

# DOE/OE Transmission Reliability R&D Load as a Resource (LaaR)

## Frequency responsive demand

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# Project objectives

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- Provide a framework to facilitate large-scale deployment of frequency responsive end-use devices
- Systematically design decentralized frequency-based load control strategies for enhanced stability performance
- Ensure applicability over wide range of operating conditions while accounting for unpredictable end-use behavior and physical device constraints
- Test and validate control strategy using large-scale simulations and field demonstrations
- Create a level-playing field for smart grid assets with conventional generators



# Recap –FY12 activities

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- Extensive studies demonstrating potential of autonomous frequency load control performed on WECC model in PSLF
- Control strategies assumed **fixed** proportional response not considering changing bulk system conditions
- No systematic way of designing gains to ensure stability over wide range of operating conditions
- Simplistic end-use load models employed ignoring end-use behavior and physical device constraints



# Recap –FY13 activities

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## Task 1: Proposed hierarchical primary frequency control strategy

- Supervisory controller design based on robust control theory to ensure stability over a wide range of operating conditions.
- Control gains updated every few minutes allows for adaptation to time-varying system operating conditions
- Local load response rules incorporate physical device constraints and respect end-use behavior
- Studies performed on 16 machine IEEE test system to demonstrate proof-of-concept



# Recap –FY13 activities contd.

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Task 2: Studied system impacts of Grid-Friendly™ Appliances for under-frequency load shedding

- Location of GFAs affects system stability performance
- Impact of location is coupled with time delay
- Need further investigation into how many GFAs to deploy across the system
- Develop systematic GFA control design such that aggregate response mimics generator “droop” like response



# FY14 tasks

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Task 1: Modify design of hierarchical control strategy

- Responds to only frequency deviation
- Respect actual response capability of load population
- Allow for simple and scalable implementation

Task 2: Validation of modified control strategy on large-scale systems

- Implement on WECC model in PowerWorld

Task 3: Modify GFA design to mimic droop response

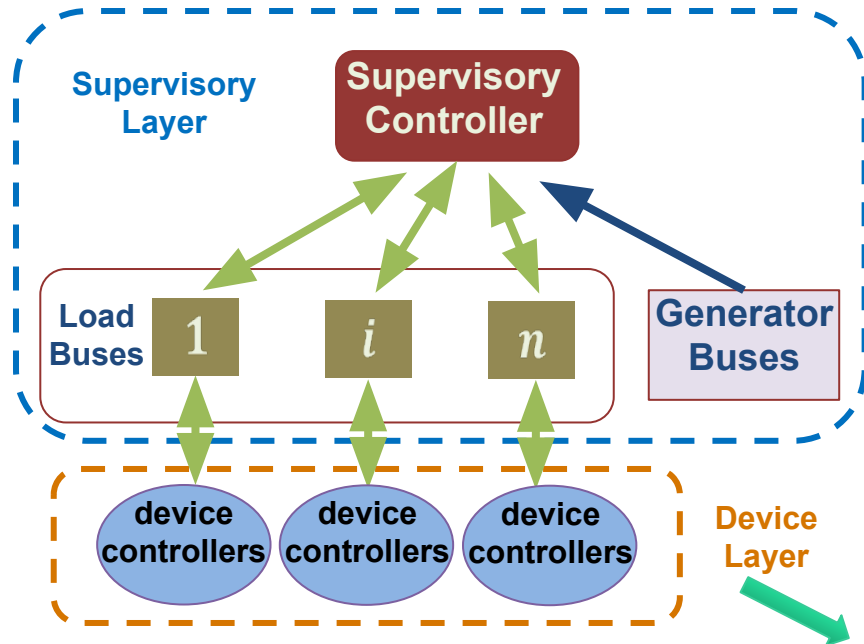


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# TASK 1: EXTEND DESIGN OF HIERARCHICAL CONTROL STRATEGY



# Hierarchical control strategy



## Every few minutes

- Collect information on current operating condition of each participating device
- Compute desired load bus control gains
- Broadcast control gains and system states to individual devices

## Real time

- Respond independently to meet desired aggregated power consumption
- Respect end-use physical constraints





# Supervisory Control Gain Design

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- Desired aggregated response  $\Delta P_i = k_i(f_i(t_k) - 60\text{hz})$

$$k_i = K_{sys} * K_{bus} = \frac{pct_{max,load} P_{load,sys}}{\Delta f_{min}} * \frac{pct_{cont,ON} P_{cont,i}}{P_{cont,sys}}$$

- Update gains only needed when there are significant changes in system load and/or controllable load

$\Delta f_{min}$  – frequency deviation threshold that activates load control before emergency under-frequency load shedding

$pct_{max,load}$  – maximum percentage of total system load that should act at  $\Delta f_{min}$

$pct_{cont,ON}$  – percentage of controllable load in ON state

$P_{cont,sys}$  – total controllable load available system-wide

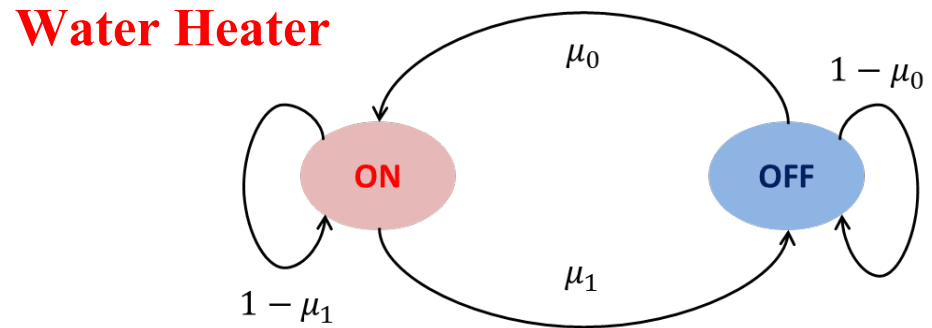
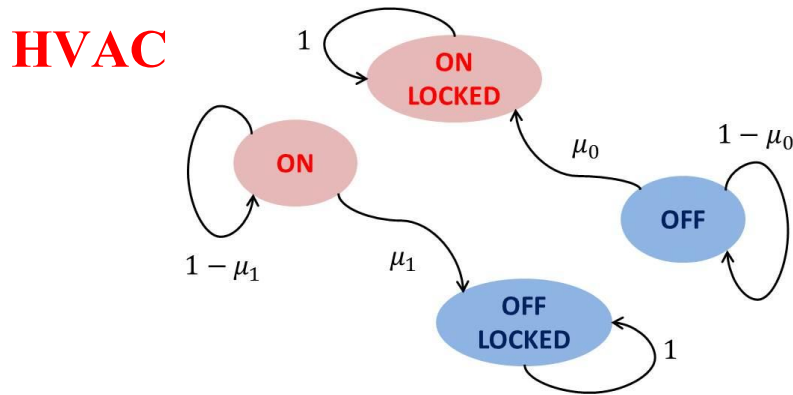
$P_{cont,i}$  – total controllable load available at a substation bus  $i$

