# CORNING

**Diesel Emission Control Review** 

Tim Johnson DEER 2010 Detroit

## Summary

- HD regulations being wrapped up, next regs being contemplated
- Further tightening of criteria regs expected. California is completing LEV3 proposal stage. EPA considering Tier 3.
- CO<sub>2</sub> mandates are proposed for HD
  - Onset of another major regulatory-driven technology evolution
- Engine technologies are addressing engine-out NOx and FC
   control, LT thermal management, advanced combustion approaches
  - control, LT thermal management, advanced compustion
- SCR is addressing "secondary" issues:
  - LT issues: ammonia sources and urea inj; NH3 storage formation, mechanisms.
  - Catalyst HT durability
  - More understanding on SCR+DPF
- New LNT compositions and designs are shown.
  - Better performance, lower cost
  - LNT+SCR systems advancing
- DPF regen, substrate properties, material, and catalysts advancing.
- DOC catalysts performance characterized
  - NO2
- LDD CO emissions can be difficult

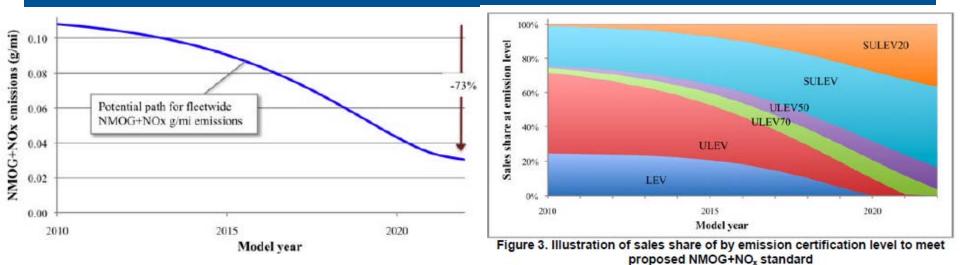
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**Regulatory Issues** 

## Emerging HD regulatory issues

- Euro VI PN comitology being finalized.
  - 6 X 10<sup>11</sup> #/kW-hr on the WHTC
    - Quite tight for clean filters, but pre-conditioning for up to 125 hrs is allowed
- Japan HD will harmonize with Europe in 2016-17
- Off-cycle emissions issues emerging
  - European report shows high urban emissions for SCR trucks
- Next stages of European non-road regs being contemplated
  - Workshops and committees formed

### CARB-Proposed LEVIII Standards for 2014-2022 SULEV Fleet Average NMOG+NOx.



Possible scenario for fleet average NMOG+NOx standards.

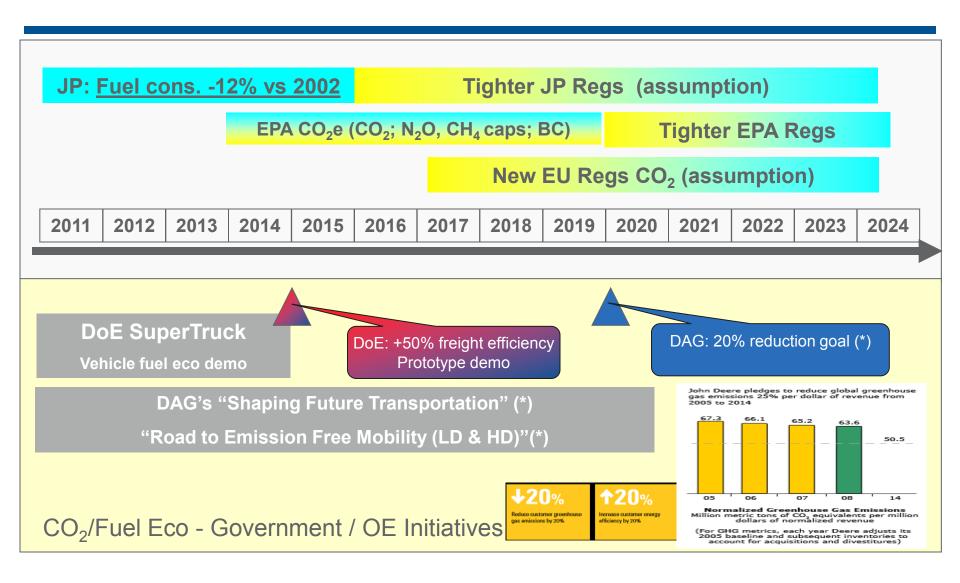
A possible scenario to meet yearly fleet average emissions targets.

PM reduced 70% to 3 mg/mi. Lower values are difficult to measure, and CARB wants a different PN reg that isn't ready yet

EPA will likely follow CARB with a Tier 3 LD regulation.

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HD CO<sub>2</sub>/Fuel Consumption Reduction: Different approaches JP: Fuel consumption, EU: CO<sub>2</sub> focus(?), EPA: CO2 focus

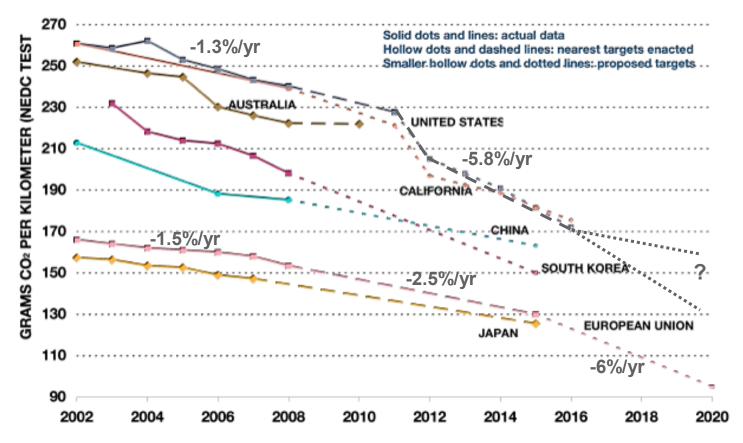


(\*): www.Daimler.com, MTZ 1-'09, http://www.cat.com/sd2009, http://www.deere.com/en\_US/globalcitizenship/stewardship/metrics.html

# Emerging CO<sub>2</sub> regulations are aggressive and will result in a paradigm shift.

Fuel consumption technologies will no longer be based on the value proposition to the customer. They will be chosen based on mandate economics.

