132.3 91.5	17.1	14.6	0.8	Dredge Spoll Orcular Contact (Probable Dredge Spoll	ML3
C255 C256 C257	41.5539100 41.5507157 41.5510998	-81.6825446	443077.2 443092.8	4600119.6							-		M13
C255 C256 C257 C259	41.5539000 41.5507157 41.5510998 41.5511747	-81.6825446 -81.6823615	443077.2 443092.8 443096.5	4600119-0	2192296.5	687590.6	12.3	91.5	15.9	14.6	0.8	Orcular Contact (Probable Dredge Spoil) Orcular Contact (Probable	0.5%
C255 C255 C257 C259 C259	41.3539140 41.35071.57 41.551.0598 45.3511747 41.3524078	-81.6825446 -81.6823615 -81.6823186	449077.2 449092.8 449096.5 449101.9	4600119.6 4600157.6 4600170.4 4600907.2	2192296.5 2192907.8	687590.6 687632.6	12.3 12.4	91.5 78.6	15.9 14.0	14.6 13.7	0.8	Orcular Contect (Probable Dredge Spoil) Orcular Contect (Probable Dredge Spoil)	
C255 C255 C257 C259 C259 C259 C260	41 3539100 41 3507137 41 3510598 41 3511747 41 3524078 41 3501032	-81.6825446 -81.6823615 -81.6823186 -81.6822663 -81.6828880	443077.3 443092.8 443096.5 443031.9 443031.5	4600129.6 4600157.6 46000270.4 4600007.2	2192296.5 2192307.8 2192317.9	687590.6 687632.6 689082.0 687243.3	12.3 12.4 12.4	91.5 78.6 49.5	15.9 14.0 1.5	14.6 13.7 1.5 1.6	0.8 0.8 0.3	Orouler Context (Probable Dredge Spoil) Orouler Context (Probable Dredge Spoil) Grouler Context (Probable Tirre) Linear Context Point Source (Probable	-
C255 C255 C257 C258 C258 C258	41 5539140 41 5507157 41 5510998 45 5511747 41 5524078 41 5524078 41 5524078 41 5524078	41.6025446 41.6023615 41.6023186 41.6023186 41.6022063 41.602063 41.6020519	443077.2 443092.8 443096.5 443036.9 443031.9 443031.5 443135.2	4600139.0 4600157.6 4600370.4 4600007.2 4600003.1 46000273.0	2192296.5 2192967.8 2192937.9 2192337.9 2393439.4 2193432.4	687590.6 687632.6 688082.0 687243.3 687971.7	12.3 12.4 12.4	91.5 78.6 49.5 564.9 30.4	15.9 14.0 1.5 3.8 1.9	14.6 13.7 1.5 1.6 0.7	0.8 0.8 0.3 0.3 0.5	Oroulier Context (Probable Dredge Spoil) Orouler Context (Probable Dredge Spoil) Orouler Context (Probable Tire) Unear Context Point Source (Probable Boulder)	-
C255 C258 C259 C259 C259 C259 C260 C261	41 5539140 41 5519598 41 5519598 41 5519598 41 5524078 41 5524078 41 5524078 41 5524078 41 5524078	41.6025446 41.6023615 41.6023615 41.6023106 41.6022063 41.602063 41.6020519 41.6010519	443077.2 443092.8 443096.5 443096.5 443001.9 443021.5 443023.5 443023.2	4600135.6 4600157.6 46000379.4 46000057.2 4600053.1 46000373.0 4600434.3	2192296.5 2192367.8 2192367.8 2192317.9 2393439.4 2193439.4 2193439.4	687590.6 687632.6 688082.0 687243.3 687971.7 688594.7	123 124 124 125	91.5 78.6 43.5 564.9 30.4 187.8	15.9 14.0 1.5 3.8 1.9 1.5	14.6 13.7 1.5 1.6 0.7 0.7	0.8 0.8 0.3 0.3 0.5	Oroular Contact (Probable Dredge Spoil) Oroular Contact (Probable Dredge Spoil) Groular Contact (Probable Tire) Unear Centact Point Source (Probable Boulder) Unear Contact	-
C255 C256 C257 C259 C259 C259 C251 C251 C251 C251	41.3539000 41.35971.57 41.3510598 41.3510598 41.3524078 41.3524078 41.3524078 41.3521021 41.3525624 41.3535624	41.6525446 41.6523615 41.6523615 41.6522663 41.6522663 41.6528990 41.6518990 41.651899 41.6514695	443077.2 443092.8 443096.5 443096.5 443096.5 443096.5 443096.5 443059.5 443059.4 443059.4 443059.4	4600133.6 4600157.6 46000379.4 46000053.1 4600053.1 4600037.0 4000434.3 4800033.7	2192296.5 2192307.8 2192307.8 2192317.9 2393439.4 2193432.4 2193432.1 2193332.1 2192390.9	687599.6 687682.6 668082.0 687243.3 687243.3 687243.3 687243.3 687243.3	123 124 124 - 125 - 125 -	91.5 78.6 43.5 364.9 30.4 187.8 155.4	15.9 14.0 1.5 3.8 1.9 1.5 7.7	14.6 13.7 1.5 1.6 0.7 0.7 0.4	0.8 0.8 0.3 0.3 0.5 0.0 0.1	Orouline Contact (Photbable Dredge Spoil) Orouline Contact (Photbable Dredge Spoil) Oroular Contact (Photbable Tire) Linear Contact Point Source Photbable Goulder) Linear Contact Linear Contact	- - - MI05
	41.5539149 41.5597137 41.5510998 43.5521747 43.5524978 43.5524978 41.5524974 41.552522 41.552522 41.552522 41.552522 41.552522	41.6525446 41.6525415 41.6523415 41.6522653 41.6522653 41.6522653 41.6521519 41.6514555 41.6514555 41.6512669 41.6509326	449077.2 449092.8 449092.8 449096.5 449101.9 449101.9 449105.4 441136.2 449109.4 449109.4 449107.5	4600119.8 4600157.6 4600070.4 4600007.2 4600051.1 4600051.1 46000273.0 4600434.3 460003.7 4600020.1	2192296.5 2192307.8 2192317.9 2192317.9 2190319.4 2190313.4 2190313.1 2190313.1 2190313.1 2190305.2	687399.6 687632.6 668082.0 687243.3 687243.3 687243.3 6877471.7 687189.2 687902.0	123 124 124 125 125 124 125	91.5 78.6 49.5 364.9 30.4 187.8 155.4 19.0	15.9 14.0 1.5 3.8 1.9 8.5 7.7 1.4	14.6 13.7 1.5 1.6 0.7 0.7 0.4 0.7	0.8 0.8 0.3 0.8 0.8 0.8 0.0 0.1 0.8	Oroular Contact (Probable Dredge Spoil) Oroular Contact (Probable Dredge Spoil) Groular Contact (Probable Tire) Unear Centact Point Source (Probable Boulder) Unear Contact	-
C255 C256 C257 C256 C256 C256 C256 C256 C256 C256 C256	41.5539140 41.5510598 41.5510598 43.5511747 41.5524378 41.5524578 41.5524578 41.5524578 41.5524578 41.5524578 41.5524578 41.5524578 41.5524578 41.5524578 41.5534578 41.5534578 41.5534578 41.5534578 41.5534578 41.5534578 41.5534578 41.555478 41.5554784 41.555478 41.555478 41.555478 41.555478 41.5554784 41.555478 41.555478 41.555478 41.5554784 41.555478 41.555478 41.555478 41.5554784 41.555478 41.555478 41.5554784 41.555478 41.5554784 41.555478 41.5554784 41.555478 41.55547	41.6525446 41.6523615 41.6523136 41.6522663 41.6522663 41.6522663 41.6522653 41.6522653 41.6522653 41.652545 41.6505925 31.6505545	443077.2 443032.8 443036.5 443036.5 443103.9 443123.5 443125.1 443125.1 443207.5 443244.0	4800119.8 4600157.6 4600070.4 4600007.2 4600053.1 4600053.1 4600013.0 4600013.7 4600013.7 4600022.1	2192296.5 2192307.# 2192317.9 2192317.9 2192432.4 2192432.4 2192533.1 2192539.9 2192589.9 2192589.2	687599.6 687682.6 688082.0 687243.3 687243.3 687243.3 6872471.7 687189.2 687802.0 687802.0	123 124 124 - 125 - 124 125 126	91.5 78.6 43.5 364.9 30.4 187.8 155.4 19.0 38.7	15.9 14.0 1.5 3.8 1.9 1.5 7.7 1.4 8.7	14.6 13.7 1.5 1.6 0.7 0.4 0.7 0.5	0.8 0.8 0.3 0.3 0.8 0.0 0.1 0.8	Orouline Contract (Probable Dredge Spot) Grouler Contract (Probable Dredge Spot) Grouler Contract (Probable Dredge Spot) Dreast Contract Dreast Contract Point Source (Probable Boulder) Dreast Contract Dreast Contract Dreast Contract	- - - MI05 -