$P_{load,sys}$  – total load available system-wide



# Device Layer Control

- Consider thermostatically controlled loads (HVACs, water heaters, etc.)



$$\mathbf{p}(t_k) = \begin{bmatrix} p_{\text{ON}}(t_k) \\ p_{\text{OFFLCK}}(t_k) \\ p_{\text{OFF}}(t_k) \\ p_{\text{ONLCK}}(t_k) \end{bmatrix} \quad \mathbf{A}(t_k) = \begin{bmatrix} 1 - \mu_1(t_k) & 0 & 0 & 0 \\ \mu_1(t_k) & 1 & 0 & 0 \\ 0 & 0 & 1 - \mu_0(t_k) & 0 \\ 0 & 0 & \mu_0(t_k) & 1 \end{bmatrix}$$

$$\mathbf{p}(t_k) = \begin{bmatrix} p_{\text{ON}}(t_k) \\ p_{\text{OFF}}(t_k) \end{bmatrix} \quad \mathbf{A}(t_k) = \begin{bmatrix} 1 - \mu_1(t_k) & \mu_1(t_k) \\ \mu_0(t_k) & 1 - \mu_0(t_k) \end{bmatrix}$$

- Derive Markov chain model  $\mathbf{p}(t_{k+1}) = \mathbf{A}(t_k)\mathbf{p}(t_k)$
- Calculate switching probabilities  $\mu_0$  and  $\mu_1$  based on desired power reference from supervisory control layer  $\Delta P_i(t_k) = k_i(f_i(t_k) - 60\text{Hz})$



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# TASK 2: VALIDATION OF MODIFIED CONTROL STRATEGY ON LARGE- SCALE SYSTEMS



# PowerWorld implementation

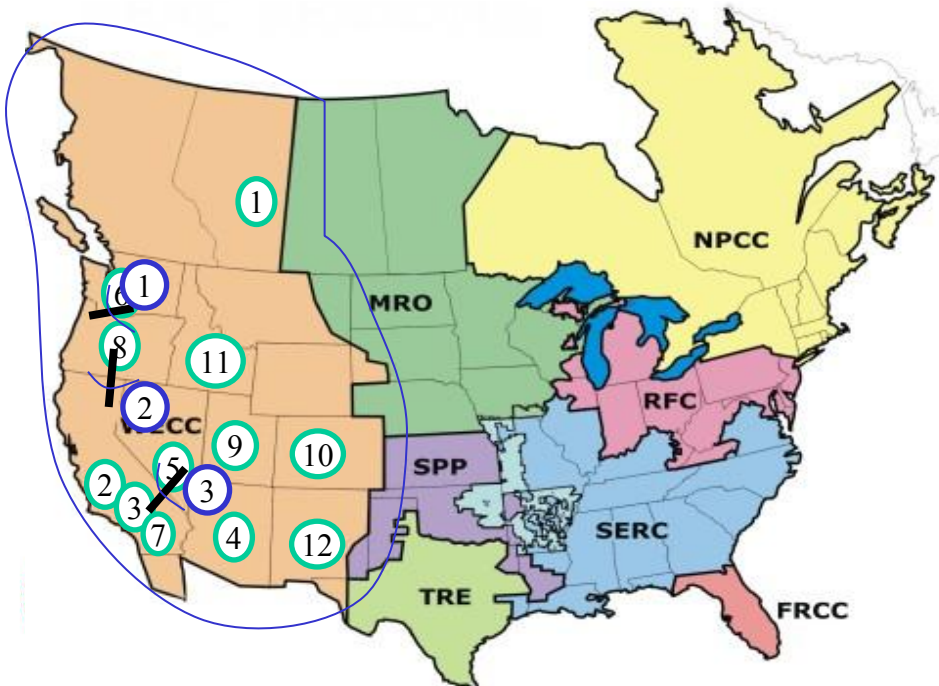
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- User defined model for loads implemented in PowerWorld (transient stability application module) using VS C++ 2010 as a DLL
- Implemented as modified WSCC load model (ZIP load)
- Active power load defined based on:
  - Controller model: Markov chain with controlled probabilities based on  $\Delta P_i = k_i(f_i(t_k) - 60\text{hz})$
  - Impedance part of ZIP load is controlled only (OK for water heaters, crude approximation for HVAC)
- Reactive power changes as portion of changes in active power to represent effect of reactive power consumptions of distribution networks and substations as the end use load changes



# WECC test scenarios

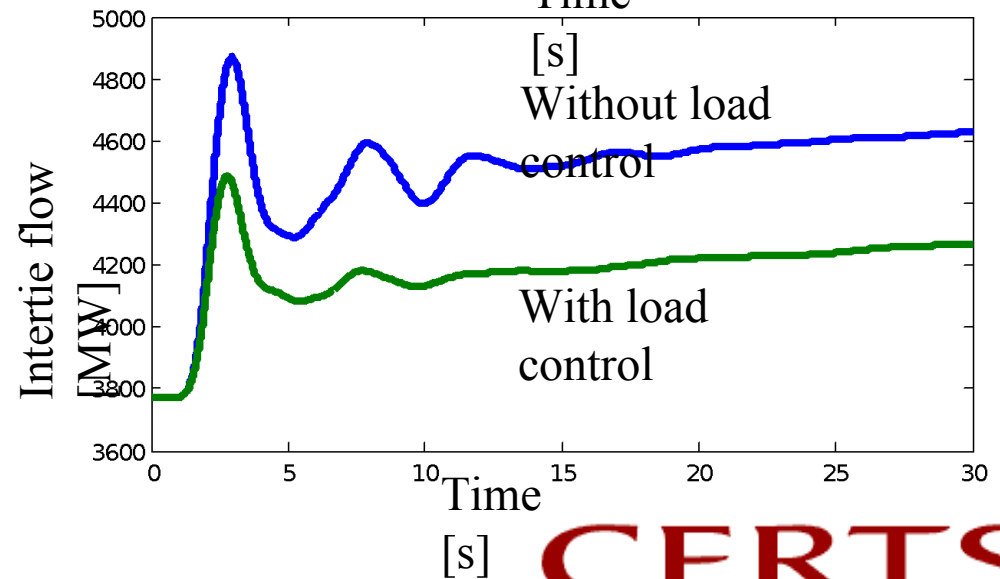
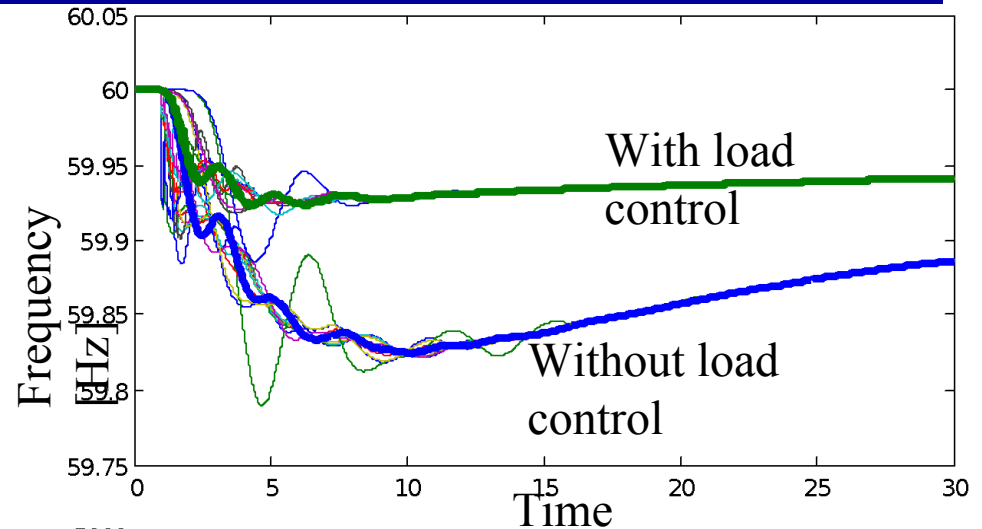
- WECC system
  - # of buses: 20,000
  - # of generators: 3,900
  - # of transmission lines: 16,000
  - # of loads: 10,800
- 12 loads monitored
- 3 interties monitored



