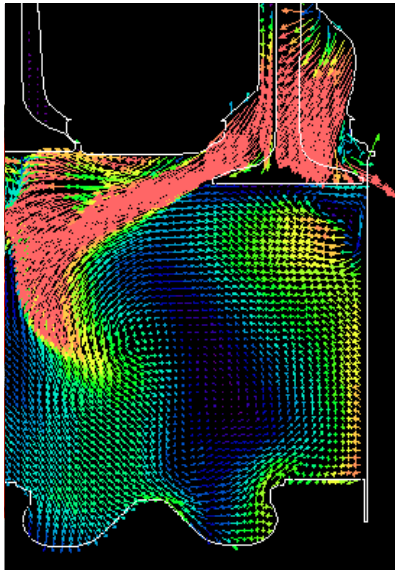
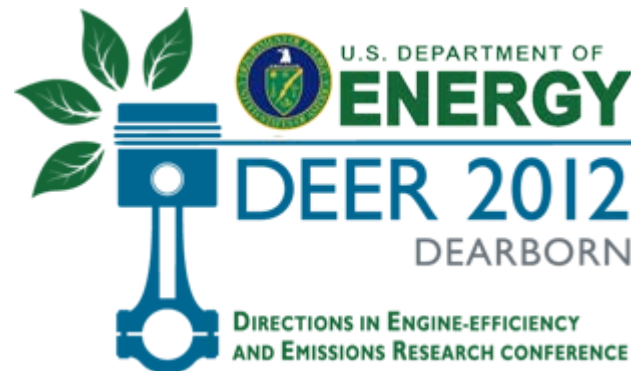


# Estimation and Control of Diesel Engine Processes Utilizing Variable Intake Valve Actuation



**Lyle E. Kocher**  
Technical Advisor  
Advanced Engineering

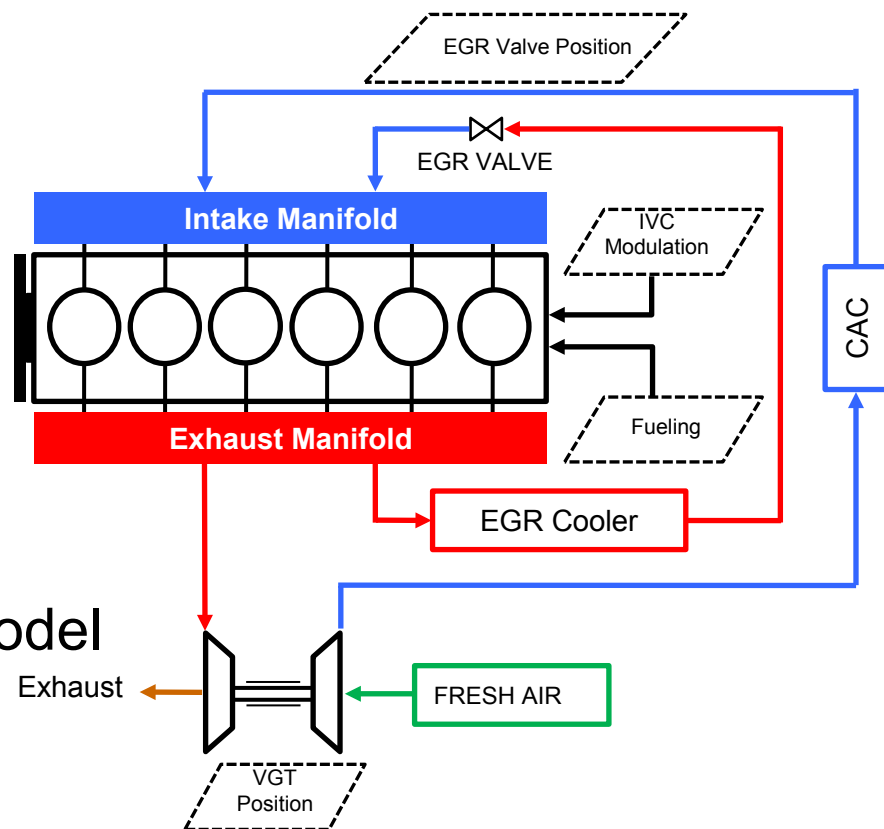




# Presentation Overview



- Experimental Test Bed
- Model Based Approach
- Gas Exchange Model
  - Manifold Filling Dynamics
  - Volumetric Efficiency
  - Oxygen Fraction Dynamics
- Combustion Model
  - PCCI Combustion Timing Model
- Controller Development
  - PCCI Combustion Timing
- Summary



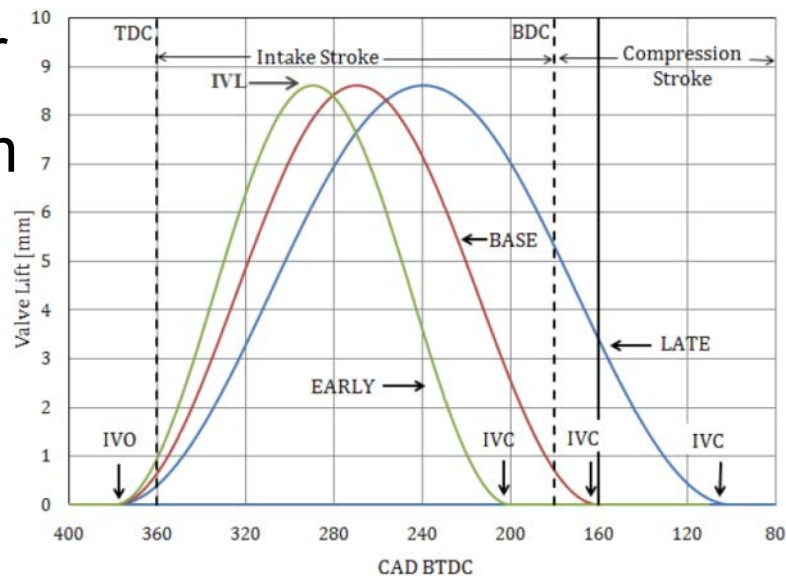
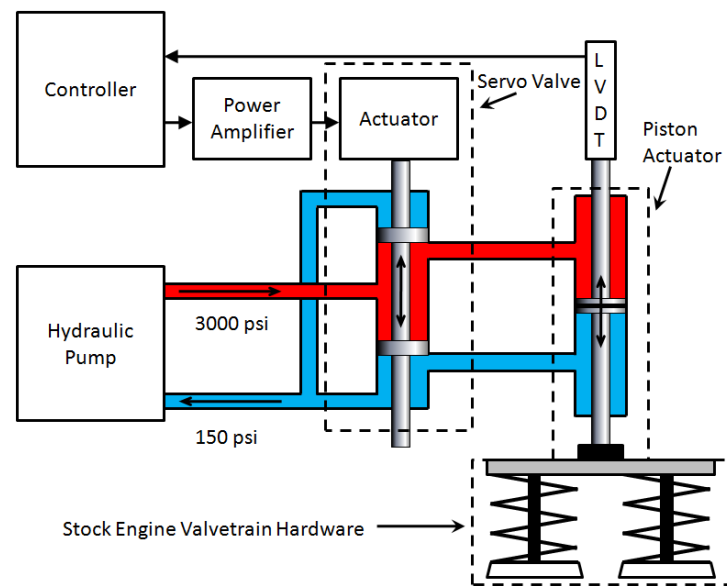