	41.5539100 41.5510598 41.5510598 41.5510598 41.5510598 41.555022 41.555024 41.555024 41.555024 41.555030 41.555030	41 6825448 41 6823415 41 6823136 41 6823136 41 682363 41 68280 41 68280 41 68280 41 682993 41 6829935 41 6899937	443077.2 443092.8 443092.8 443096.5 443096.5 443105.9 443105.2 443105.1 443105.1 443105.1 443207.5 443205.0	4600139.8 4600157.6 46000370.4 46000370.4 4600037.2 4600033.1 4600033.3 4800003.7 4800020.1 4800020.1	2192296.5 2192307.8 2192307.8 2192317.9 2192317.9 2192331.4 2192331.4 2192331.4 219233.0 2192580.9 2192580.9 2192580.0	687593.6 687582.6 689582.0 687243.3 687943.3 687951.7 687199.2 687199.2 687199.2 687190.9 68719.5	123 124 124 125 124 125 126 126	91.5 78.6 49.5 364.9 30.4 187.8 135.4 19.0 383.7 142.3	15.9 14.0 1.5 2.8 1.9 1.5 7.7 1.4 8.7 3.5	14.6 13.7 1.5 1.6 0.7 0.4 0.7 0.5 0.5 0.5	0.8 0.8 0.3 0.8 0.8 0.8 0.0 0.1 0.8	Orouler Contact (Probable Dredge Spot) Orouler Contact (Probable Dredge Spot) Grouber Contact (Probable Trues Contact Point Source (Probable Boulder) Linear Contact Point Source (Probable Boulder) Dreit Source (Probable Boulder) Linear Contact Dreit Source (Probable Boulder) Linear Contact	- - - M105
	41.5539100 41.551757 41.551747 41.551747 41.551747 41.552474 41.552474 41.5524524 41.5524524 41.553944 41.55394 41.55394 41.55394 41.5549888 41.5499888	d1 6825446 d1 6823485 d1 6823186 d1 6823186 d1 6823186 d1 682368 d1 682268 d1 6818880 d1 6818980 d1 6819926 d1 680926 d1 6809545 d1 68095645 d1 689926 d1 689926	443077.2 443092.8 443096.5 443096.5 443103.9 443103.9 443103.4 443103.4 443103.4 443203.5	4800113-8 4600157.6 460020.4 460020.4 460020.1 460020.1 460020.1 4600220.1 4600220.1 4600220.1 4600220.1	2192296.5 2192307.8 2192307.8 2192317.9 21903130.4 2190353.1 2190353.1 2190353.1 2190353.2 2190353.2 2190355.2 2190355.2 2190355.2	687590.6 687682.6 689082.0 687248.3 687971.7 687971.7 687971.7 687971.7 687971.0 687902.0 687902.0 687902.0 687902.0	12.3 12.4 12.4 12.5 12.5 12.4 12.5 12.6 12.6 12.6 12.6 12.4	91.5 78.6 49.5 264.9 30.4 195.6 19.0 38.7 142.3 152.8	15.9 14.0 1.5 3.8 1.0 8.5 7.7 1.4 8.7 3.5 2.0	14.5 13.7 1.5 1.6 0.7 0.4 0.7 0.7 0.7 0.5 0.5 1.5	0.8 0.8 0.3 0.3 0.8 0.0 0.1 0.8 0.1 0.4 -	Orouline Contact (Roobable Deedge Spoll) Orouline Contact (Roobable Deedge Spoll) Orouline Contact (Roobable Trie) Direser Contact Point Source (Roobable Goulder) Lineer Contact Deat Source (Roobable Goulder) Lineer Contact Direser Contact Lineer Contact Reich goulder)	- - - MI05 -
	41.5539100 41.551757 41.551747 41.551747 41.551747 41.552474 41.552474 41.5524524 41.5524524 41.553944 41.55394 41.55394 41.55394 41.5549888 41.5499888	41 6825448 41 6823415 41 6823136 41 6823136 41 682363 41 68280 41 68280 41 68280 41 682993 41 6829935 41 6899937	443077.2 443092.8 443096.5 443096.5 443103.9 443103.9 443103.4 443103.4 443103.4 443203.5	4600139.8 4600157.6 46000370.4 46000370.4 4600037.2 4600033.1 4600033.3 4800003.7 4800020.1 4800020.1	2192296.5 2192307.8 2192307.8 2192317.9 2192317.9 2192331.4 2192331.4 2192331.4 219233.0 2192580.9 2192580.9 2192580.0	687593.6 687582.6 689582.0 687243.3 687943.3 687951.7 687199.2 687199.2 687199.2 687190.9 68719.5	123 124 124 125 124 125 126 126	91.5 78.6 49.5 364.9 30.4 187.8 135.4 19.0 383.7 142.3	15.9 14.0 1.5 2.8 1.9 1.5 7.7 1.4 8.7 3.5	14.6 13.7 1.5 1.6 0.7 0.4 0.7 0.5 0.5 0.5	0.8 0.8 0.3 0.3 0.8 0.0 0.1 0.8	Orouler Contact (Probable Dredge Spot) Orouler Contact (Probable Dredge Spot) Grouber Contact (Probable Trues Contact Point Source (Probable Boulder) Linear Contact Point Source (Probable Boulder) Dreit Source (Probable Boulder) Linear Contact Dreit Source (Probable Boulder) Linear Contact	- - - MI05 -
	41.5539100 41.551757 41.551747 41.551747 41.551747 41.552474 41.552474 41.5524524 41.5524524 41.553944 41.55394 41.55394 41.55394 41.5549888 41.5499888	d1 6825446 d1 6823635 d1 6823136 d1 6823136 d1 682263 d1 682263 d1 6818380 d1 6818380 d1 681835 d1 681835 d1 6819536 d1 6809536 d1 6809546 d1 680956 d1 6809566 d1 6809566 d1 6809566 d1 6809566 d1 6809566	443077.2 443092.8 443096.5 443096.5 443103.9 443103.5 443105.4 443105.4 443105.4 443292.5 443292.5 443292.5 443292.5	4800113-8 4600157.6 460020.4 460020.4 460020.1 460020.1 460020.1 4600220.1 4600220.1 4600220.1 4600220.1	2192296.5 2192307.8 2192307.8 2192317.9 21903130.4 2190353.1 2190353.1 2190353.1 2190353.2 2190353.2 2190355.2 2190355.2 2190355.2	687590.6 687682.6 689082.0 687248.3 687971.7 687971.7 687971.7 687971.7 687971.0 687902.0 687902.0 687902.0 687902.0	12.3 12.4 12.4 12.5 12.5 12.4 12.5 12.6 12.6 12.6 12.6 12.4	91.5 78.6 49.5 264.9 30.4 195.6 19.0 38.7 142.3 152.8	15.9 14.0 1.5 3.8 1.0 8.5 7.7 1.4 8.7 3.5 2.0	14.5 13.7 1.5 1.6 0.7 0.4 0.7 0.7 0.7 0.5 0.5 1.5	0.8 0.8 0.3 0.3 0.8 0.0 0.1 0.8 0.1 0.4 -	Orouler Contact (Mobable Dredge Spot) Orouler Contact (Mobable Dredge Spot) Orouler Contact (Mobable Tirre) Linear Contact Point Source (Probable Boulder) Linear Contact Point Source (Probable Boulder) Linear Contact Linear Contact Linear Contact Linear Contact Linear Contact Linear Contact Linear Contact Linear Contact	- - - MI05 -