#### ACTUAL FLEET AVERAGE GHG EMISSIONS DATA THROUGH MY2008 AND NEAREST TARGETS ENACTED OR PROPOSED THEREAFTER BY REGION

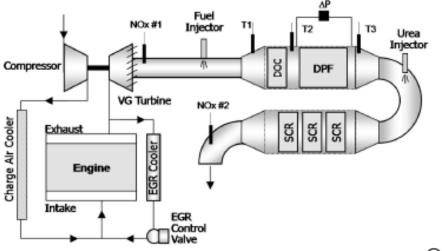


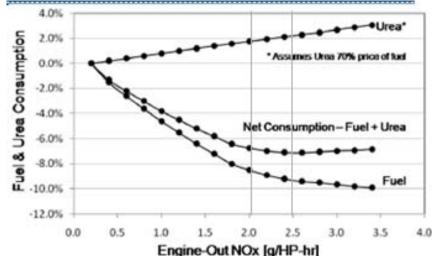
TheICCT.org, updated 11/09

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**Engine Technologies** 

# Hardware and general strategy for meeting US2010 are described.





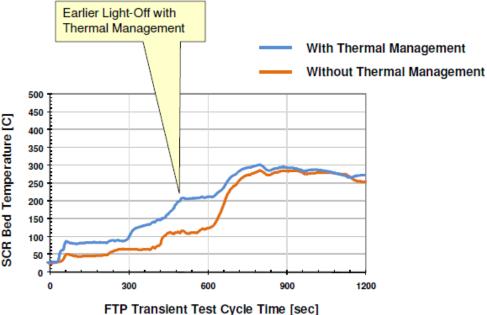
The engine is equipped with VGT to allow optimum EGR control, and 2200 bar CR injection.

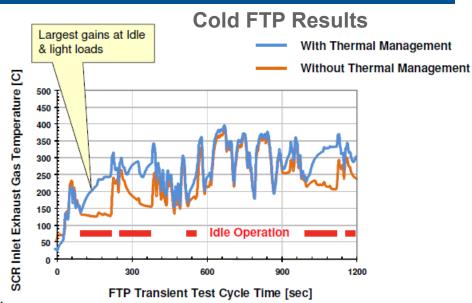
Operating strategy minimizes fuel and urea consumption, with engine-out NOx from 2.0 to 2.5 g/bhp-hr being optimum.

## Thermal management is used to reduce cold or lowload NOx. Minimal fuel penalty possible.

#### Thermal Management

- Control of fuel injection and air handling parameters
- Utilizes the flexibility of the XPI common rail and variable geometry turbocharger
- Allows faster warm-up and SCR light-off
- Minimizes cooling effects of idle and light load operations





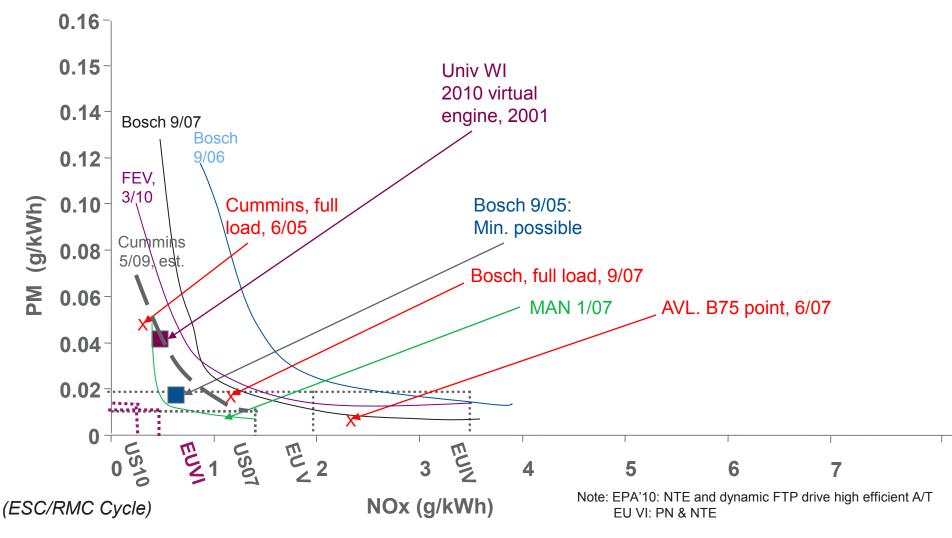
T up from 150 to 250C in 2 minutes under idle conditions.

FTP Phase	Without Thermal Mgt	With Thermal Mgt
Cold Cycle	0.364 g/HP-hr	0.301 g/HP-hr
Hot Cycle	0.357 g/HP-hr	0.031 g/HP-hr
Composite	0.358 g/HP-hr	0.069 g/HP-hr

Cummins, MinNOx Conf, 6-10

# Historical research engines help predict future production engine capability.

Significant engine NOx threshold at ~0.2-0.3 g/kW-hr NOx. Very low PM at higher NOx regimes.



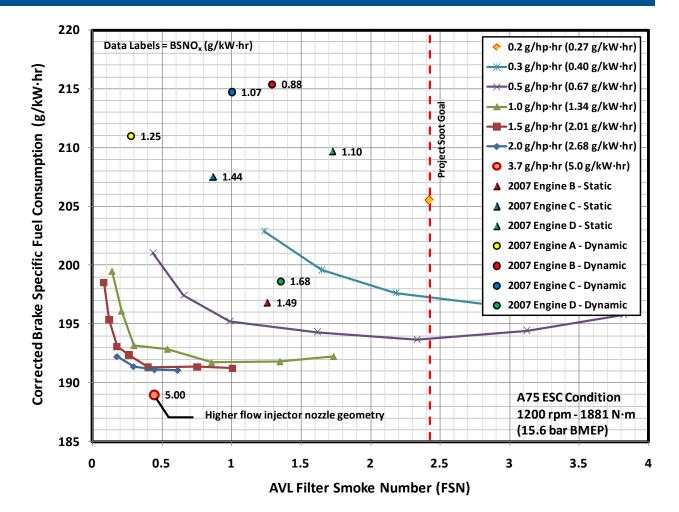
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## Massive EGR Engine – No NO<sub>X</sub> Aftertreatment