- 140 loads are controlled
  - Total 40,100 MW
  - Test cases with 30% and 100% controllable
  - Test cases with initial state of loads: 40% and 80% in on state
- WECC high summer 2014
  - Total load: 167 GW
  - Total generation output: 173 GW
- WECC low winter 2022
  - Total load: 109 GW
  - Total generation output: 113 GW

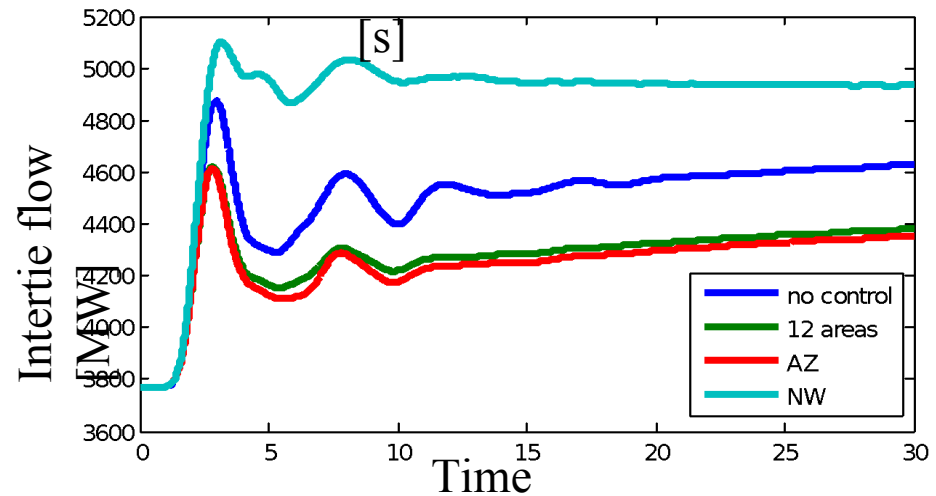
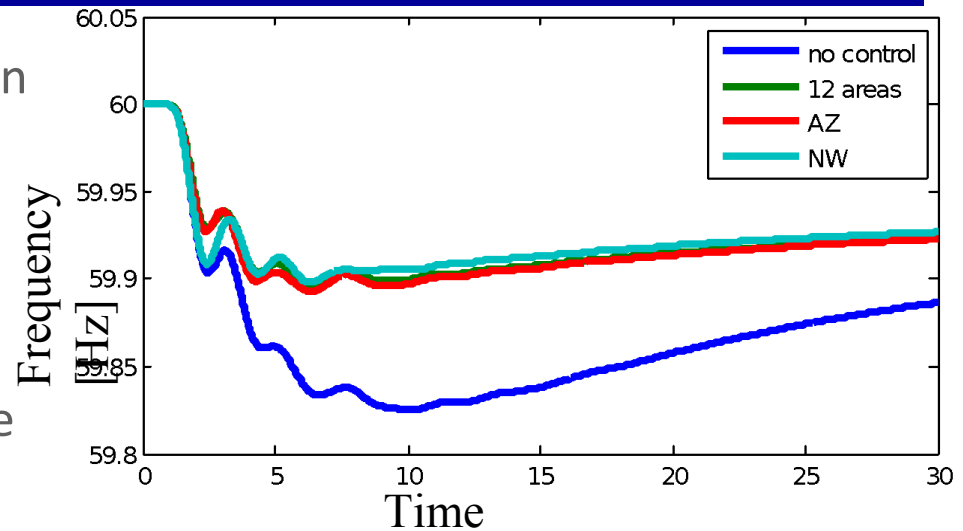
# WECC with and without control

- WECC high summer 2014 case considered
- Better frequency recovery in terms of steady state error and maximum frequency deviation
- Less transmission capacity needed for PFC in intertie 2 (North to South transfer)