1.38	MADES C	iographic	MADER U	TM Zone 37	NADER ONLY S	tate Plane North	scan Sonar Con	Distance from	1000	-		The second of the	
10	Latitude	Longitude	East(m)	North (m)	East(US servey feet)	North (US sarvey feet)	Bathyreetry (m)	Proposed Route (m)	(m)	(m)	(m)	Description	Associated t Anomaly I
C273	41,5510900	-81.6787136	443397.0	4600155.3	2159294.9	687600.1	12.6	85.1	1.7	0.6	0.6	Point Source (Probable Boulder)	0 1. 2970
G272	41.5515349	-81.6763774	643433.0	4600207.7	2189412.7	687774.2	12.5	118.9	1.7	0.6	0.6	Point Source (Prohable Boalder)	1.000
C273 C274	41.5510539	-81.6781199 -81.6779915	643336.9 443455.4	4600154.2	219345£.5 2193496.1	687599.4 687226.3	12.6	78.6	4.1	0.9	0.2	Linear Contact Linear Contact	
C275	41.3511725	-81.6779343	445462.1	4500157.2	2155507.8	687645.0	12.6	97.4	1.0	0.7	0.6	Point Source (Probable Boulder)	1
C278	41.5518835	-81.6776264	443455.4	4600243.8	2155569.7	667695.6		177.0	1.5	1.0	0.7	Point Source (Probable Boulder)	1.00
6277	41.5519197	\$1.6775816	443492.2	4600250.0	2159601.8	687916.2		184.3	1.4	1.2	0.6	Point Source (Probable Boulder)	
Q78 Q78	41.9507812	-81.6770972 -81.6769191	443531.6	4600123.2	2159736.3 2159786.2	687502.6 687588.9	12.5 12.6	93.0 \$28.0	3.3	0.2	0.1	Linear Contact Linear Contact	
Q40	41.5510285	-81.6768499	443552.8	4600149.5	2159806.2	687593.4	12.6	127.1	3.3	0.2	0.5	Linear Contact	+
C281	41.5482126		663569.9	4589637.8	2100880.2	686568.0	11.0	137.6	16.4	15.9	0.6	Groular Contact (Probable Oradge Spoil)	100
C282		-81.6765111	643569.9 445590.3	4599637.8 4599658.A	2193860.2 2193945.5	606568.0	12.5	100.7	5.6 13.0	1.0		Linear Contact Orcular Contact (Probable	-
-											-	Oredge Spoil) Orcular Contect (Probable	-
C283	41.5484909		443595.7 443595.7	4599068.3	2198556.4 2198545.7	686670.1 687441.0	12.5	91.5	19.6	17.3	1.5	Oredge Spoll) Lineer Contect	
(215	41.5485524	1000000000	443997.2	4599675.3	2199967.7	686692.7	12.5	136.0	11.9	15.9	0.6	Circular Contact (Probable Oredge Spoil)	M34, M2
C285	41.5508125	-81.6760985	443634.9	4600126.1	2154011.5	687516.6	11.9	70.4	5.7	0.3	+	Linear Contact	
C287	41.5485795	-81.6760747	443415.1	4599689.2	2104035.4	686739.5	11.5	61.5	14.4	36.9	0.7	Groular Contact (Probable Ovedge Spoil)	M165
C288	41.5487472	-81.6759931	443621.9	4599696.7	2104047.5	606764.4	11.6	43.6	17.3	18.4	13	Circular Contact (Probable Oredge Spoil)	N200
C288	41.5488684	-81.6758657	443632.6	4599030.1	2154061.9	686838.9	12.0	245.8	14.7	30.8	0.7	Circular Contect (Probable Credge Spoil)	1.00
C290	41.5463369	-81.6747615	443722.5	4599628.3	2154392.9	685889.4	12.4	155.2	0.9	0.7	0.7	Point Source (Probable Soulder)	1.543
C251 C252	41.5504215	-81.6746781	443733.0	4600081.7	2154401.7 2154480.2	687377.8 685952.4	11.5	216.3 229.3	4.4	0.3		Linear Contact Linear Contact	
		-81.6737736	443304.7	4599601.5	2154664.1	685935.4	12.4	132.8	1.8	0.8	0.4	Point Source (Probable	
(214	41 5497834	-81 6736.943	663815.4	4600009.9	2154675.9	687146.0		584.0	1.0	0.6	0.6	Boukler) Point Source (Probable	1 22
100		-81.6735217	443822.7	4599212.3	2104785.2	681530.0	12.2	208.7	1.1	0.6	1.9	Boukler) Point Source	-
C214	41.5462036	-01.6735062	445527.0	4599612.7	2194738.4	605844.0	12.0	224.8	1.5	1.1	0.9	Point Source (Probable Boulder)	1.14
	the second s	-81.6724721 -81.6724516	443912.9	4599546.6 4599543.4	2156022.1 2156027.8	605631.9 605621.5	12.0	226.7	1.5	0.9	0.2	Linear Contact Linear Contact	
	41,5466707	the second se	443935.7	4599663.7	2155090.2	686017.6	12.1	10.8	1.4	0.8	0.4	Lineer Contact	
_		-81.6719941	443954.6	4599792.8	2195145.2	686442.4	12.2	128.5	1.3	0.8	0.6	Point Source (Probable Boulder)	
		-81.6719892 -81.6715162	443956.1 4439993.7	4589526.7 4599691.2	2155342.4 2155279.2	685381.9 686111.2	12.2	59.0 69.1	2.9	1.0	0.5	Linear Contact Linear Contact	-
C303	41.5466584	-81.6711224	4440326.3	4599661.6	2195387.9	686036.0	11.2	\$33.2	1.8	0.9	0.5	Point Source (Prolitable Boulder)	
	and the second se	-81.6710955		4596962.8	2105417.1	603722.7	11.3	385.6	2.6	4.1 1.P	0.9	Point Source Linear Contact	10 V.F.
C306		-\$1.6707047	444051.9	4599757.9	2155499.2	606333.7	12.1	29.5	1.1	0.9	0.7	Point Source (Probable Boulder)	
C307	41.5499187	-\$1.6706619	444265.0	4599690/0	2356818.1	608111.3		711.7	1.9	0.6	0.6	Point Source (Probable Soulder)	1.00
	41.5531004	41.6701272 -81.6701856	444389.4 444104.5	4598382.5	2155679.7	681100.2 686047.5	12.0	25.9	12.7	0.5	0.2	Lineer Contect	
	41.5408811	-\$1.6701475	444102.7	4599025.6	2195674.8	689913.5	11.7	184.0	2.7	0.7	0.7	Linear Contact Linear Contact	-
cass	41.5645263		464113.8	4599424.2	2155665.3	685241.9	12.1	71.7	21.8	14.3		Low Reflectivity Patch (Possible Slag)	1.00
G12	41.5500676	-81.6699525	444122.7	4599600.6	2195705.6	685821.0	10.6	541.4 85.1	2.6	0.8		Linear Contact Low Reflectivity Patch (Possible	
C314	41.5477103	-01.6690294	444125.1	4599777.6	2155788.2	606-902.6	12.1	32.7	10.4	0.4	0.2	Slagj Linear Contact	
C315 C315	41.5464878	-81.6697967 -81.6697290	444136.8	4599641.8	2156751.4 2156770.3	605957.2 605944.2	12.1	33.1 569.0	4.5	0.7	0.1	Linear Contact Linear Contact	
		-81.6697192		4588573.3	2195806.0	682450.8	10.6	528.1	33.1	14.8	-	Low Reflectivity Patch (Possible	(
		-81.6696852		4598700.2	2159811.3	682867.5	10.0	854.7	5.0	1.8		Sleg! Grovier Contect	M71
C315 C320	41.5334407 41.5375090		444146.5 444150.8	4596193.2	2195865.4 2195853.9	681204.1 682685.3	10.5	532.9	0.7	0.6	0.2	Groular Contact Linear Contact	
C323	41.5405298	-81.6694702	444158.9	4596900.2	2195863.4	683787.3	11.5	415.4	2.8	0.5	0.3	Linear Contact	M139
C322 C323		-81.6694588	444159.8	4596576.8	2105864.6 2105904.6	683776.4 683163.8	11.0	473.0	2.9	0.8	0.3	Linear Contact Linear Contact	-
C324	41.5462797	-41.6693122	444177.0	4599618.4	2195884.7	605282.7	9.8	\$34.5	11.9	3.9		Linear Contact	+
C325		-81.6693049 -81.6693047		4596237.2	2195930.5	601283.9	12.0	133.0 506.6	1.1	0.8	0.8	Orouler Contect Point Source (Probable	
	124201012	-81.6690645	1022-1122-1	4599309.7	2155966.4	684214.2	11.9	129.0	7.6	1.2		Boulder) Linear Contact	+
C328 C325	41.5477931 41.5459050		444209.8 444209.2	4599786.2	2155962.8 2155992.9	686435.1 685747.2	12.0	16.3	3.5	0.9	0.7	Linear Contact Linear Contact	
		-81.6682946		4599782.3	2195999.9	686422.4	11.9	137.4	1.5	1.0	0.8	Point Source (Probable	1.000
		-81 6683087			2106300.9	681528.7	9.9	541.8	3.2	0.8	0.1	Boulder) Linear Contact	
cita	41.5397000	-01.6681239	444270.5	4596296.9	2196213.5	603520.5	11.4	144.3	14	1.5	0.0	Point Source (Probable Goulder)	1.23
CI 34	42.5392443	-61.6680/857	444273.2	4596625.5	2196245.2	603286.0	11.1	362.8	1.6	12	0.6	Point Source (Probable Boulder)	
		-01.6680146		4596575.1	2196272.5	602464.8	10.0	482.5	3.8	0.7	-	Lineer Contact	
		-81.6679282 -81.6678937	444285.5 444285.8	4596855.3	2156267.A 2156811.3	681365.9	5.7	341.3 477.9	12.9	0.5	0.2	Linear Contact Linear Contact	
C338		-81.6678419	444299.7	4589622.6	2196287.0	605903.4	11.9	83.7	3.1	0.4	0.1	Lineer Contact Point Source (Probable	
C338	1.			ADDRESS P.	A CONTRACTOR OF A	681538.9	9.7	488.4	1.7	1.9	1.4	A STATISTICS IN ADDRESS	S
C338 C340		-81.6676473		4598282.5	2196381.9		1000	10000			-	Boukler) Dolat Source (Doubable	1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1
C338 C340 C341	41.53887399	-81.6676473 -81.6676224 -81.6676368	444311.6	4598232.5	2196378.0	602109.0	11.1	234.9	1.5	0.9	0.5	Boukler) Point Sounce (Probable Boukler) Linear Contact	