#### Performance Comparison at Higher NOx levels

 Results compared with four 2007 heavy duty diesel engines
 Engine operation has been optimized for low engine speeds
 At similar NO<sub>x</sub> levels the Massive EGR provides dramatically improved performance

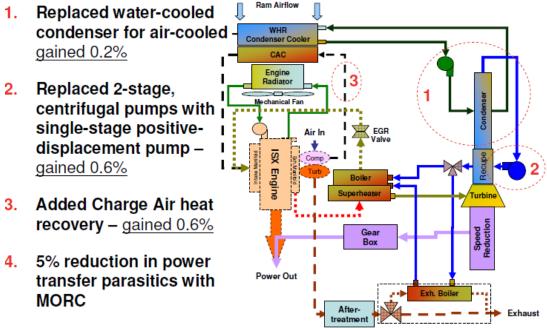
 Massive EGR engine was not optimized to operate at higher NOx levels, so further improvements are still possible



SwRI, Clean Diesel 5 Consortium 8/10

# Second generation waste heat recovery system shown.

Improvements gain 1.4% FC impact, on top of 6.2% for generation 1.



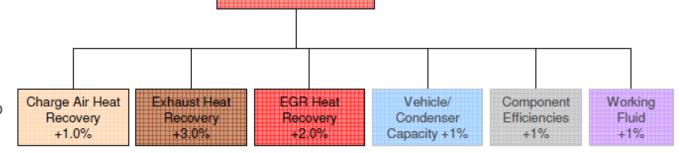
Second generation Organic Rankine Cycle (ORC) improvements include the condenser, pumps, added heat source, lower parasitic losses, and new working fluid.

#### **Future Directions**

- System Architecture and Controls
- Turbine Expander
- Expander to Engine Geartrain
- Heat Exchangers on and off engine
- Feedpump and instrumentation
- Fluid Development (low GWP alternatives)
- Vehicle Packaging
- Cost Focus

Cummins, Emissions 2010 Conf, 6/10

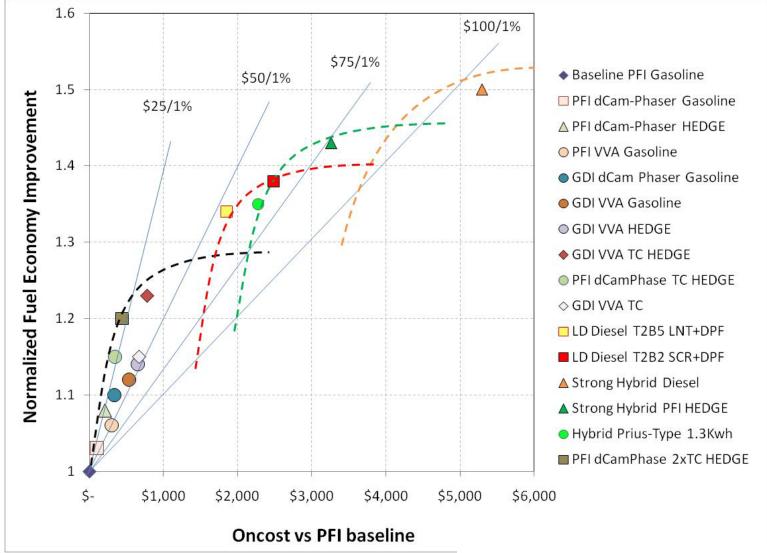
Potential benefit of 9% energy from WHR. 6.2% realized in generation 1.



WHR BTE Benefit

# 20% improvements in CO2 cost about \$25-\$50/%. 30-45% improvements will be \$50-\$100/%.

Gasoline technologies might peak out at 25-30% improvement, diesel at 40%.



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SwRI Powertrain Consulting Service 8/10

The coming  $CO_2$  regulations will be more difficult to attain than the criteria pollutant regulations. Engine research should focus on  $CO_2$  reductions. Aftertreatment solutions available for any challenge.

- Three-way catalysts: 1995 vs. 2010
  - Cost -50 to -70%
  - Emissions -98%
- SCR: 2004 vs. 2010
  - Cost -20%
  - Emissions -75%
- LNT: 2005 vs. 2010
  - Cost -70%
  - Emissions -75%
  - Fuel consumption -30%
- DPF: 2003 vs. 2010
  - Cost -50%

Most significant challenge: LT lean deNOX

- •LT NH3 injection and thermal management
- •LNT + reformer
- Cu-zeolite SCR with NH<sub>3</sub>
- pre-turbo components

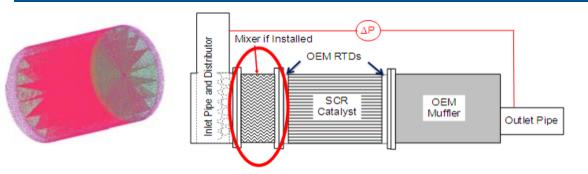
Evolution trends: Performance improvement at similar cost (like electronics), then more cost reduction while enhancing performance.

\* These are rough estimates of cutting edge improvements to illustrate

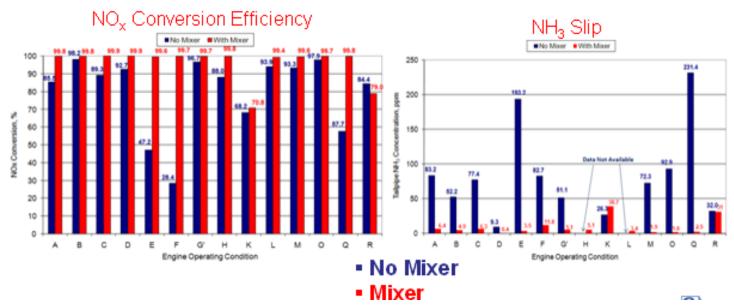
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SCR

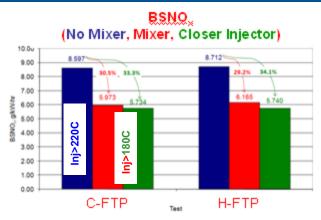
### New mixer allows urea injection at T>180C



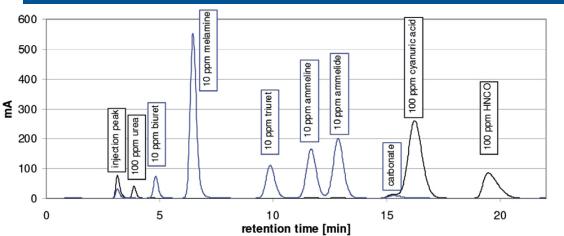
Mixer has low pressure drop and high surface area. 4.8% max pressure drop in ESC



The new mixer with revised calibration shows higher efficiency than OROM without at all points. Point E is 181C; F is 225C.

