

Phantom

Design, Fabrication, and Test of a 5 kWh Flywheel Energy Storage System Utilizing a High Temperature Superconducting Magnetic Bearing – Phase III

Phil Johnson
Program Manager
Boeing Phantom Works

Energy Storage Systems
DOE Peer Review - Sept, 2007

Flywheel Energy Storage Systems

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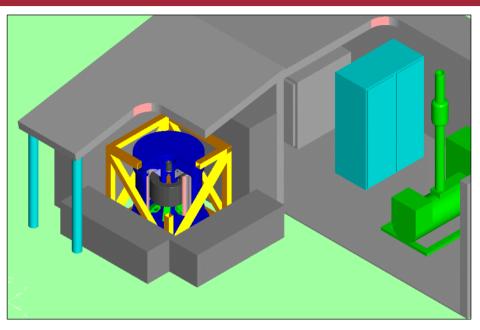
Superconducting Flywheel Development

Objective:

•Design, build and deliver flywheel energy storage systems utilizing high temperature superconducting (HTS) bearings tailored for uninterruptible power systems and off-grid applications

Goal:

•Successfully integrate FESS into a demonstration site through cooperative agreements with DOE and contracts with Sandia National Labs



Deployment of a demo system, shown in relation to diesel genset and balance of system.

Status:

- •The 1 kWh / 3 kW test was successful
- •The 5 kWh rotor is complete
- •The direct cooled High Temperature Superconducting bearing was successfully tested at ~15,000 RPM
- System design near completion

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Flywheel Energy Storage System

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Superconducting Flywheel Development

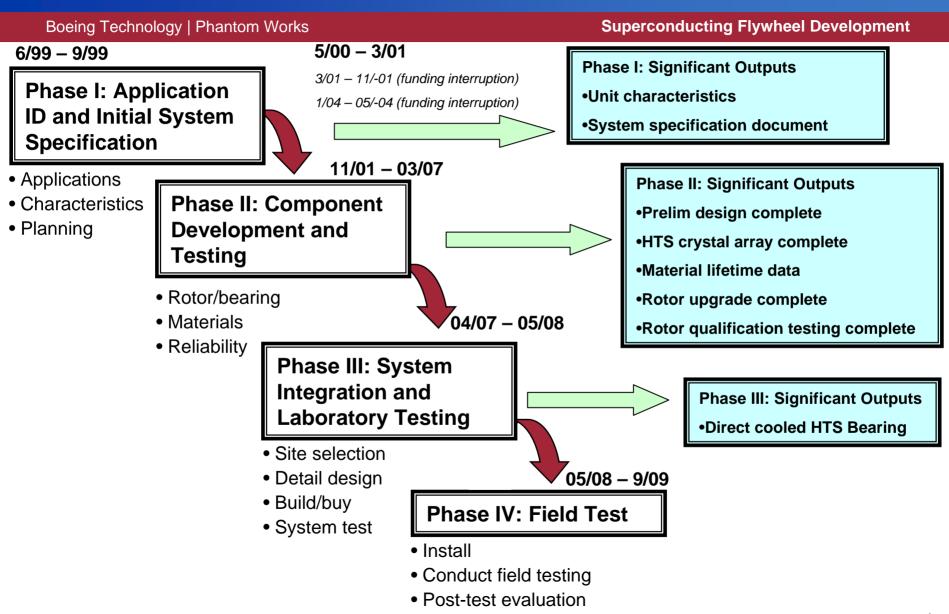
Why Pursue Flywheel Energy Storage?

- Non-toxic and low maintenance
- Potential for high power density (W/kg) and high energy density (W-Hr/kg)
- Fast charge / discharge times possible
- Cycle life times of >25 years
- Broad operating temperature range

Why use high temperature superconducting bearings?

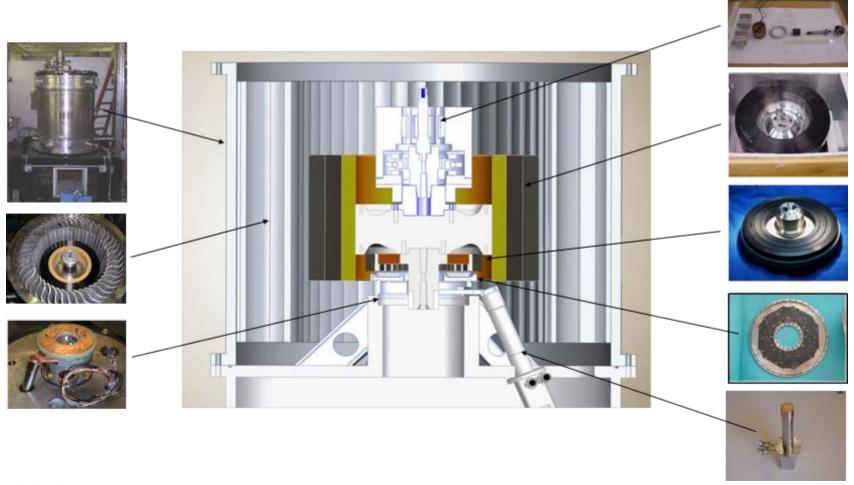
- Very low bearing losses to extend the idle mode
- HTS bearings will support ultra high-speed flywheels
 - (Energy = (1/2) (Moment of Inertia) (Spin Speed)^2)