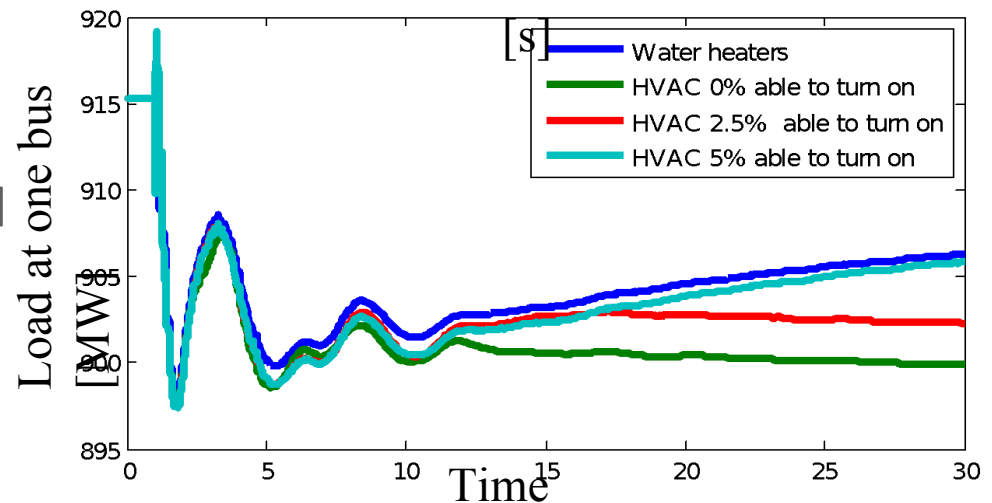
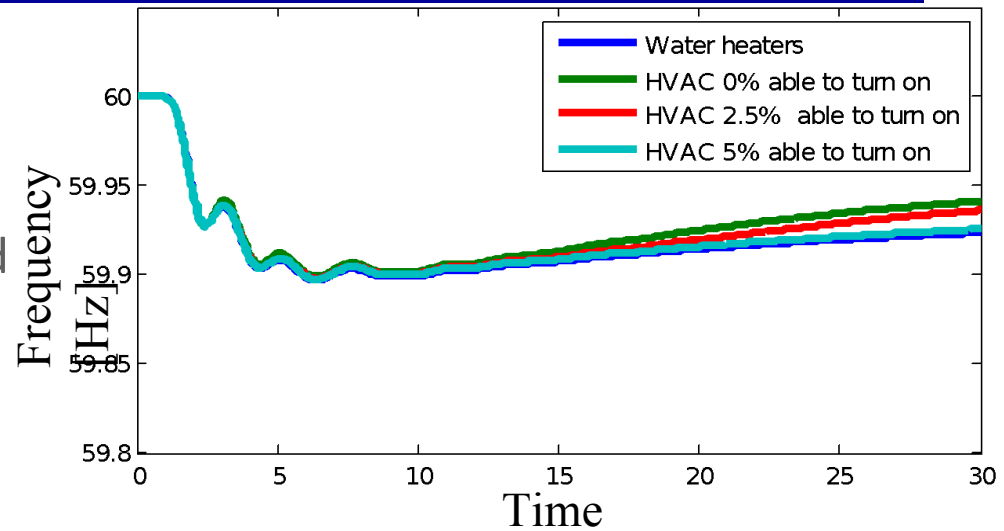
# Sensitivity to location of controllable loads

- Controllable load concentrated in different locations:
  - Arizona (AZ)
  - Northwest (NW)
  - Distributed (12 areas)
- Disturbance located South of the system
- Inertie power flow response depends on relative location of disturbance and load/generation providing PFC
- Load control could be used as additional resource in areas with lack of generation, like south of WECC in summer



# Sensitivity to type of loads

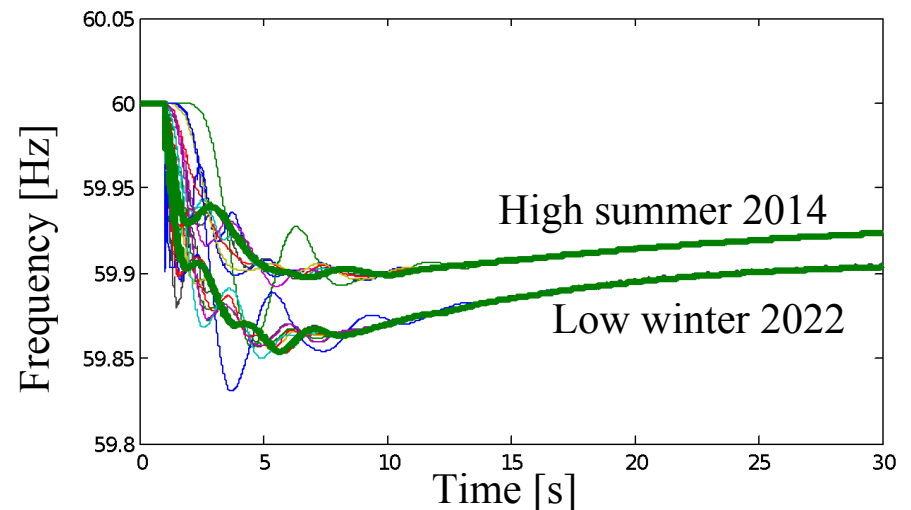
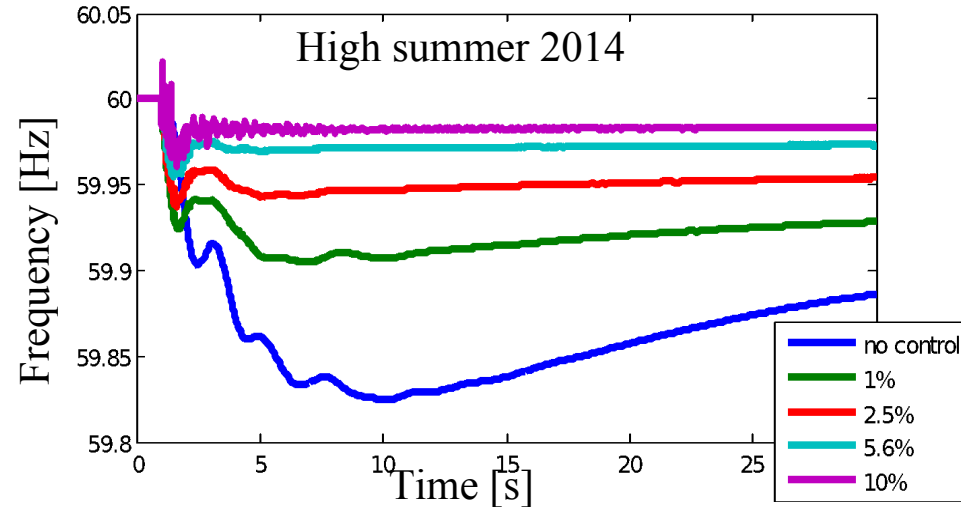
- HVAC loads compared with water heaters
  - HVAC lock out time modeled
  - Different % of HVAC in OFF state that can be turned back ON when frequency recovers
- HVAC cycle dynamics affect steady-state frequency and has a high impact on bus load response





# Sensitivity to control gain parameters

- High penetration of controllable load increases gain which decreases steady state error & improves transient response
- Large gains (10% penetration) produces “chattering” associated with discrete nature of implementation
- 1% penetration case also tested in future case of 2022 obtaining acceptable performance



# Conclusions -Tasks 1& 2

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- Control strategy implemented and tested on WECC 2014 and 2022 scenarios
  - Improved frequency recovery in terms of steady state error and maximum frequency deviation
  - Inertie power flow response depends on relative location of disturbance and responsive load/generation
- Load control could be used as additional resource in areas with lack of generation (e.g. south of WECC in summer)
- Dynamics of different types of end-use loads (i.e. HVAC vs. water heaters) affect control performance
- Control gain can be adapted based on desired penetration and changing operating conditions