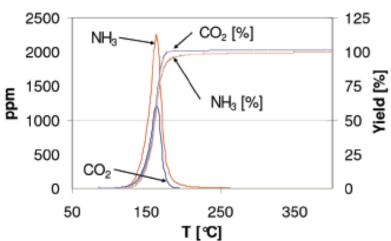


Urea decomposition products are measured using a new thermal/gas analysis procedure. TiO2 is an effective urea decomposition catalyst.



Urea decomposition products released into a flowing model gas stream. Heat rate 10C°/min, 40-550°C.

- Biuret decomposition NH3 peak is at 160C.
- Cyanuric acid and melamine NH3 peaks are at 250C.

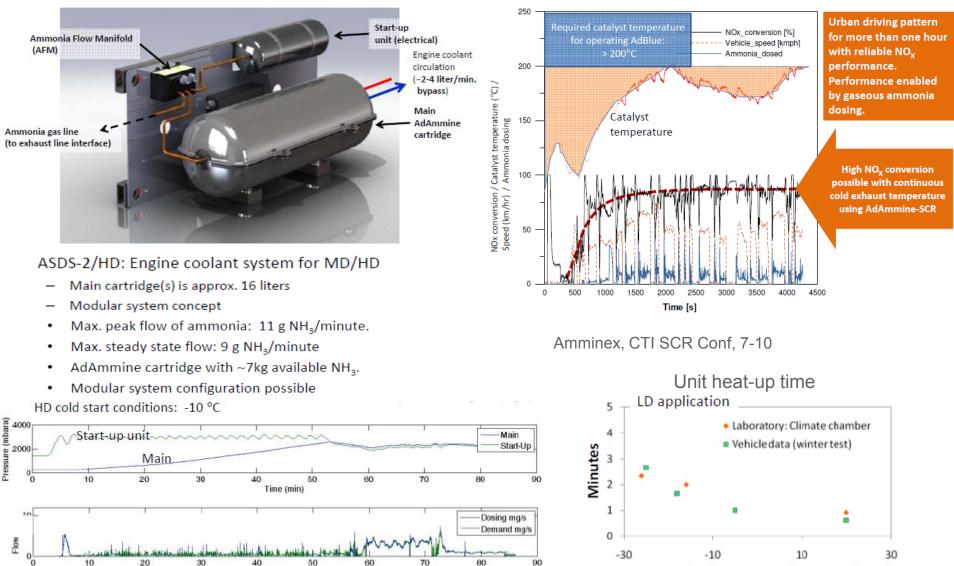


Urea decomposition on a TiO2 catalyst. No by-products were formed. Urea decomposition is not purely a thermal process.

PSI, AVL PM Forum, 3/10

# Update on ammonia adsorption SCR. First commercial contract. Production trial in 2011.

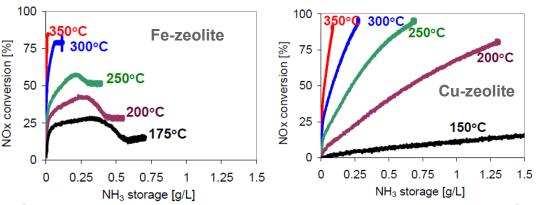
Time (min)



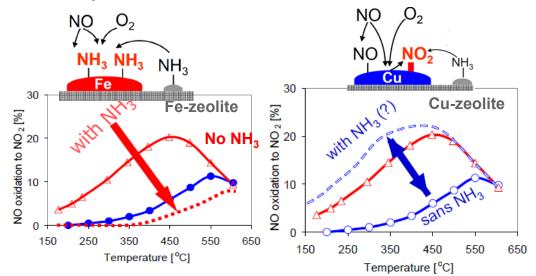
Initial cold-soak temperature of storage unit (deg. C)

## Better transient efficiency of Fe-zeolites is explained.

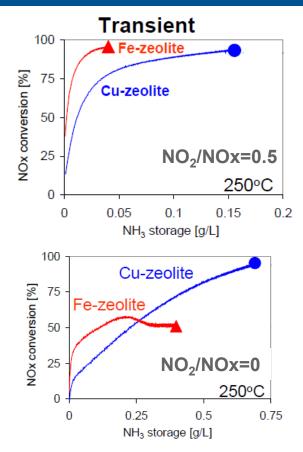
Lower NH3 adsorption and impact on in situ NO oxidation.



NOx conversion on Fe-zeolites is much more impacted by  $NH_3$  than on Cuzeolites.  $NH_3$  adsorbs on acidic Fe deNOx sites, not on basic deNOx Cu sites.



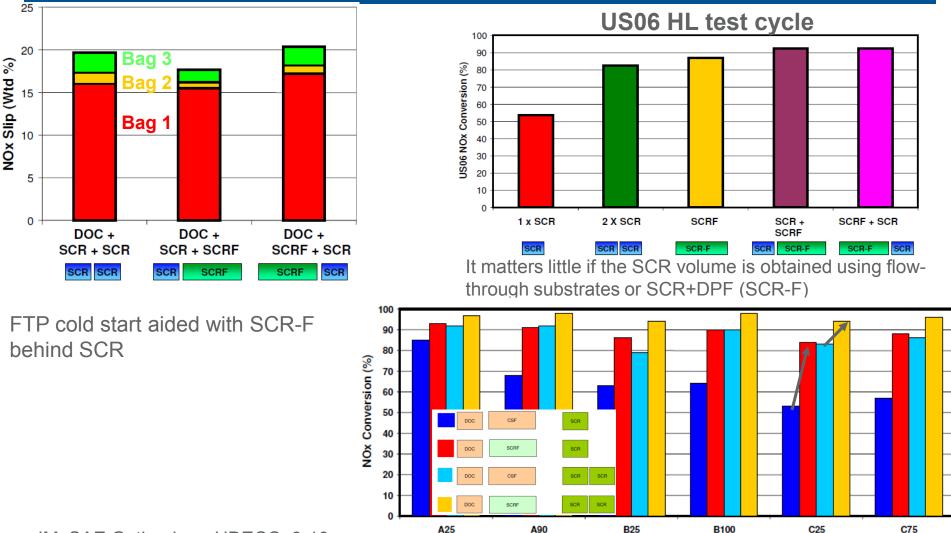
Adsorbed  $NH_3$  inhibits NO oxidation on Fe-zeolites.  $NO_2$  adsorption (poisoning) may inhibit NO oxidation on Cu-zeolites.  $NH_3$  may clean Cu sites of  $NO_2$ 



In transients Fe-zeolite converges to  $NH_3$  adsorption equilibrium faster than Cu-zeolite.  $NH_3$  reduces NOx instead of adsorbing (top). Fe-zeolites can oxidize NO more effectively in transients (bottom).