- 92	MADES C	ieographic	MADES U	ITM Zone 17	NADER ONLY S	tate Plane North	ican Senar Cen	Distance from					
10	Latitude	Longitude	East(m)	North (m)	East (US servey feet)	North (US sarvey feet)	Bathyneetry (m)	Proposed Route (ni)	Length (m)	(m)	Height (m)	Description	Associated M. Anomaly ID
(344	41.5433712	-\$1.6673183	444340.8	4599294.2	2156440.6	684828.2	11.5	80.3	2.2	13	0.6	Point Source (Probable Boulder)	1 1957 -
C345	41.5428351	-81.6672239	444348.2	4599234.7	2196468.3	691633.1	114	110.0	2.0	1.5	0.6	Point Source (Proitable	9
C946	41.5390907	-81.6670194	444362.0	4596215.5	2196537.4	683258.4	11.1	280.8	6.9	0.8		Roulder) Linear Contact	
C347	41.5600290	-01.6660459	444377.3	4596934.1	2196581.5	603615.6	11.5	234.2	4.6	1.1		Ortuiler Contact Delet Seurce (Dechable	
C548	41.3448288	-81.6667617	444388.5	4599455.7	2156587.9	605360.7	11.5	54.7	14	0.6	0.6	Point Source (Probable Boulder)	÷+
C345		-81.0006675	444359.1	4596523.7	2196642.9	662302.3	10.0	540.6 282.2	4.5	0.5	0.1	Lineer Contect	+
C350 C351	41.5377070 41.5555920		444405.9	4596664.8	2156693.1 2156712.9	682765.6 681996.1	10.5	262.2	3.9	0.6 I.6	0.1	Linear Contact Groular Contact	
353	41.5557122		444410.5	4556443.3	2196717.7	682039.9	10.1	348.1	3.1	2.4	0.4	Rectangular Contact	
352	41.5355430		444411.8 444433.0	4598424.5	2156722.9 2156799.1	681978.3 681948.5	10.1	343.8 330.5	2.7	2.1	0.5	Gircular Contact Linear Contact	M34
(355	41.5359835	-81.6660122	444343,4	4598479.2	2156823.9	682139.8	±0.0	308.6	2.0	2.0	0.4	Rectangular Contact	+
C156	41.5608358	-81.6659965	44448.5	4596967.5	2196812.6	683762.1	11.5	153.5	17	1.0	0.5	Point Source (Probable Boulder)	1.000
C357	41.5668531	-41 6659764	666454.0	4599457.9	2106802.8	685371.6	11.5	108.4	2.2	0.4	0.2	Linear Contact	
C358 C359	41.5394163 41.5393836	-81.6659338 -81.6659024	444452.9	4596654.3	2196813.4	603377.9	11.1	182,5	3.0	0.5	0.3	Lineer Contect Lineer Contect	
C350	41.5355404	-81.6658774	444454.3	4598423.9	2196862.5	601978.7	10.1	\$07.6	10.6	1.2	. · A	Linear Contact	+
C362 C363	41.5393155 41.5394764	-81.6657848 -81.6655826	499965.2	4586843.0	2156874.5 2156525.3	683354.4 683413.6	11.0	174.1	2.6	0.5	0.1	Linear Contact Linear Contact	M164
(364	41.5405681		444399.1	4598581.8	2196977.6	683811.9	11.5	100.9	1.7	0.9	0.6	Point Source (Probable	
C365	41.5383879	-81.6653599	444799.9	4596739.7	2106894.1	683017.6	10.4	171.9	3.8	0.4	~**	Boulder) Linear Context	M166
C366	41.5413167	-81.6653200	444505.7	4599064.9	2196994.8	684084.8	11.4	70.2	6.1	0.5		Linear Contact	+
C167	41.53666880	-81 6652979	444503.6	4598548.7	2107017.0	682391.1	10.D	223.0	10.7	2.8	3	Point Source (Probable Boalder)	1.20
C358	41.5412080	-41.6653677	444510.0	4599052.0	2197000.5	601045.3	11.4	69.7	6.0	.0.3	0.1	Lineer Contact	
C389	41.5405985	-81.6651522	444510.0	4596909.5	2197015.7	663837.9	11.1	87.5	11.5	0.7	0.2	Linear Contact	+
C170 C171	41.5436900 41.5429487	-81.6651512 -81.6649808	444521.7	4599029.2	2157052.1 2357061.9	604953.2 664690.3	11.5	40.5	3.4	2.4		Orcular Contect Linear Contact	
C372	41.5505556	-51.0048749	444535.5	4596544.2	2157152.9	602390.4	10.0	191.3	2.7	2.2		Rectangular Contact	
C373 C374	41.5404384 41.5441247	-81.6646158 -81.6645217	444563.7 444591.4	4596566.9	2157150.6 2357258.2	683766.6 685110.5	11.1	43.5	6.7	0.5	0.1	Linear Contact Linear Contact	
(375	41.5398762	-81.6641478	444593.9	4596904.2	2197293.4	683562.8	10.9	33.0	5.0	0.4	0.1	Unser Contect	
(376	41.5402326	-81.6642375	444595.1	4598943.8	2197294.9	689692.7	11-0	20.8	5.8	0.4		Linear Contact	-
C377	41.5429576	-81.6642185	444599.0	45999357.3	2107297.1	685049.9	11.5	164.9	10.4	3.2	. 38	Low Aeflectivity Patch (Possible Slag)	( ÷
C978	41.5398078	-81 6642158	444596.5	4596696.6	2107300.3	623537.9	10.9	32.8	9.5	0.6	1.4	Linear Contact	-
C879	41.541.9479	-81.6639784	499617.6	4599067.5	2197361.9	604039.7	11.5	37.6	1.2	1.0	0.6	Point Source (Probable Boulder)	
C100	41.5419327	-01.6639251	444622.7	4599132.4	2197875.0	604312.9	11.5	61.5	5.B	0.7	0.1	Linear Contact	
GEL	41.5416010	41.6637215	444639.3	4599085.4	2197431.3	684192.6	11.2	65.5	2.9	2.7	0.6	Point Source (Probable Boulder)	(14)
C382	41.5407071	-81.6635943	444649.1	4556596.1	2197469.5	683967.2	11.1	46.T	3.3	0.5	0.1	Linear Contact	5
38	41.5367471 41.5376005	-81.6635730 -81.6634348	444547.5	4598556.4	2157485/0 2157533.8	682424.4 682735.7	9.8 10.1	84.0 44.5	4.9	2.5	-	Rectanguler Contact Rectanguler Contact	-
085	41.5411380	-81.6634188	444554.1	4599043.8	2197515.8	684024.7	11.2	75.1	11.0	0.5	0.1	Linear Centact	M29
G15 G17	41.5402331	-81.6633750 -81.6633317	4449971.0	4596543.3	2197531.0 2197538.3	683695.1 684066.6	10.9	48.8	10.9	0.4	0.2	Linear Contact Linear Contact	
C388	41.5426937	-81.6631525	444697.7	4599236.3	2107563.3	604592.2	11.3	151.9	19.3	0.6	0.4	Linear Contact	-
C389	41.5409948	-01.6631201	444688.3	4599027.7	2197505.9	603973.3	11.1	95.4	1.7	0.7	0.6	Paint Source (Probable	
(350	41.5572015	-81.6629816	444697.2	4596606.5	2197649.3	682591.5	10.0	21.8	1.7	1.0	14	Boulder) Point Source (Probable	
(391	41.5412620	-81.6629308	444704.9	4599057.3	2157649.0	684071.2	11.1	118.0	16.5	0.5	0.2	Soulder) Linear Contect	
C\$92	41.5412085	-\$1.6619304	444704.9	4599051.3	2157645.3	664051.7	11.1	116.3	5.1	0.7	0.D	Lineer Contect	
(393	41.5412250 41.5401107	-81.6627034 -81.6625952	444723.9	4599053.0	2157711.4 2157744.9	684058.3 689652.5	11.0	134.9 106.2	6.9	0.4	0.1	Linear Contact Linear Contact	
	45.5405335	-81.6615764	444733.5	4598993.7	2197749.9	683660.8	10.6	108.5	5.0	0.8		Linear Cantach	
C356	41.5410908	-81.6625411	444737.8	4599038.0	2107756.3	681009.8	11.0	143.3	6.0	0.6	-	Linear Contact Linear Contact	-
204.61	41.5421236		444765.0	4599152.5	2107844.0	604387.0	11.1	204.4	7.0	0.5	-	Linear Contact	-
(399	41.5378287	-81.6621331	444768.6	4506875.6	2107079.4	602022.3	10.2	66.T	2.5	3.7	11	Point Source (Probable	1.00
												Soulder) Point Source (Probable	
C400	41.5378276	-81.6621031	4447711	4596875.4	2157887.6	681822.0	10.2	69.1	1.8	12	0.6	Boulder)	
		-\$1.6620963			2197877.2	684.092.9	11.0	186.2	15.8	0.5		Linear Contact Point Source (Probable	
6482	41.5879908	-81.6620264	444777.5	4598686.8	2197908.2	681859.8	10.2	78.6	2.0	1.5	12	Boulder)	1.00
CADA	41.5418485	-81.6620173	444781.6	4599121.8	2197897.0	684287.2	11.1	210.8	1.2	0.7	0.5	Point Source (Probable Boukler)	1 223
GIDI	41.5409520	-81.6619165	444789.5	4599022.2	2107927.7	683961.9	10.8	188.3	4.0	0.3	0.1	Linear Contact	
Ç416	41.5611253	-81.6612759	444792.0	4599041.6	2167938.2	694024.1	10.9	197.4	9.2	0.4	1.10	Linear Contact Point Source (Probable	<u></u>
CADE	41.5419295	-01.6610404	444795.0	4599128.5	2197943.0	604310.0	11.1	225.8	1.5	0.0	3.0	Boulder)	1.25
CAD7	41.5409961	411.6616459	444905.6	4589026.9	2107900.7	663977.5	10.8	208.2	5.6	0.5	0.1	Linear Contact	( ) e )
6408	41.5580128	-\$1.6616176	004811.7	4598855.7	2150015.8	652890.7	10.1	115.9	1.9	0.5	0.8	Point Source (Probable Boulder)	
C405	41.5412277	41.6614278	444538.3	4599052.5	2190060.5	684062.6	10.8	256.4	5.7	0.4	0.1	Lineer Contect	+
6410	41.5383226	-81.6611910	444839.2	4598729.9	2199108.2	683034.5	10.2	150.2	2.7	1.6	0.7	Point Source (Probable Boulder)	1.00
G813	41 5383523	-81 6611642	444949.0	4599733.1	2198142.0	683015.6	10.1	161.3	1.5	1.0	0.5	Point Source (Probable	
		-81 6611077	44454.6	4856758.4		683024.3					-	Boulder) Point Source (Probable	1000
C812	43.3483755	-81 0611077	094838.6	4596735.6	2100150.2	COLUMN 3	10.2	166.6	3.1	12	0.9	Boulder)	
G#13	41.5386757	-81.6610147	444852.4	4598746.7	2100183.3	683061.0	10.3	177.3	12	0.7	0.4	Point Source (Probable Boulder)	1.000
6454	41 338544	-81 6606008	444597.0	4598758.7	2156256.2	683102.4	10.5	215.9	3.1	1.0	1.0	Point Source (Probable	
							22.5		21	+0		Soulderj Doint Source (Doinable	
6415	41.5586604	-81.6605-811	444898.7	4598766.9	2156301.5	683129.4	10.5	218.0	2.2	1.5	0.7	Polint Source (Probable Boulder)	1.51
6416	41.5387020	-81.6605765	444899.1	4588771.5	2198362.4	683144.6	10.5	219.7	2.5	1.2	0.7	Point Source (Probable	
							1000				-	Boulder) Point Source (Probable	-
		-81.6605402		4598768.1	2196312.5	683133.4	10.6	221.6	2.5	0.7	0.7	Bouldery	
6418	41.5391259	-81.6604032	444914.0	4598818.5	2196348.4	683299.5	10.5	247.7	3.4	1.8	0.6	Rectangular Contact	M106
		-01.6604102	1.00.010.00.00	and the second								Point Source (Probable	