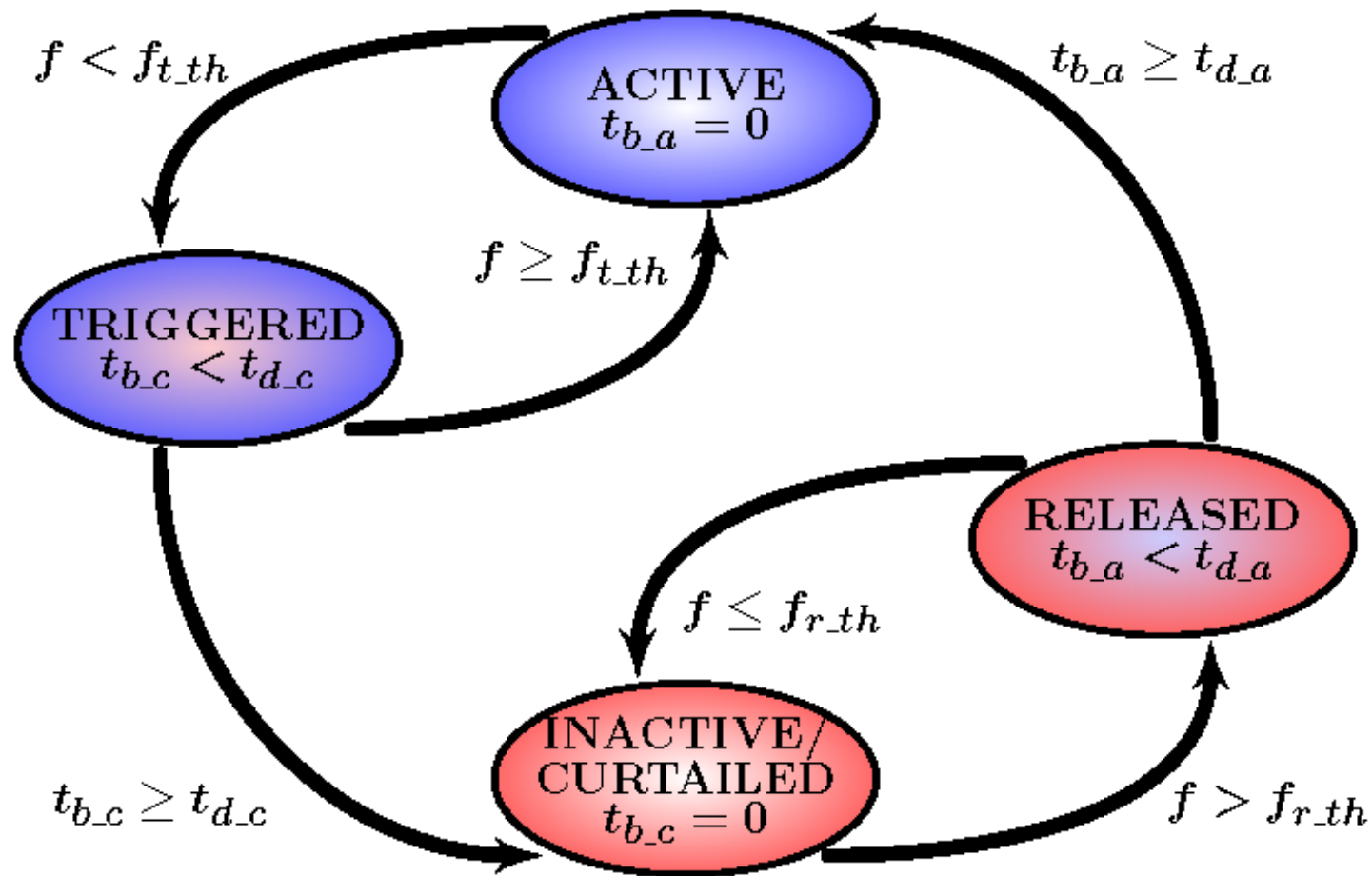


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# TASK 3: MODIFY GFA DESIGN TO MIMIC DROOP RESPONSE



# Grid Friendly Appliance Control Logic



# Controller Design and Analysis

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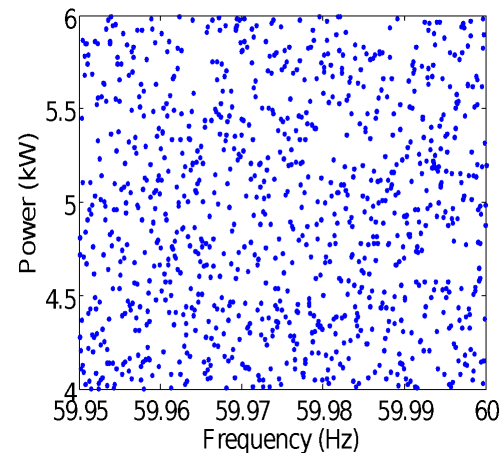
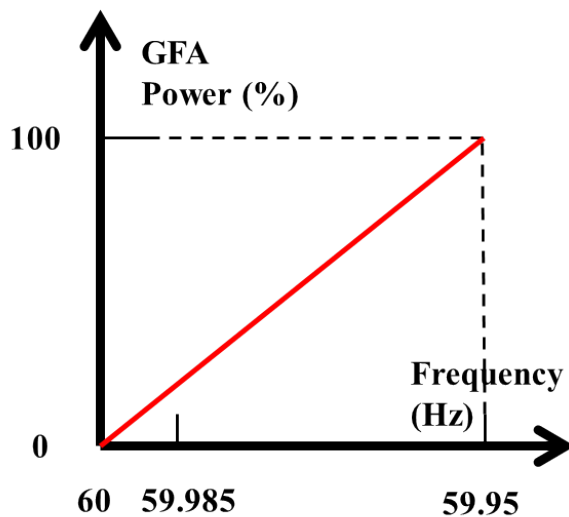
- Cutoff frequency  $f_{t_{th}}$  of each GFA controller is randomly selected from prescribed frequency range between 59.95 Hz and 59.985 Hz
- Autonomous response may not mimic droop-like response in practice
  - Cutoff frequencies of GFAs currently ON may not be uniformly distributed
  - Power of each GFA currently ON can be quite different



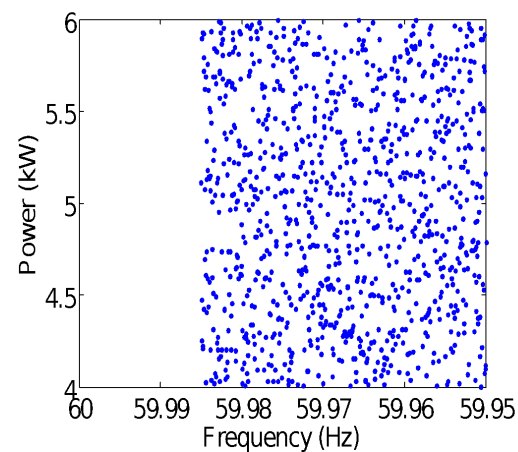
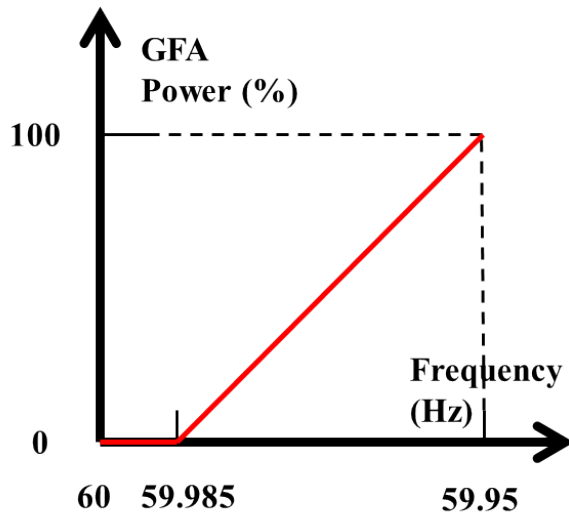
# Power reduction vs frequency deviation