### SCR+DPF adds options to improve deNOx performance.

Increased volume is as effective as for flow-through catalysts. Adding catalyst to the DPF can drop emissions 60-65% at low deNOx points.



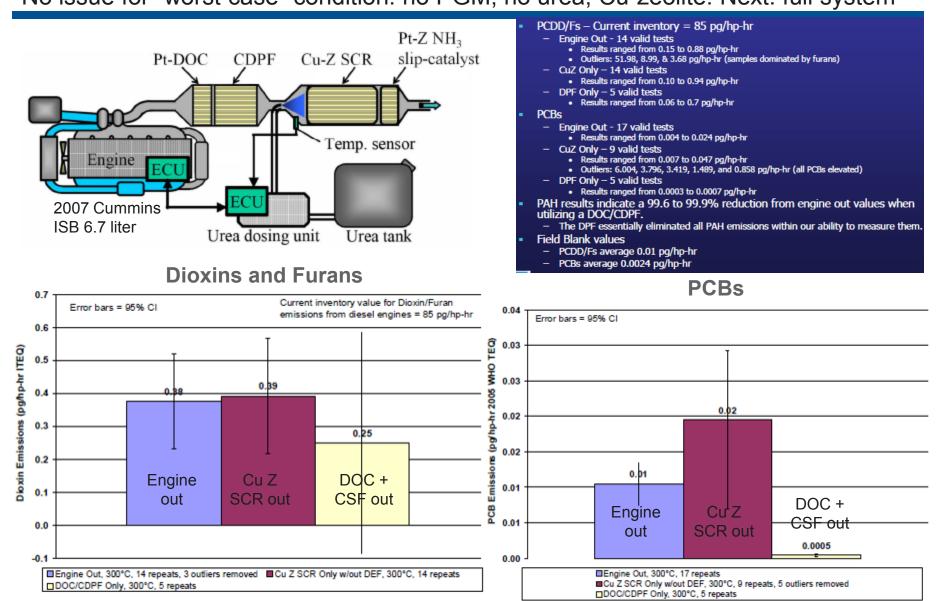
JM, SAE Gothenburg HDECC, 9-10

SCR on the DPF cuts emissions about 60-65% at the C25 load point.

**Engine Operating Point** 

#### US EPA, SAE Congress 4/10

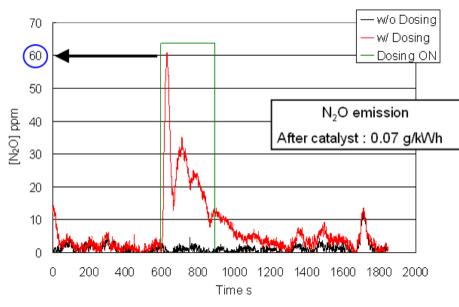
#### EPA reported on the first phase of the dioxin study. No issue for "worst case" condition: no PGM, no urea, Cu-zeolite. Next: full system



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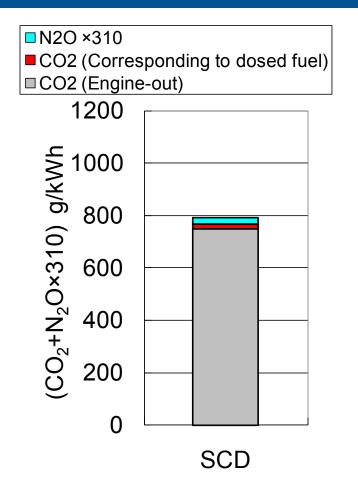
HC-deNOx

### LNT can emit N<sub>2</sub>O. 3% of total carbon footprint.



LNT can emit N2O during rich cycle on J05 transient test

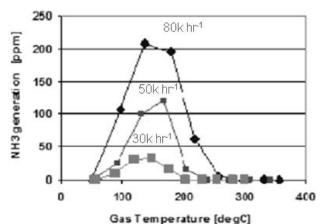
#### New ACE, SAE 2010-01-1066



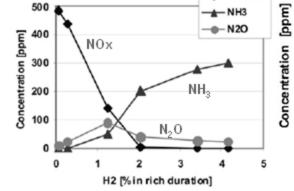
Dosed fuel is 2.4% of total.  $N_2O$  is 3% of carbon footprint.

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# Parameters affecting NH<sub>3</sub> production in an LNT are investigated. Flow rate and hydrogen are major factors.

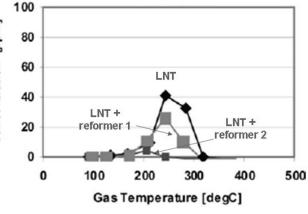


NH3 production in the LNT increases with flow rate for parts of equal length. However, decreasing length at the same flow to achieve high SV did not increase NH3 (not shown). 80K SV with shorter parts performed similarly to the 50K curve here.



Hydrogen has a big impact on NH3. Here 2% is stoichiometry for the amount of NOx.

-NOx-out



WGS catalysts did not improve ammonia formation. However, system NOx conversion was improved, especially at LT.

3 g/liter PGM

Other impacts:

•Shorter LNT substrates did not appreciably impact system deNOx performance

•Longer rich times increase NH3 and decrease N2O.

•NO/NOx ratio has little impact.

