

Sulfur Effect and Performance Recovery of a DOC + CSF + Cu-Zeolite SCR System

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- Introduction
 - Zeolite-based SCR behavior
 - Performance
 - Sulfation issue: literature
- Reactor experiments to simulate transient behavior
 - Accelerated low temperature sulfation behavior
 - Sulfation effects and mechanism
 - Desulfation methods
- Summary

Recent developments have led to Cu-zeolite SCR catalysts with remarkably improved low temperature activity and high thermal stability

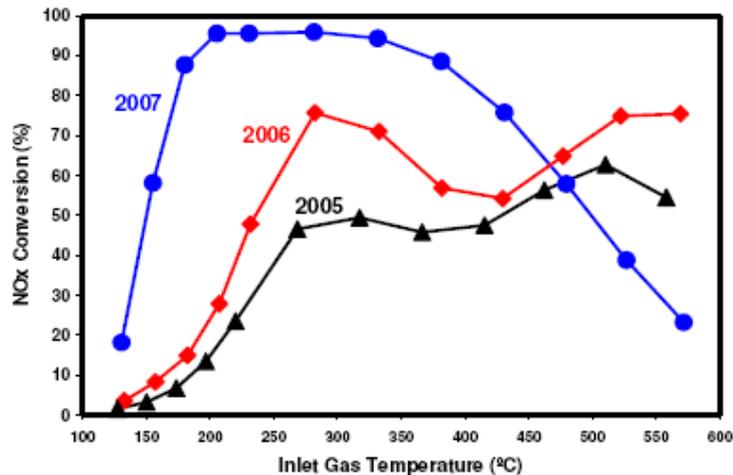


FIGURE 7. NO_x conversion of best in class SCR catalyst formulations from 2005 – 2007 after hydrothermal aging for 1 hour at 900°C.

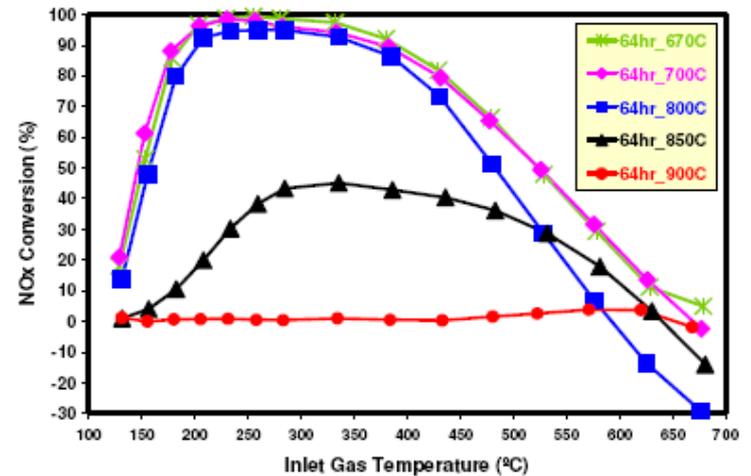
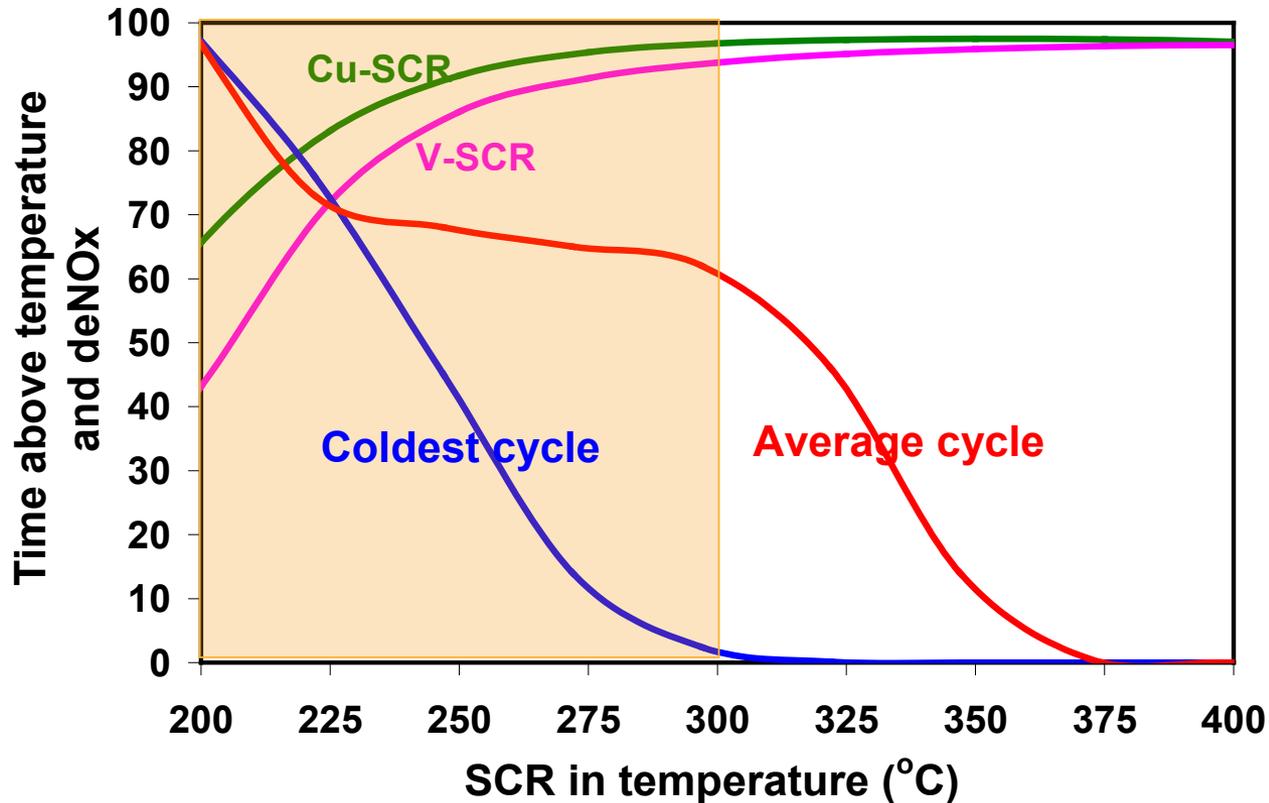


FIGURE 13. NO_x conversion results for the STANDARD SCR REACTION. SCR samples hydrothermally aged at 64 hours from 670°C – 900°C.