# Experimental Test Bed



## 2010 Cummins ISB

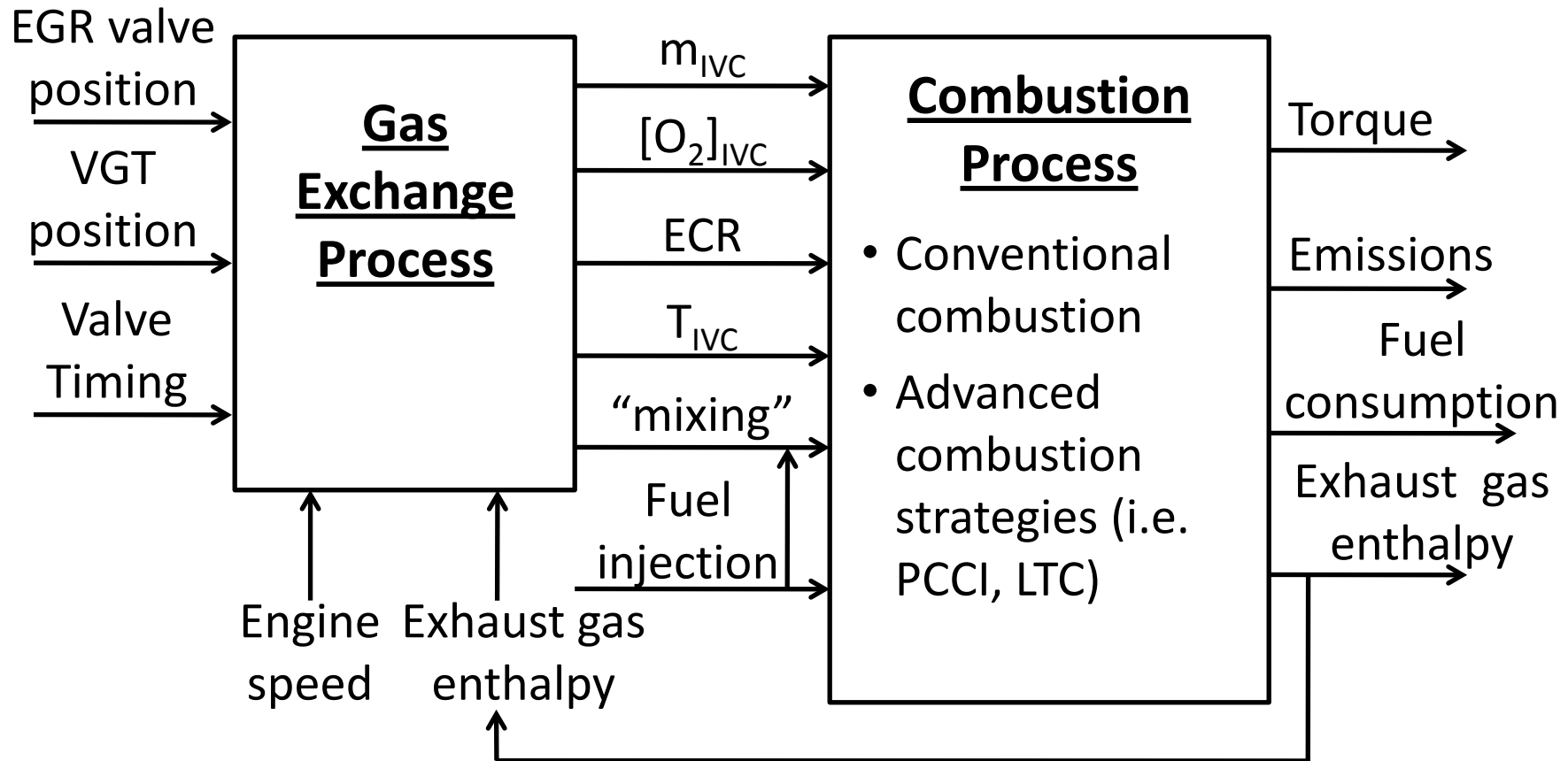
- 360 HP (268 kW)
- 17.3:1 Compression Ratio
- Common Rail Fuel Injection
- Air-Handling System
  - Exhaust Gas Recirculation Valve
  - Variable Geometry Turbocharger
- Variable Valve Actuation System
  - Electro-Hydraulic System
  - Cylinder Independent
  - Cycle-to-cycle



Innovation You Can Depend On



# Model Based Approach



- Physically-based generalizable models
- Validated experimentally
- Validated via analysis (math-based stability, convergence rate, and sensitivity/uncertainty analysis)