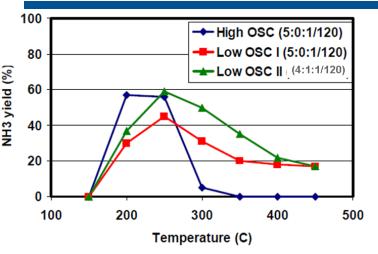
• Residual oxygen in the rich gas can have a large negative impact on ammonia production

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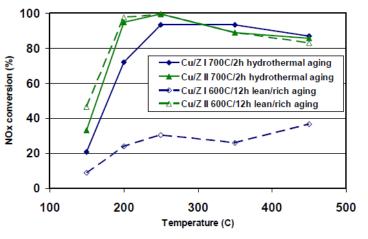
MIT, SAE 2010-01-1071

## Performance of an NAC+SCR system is improved.

NAC NH3 formation enhanced with Pd and low-OSC. SCR durability improved.



Reducing the OSC and replacing 20% of the Pt with Pd improves the NAC ammonia generation.



3.5L 2.5L 0.6L 3.2L 3.0L 2007MY E320 Bluetec CSF NAC SCR OEM Cal. 2:1:0/105 10:8:3/84 1:0:0/20 100 80 NOx Conversion (%) 60 40 20 0 NOX NAC NOX SCR NOx Total

The improved combination system delivers 93% using the OEM calibration. The SCR increased overall performance of the low-PGM NAC by 17%.

Improvements are made to the lean-rich HC cycle durability of the Cu-zeolite catalyst.

JM, SAE 2010-01-0302

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DPF

### Ford demonstrates characteristics of active and passive DPF

regen. Active: No O2 impact (>2%), soot load important, little PGM influence; Passive: NO2 2.5X than w/o, Pt is key, zeolite had no impact.

Sample ID	Soot wt (g)	Loading (g/L)	Soot Burn Rate (mg/h
High temper	ature active 600	)° C active 5%O $_2$	(0.15 NO 2:NO x)
Pt, 5 g/ft3	0.1575	5.439	384.4
Pd, 5 g/ft3	0.1832	6.326	394.9
Cu-zeol	0.1590	5.491	348.0
Pt-Pd, 5 g/ft3	0.2091	7.221	431.4
Uncoated	0.2914	10.063	617.1
Pt, 30 g/ft3	0.2787	9.624	621.3
High temper	ature active 600	0° C Active 2%O <sub>2</sub>	(0.15 NO 2:NO x)
Pt, 5 g/ft3	0.1551	5.356	372.2
Pd, 5 g/ft3	0.1906	6.582	412.1
Cu-zeol	0.1619	5.591	399.2
Pt-Pd, 5 g/ft3	0.1550	5.353	383.5
Uncoated	0.2874	9.925	512.2
Pt, 30 g/ft3	0.2834	9.787	624.0

#### Active Degenerations

- Little impact between 2 and 5% O2 (1-4 vs. 7a. 10). 1% needs 50C higher inlet.
- Soot mass more dominant (5&6 and 11&12 vs. b. others) Auxiliary results not shown.
- Pt and Pd are similar (1 vs. 2, 7 vs. 8) and C. convert to CO2. Cu-Z similar to uncoated (CO:CO2=60:40). PGM had no impact on rate.

#### Other:

- Active regen costs 0.5 MPG
- Passive extends regen freg from 400 to 467 miles, saves 0.1 MPG
- HNCO needs to be counted for regen of uncoated filters

Passive	Regenerations
---------	---------------

	Sample ID	Soot wt	Burnt Soot	Soot Loading	<b>Reaction Rate</b>		
		(g)	(g)	(g/L)	(mg/hr)		
[	Passive 370 $^\circ$	C 5%0 <sub>2</sub> (	0.15 NO <sub>2</sub> :NO <sub>x</sub> ,	)			
1	Pt, 5 g/ft3	0.2076	0.1735	7.169	30.9		
2	Pd, 5 g/ft3	0.2300	0.1645	7.942	28.2		
3	Cu-zeol	0.1346	0.0981	4.648	17.7		
4	Pt-Pd, 5 g/ft3	0.2200	0.2035	7.597	31.4		
5	Uncoated	0.2453	0.0433	8.471	12.0		
6	Pt, 30 g/ft3	0.2585	0.1868	8.927	30.6		
	Passive 370°	C 5%0 <sub>2</sub> (	0.5 NO 2:NO x)				
7	Pt, 5 g/ft3	0.1808	0.1808	6.243	57.9		
В	Pd, 5 g/ft3	0.1959	0.1959	6.765	50.5		
9	Cu-zeol	0.1560	0.1560	5.387	41.7		
0	Pt-Pd, 5 g/ft3	0.2067	0.2067	7.138	53.7		
1	Uncoated	0.3007	0.3007	10.384	76.4		
2	Pt, 30 g/ft3	0.2877	0.2877	9.935	83.3		
Ī	High temp pa	ssive 485°	C 5%O2 (0.15)	NO 2:NO 2)			
3	Pt, 5 g/ft3	0.1862	0.1862	6.430	19.9		
4	Pd, 5 g/ft3	0.1827	0.1827	6.309	20.9		
5	Cu-zeol	0.1625	0.1625	5.612	11.2		
6	Pt-Pd, 5 g/ft3	0.1498	0.1498	5.173	16.2		
7	Uncoated	0.2616	0.2616	9.034	13.7		
8	Pt, 30 g/ft3	0.2680	0.2680	9.255	24.4		

- 50% NO2 gives 2.5X faster rate (1-6 vs. 7-12) a.
- NO2 is more effective at 370C than at 485C (7-12 vs b. 13-18
- Pt samples at 370C and 50% NO2 are 15% faster (7, C. 10, 12 vs. 8, 9, 11); at 485C: 25% faster
- d. Cu-Z similar to uncoated.

Ford, SAE 2010-01-0533

# Direct oxidation soot catalyst is advanced.

Low or no PGM. Oxidation at 200C without NO<sub>2</sub>

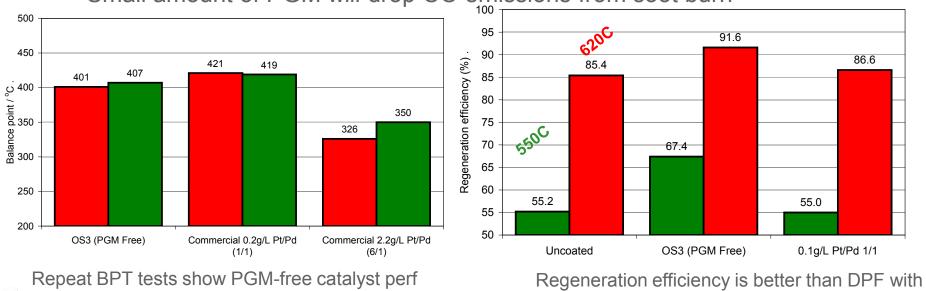
better than light PGM DPF.