SAE 2008-01-1025: Enhanced Durability of a Cu/Zelolite Based SCR Catalyst. Giovanni Cavataio, et al

On the other hand, Cu-zeolite SCR also provides benefit over V/Ti SCR for applications with “cold” exhaust that never see high temperatures

Temperature window of one HDD engine platform and SCR NO_x conversion



Zeolite SCR sulfation issue: literature

- Several recent presentations have highlighted effects of sulfur compounds on zeolite-based SCR performance
 - “The Effects of SO₂ and SO₃ Poisoning on Cu/Zeolite SCR Catalysts”. Christine Lambert, et al: SAE 2009-01-0898
 - “Investigation of Sulfur Deactivation on Cu/Zeolite SCR Catalysts in Diesel Application”. Yisun Cheng, et al: 2009 DEER Conference
 - “The Effects of Sulfur Poisoning and Desulfation Temperature on the NO_x Conversion of LNT+SCR Systems for Diesel Applications”. Joe Theis, et al: SAE 2010-01-0300
- Past experience from Euro IV applications has shown V/Ti SCR to be insensitive to sulfation, although overall NO_x conversion may be lower than zeolite-based SCR

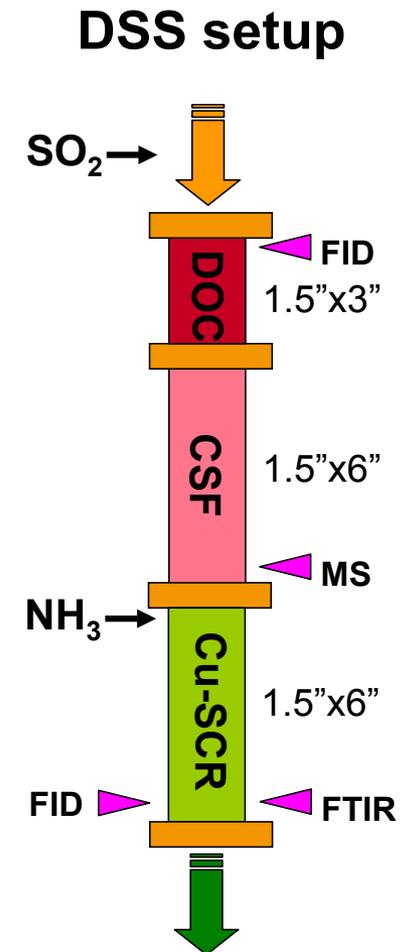
Background and motivation

- Background:
 - Systems with active regeneration used in low sulfur environments have shown stable, sustained performance to end-of-useful life*
 - Some systems running under high sulfur conditions and/or extended low temperature operation have shown performance loss
- Motivation:
 - Better understanding of degradation mechanism
 - Generate system-level performance features with realistic SCR-inlet SO_2/SO_3 and NO_2/NO_x in a DOC + CSF + Cu-SCR system
 - Determination of conditions for system performance recovery

* The New Challenge -Heavy Duty Diesel Engine Emission Control. Sanath V Kumar; SIAT 2011 Keynote Presentation

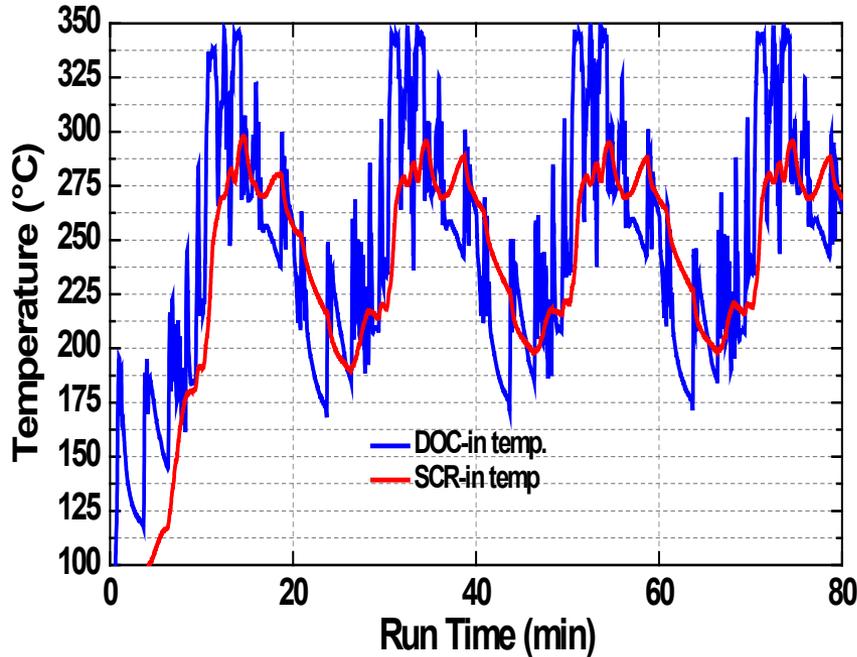
Laboratory study of sulfation effect at system level