	1						ncan Sonar Con	units	_	_	_	r	
10	Latitude	iongitude	East(m)	North (m)	East (US servey feet)	Neeth (US servey Seet)	Bathyraetry (m)	Distance from Proposed Route (nr)	Length (m)	Wixeh (m)	Haight (m)	Description	Associated Ma Anomaly ID
Ç420	41.5385383	-81.6603481	466918,1	4598753.2	2196365.5	683085.5	10.5	232.4	1.7	0.7	0.5	Point Source (Probable Boulder)	2 100
6421	41.5387309	-\$1.6602.029	444923.2	4598774.6	2106363.1	623155.9	10.7	243.6	4.0	2.2	0.7	Point Source (Probable Boalder)	100
6422	41.5586188	-81.6602/872	444923.4	4598794.3	2150381.2	605187.9	10.5	246.6	1.9	2.2	0.0	Point Source (Probable Boulder)	-
CA25	41.5599555	-\$1.6601601	444934.9	4596511.7	2196412.0	603906.5	10.4	295.1	6.0	0.7	0.2	Lineer Contect	- C+ C+
6434	41.5386927	-81.6601584	444934.0	4598770.2	2156415.9	683142.3	10.6	252.7	2.8	1.1	0.8	Point Source (Probable Soukler)	
6425	41.5389034	-81.6601138	444937.9	4598793.6	2356428.4	683219.3	10.5	263.3	1.9	1.0	0.7	Point Source (Probable Boulder)	
(435	43.5407736	-81.6600747	444942.8	4599001.2	2396432.5	683900.T	10.5	8.916.9	2.1	1.7	0.6	Groular Contact	M26
6427	41.5889287	-81.6600659	444941.9	4598296.4	2108443.4	689728.5	10.5	267.9	1.6	1.0	0.9	Point Source (Probable Boulder)	100
Q128	41.5396366	41.6599435	444952.7	4596874.9	2398472.4	683-495.8	10.5	301.3	2.2	2.0	0.6	Rectangular Contact	
C429	41.5589773	-81.6599406	444952.4	4596801.7	2190475.5	683246.6	10.6	279.5	2.9	1.1	0.4	Polint Source (Probable Boulder)	1
6430	41.5390395	-81.6599005	444955.0	4506008.6	2156466.3	663269.3	10.5	284.8	3.0	1.2	0.7	Linear Contact :	
6431	41.5591901	-81.6595928	444981.6	4598825.1	2196570.0	688325.0	10.4	314.3	2.2	2.3	0.7	Point Source (Probable Boukler)	M52
6432	41.5395059	-81.6594679	444992.3	4598860.1	2198603.1	683440.4	10.6	334.8	2.1	1.6		Rectangular Contect	M36
6434	41.5412463	-81.6591813	449017.7	4599053.1	2156675.4	684075.3	0.0	415.7	2.2	1.6	1.2	Point Source (Probable Boakler)	4.5
Ç435	41.5395486	-41.6591395	445019.6	4596042.4	2199699.5	623364.0	10.6	155.6	2.2	1.0	1.3	Point Source (Probable	
C458	41.5594000	-61.6590536	445026.8	4500049.0	2196716.6	605406.1	10.5	364.5	2.5	1.4	0.7	Point Source (Probable Boulder)	-
C457	41.5394521	-61.6590459	445027.5	4596653.8	2156718.8	603421.9	10.6	366.5	2.7	1.0	0.9	Point Source (Probable Boulder)	1.000
6438	41,5397920	41.6590282	445029.2	4596693.0	2156722.5	663543.8	10.7	\$75,3	5.2	2.3	0.5	Rectangular Contact	
6439	41.5394321	-81.6590259	445029.1	4586851.6	2198734.3	683414.7	10.6	367.5	2.2	0.9	0.6	Point Source (Probable Boulder)	1.0
6440	41.5394747	-81.6589939	449031.8	4996856.3	2166733.0	683430.3	10.6	371.4	2.7	1.1	1.2	Porint Source (Prolivable Sourcer)	1.00
(44)	41.5398344	-81.6590029	445031.0	4596892.9	2198728.3	683550.4	e	343.2	2.0	2.4		Rectangular Contact	1.000
0442	41.5395629	-01.6589004	445239.0	4556568.3	2150756.0	603470.0	10.7	101.0	13	0.5	1.D	Point Source (Probable Boulder)	-
C443	41.5594981	-81.6587317	445053.6	4598848.5	2156805.0	0.004233	10.7	390.0	1.5	14	0.7	Point Source (Probable Soulder)	
6444	42.5398521	411.6586279	445062.7	4586896.0	2196831.6	683568.0		413.2	15	1.6	0.6	Rectangular Contact	
6445	41.5595078	41.6586050	445064.3	4598859.7	2156835.3	663443.4	- 94	403.5	2.8	0.8	0.6	Point Source (Probable Boulder)	
6446	41.5396563	-81.6585672	445067.5	4596876.2	2198849.1	689497.6	19	411.4	1.4	1.0	0.5	Point Source (Probable Boulder)	1. A (
ç647	41.5391272	-81.6584060	445285.1	4590295.1	2156892.7	643560.3		430.0	1.6	0.0	1.0	Polint Source (Prolivable Boulder)	1.000
C448	41.5397896	-01.6585/021	445003.1	4590250.4	2105890.3	603546.3	1.54	430.6	2.5	1.0	0.6	Point Source (Probable Soulder)	
6445	41.5599923	-01.6582954	445090.5	4596513.3	2356522.4	665620.7	1.00	444.3	2.5	2.5	0.7	Point Source (Probable Boulder)	
6450	41.5398635	41.6581472	445294.4	4556838.9	2156936.0	683573.8	200	443.8	2.4	2.2	0.8	Point Source (Probable Soulder)	1.000
6450	41.5399992	-\$1,6581051	445098.0	4556508.6	2156547.2	688605.6	194	450.1	1.8	0.7	0.9	Point Source (Probable Boulder)	1.00
6452	41.5600100	-81.6581874	445099.5	4596915.2	2199951.9	683627.5	19	453.5	2.1	1.0	1.0	Point Source (Probable Boakter)	
C453	41.5402440	-01.6577455	445135.6	4598940.9	2199072.0	683713.9	1.00	496.5	2.1	17	0.9	Poirt Source (Probable Boalder)	1.00
0454	41.5402700	-81.6575067	4451.55.5	4596543.7	2199137.3	603724.0		516.3	1.7	0.8	0.6	Point Source (Probable Boulder)	1.000
GISS	41.5402653	-81.6572468	445178.2	4596543.0	2199206.4	683723.0		536.8	1.7	1.4	-	Gimular Contact	