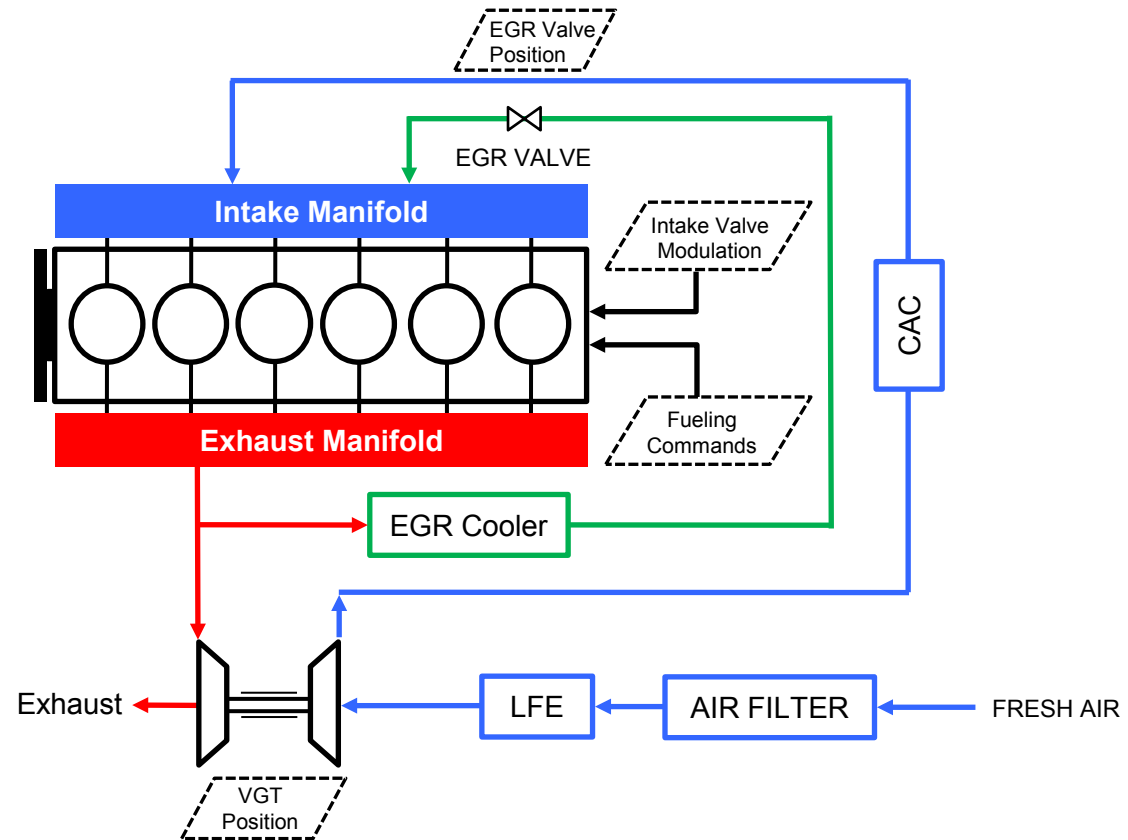




# Gas Exchange Model



- 5 Model States
  - Intake Manifold
    - Pressure
    - Temperature
  - Exhaust Manifold
    - Pressure
    - Temperature
  - Turbo Shaft Speed





# Gas Exchange Model



## Intake Manifold State Equations

$$\dot{p}_{im} = \frac{\gamma_{im} R_{im}}{V_{im}} (W_{egr} T_{egr} + W_c T_{cac} - W_e T_{im})$$

$$\dot{T}_{im} = \frac{R_{im} T_{im}}{P_{im} V_{im}} \left[ W_{egr} (\gamma_{im} T_{egr} - T_{im}) + W_c (\gamma_{im} T_{cac} - T_{im}) + W_e (T_{im} - \gamma_{im} T_{im}) \right]$$

## Exhaust Manifold State Equations

$$\dot{p}_{em} = \frac{\gamma_{exh} R_{exh}}{V_{em}} \left[ (W_e + W_f) T_{exh} - W_{egr} T_{em} - W_t T_{em} \right]$$

$$\dot{T}_{em} = \frac{R_{em} T_{em}}{P_{em} V_{em}} \left[ (W_e + W_f) (\gamma_{em} T_{exh} - T_{em}) + W_{egr} (T_{em} - \gamma_{em} T_{em}) + W_t (T_{em} - \gamma_{em} T_{em}) \right]$$

## Turbocharger Speed State Equation

$$\dot{\omega}_{tc} = \frac{\eta_m P_{turb} - P_{comp}}{I_{turb} \omega_{tc}} \quad P_{turb} = W_{turb} c_{p,exh} \eta_t T_{em} \left[ 1 - \left( \frac{P_{amb}}{P_{em}} \right)^{\frac{\gamma-1}{\gamma}} \right] \quad P_{comp} = \frac{W_{comp} c_{p,amb} T_{amb}}{\eta_c} \left[ \left( \frac{P_{cac}}{P_{amb}} \right)^{\frac{\gamma-1}{\gamma}} - 1 \right]$$





# Gas Exchange Model



## Volumetric Efficiency Model

$$W_e = \rho_{im} \eta_{vol} V_d \frac{N}{2}$$

$$\eta_{vol} = \frac{\left( P_{im} \left( \frac{V_{ivc_{eff}}}{V_{ivc}} \right)^k V_{ivc} c_v - P_{em} V_{ivo} c_v - P_{em} (V_{evc} - V_{ivo}) c_p + P_{im} (V_{ivc_{eff}} - V_{ivo}) R - h_{ivo-ivc} (T_{wall} - T_{im}) A_{s_{ivo-ivc}} R \right)}{P_{im} V_d c_p}$$

## Exhaust Enthalpy Model

$$T_{evo} = \frac{P_{im}}{m_c R_{im}} \frac{ECR^{k_a}}{V_{evo}^{k_e - 1}} \left( \frac{k_e - 1}{k_e} \frac{(a \cdot N + b) m_f Q_{LHV}}{P_{im} ECR^{k_a}} + V_{tdc} \right)^{k_e}$$