- Diesel System Simulator (DSS)
 - System level study
 - Capable of simulating various transient cycles
 - By matching temperature, space velocity and compositions from engine experiments
- Catalyst size
 - DOC: 1.5"x3"
 - CSF: 1.5"x6"
 - SCR: 1.5"x6"



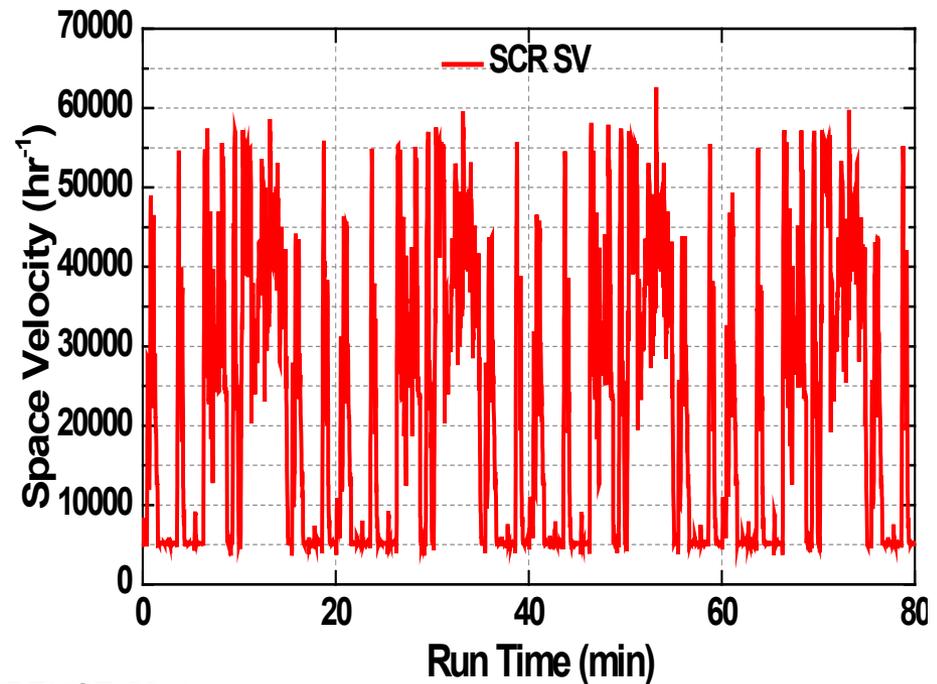
Engine HDFTP data “derated” to simulate cold engine operation

Temperatures in the first 4 FTP cycles of D3C3S6_061209_3 sulfation runs



Transient temperature and space velocity profiles in the first four cycles

(200-300 C SCR inlet
~55,000 h⁻¹ peak SCR SV)

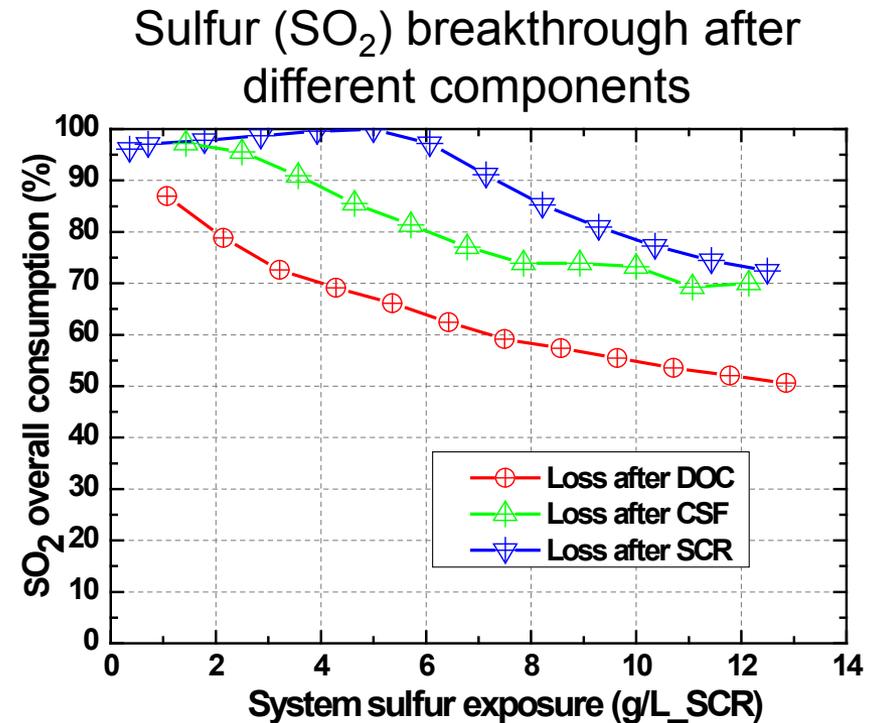
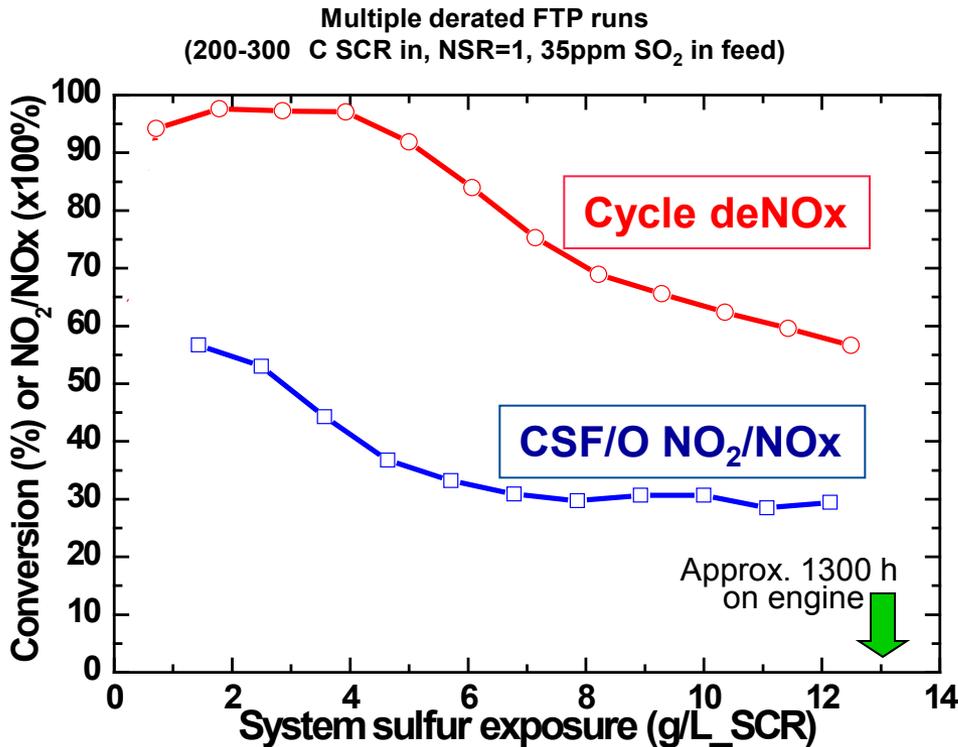