## -Normal case

Desired behavior  
(droop-like)



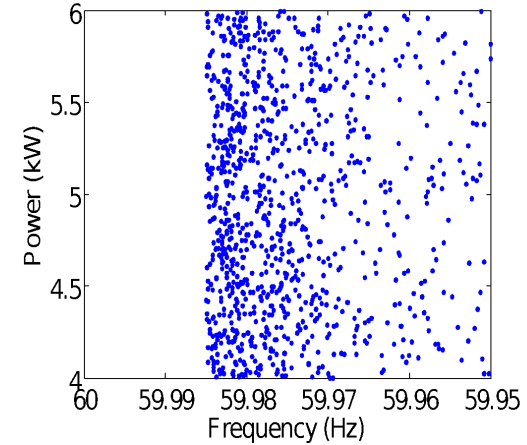
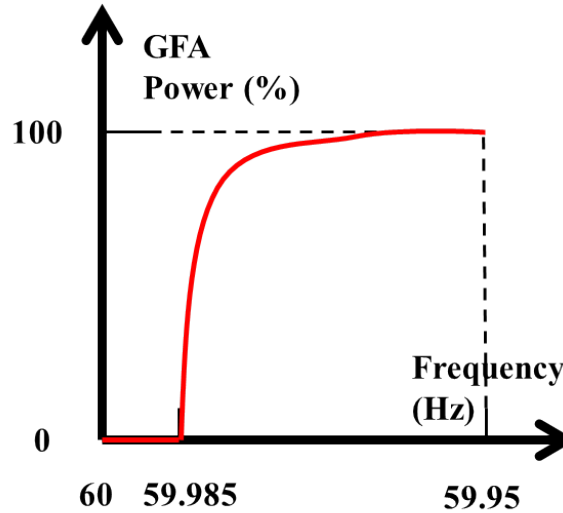
Normal behavior  
(cutoff frequencies  
are uniformly  
distributed)



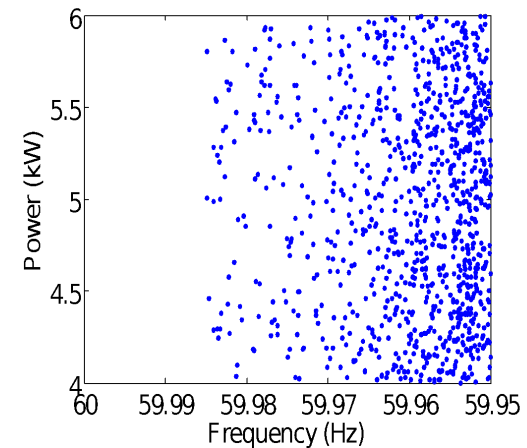
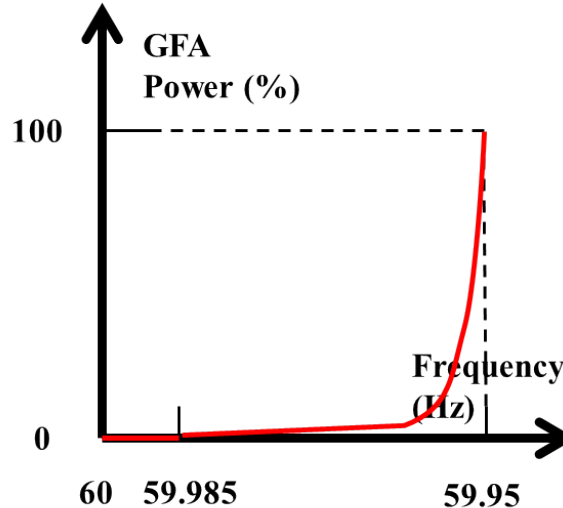
# Power reduction vs frequency deviation

## –Extreme cases

Unexpected behavior (cutoff frequencies are biased to the left)

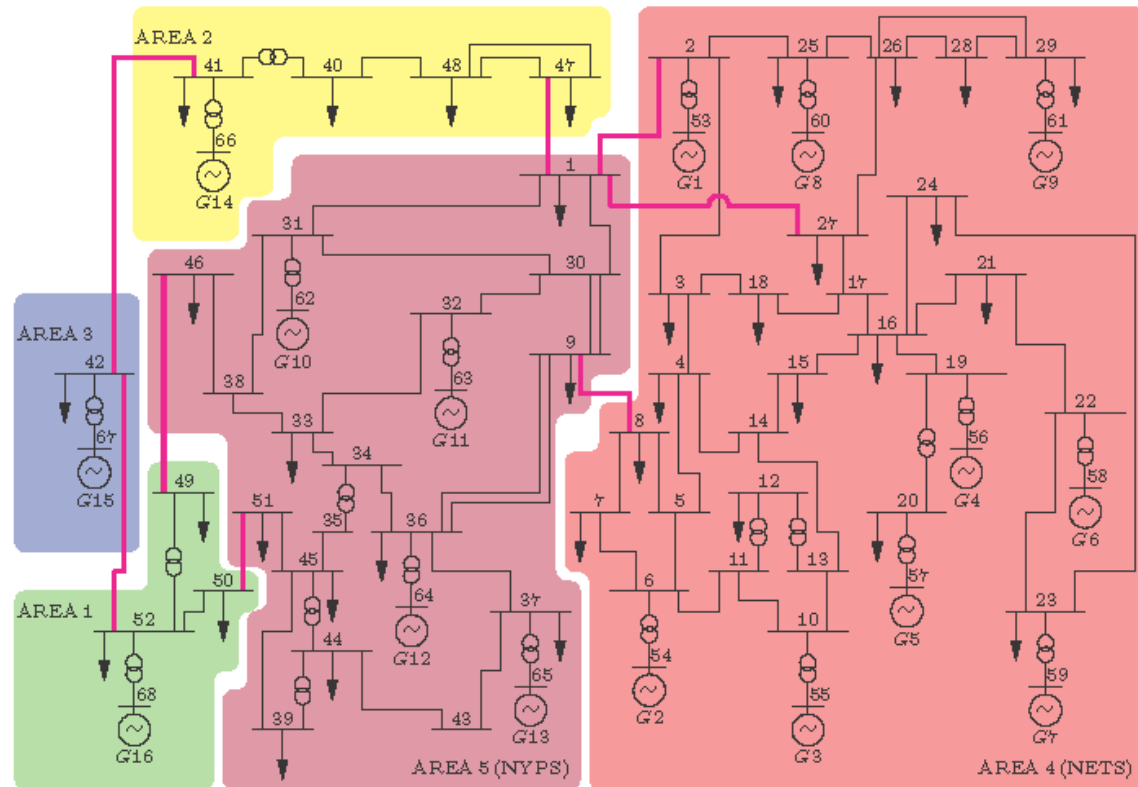


Unexpected behavior (cutoff frequencies are biased to the right)