## Analytical Turbocharger Performance Functions

$$W_c = f(PR_c, N_{turb}) \quad W_t = f(PR_t, N_{turb})$$

$$\eta_c = f(PR_c, N_{turb}) \quad \eta_t = f(PR_t, N_{turb})$$



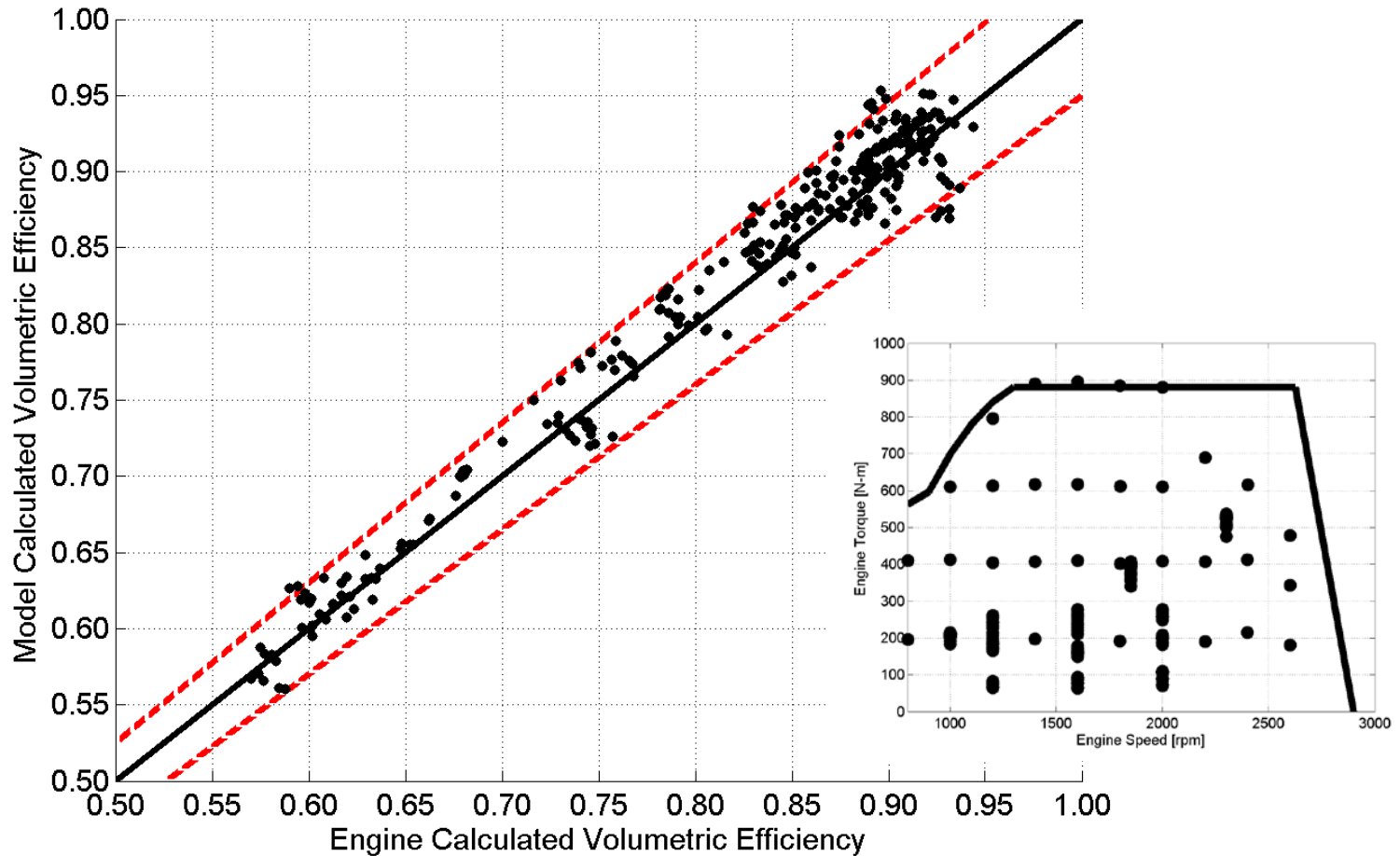




# Gas Exchange Model



## Volumetric Efficiency Model Results



$\pm 5\%$  Lines    2.5% RMS Error