High SO₂ in feed to simulate extended sulfur exposure on engine:

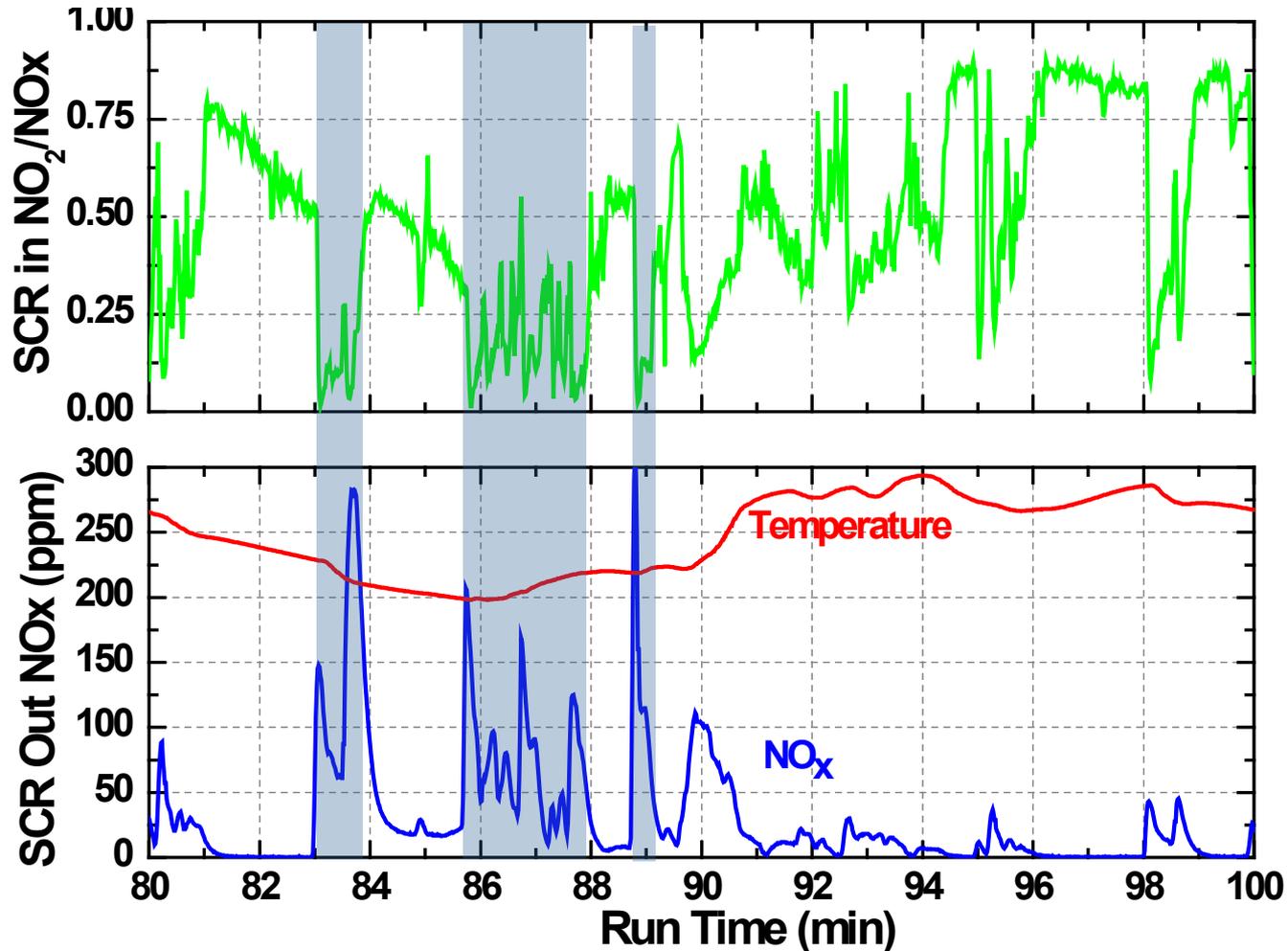
- ~1.0 g/L sulfur exposure = 100 h on engine (using ULSD fuel)
- ~12.5 g/L sulfur exposure on reactor \cong 1250 h on engine (~35 PPM SO₂ for 12 h in reactor)