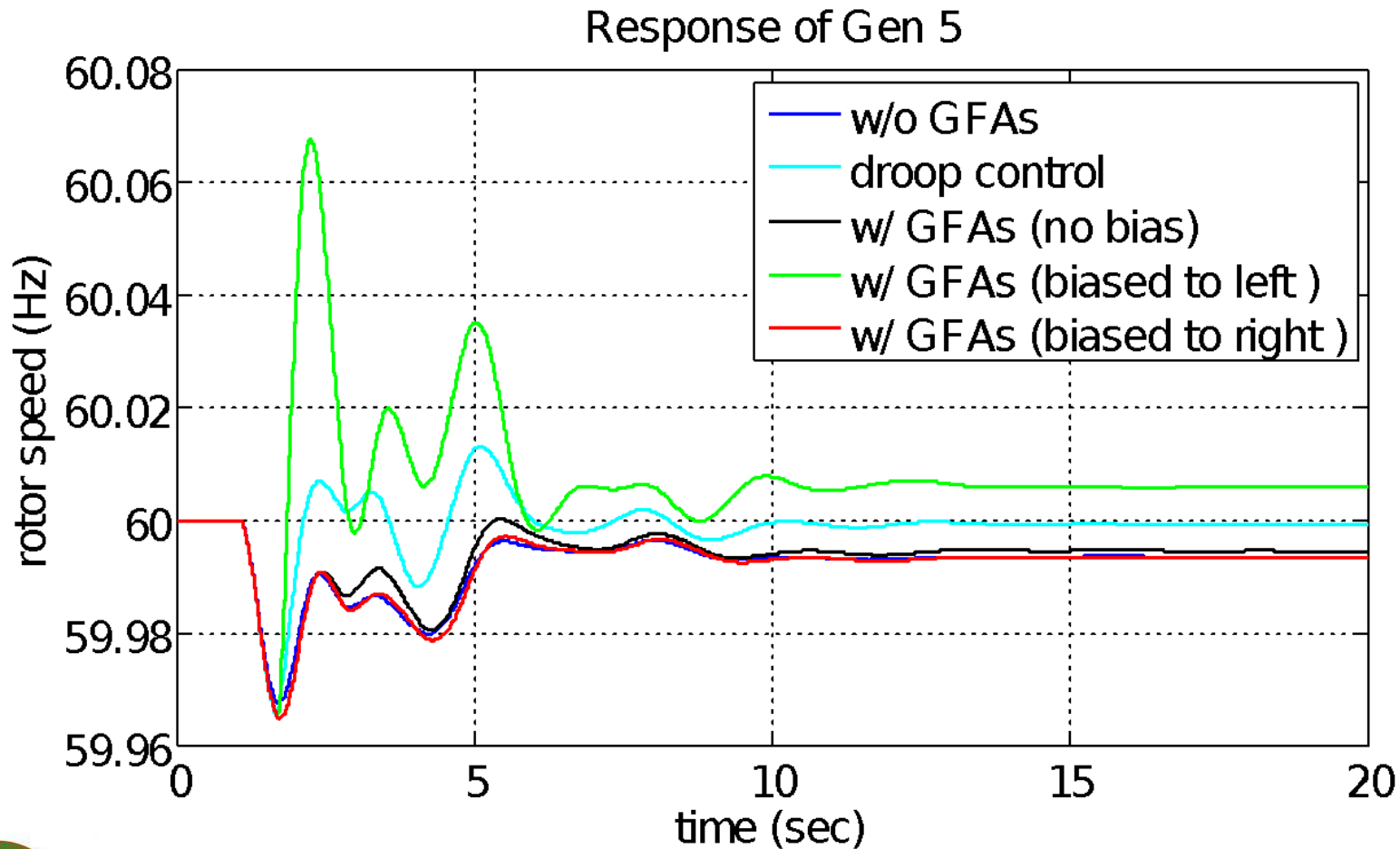
# Test System

- IEEE 68-bus system
- GFA = Water heater
- 11% of total load in area 4 and area 5 (~1350 MW)
- Evenly distributed in area 4 and area 5
- Case One: Generator 1 was tripped
- Case Two: Generator 12 was tripped