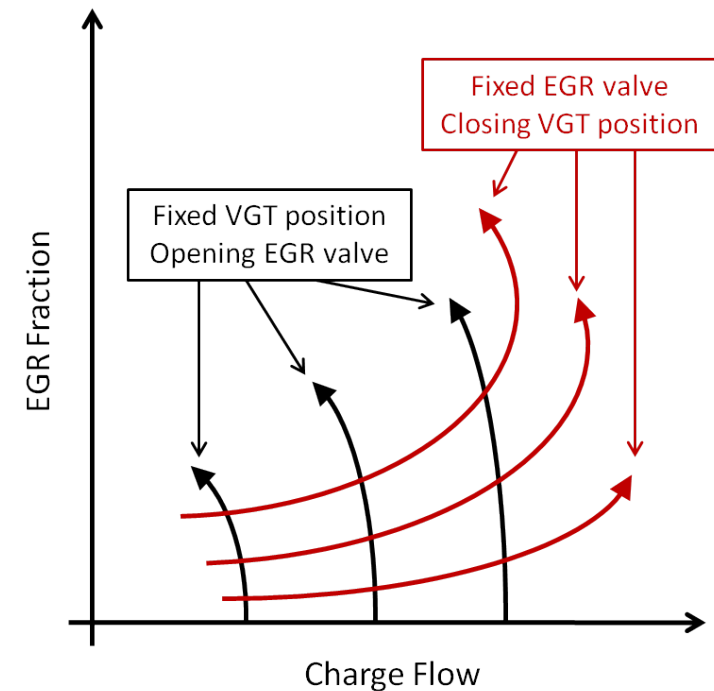
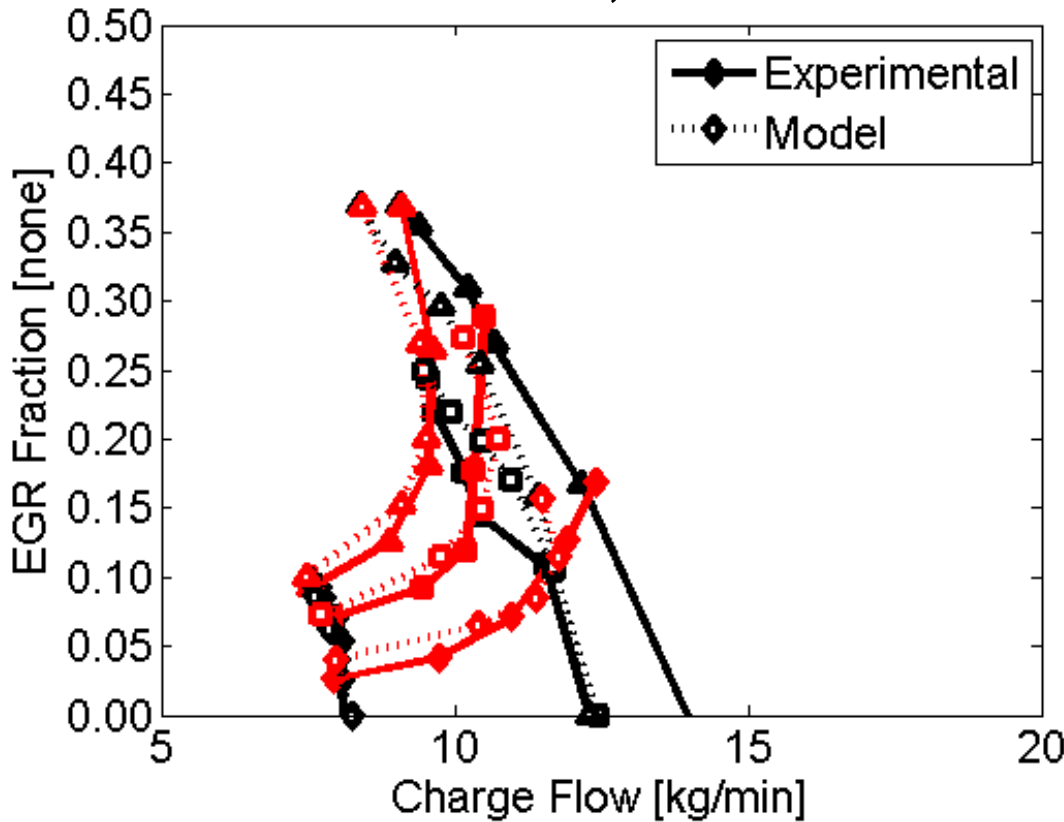


# Gas Exchange Model



## Gas Exchange Model Results

1850 RPM, 300 ft-lb





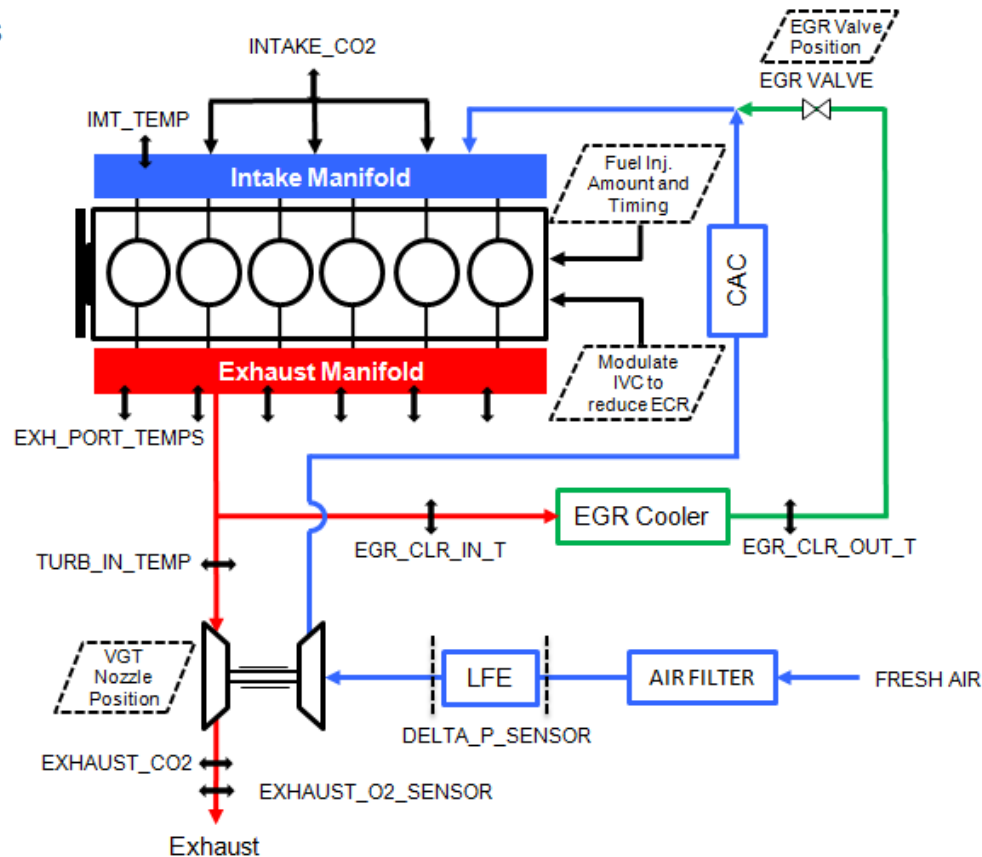
# Gas Exchange Model



$$\dot{F}_{im} = \frac{RT_{im}}{P_{im}V_{im}} \left[ F_{amb}W_c + F_{em}W_{egr} - F_{im}W_e \right]$$