System deactivation after accelerated sulfur exposure at low temperature

System response to 12h continuous derated HDFTP cycles under 35 ppm SO₂ in feed conditions

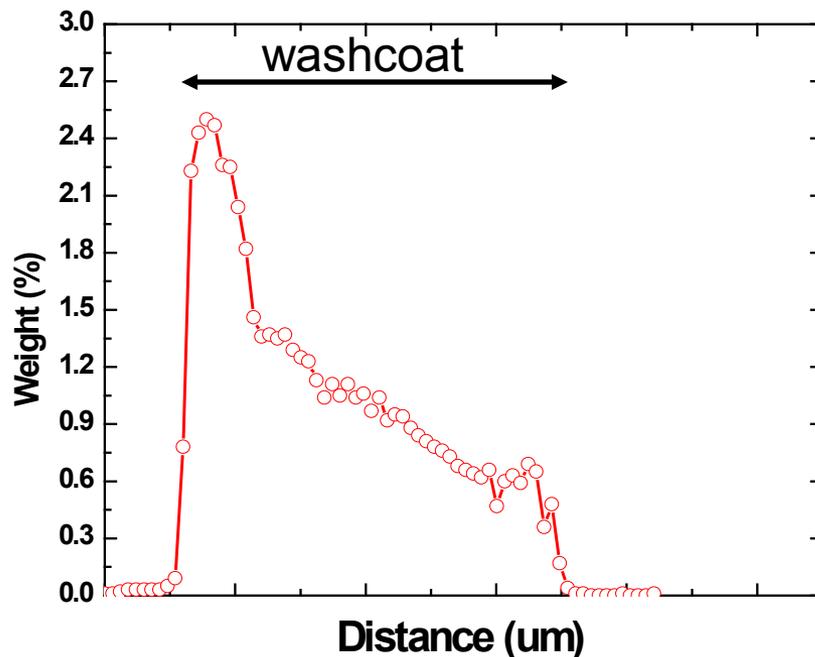


After sulfur exposure, Cu-zeolite SCR became sensitive to NO_2/NO_x ratio, especially for $T < 250 \text{ }^\circ\text{C}$



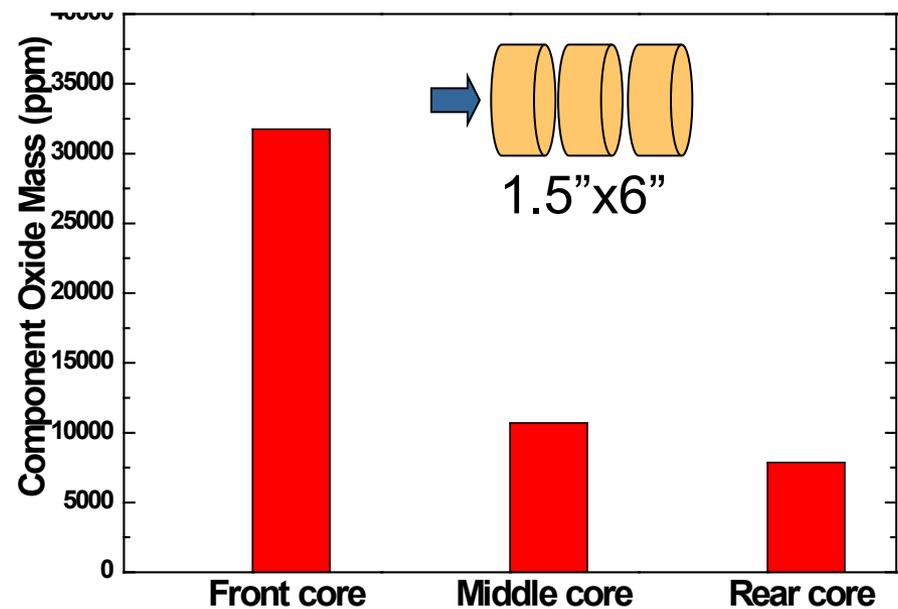
Sulfur concentration gradients in Cu-SCR after 13 g/L_SCR sulfur exposure