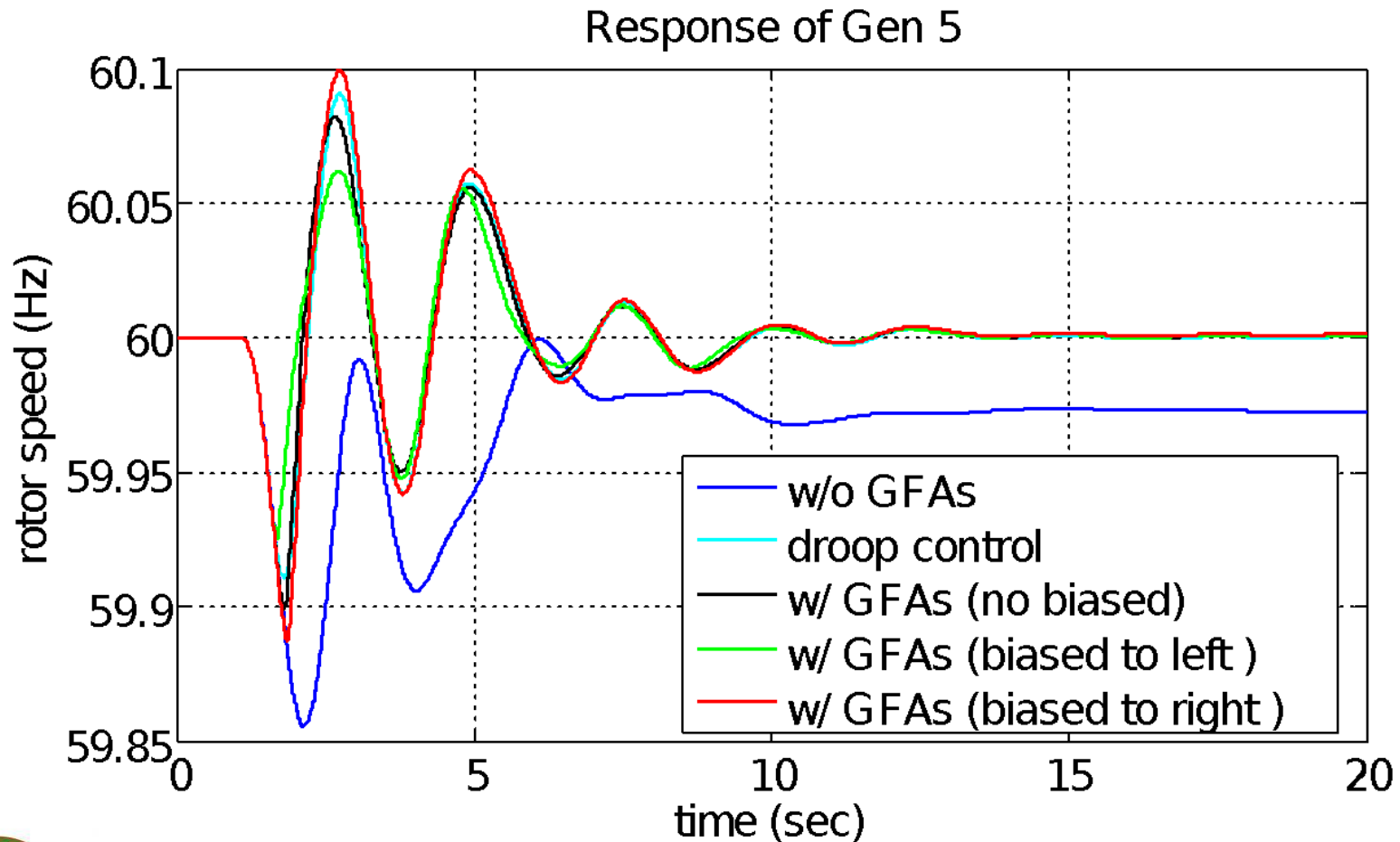




# Case One — Small Disturbance



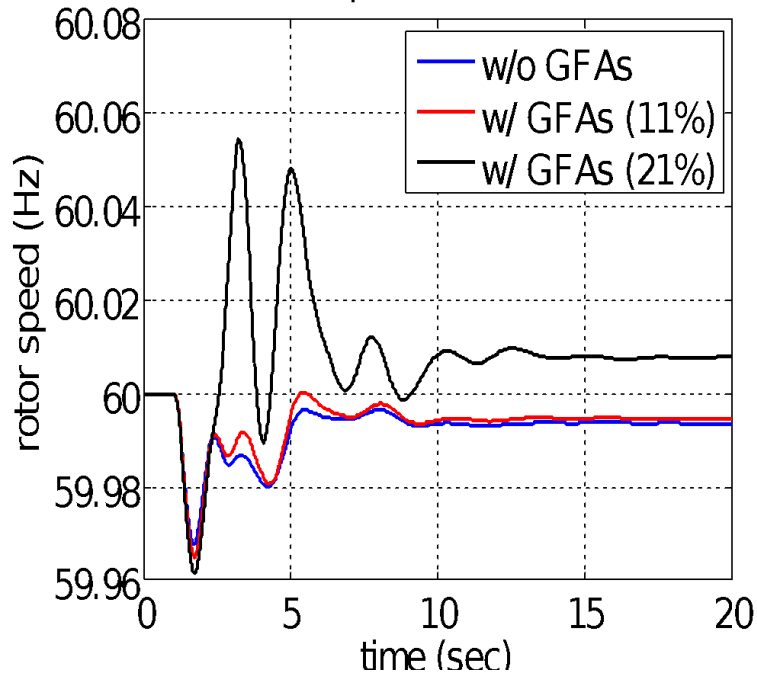
# Case Two — Large Disturbance



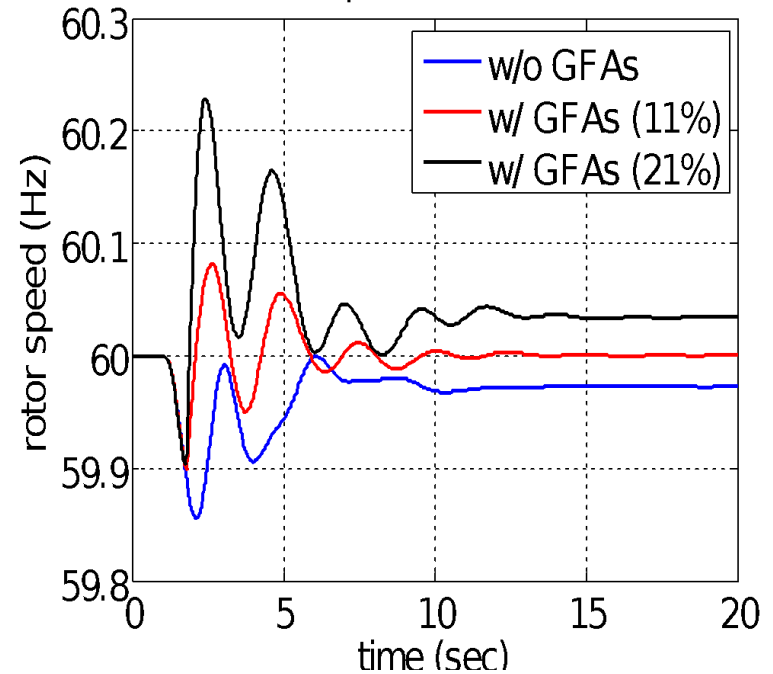
# Higher penetration of GFAs

- 21% of total load in area 4 and area 5 (~2700 MW)

Small Disturbance  
Response of Gen 5



Large Disturbance  
Response of Gen 5



# Conclusions –Task 3

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- Derived boundaries to characterize system frequency performance under GFA control
- Droop-like desired response can not always be guaranteed due to random selection of cut-off frequencies
  - For small disturbances difference between desired response and actual response could be substantial
  - For large disturbances such differences are small
- Increasing penetration level leads to worse performance due to fixed cut-off frequency range



# FY15 & beyond planned activities

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- Hierarchical control strategy
  - Analyze interactions and integration of proposed control strategy with primary and secondary generator frequency controls and UFLS schemes
  - Study voltage “side effects” i.e. unintended consequences related to inherent modulation of reactive component of load while load is under primary frequency control
- Large-scale testing and validation studies
  - Improve representation of effect of distribution network and type of loads (e.g.; WECC composite load model or combine with feeder models in GridLAB-D)
  - Implement proposed hierarchical control strategy in integrated transmission & distribution environment (e.g. PowerWorld+ GridLAB-D)



# FY15 & beyond planned activities

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- GFA modeling and control design
  - Implement new GFA design in PowerWorld on the WECC system model
  - Perform extensive simulation studies to confirm FY14 findings regarding system response characterization
  - Enhance existing control design to deal with high penetration levels
- Preliminary field testing
  - Perform hardware-in-the-loop tests in PNNL lab homes for primary frequency control
- Outreach
  - Develop roadmap that outlines a strategy engaging various stakeholders (e.g. industry, utilities, WECC)