• Basis is direct oxidation of soot by oxygen at the soot-catalyst interface. O<sup>2-</sup> conducting catalyst; no  $NO_2$ 

•Catalyst oxidizes soot at temperatures as low at 160C. Oxidation complete at 220C. No or low PGM

• Aided by good soot contact, but propagation occurs via exotherm. Low thermal mass DPF is beneficial.





light PGM loading.

### SiC membrane added to DPF drops activation energy and ignition temperature for soot burning. Shift in reaction mechanism is shown.

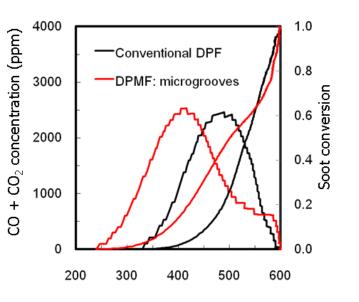
0

-2

-4

-6

ln ≮



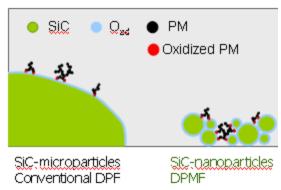
The DPF with SiC membrane reacts about 100C lower than conventional

-8 -10 0.0011 0.0013 0.0015 0.0017 0.0019 636 °C  $1/T(K^{-1})$ 253 °C The activation energy of soot burning makes it the predominant with the SiC membrane is lower (80

<sup>o</sup> Conventional DPF

DPMF: uniform

DPMF: microgrooves

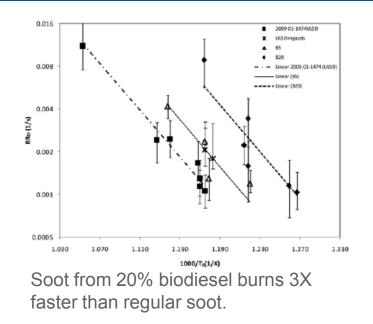


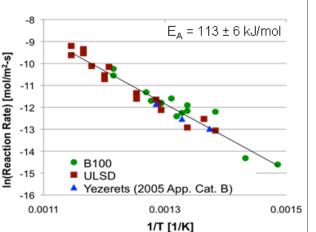
SiC has an adsorbed layer of oxygen. The high surface area oxidation mechanism.

Tokyo Inst Tech, SAE 2010-01-0808

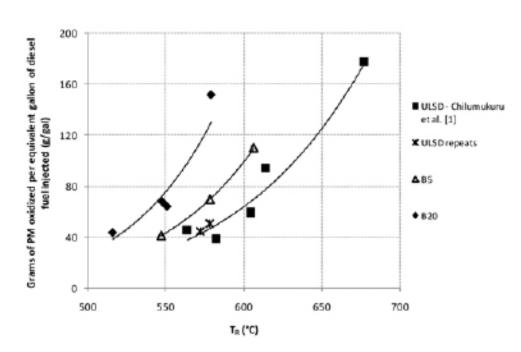
vs. 130 kJ/mole).

# Biodiesel blends burn faster and consume less fuel for regeneration.





MTU, SAE 2010-01-0557



3X more soot is burned per unit of fuel when 20% biodiesel is used.

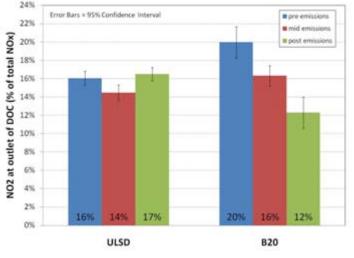
Biodiesel soot has more initial surface area. When this is normalized, reaction rates converge. (ORNL, CLEERS, 2010)

# Preliminary results are available on the effect of B20 ash on DPFs and DOCs.

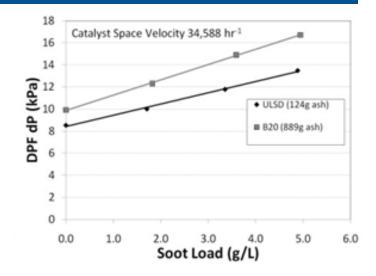
				-		-			
		Cord.	Cord.	SIC	SiC	AT	AT	Cord.ª	Cord. a
	Units	ULSD	B20	ULSD	B20	ULSD	B20	ULSD	B20
Ash loading	g/L	0.8	13.4	2.3	17.1	2.2	12.2	7.3	52.3
DPF T (avg)	°C	565	576	576	583	598	599	599	602
<650° C	hours	25.0	26.6	24.4	24.7	24.2	24.4	72.9	74.4
650°C to 750°C	hours	48.8	49.5	49.3	49.5	49.6	49.6	152.7	153.2
750°C to 850°C	hours	4.3	3.5	1.4	1.9	2.7	2.1	7.3	3.0
>850° C	hours	0.1	1.1	3.2	2.5	2.2	2.5	2.2	6.2

\* Accelerated durability tests conducted to 435,000 miles

B20 ash was at the maximum spec for Ca+Mg and alkali in accelerated loading (27X higher levels in fuel). Cordierite exposed to T>750C for >3-4 hrs.



150,000 mile effect of B20 on DOC NO2 formation.