Energy Storage Program 5 kWh / 3 kW Flywheel Energy Storage System Project Roadmap



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Design is based on 5 kWh rotor / 3kW generator

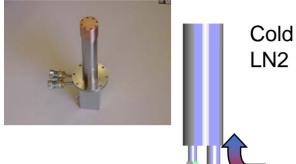


Past DOE/Boeing Flywheel Cryogenics

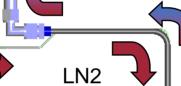
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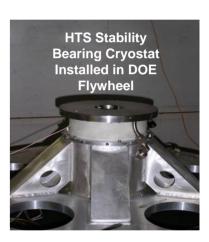
Thermosyphon Operation



Cold Head & LN2 Reservoir

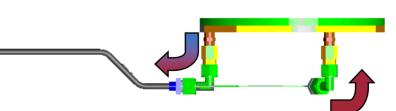


LN2 & N2 (Two phase flow)



HTS Bearing losses at 0.1% / hr including a cryogenic overhead factor of 20 at 77K

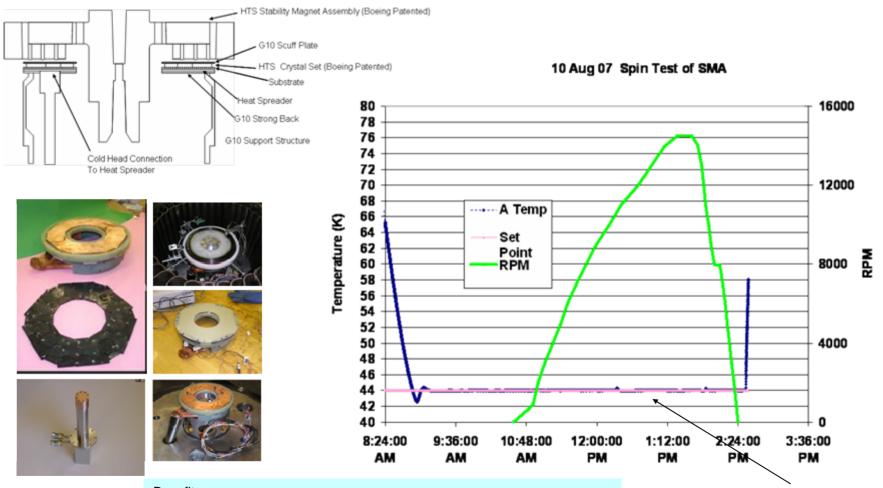
Cryostat (HTS)



Direct Cooling of HTS Bearing

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Benefits:

- •>50% reduction in parts
- •Power dropped from 60 Watts to an approximate 30 Watts of HTS cooling, with future refinements estimated to drop to <15 Watts
- •Eliminated the requirement for liquid nitrogen

HTS Bearing Well Regulated at 44K

Summary of Direct Cooled HTS Bearing Tests

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The direct cooled HTS bearing performed per design



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- Key Notes:
 - The HTS temperature was well regulated throughout the test sequence
 - The rotational losses decrease with decreasing HTS temperature
 - For temperatures that can be obtained in a liquid-nitrogen thermosiphon system, at a given speed and gap, the loss of the conduction-cooled HTS bearing is not significantly higher than the loss of a nearly identical HTS bearing cooled by flowing nitrogen from the thermosiphon
 - The contribution of the conduction-cooling apparatus to the eddy current loss in the bearing seems to be much lower than the eddy current loss in the SMA itself due to magnetization of the HTS
 - At 50 K, the expected contribution at a rotational rate of 20,000 rpm would be roughly the same as the hysteretic loss in the bearing (At 20,000 rpm, this would amount to 1.54 rpm/min)

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- The 1 kWh / 3 kW test was successful
- The 5 kWh rotor is complete
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- System design near completion
- Purchase order for motor controller are near release
- Starting to begin system integration

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