#### **5.2 Magnetometer Results**

A review of 271 line km of magnetometer data showed no historic structures (such as shipwrecks) present within the turbine and export cable survey areas.

A total of 178 magnetic anomalies were identified and mapped from the magnetometer data acquired over the Icebreaker Wind survey area. The anomaly location, type, magnitude and observations from the sidescan sonar in the area of each anomaly are listed in Table 3. Profiles of the magnetic anomalies within a 150 m (495 feet) corridor centered on the proposed route. Profiles of those outside the corridor can be found in Appendix A.

# Table 3 Magnetic Anomalies Contact List

	NAD83 G	eographic	NAD83 UT	M Zone 17		tometer Anomalie tate Plane North	Street and street and st	Distance	Concernent State		Associate
ID	Latitude	Longitude	Easting (m)	Northing (m)	East (US survey	North (US survey	Bathymetry (m)	from	Polarity	Amplitude (nT)	Sidescar
MI	41.5950349	-81.7914838	434038.0	4605228.5	feet) 2162296.1	feet) 703716.7	16.9	Proposed 93.1	Monopole	66.9	Contact I
M12	41.5727049	-81.7348227	438738.1	4602596.6	2177868.5	695347.0	15.4	92.1	Dipole	63.9	-
M3	41.5707487	-81.7299932	439138.9	4602376.0	2179196.2	694645.8	15.3	88.6	Monopole	43.4	
5/14	41.5684997	-81.7245598	439589.8	4602122.5	2180690.2	693839.5	15.0	89.4	Monopole	78.5	
MS	41.5649288	-81.7160083	440299.5	4601720.1	2183041.8	692559.4	14.3	93.6	Dipole	37.0	
M6 M2	41.5629714 41.5621961	-81.7112339 -81.7094409	440695.8 440844.6	4601499.5 4601412.2	2184354.8 2184848.0	691857.9 691579.9	14.5	92.4	Dipole	23.3	-
M8	41.5568402	-81.6963557	441930.9	4600808.7	2188446.8	689561.1	13.2	91.4	Monopole	68.6	-
M19	41.5567475	-81.6961940	441944.3	4600798.3	2188491.4	689627.8	13.2	93.9	Dipole	26.7	
10	41.5540823	-81.6897585	442478.6	4600498.1	2190261.7	688673.0	12.8	94.6	Monopole	59.6	
111	41.5522990	-81.6853676	442843.2	4600297.2	2191469.5	688034.4	12.5	91.7	Monopole	30,7	
412	41.5513733	-81.6830568	443035.1	4600192.9	2192105.1	687703.0	12.4	88.9	Dipple	21.3	£252
/13 //14	41.5510943 41.5485383	-81.6824088 -81.6762752	443088.9 443598.2	4600161.5 4599873.7	2192283.4 2193971.0	687603.1 686687.5	12.4	90.0	Dipole	52.6	C257 C285
415	41.5397510	-81.6714626	443992.0	4598895.0	2195318.7	683498.3	11.1	598.8	Monopole	10.8	
418	41.5418464	-81.6725876	443901.7	4599350.4	2194996.6	584997.5	11.6	396.0	Monopole	15.6	
419	41.5486196	-81.6762341	443601.7	4599882.7	2193982.0	686717.3	12.3	82.6	Dipole	107.7	C285
420	41.5404086	-81.6720712	443941.8	4598968.4	2195149.8	683736.3	11.3	594.9	Dipole	29.2	
124	41.5369037	-81.6676089	444311.0	4598576.4	2196383.5	682470.9	10,1	399.8	Monopole	26.3	-
125	41.5315404 41.5407863	-81.6747700 -81.6600479	443709.0	4597985.6 4599002.6	2194441.6 2198439.8	680498.1 683905.4	0.0	1091.5	Dipole	145.1 108.9	C426
126	41.5407863	-81.6635191	444945.0	4598800.4	2198419.8 2197496.0	683225.4	10.5	6.2	Monopole	32.5	0,420
123	41.5348691	-81.6682138	444053.9	4598350.9	2196225.0	681728.0	9.7	515.9	Monopole	54.7	
129	41.5376216	-81.6634084	444662.0	4598653,4	2197531.0	682743.5	10.1	41.7	Dipole	27.6	C384
130	41.5394153	-81.6600664	444942.3	4598850.4	2198439.6	683405.8	30.4	284.1	Monopole	23.8	
132	41.5410904	+81.6590152	445031.4	4599035.7	2198721.5	684018.9	0.0	423.7	Manopale	57.5	1
133	41.5408670	-81.6593186	445005.9	4599011.1	2198639.2	683936.7	0.0	392.1	Dipole	136.6	1.
134	41.5355832	-81.6663726	444413.0	4598429.0	2196726.6	681993.0	10.1	345.6	Monopola	22.3	C352
135	41.5362778 41.5395686	-81.6651042 -81.6594086	444519.4 444997.5	4598505.3 4598867.0	2197071.4 2198619.1	682249.4 683463.4	10.0	221.5 341.6	Dipole Monopole	68.7 38.6	C432
120	41.5394539	-81.6602418	444927.7	4598854.8	2198391.4	683419.4	10.6	271.5	Monopole	42.6	Crai
141	41.5604476	-81.6996252	441661.5	4601211.4	2187540.0	690967.3	18.1	128.3	Monopole	15.0	1
142	41.5631635	-81.7063681	441101.7	4601517.5	2185685.7	691940.0	14.2	121.7	Dipole	23,9	1.1
143	41.5660867	-81.7134617	440512.9	4601846.9	2183734.9	692987.5	14.3	121.3	Dipole	18.4	
144	41.5676671	-81.7172859	440195.5	4602025.0	2182683.3	693554.0	14.9	121.6	Dipole	69.5	
145	41.5682266	-81.7187086	440077.4	4602088.1	2182292.1	693754.3	14.9	118.9	Dipole	24.7	-
146	41.5690275	-81.7205561	439924.1	4602178.3	2181784.0	694041.6	14.9	122.7	Monopole Monopole	88.5	-
148	41.5713855 41.6028184	-81.7263001 -81.8026381	439447.4 433115.4	4602444.1 4605990.2	2180204.6 2159225.4	694886.8 706163.8	15.3	121.6	Monopole	122.2	
149	41.6008315	-81.8006887	433275.8	4605768.1	2159764.4	705444.1	17.1	1.9	Monopole	61.0	C8
150	41.6007495	-81.8008125	433265.4	4605759.1	2159730.8	705413.9	17.1	15.6	Monopole	49.1	CB.
451	41.6001685	-81.7991386	433404.3	4605693.3	2160190.3	705205.9	17.1	2.7	Monopole	17.0	
452	41.5984615	-81.7950101	433746.6	4605500.6	2161324.5	704593.0	17.0	1.8	Monopole	30.2	-
153	41.5733222	-81.7339397	438812.3	4602664.5	2178108.1	695574.0	15.5	3.5	Monopole	98.0	-
154	41.5710419 41.5705945	-81.7284984 -81.7274535	439263.8 439350.5	4602407.5 4602357.1	2179604.2 2179691.6	694756.3 694595.8	15.3	0.1	Monopole	16.4	-
156	41.5679312	-81.7210021	439885.9	4602056.9	2181665.5	693641.1	14.7	1.9	Dipole	16.6	-
157	41.5651370	-81.7166729	440245.2	4601854.7	2182856.0	692998.0	14.8	2.7	Dipole	155.3	
458	41 5658378	-81.7159728	440303.3	4601821.0	2183048.6	692890.7	14.6	3.7	Dipole	84.8	
159	41.5656580	-81.7154803	440344.2	4601800.7	2183183.9	692826.4	14.4	1.4	Monopole	134.0	-
160	41.5576602	-81.6960083	441960.6	4600899.5	2188539.1	689960.8	13.3	2.4	Monopole	9.6	-
463	41.5512867	-81.6806541	443235.4	4600181.7	2192763.0	687677.7	12.6	8.0	Monopole	9.7	
162	41.5391598 41.5410308	-81.6595351 -81.6583996	444986.4	4598821.7	2198585.9	683314.1 683998.8	20.4	317.9 470.7	Monopole	41.5	6431
165	41.5410308	-81.6585305	445082.7 445071.7	4599028,7 4599019.0	2198890.2 2198854.7	683966.4	0.0	470.7	Monopole Monopole	125.3	
167	41.5335442	-81.6689649	444195.0	4598204.3	2196024.0	681243.3	9.6	606.2	Monopole	25.0	
169	41.5479070	-81.5751860	443688.5	4599802.9	2194271.3	686460.3	12.1	309.8	Monopole	29.1	
170	41.5407007	-81.6714029	443997.8	4599000.4	2195331,7	683844.5	11,3	530.9	Dipole	60.0	
171	41.5378505	-81.6696039	444145.4	4598682.8	2195834.1	682810.7	10.5	\$26.B	Monopole	31.2	C118
174	41.5531703	-81.6813766	443176.8 442774.4	4600391.3	2192558.8 2191225.6	688362.1	12.4	153.4	Dipole	23.2	C334
175	41.5551699 41.5629892	-81.6862229 -81.7051321	442774.4	4600616.5 4601497.3	2191225.6	689078.3 691879.6	12.7	153.2	Monopole Monopole	29.0	C226
177	41.5634985	-81.7063778	441101.2	4601554.7	2185681.9	692062.1	14.2	153.9	Monopole	47.1	
178	41.5649951	-81.7102511	440779.6	4601723.5	2184617.0	692597.7	14.5	344.0	Monopole	15.9	0
179	41.5671708	-81.7152571	440364.2	4601968.5	2183240.0	693378.1	34.7	154.7	Monopole	13.3	-
180	41.5675736	-81.7162534	440281.5	4602013.9	2182966.1	693522.4	14.8	153.9	Monopole	18.0	-
181	41.5695702	-81.7210491	439883.5	4602238.9	2181647.3	694238.2	15.0	155.7	Monopole	27.9	-
18.2	41.5717140 41.5797575	-81.7261910 -81.7457494	439456.8 437833.9	4602480.5 4603387.4	2180233.4 2174856.6	695006.8 697890.6	15.3	157.9	Monopole Monopole	19.3	C83
16.4	41.6044681	-81.9025638	437855.9	4606173.3	2159241.0	706765.0	17.2	115.9	Monopole	123.9	C6
186	41.6028804	-81.8045865	432953.1	4605998.6	2158692.4	706182.1	17,2	123.9	Monopole	130.4	
187	41.6081027	-81.8084546	432636.2	4606581.4	2157619.4	708076.5	37.4	31.5	Monopole	20.7	
189	41.6010727	-81,8019985	433166.9	4605795.9	2159405.5	705529.1	17.1	72.8	Dipole	50.2	
190	41.5994800	-81.8012672	433226.2	4605618.5	2159610.1	704950.4	17.1	149.6	Monopole	26.3	1
191	41.5723577	-81.7353154	438695.7	4602558.4	2177734.8	695219.3	15.4	345.6	Monopole	142.0	244
192	41.5694135	-81.7283386	439275.6	4602226.6	2179653.2	694163.3	15.2	152.1	Dipole	79.6	C63
193 194	41.5681926 41.5677188	-81.7252617 -81.7242741	439531.0 439612.9	4602088.9	2180499.1 2180770.9	693725.9 693555.7	15.0	147.4	Dipole	17.1 16.7	
195	41.5658153	-81.7242741	439612.9	4602035.6 4601821.1	2180770.3	692873.3	15.1	156.5	Dipole	33.5	-
195	41.5654690	-81.7187908	440068.0	4601782.0	2182278.6	692749.4	14.8	152.7	Dipole	18.6	
197	41.5649433	-81.7177223	440156.6	4601722.9	2182572.7	692560.4	14.7	161.0	Monopole	44.1	
198	41.5646518	-81.7170716	440210.6	4601691.2	2182751.7	692459.5	14.5	162.3	Dipole	20.2	1
199	41.5644116	-81.7160350	440296.8	4601662.7	2183036.2	692370.9	14.3	145.0	Monopole	79,4	
100	41.5598377	-81.7048125	441228.4	4601147.2	2186122.4	690732.1	13.9	139.4	Monopole	22.4	-
101	41.5589784	-81.7028964	441387.4	4601050.5	2186649.6	690423.8	13.4	146.0	Monopole	48.4	and the second