Washcoat surface to substrate



Washcoat sulfur profile via EPMA

Front to rear



Sulfate content via ICP wet analysis

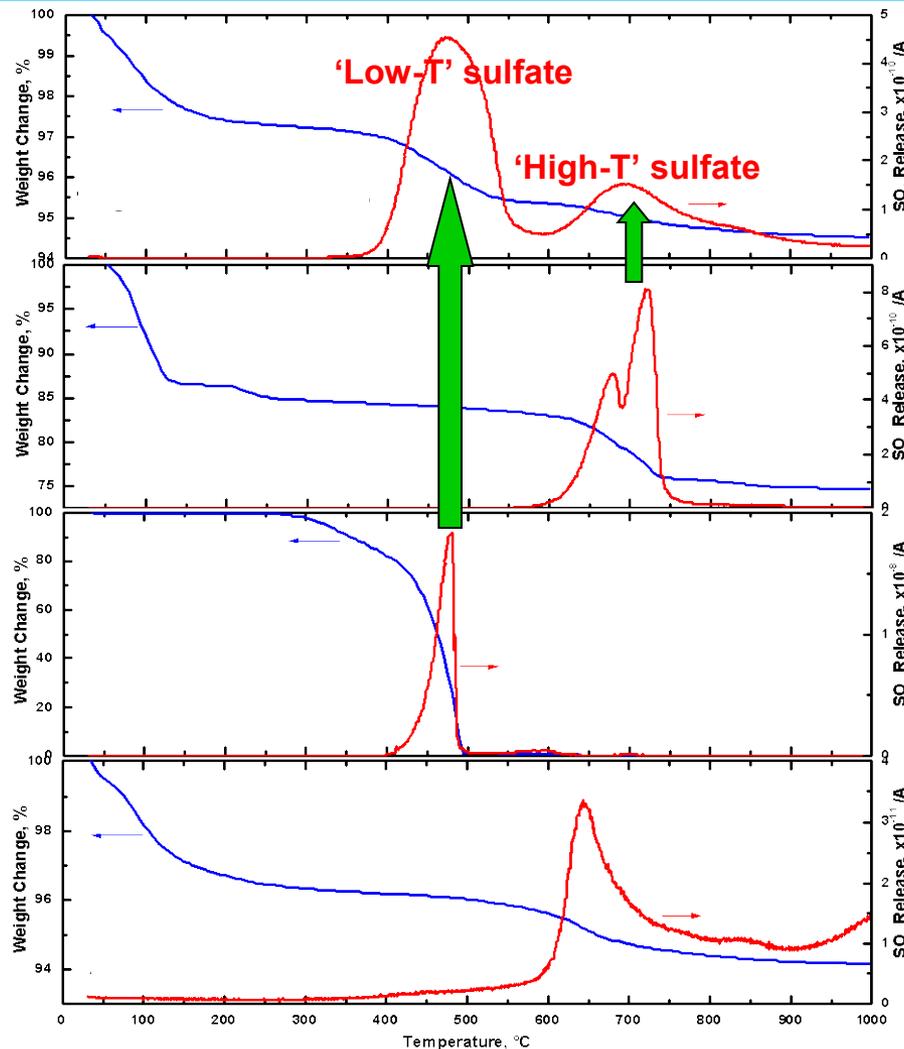
TGA/DTA-MS of sulfated sample shows two major sulfation modes

(a) Sulfated
Cu-SCR

(b) CuSO_4

(c) $(\text{NH}_4)_2\text{SO}_4$

(d) Sulfated
Cu-SCR
(w/o NH_3)

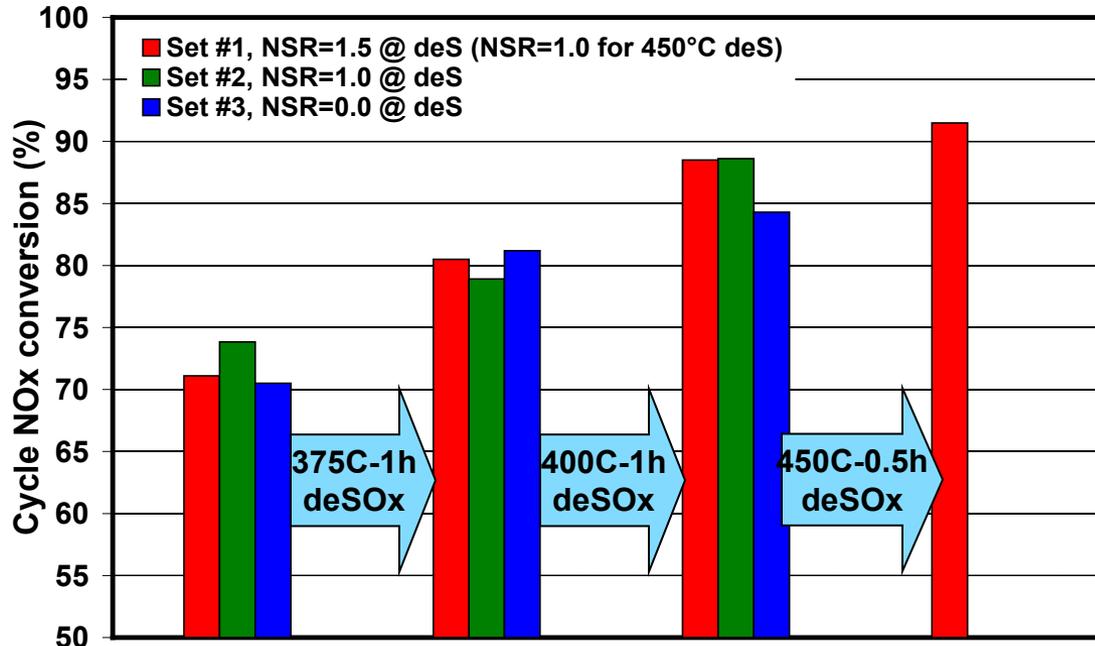


Sulfur release
and **weight loss**

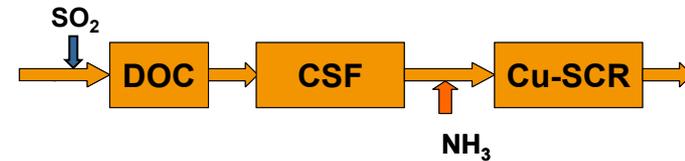
NOx conversion recovery is incremental with temperature

- Parametric study for desulfation effectiveness
 - NSR (NH₃/NOx) = 0.0, 1.0, 1.5
 - Durations = 0.5, 1.0 hr
 - Temperature = 375, 400, 450, 500, 600 C (SCR in)