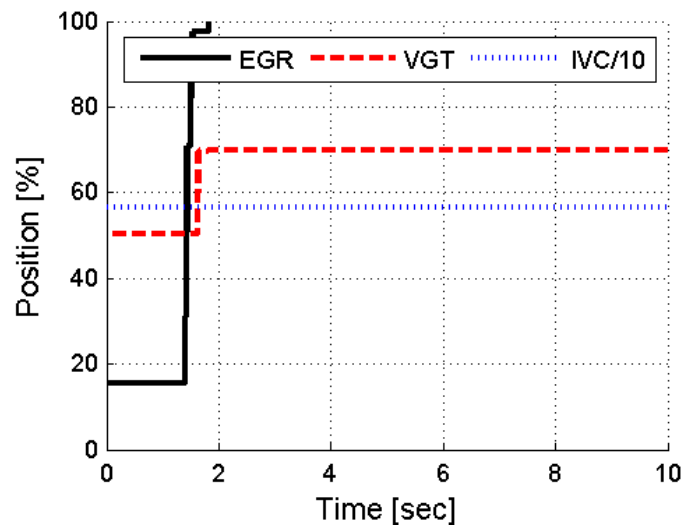
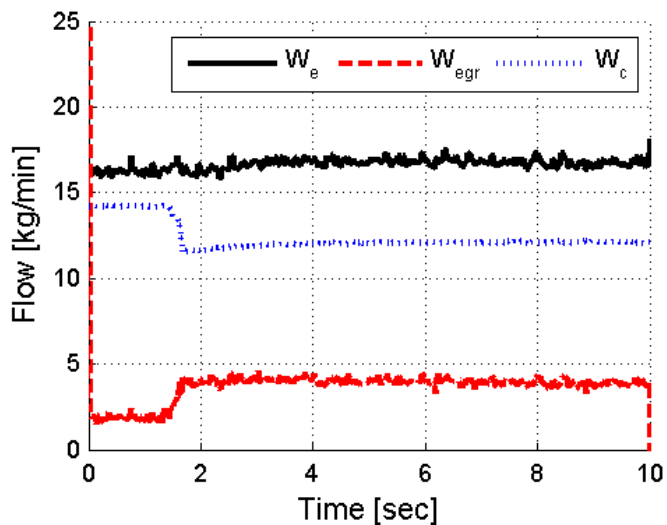
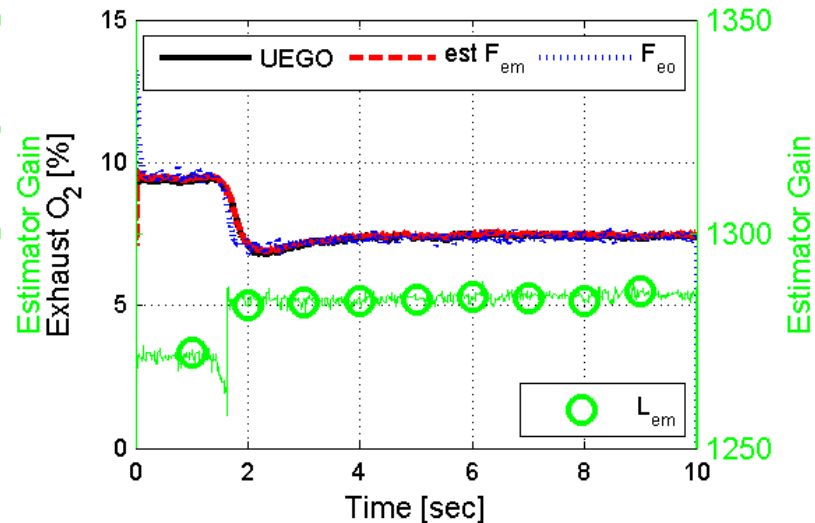
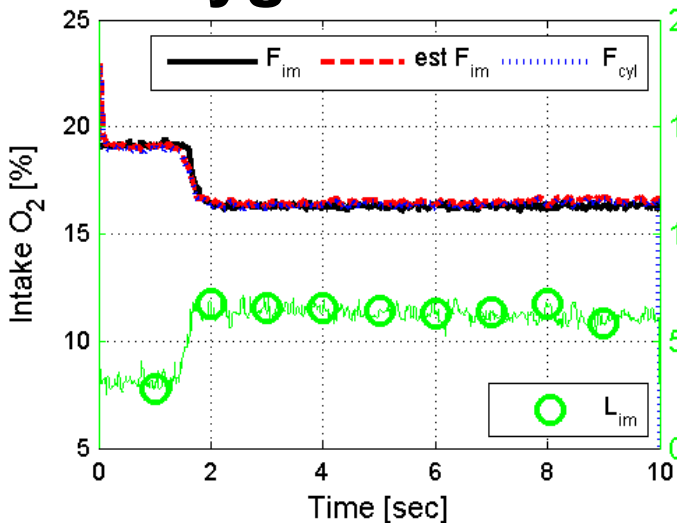
$$\dot{F}_{em} = \frac{RT_{em}}{P_{em}V_{em}} \left[ F_{eo} (W_e + W_f) - F_{em}W_{egr} - F_{em}W_t \right]$$