1.00	NAD83 G	eographic	NADES UT	IM Zone 17		etometer Anomalie tate Plane North		Distance			Associate
ID	Latitude	Longitude	Easting (m)	Northing (m)		North (US survey feet)	Bathymetry (m)	from Proposed	Polarity	Amplitude (nT)	Sidescan Contact II
M103	41.5500740	-81.6813081	443179.8	4600047.5	2192588.2	687234.1	12.5	145.0	Dipole	65.3	C263
M106	41.5391328	-81.6603260	444920.4	4598819.2	2198369.5	683302.2	10.5	254.0	Monopole	17.8	C418
M107	41.5540152	-81.6850092	442874.6	4600487.5	2191561.7	688660.6	12.6	89.7	Dipole	10.2	-
M108	41.5676584	-81.7179539	440139.8	4602024.5	2182500.5	693549.1	14.9	98.9	Dipole	75.2	3
M109	41.5691766	+81.7217620	439823.7	4602195.7	2181453.5	694093.0	15.0	88.8	monopole	85.5	
M111	41.5700593	-81.7239224	439644.4	4602295.2	2180859.5	694409.4	14.9	88.0	Dipole	20.9	2
M112	41.5708789	-81.7259358	439477.3	4602387.6	2180306.0	694703.1	15.2	86.9	Dipole	20.4	C87
M113	41.5710823	-81.7263759	439440.8	4602410.5	2180184.9	694776.1	15.3	89.0	Dipole	25.6	C82
M115	41.5739316	-81.7332821	438867.7	4602731.7	2178286.1	695797.6	15.6	89.2	Monopole	23.9	2 . Care
M116	41.5744240	-81.7344668	438769.4	4602787.2	2177960.4	695974.2	15.6	89.5	Dipole	14.8	
M117	41.5872063	-81.7656452	436182.7	4604228.9	2169390.5	700558.3	15.7	83.0	Monopole	11.8	
M118	41.5960000	-81.7867306	434434.1	4605221.0	2163596.3	703714.5	16.9	93.9	Monopole	21.9	1.1
M120	41.6024963	-B1.8010345	433248.7	4605953.2	2159665.0	706049.9	17.1	86.5	Monopole	20.2	
M121	41.6053231	-81.8038295	433018.7	4606269.2	2158892.3	707073.8	17.3	89.9	Monopole	22.5	
M122	41.5736267	-81.7333638	438860.6	4602697.9	2178264.7	695686.3	15.5	56.2	Monopole	74.9	
M123	41.5669524	-81.7170705	440212.8	4601945.5	2182744.5	693294.1	14.9	60.7	Dipole	26.2	
M124	41.5657431	-81.7141164	440458.0	4601809.2	2183556.9	692860.7	14.3	61.6	Monopole	38.1	-
M127	41.5354138	-81.6669817	444362.9	4598521.6	2196556.9	682294.1	10.0	366.3	Monopole	20.1	
M128	41.5354060	-81.6674209	444325.4	4598410.0	2196440.2	681925.7	9.8	434.9	Dipole	35.6	
M129	41.5360893	-81.6679494	444281.9	4598486.2	2196293.2	682173.3	9.9	454.1	Monopole	37.5	· · · · ·
M131	41.5373226	-81.6685387	444233.8	4598623.5	2196127.5	682621.1	10.3	459.8	monopole	39.7	
M133	41.5400208	-81.6699860	444115.4	4598924.0	2195722.0	683600.5	11.4	482.6	Monopole	21.6	
M134	41.5408592	-81.6687921	444215.7	4599016.3	2196045.9	683909.0	11.5	347.0	Monopole	31.6	
M135	41.5374646	-81.6670369	444359.2	4598638.3	2196538.2	682676.8	10.2	335.5	Monopole	21.6	
M138	41.5389967	-81.6686015	444230.0	4598809.4	2196104.5	683230.9	\$1.0	408.8	Monopole	20.2	-
И139	41.5405997	-81.6694249	444162.7	4598987.9	2195873.6	683812.8	11.5	406.4	Dipole	5.8	C321
M140	41.5508761	-81.6824508	443085.2	4600137.3	2192272.7	687523.4	12.5	112.9	Monopole	15.3	C256
M141	41.5512989	-81.6836088	442989.0	4600185.0	2191954.3	687674.5	12.4	118.3	Monopole	14.3	
M142	41.5524452	-81.6863740	442759.4	4600314.1	2191193.5	688085.1	12.6	117.9	Dipole	72.3	-
M143	41.5565323	-81.6963428	441931.7	4600774.5	2188451.4	689549.0	13.2	120.8	Monopole	17.2	C197
W144	41.5620845	-81.7098618	440809.4	4601400.1	2184733.2	691538.2	14.4	123.5	Monopole	10.6	C167
W147	41.5653679	-81.7178134	440149.4	4601770.1	2182546.4	692714.9	14.8	123.3	Dipole	128.2	
M148	41.5725375	-81.7352346	438703.6	4602578.3	2177756.3	695285.0	15.4	124.9	Dipole	256.8	
W149	41.5990424	-81.7993035	433389.4	4605568.4	2160148.5	704795.2	17.1	113.6	Manopole	19.0	
W150	41.5999644	-81.8015504	433203.1	4605672.5	2159531.2	705126.2	17.1	118.5	Monopole	30.2	
W151	41.6010881	-81.8005671	433286.2	4605796.5	2159796.9	705537.8	17.1	23.4	Monopole	23.5	
M153	41.6006404	-81.7995452	433370.9	4605746.0	2160077.7	705377.0	17.1	32.3	Monopole	18.5	
W154	41.5735256	-81.7336781	438834.3	4602686.9	2178179.0	695648.7	15.5	33.7	Monopole	101.9	
M155	41.5693697	-81.7237252	439660.2	4602218.5	2180915.7	694158.6	14.9	28.8	Monopole	13.7	C102
M156	41.5686945	-81.7219413	439808.3	4602142.3	2181406.0	693916.9	14.9	34.7	Dipole	36.7	C121
M157	41.5683751	-81.7213093	439860.7	4602106.4	2181580.0	693802.1	14.8	29.0	Monopole	11.5	C129
M158	41.5675903	-81.7194811	440012.4	4602018.0	2182082.8	693520.6	14.8	26.0	Monopole	25.1	C138
M159	41.5663746	-81.7165652	440254.4	4601881.0	2182884.7	693084.8	14.8	24.7	Dipole	58.7	
M161	41.5653242	-81.7139834	440468.7	4601762.6	2183594.6	692708.4	14.2	26.2	Dipole	28.0	-
M163 M164	41.5652091 41.5396470	-81.7135192 -81.6654948	440507.3 444489.7	4601749.5 4598879.6	2183722.0 2196952.7	692667.6 683476.0	14.2	33.6 139.9	Dipole	91.4	C363
M165	41.5356470	-81.6761189	443611.4	4599894.1	2194013.1	686755.2	12.3	67.9	and the second se	108.8	C287
M166	41.5382546	-81.6654769	444490.0	4598725.0	2196962.5	682968.7	10.4	185.0	Dipole	25.8	C365
M167	41.5384707	-81.6661133	444437.1	4598749.4	2196787.5	683045.8	10.6	228.4	Dipole	144.4	6305
M169	41.5526855	-81.6847601	442894.2	4600339.7	2191634.4	688176.8	12.5	29.7	Monopole	11.0	
W170	41.5529418	-81.6852665	442852.2	4600355.7	2191495.0	688268.9	12.6	25.1	Dipole	26.6	
W171	41.5569863	-81.6951401	442032.4	4600824.1	2188779.0	689717.4	13.1	28.3	Monopole	52.0	-
#172	41.5572905	-81.6960727	441954.9	4600858.5	2188522.8	689825.9	13.2	36.2	Monopole	21.4	
W172	41.5573735	-81.6962019	441954.9	4600857.8	2188487.1	689855.8	13.2	33.3	Monopole	7.4	-
v174	41.5572908	-81.6959600	441964.3	4600858.4	2188553.6	689826.1	13.2	31.7	Dipole	75.1	
W175	41.5573982	-81.6961362	441949.7	4600870.5	2188505.0	689865.0	13.2	28.3	Monopole	12.3	
W176	41.5582030	-81.6981451	441782.9	4600961.2	2187952.5	690153.2	13.5	30.7	Monopole	17.5	
w177	41.5647373	-81.7140549	440462.2	4601697.5	2183577.0	692494.4	14.2	33.8	Dipole	58.7	
M179	41.5718504	-81.7312471	439035.4	4602499.2	2178849.6	695044.2	15.2	31.7	Dipole	32.0	CSD
W181	41.5758412	-81.7415576	438179.6	4602949.6	2176015.8	696473.6	15.7	57.1	Monopole	9.3	
V182	41.5920046	-81.7800926	434983.3	4604772.4	2165423.9	702273.7	16.8	29.0	Monopole	11.3	
4184	41.6004022	-81.8011538	433236.6	4605720.8	2159638.4	705286.6	17.1	61.6	Manopale	15.8	
4185	41.5992251	-81.7985377	433453.4	4605588.1	2160357.4	704863.5	17.0	65.1	Monopole	19.8	-
A186	41.5772457	-81.7451496	437881.5	4603108.1	2175028.6	696976.8	15.6	64.5	Monopole	11.1	1
1187	41.5729492	-81.7345112	438764.3	4602623.5	2177952.9	695436.7	15.4	55.8	Monopole	11.6	-
1188	41.5716811	-81.7313903	439023.3	4602480.5	2178810.9	694982.2	15.2	53.9	Dipole	9.7	
1189	41.5703497	-81.7282867	439280.8	4602330.5	2179664.4	694504.6	15.2	59.0	Dipole	11.2	
/190	41.5685808	-81.7239886	439637.5	4602131.1	2180846.2	693870.5	15.0	58.6	Monopole	8.7	
4191	41.5679971	-81.7225513	439756.8	4602065.3	2181241.4	693661.3	14.9	57.7	Dipole	9.5	
192	41.5668192	-81.7197856	439986.3	4601932.6	2182002.0	693238.9	14.6	61.3	Dipole	24.8	C137
4193	41.5594978	-81.7020637	441457.3	4601107.6	2186875.8	690615.1	13.3	62.1	Dipole	20.6	
/194	41.5594349	-81.7018892	441471.8	4601100.5	2186923.8	690592.6	13.3	61.2	Monopole	13.9	
/195	41.5579714	-81.6983177	441768.3	4600935.6	2187906.1	690068.4	13.5	60.1	Monopole	8.2	
/196	41.5571836	-81.6964709	441921.6	4600846.9	2188414.1	689786.0	13.3	62.6	Monopole	6,7	
4197	41.5566534	-81.6950753	442037.5	4600787.1	2188797.9	689596.3	13.1	58.1	Monopole	16.B	
/198	41.5526142	-81.6852246	442855.4	4600332.1	2191507.6	688149.6	12.5	55.3	Dipole	50.7	
4199	41.5506155	-81.6805272	443245.4	4600107.1	2192800.1	687433.4	12.5	61.0	Dipole	85.2	Concerned and
4200	41.5487343	-81.6760171	443619.9	4599895.3	2194041.0	686759.6	11.9	62.7	Dipole	163.8	C288
4201	41.5516852	-81.6790551	443369.1	4600224.9	2193199.3	687827.0	12.4	102.2	Dipole	27.6	
	41.5518646	-81.6788879	443383.2	4600244.7	2193244.5	687892.8	12.4	126.4	Monopole	7.9	
1202	41.5599115	-81.7003941	441595.9	4601152.4	2187331.3	690770.0	13.1	45.2	Monopole	8.4	0
						690949.2	14.1	162.2	Monopole	4.8	
4203	41.5604475	-81.7068565	441058.5	4601216.3	2185561.0	0000942.2	47.4			7.0	
4203 4204		-81.7068565 -81.7100979	441058.5 440792.8	4601216.3 4601775.7	2184657.4	692769.8	0.0	196.0	Dipole	61.2	
4202 4203 4204 4205 4206	41.5604475										-