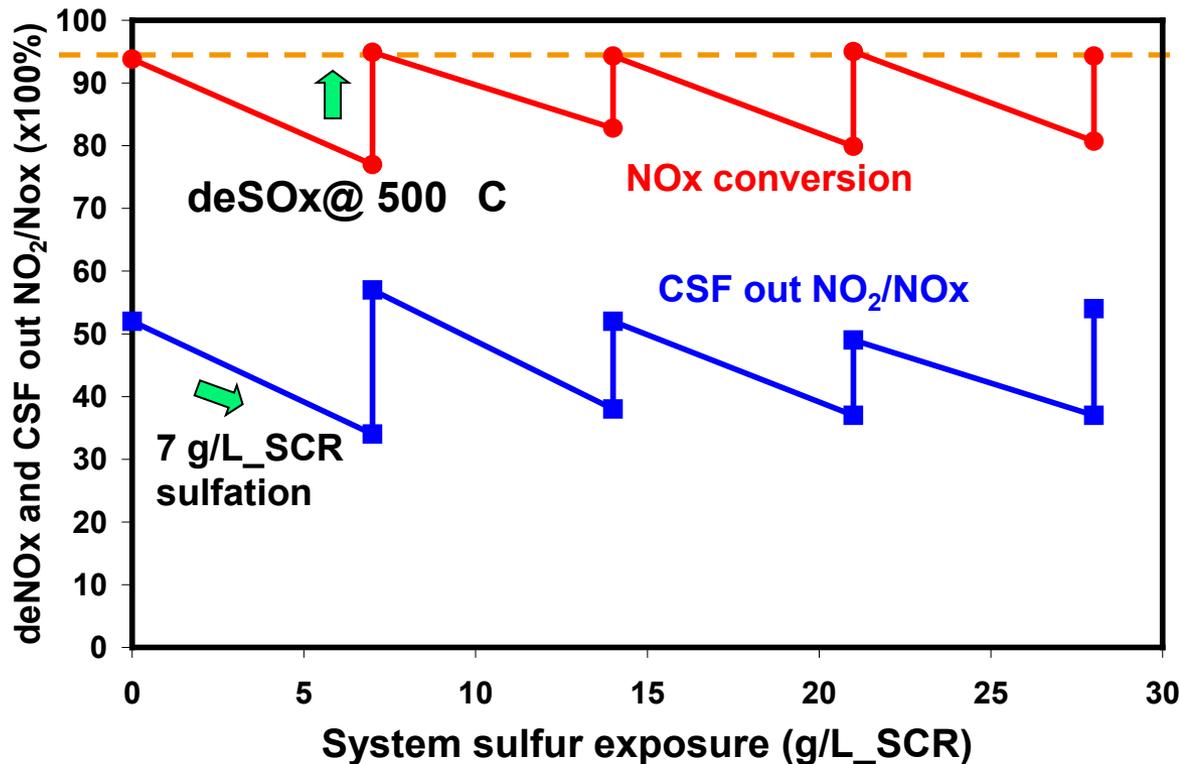
NOx conversion (Baseline: ~95%, all evaluated at NSR=1.0)



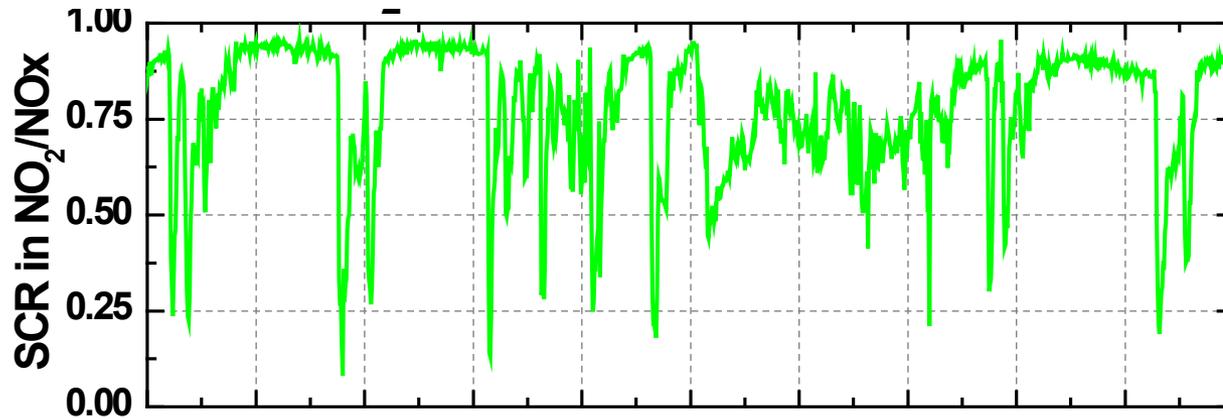
Full performance recovered at 500 °C deSOx ... and does not further degrade during multiple sulfation-desulfation cycles



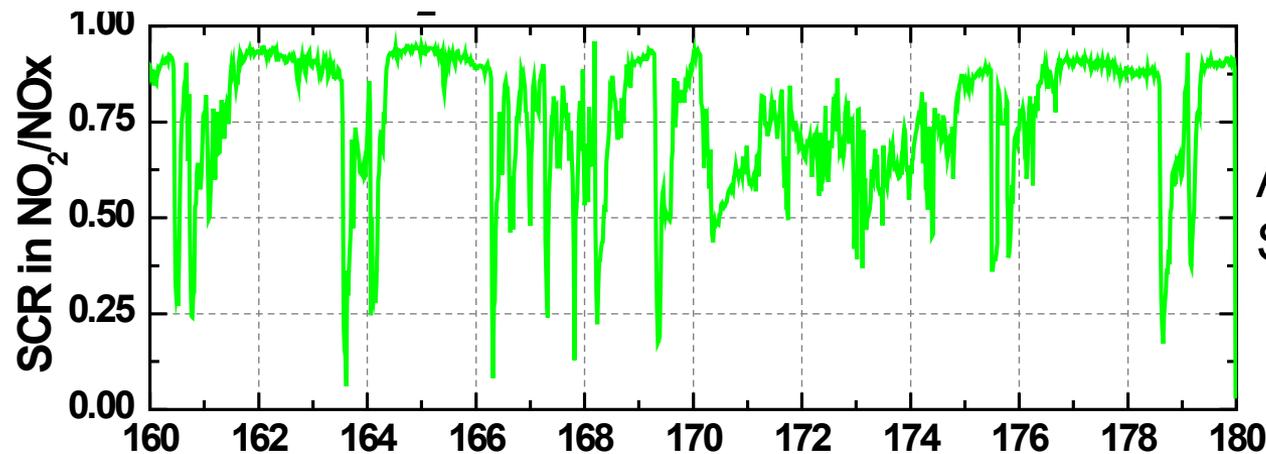
**NO₂/NO_x ratio and NO_x conversion
after sulfation and desulfation**