- EXHAUST GAS
- FRESH AIR
- EGR FLOW





## Oxygen Fraction Estimator Results





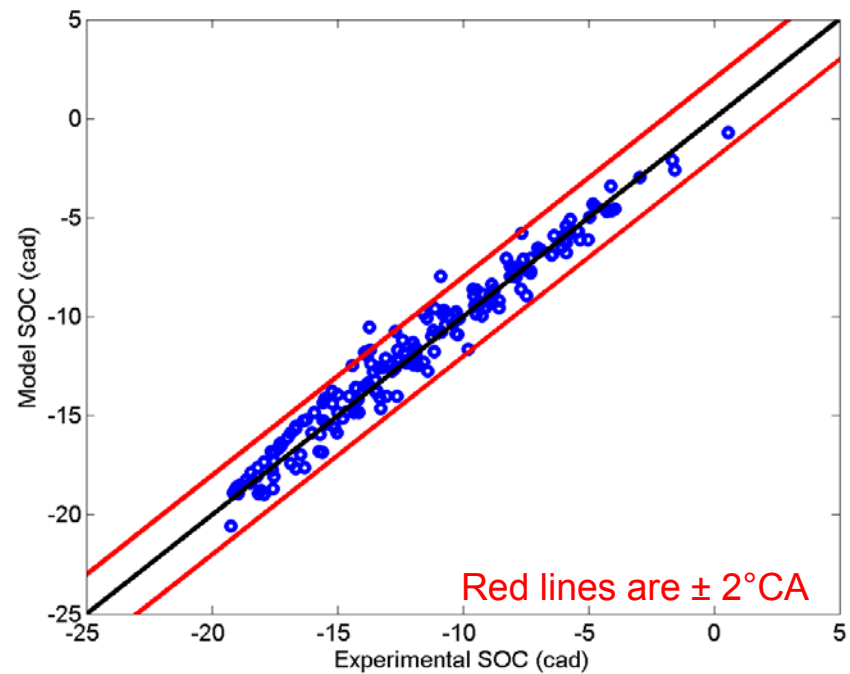
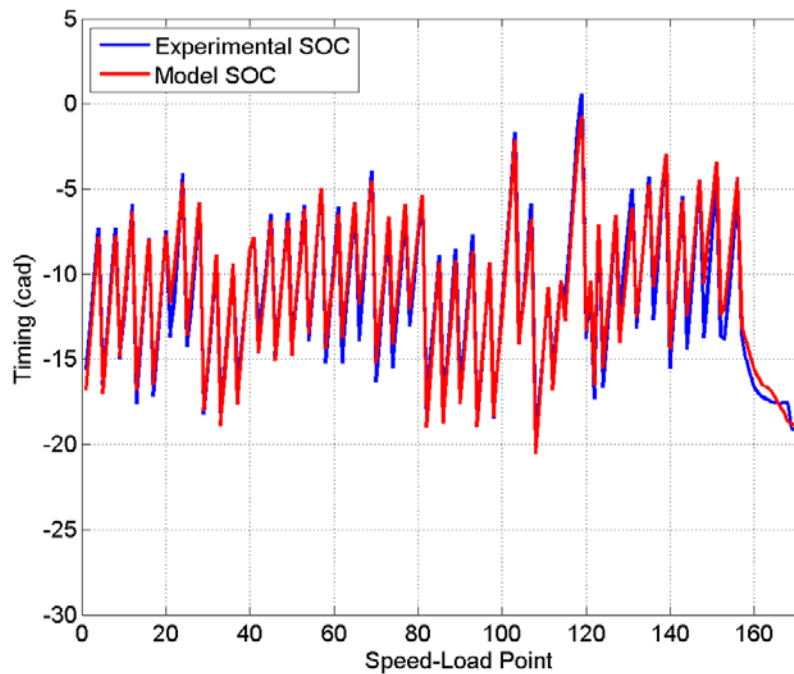
# PCCI Combustion Timing Model



## Start of Combustion Prediction

$$SOC = \tau_{elec} + \tau_{hyd} + \tau_{id} + SOI_{ecm}$$

$$SOC = 1.2 + 0.0018\omega + 0.006\omega \left( 0.051\chi_{O_2}^{-1.14} \bar{P}^{-0.51} e^{\left(\frac{2100}{T}\right)} \right) + SOI_{ecm}$$



Innovation You Can Depend On





# PCCI Combustion Timing Model



- What needs to be controlled to control PCCI combustion timing?

$$SOC = 1.2 + 0.0018\omega + 0.006\omega \left( 0.05 \chi_{O_2}^{-1.14} \bar{P}^{-0.51} e^{\left(\frac{2100}{T}\right)} \right) + SOI_{ecm}$$

- Can we separate dynamics?

**Slower dynamics driven by gas exchange process**

**Faster dynamics driven by fuel injection process**

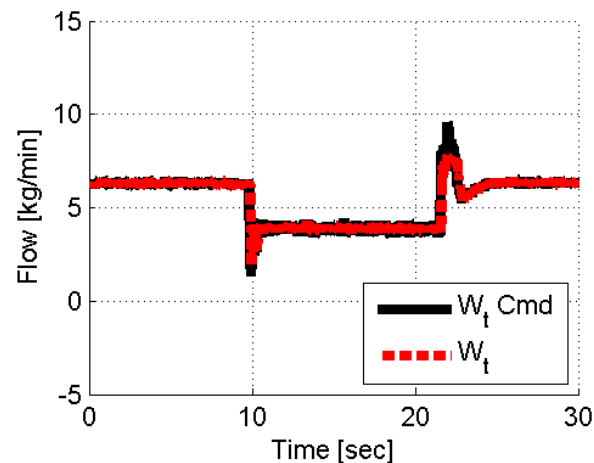
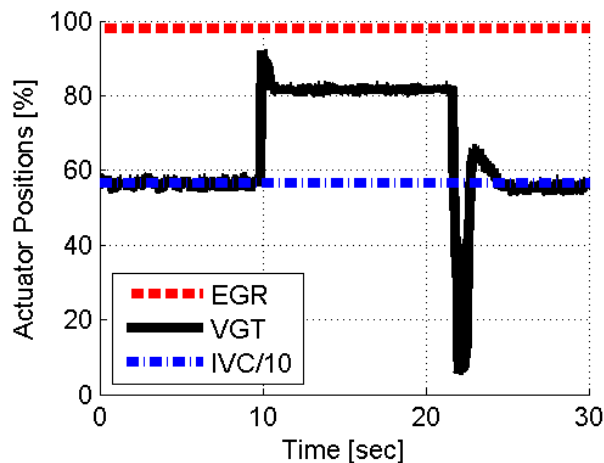
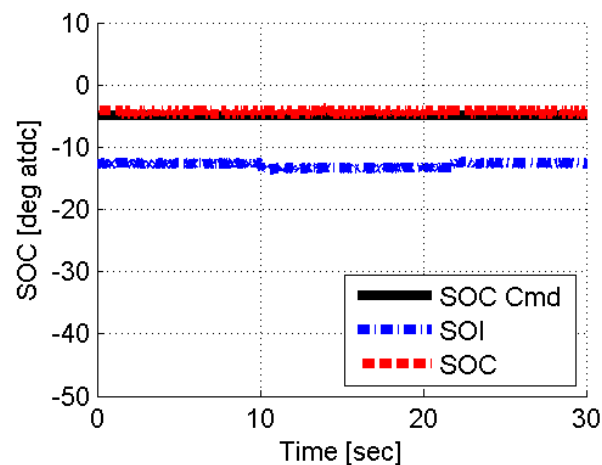
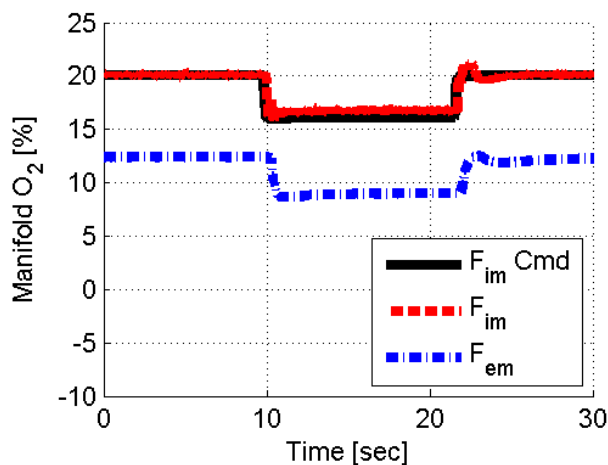