					Marine Magne	stometer Anomalie	8) ()				
	NAD83 G	eographic	NAD83 UTM Zone 17		NAD83 Ohio S	tate Plane North	the share share to be	Distance		Amplitude	Associated
ID	Latitude	Longitude	Easting (m)	Northing (m)	East (US survey feet)	North (US survey feet)	Bathymetry (m)	from Proposed	Polarity	(nT)	Sidescan Contact ID
M211	41.5683874	-81.7216561	439831.8	4602108.0	2181485.1	693805.7	14.8	16.2	Monopole	22.7	C125
M214	41.5711257	-81.7263560	439442.5	4602415.3	2180190.2	694792.0	15.3	94.1	Monopole	14.1	C82
M215	41.5713403	-81.7261749	439457.8	4602439.0	2180239.0	694870.6	15.3	122.2	Monopole	61.7	C85
M216	41.5715103	-81.7260724	439466.5	4602457.8	2180266.5	694932.8	15.3	142.9	Monopole	14.0	C86
M217	41.6001150	-81.8016471	433195.2	4605689.3	2159504.4	705180.9	17.1	113.6	Monopole	32.9	
M218	41.6028241	-81.8045222	432958.4	4605992.3	2158710.1	706161.7	17.2	123.4	Dipole	79,7	1

Some of the magnetic anomalies were correlated to known sidescan contacts (targets). The remaining magnetic anomalies were not correlated to a sidescan contact or known lakebed installation such as a pipe or cable. There are a number of anomalies mapped on adjacent survey lines that may indicate the presence of a linear ferrous feature perpendicular to the proposed route at EKP 6.3 (Figure 18). This feature could not be identified from the sidescan or subbottom profiler data acquired over this area. An analysis of the magnetic data shows that the feature is most likely a buried steel or iron buoy block or anchor at the southwest contact with associated cable running to the northeast.

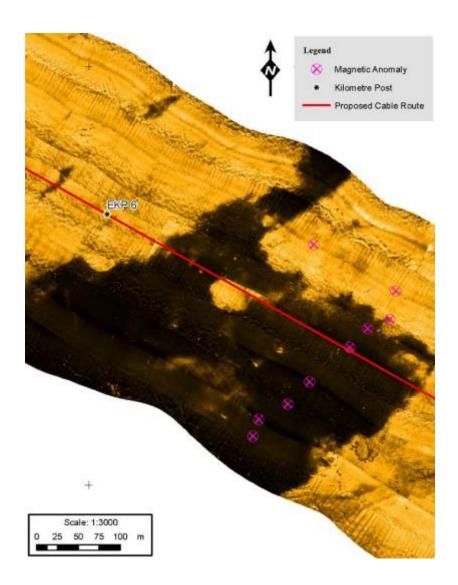


Figure 18 Location of linearly-aligned magnetic anomalies between EKP 6 and EKP 6.5. (CSR)

Past magnetic surveys in this area of the lake have also shown no correlation between the magnetic data and sidescan sonar imagery, with most of the magnetic hits having very small pole-to-pole distances indicating small or thin objects (Alpine, 2010)(VanZandt, 2015). This is primarily due to the proximity of the area being close to shore and used as a dumping ground for the past 200 years. Even today there are 5 dumping grounds identified on the latest Moss Point to Vermilion NOAA chart 14826 (Figure 19).

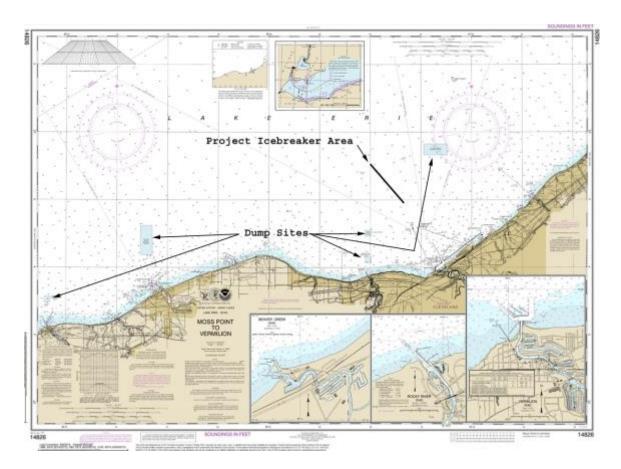


Figure 19 Current Dump Sites in Survey Areas (NOAA, VanZandt Engineering)

It is possible that some of the more magnetically intense anomalies are manmade but have no archaeological context, thus do not represent potentially significant resources. The less magnetically intense objects are most likely a function of geology, perhaps representing small pockets of glacial till or other magnetic rocks/sediment near the surface. In both cases, the Sidescan sonar imagery did not show any objects that would correlate with the anomalies. The lack of correlation is likely due to the magnetic objects being masked by overlying sediment.

## 5.3 Sub-bottom Data Analysis

A review of 271 line km of sub-bottom data showed no historic structures (such as shipwrecks) or artifacts were present within the turbine, export cable, and inner harbor areas.

The presence of gas charged sediments within the Icebreaker survey area was interpreted from chirp sub-bottom profiler and boomer seismic data. The presence of gas charged sediments can accentuate sub-bottom reflectors causing "bright spots" as well as prevent the penetration of the acoustic energy from the profiling system, thereby masking the acoustic signal.

The origin of the near surface gas in the survey area cannot be determined from the data collected from this survey. This gas may originate from shallow decomposed organic material (biogenic) or from deep underlying bedrock formations (petrogenic). In this area the biogenic source is plausible since vegetation has been buried during the numerous lake transgressions. This burial and subsequent decomposition could account for the presence of sub-surface gas.

Small localized erosional depressions or channels have been identified near the proposed WTG ICE1 turbine location (Figure 20) and over the near shore survey area. These features are infilled and were likely formed by glacial fluvial processes.

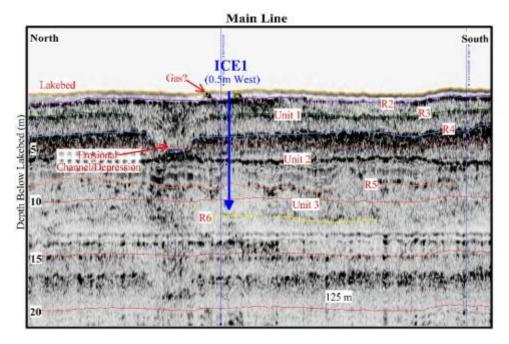


Figure 20 ICE 1 Erosional Depression or Channel (CSR)

#### 6.0 SECTION 106 REVIEW RESULTS

The purpose of this review was to determine if any prehistoric/historically significant artifacts, such as shipwrecks or human occupation sites, might be present in the three APEs in the construction area of the Icebreaker Wind project.

## **6.1 Prehistoric Results**

During the period from ~12,000 YBP to ~5,400 YBP the lake level was below the survey site so the possibility of prehistoric occupation sites does exist. A review of the Dames & Moore and Alpine geological data does not indicate the existence of any potential river systems or water sources that may have provided occupation sites for Paleoindians. A further literature review did not identify any past or ongoing research for the identification of prehistoric Lake Erie river systems.

Several small localized erosional depressions or channels were identified near the proposed ICE1 turbine location and over the nearshore survey area. These features are infilled and were likely formed by glacial fluvial processes. It is highly unlikely that these features contain prehistoric artifacts because erosional and sedimentation processes would have affected any prehistoric sites. This erosion would have mixed -- and destroyed -- the context of any site (Gray & Pape, 2014).

The impact of the project's construction to any prehistoric archaeological sites in the area would be negligible due to the small footprint that the foundation will occupy. Even though the mono bucket will be approximately 17.5 m (57 feet) in diameter and penetrate a maximum of 10 m (33 feet) deep into the lake bed and also into the glacial till layer, the disturbance area is small. This is due to the fact that the portion penetrating the lake bottom is only a cylindrical shell, like a biscuit cutter, not a solid object. The skirt thickness of the mono bucket is 3.175 cm (1.25 inches). The estimated surface area of disturbance for each WTG site is only 3.5 square meters (38 square feet). This coupled with the fact that the sub-bottom geology does not indicate any riverine structures leads to the conclusion that it is very unlikely that any prehistoric sites existed

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in the turbine APE or that its installation would impact such a site if it were to penetrate one at a thickness of 3.175 cm (1.25 inches.)

The interconnect cables in the turbine APE are buried at a depth of 1.5 m (4.5 feet) which is above these glacial till deposits. Their installation would not impact any potential prehistoric site.

The export cable, running to shore, is buried at a depth of 1.5 m (4.5 feet) and disturbance width of 1.5 m (4.5 feet). Several possible paleo-depressions/channels have been interpreted from the sub-bottom geology data and these are below the burial depth of the export cable. Any disturbance to any possible prehistoric site due to the small disturbance area seem unlikely.

The borehole for the HDD export cable will be well below any potential prehistoric site. The 0.6 m (18 inch) borehole will run from the breakwater, through the inner harbor, and exit at the CPP substation at a total depth of 18 - 27 m (60 - 90 feet) bottom level and a minimum of 4 m (12 feet) below the foundation of the breakwater.

## **6.2 Historic Results**

No properties of historical significance were identified by the survey at the Icebreaker Wind APEs.

## 7.0 CONCLUSIONS AND RECOMMENDATIONS

Results from the Section 106 review have confirmed that there were no artifacts or properties of historical significance identified within the Icebreaker Wind APEs. Moreover, the literature search produced no evidence of the existence of any artifacts or properties within the project's proposed APEs.

Based on this review, VanZandt Engineering concludes that the Icebreaker Wind project will have no impact on historic properties. VanZandt Engineering believes that no further archaeological investigation is required for this project and that project construction be approved. However, while the research and survey work for this project were thorough, no survey technique is completely adequate to identify all cultural resources in a given area. In the unlikely event any historic or prehistoric remains are discovered during project construction, the SHPO and/or VanZandt Engineering should be contacted to investigate and evaluate the significance of any such finds.

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