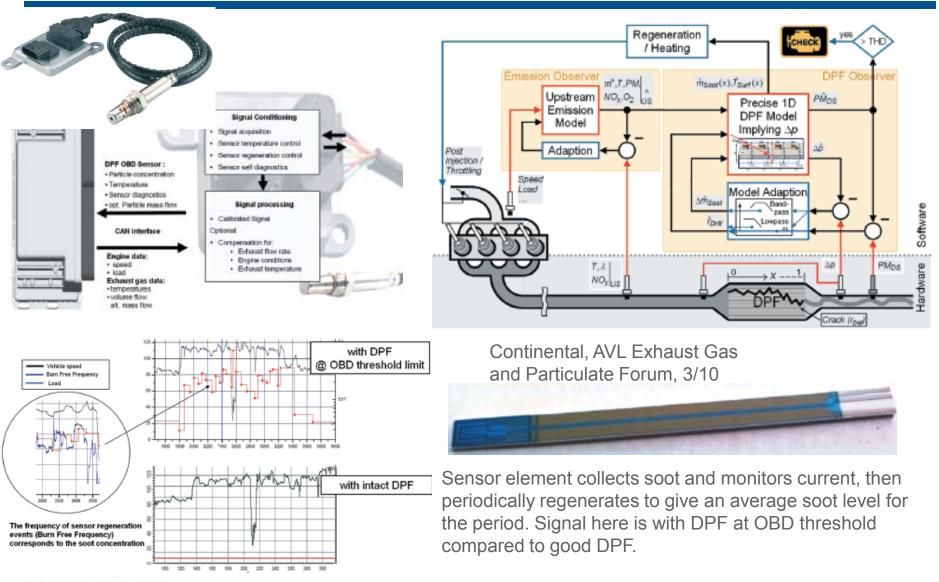
435,000 mile B20 ash loads results in 25% higher back pressure

• Filter properties of cordierite at 150,000 mile were the same for B20 and ULSD.

• Alkali was shown to chemically penetrate up to 30% into the cordierite wall.

NREL, 8-10

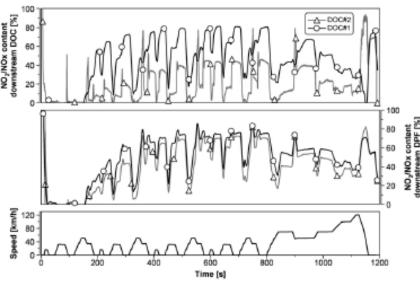
### PM sensor for OBD is reported.



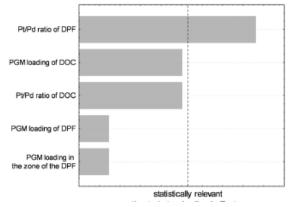
# CORNING

**Oxidation Catalysts** 

### NO<sub>2</sub> coming out of DPF is strongly dependent on DOC CO+HC removal efficiency and Pt loading of DPF. NO2 out of DOC minor impact. Zone coated DPF not effective



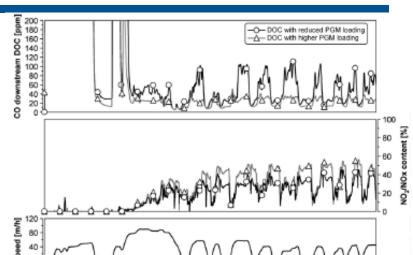
NO2 level coming out of CSF is generally independent of NO2 coming out of DOC. Both DOCs remove HC+CO efficiently.



Other:

•Zone coated DPF not as good as homogeneous coating. Even though front high loading cuts CO+HC, low rear loading can't form NO2

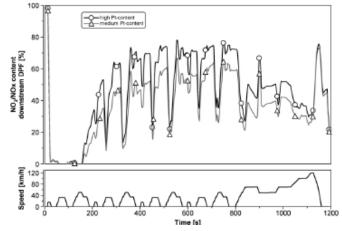
Umicore, AVL PM Forum 3/10



On the other hand, NO2 coming out of CSF is much more dependent on CO+HC coming out of DOC.

Time [s]

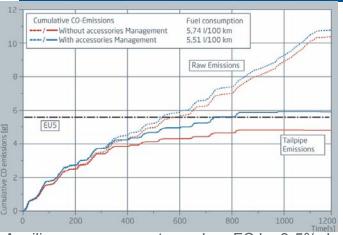
300



Impact of high Pt/Pd ratio in DPF. Same total loading

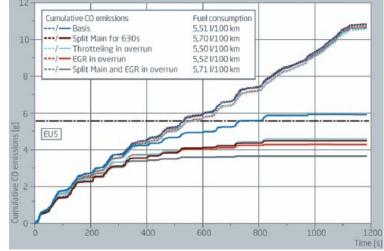
Pt/Pd ratio on DPF far outweighs PGM loading on DPF for NO2 formation.

### Fuel conservation measures can drop exhaust temperatures 5-10C°, resulting in CO increases. Intake throttling and EGR cutoff are effective measures to keep DOC hot.



Auxiliary management can drop FC by 3-5%, but exhaust T drops 5-10C°. CO emissions can increase 20%. 2 liter Euro 5, 1590 kg, 2-stage turbo.

IAV, AVL PM Symposium 3/10.



(1. Reduction of CO raw emissions by:

- 1.1 Optimization of pilot injection quantities
- 1.2 Shortening of pilot injection intervals
- 1.3 Optimization of rail pressure
- 1.4 Increasing of air mass

NVH concerns

- Increase exhaust-gas temperature to improve CO conversion by:
  - 2.1 Retarding of main injection
  - 2.2 Reduction of rail pressure
  - 2.3 Splitting of main injection into two injection events ("split main")
  - 2.4 Activation of the throttle valve while coasting
  - 2.5 Activation of exhaust-gas recirculation (EGR) while coasting (includ the necessary throttle valve control)

#### CORNERG

Measures increase exh T by 10-30C. EGR and throttling upon coasting are effective for this veh w/o FC incr.

## Summary

- HD regulations being wrapped up, next regs being contemplated
- Further tightening of criteria regs expected. California is beginning LEV3 proposal stage. EPA considering Tier 3.
- CO<sub>2</sub> mandates are proposed for HD
  - Onset of another major regulatory-driven technology evolution
- Engine technologies are addressing engine-out NOx and FC
  control LT thermal management, advanced combustion enpress
  - control, LT thermal management, advanced combustion approaches
- SCR is addressing "secondary" issues:
  - LT issues: ammonia sources and urea inj; NH3 storage formation, mechanisms.
  - Catalyst HT
  - More understanding on SCR+DPF
- New LNT compositions and designs are shown.
  - Better performance, lower cost
  - LNT+SCR systems advancing
- DPF regen, substrate properties, material, and catalysts advancing.
- DOC catalysts performance characterized
  - NO2
- LDD CO emissions can be difficult

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