# PCCI Combustion Timing Controller



## 1600 rpm & 140 ft-lbf $F_{im}$ Command Step Change

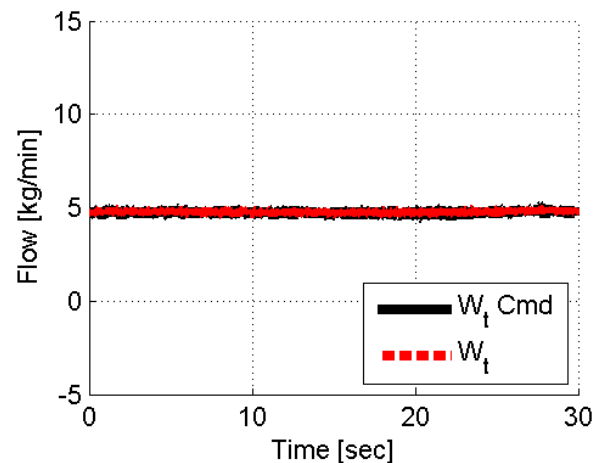
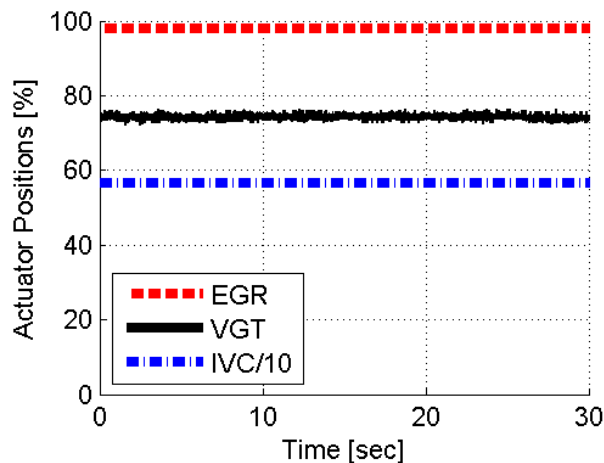
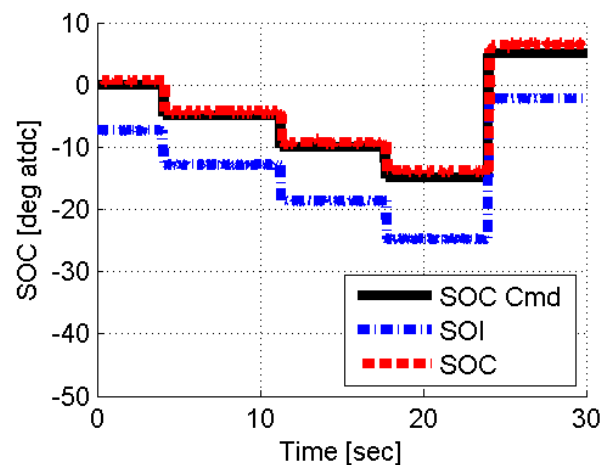
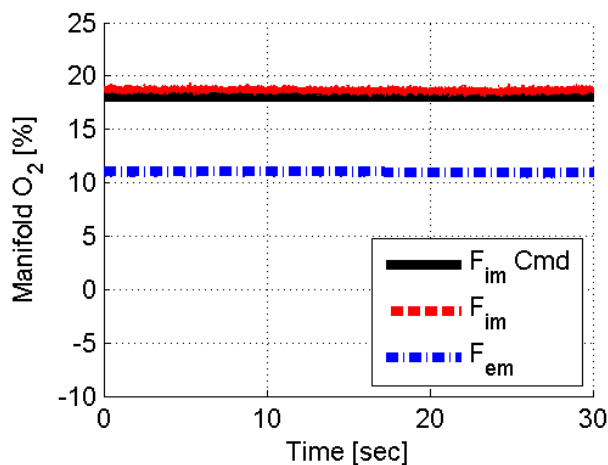




# PCCI Combustion Timing Controller



## 1600 rpm & 140 ft-lbf SOC Command Step Change



Innovation You Can Depend On







# Summary



- Experimental Test Bed
- Model Based Approach
- Gas Exchange Model
  - Manifold Filling Dynamics
  - Volumetric Efficiency
  - Oxygen Fraction Dynamics
- Combustion Model
  - PCCI Combustion Timing Model
- Controller Development
  - PCCI Combustion Timing
- Summary