DOC/CSF generated fairly repeatable HDFTP NO₂/NO_x profile in post-deSO_x evaluations

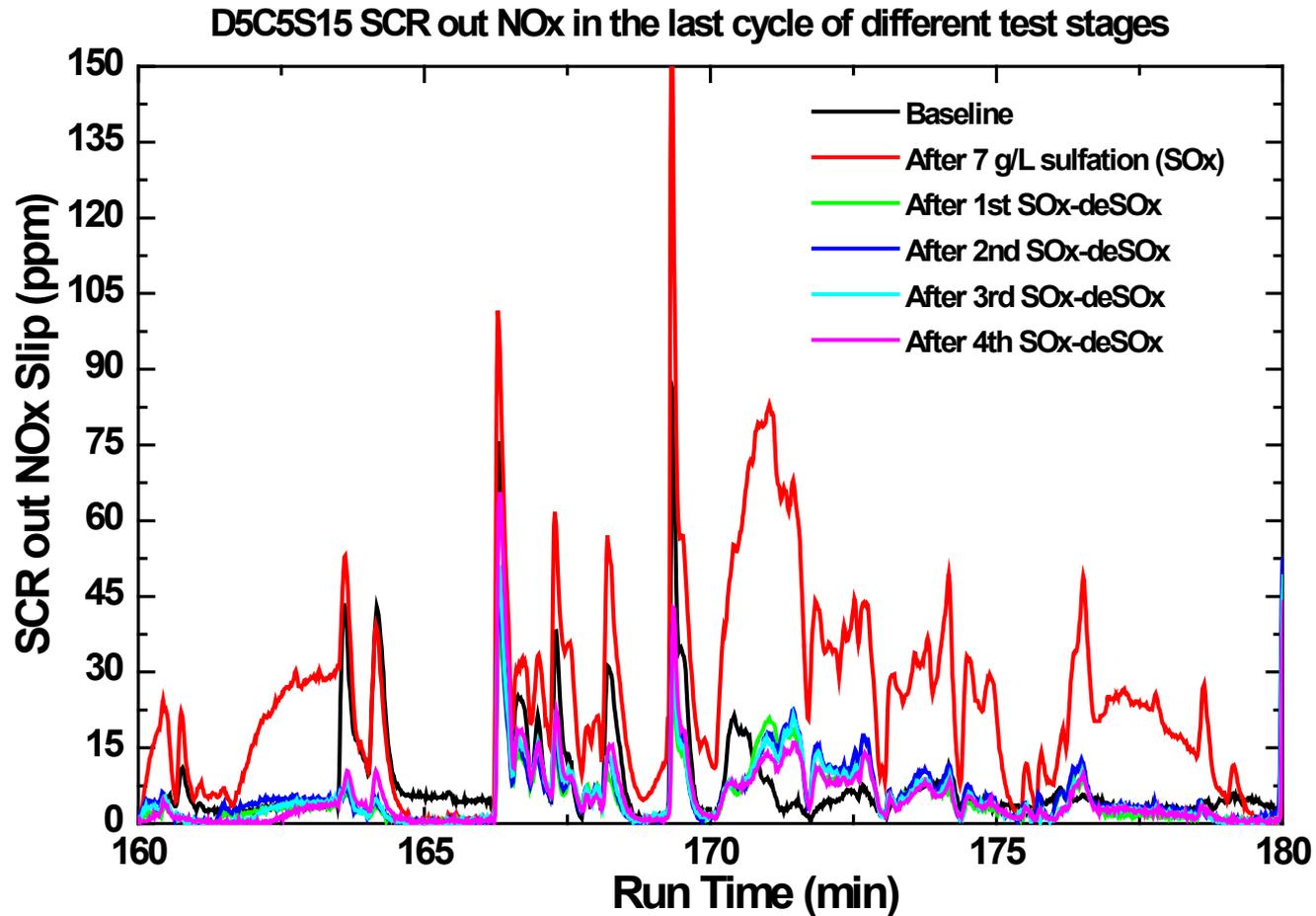


After 1st
Sulfation-deSO_x



After 3rd
Sulfation-deSO_x

SCR-out NOx slip values were very similar after 500 °C deSOx



Summary

- Zeolite-based SCR provides high thermal stability and durability in active regeneration systems with periodic high temperature exposures
- Literature reveals all zeolite-based SCR are susceptible to sulfation under low temperature SO₃ exposure
- This study has shown that Cu-Zeolite SCR degrades after severe sulfur exposure under extended low temperature conditions
 - Two major sulfation modes are most likely involved
 - Formation of (NH₄)₂SO₄ or (NH₄)HSO₄
 - Formation of CuSO₄
- System performance can be recovered
 - Temperature is the most important factor determining desulfation efficiency
 - The system recovered most but not all of its performance after 450 °C desulfation
 - Upon 500 °C desulfation, NO_x conversion efficiency was fully restored and sustained in multiple sulfation-desulfation experiments

Thank You!

