




Radioactive Air Emissions Application
for Approval to Construct or Modify
H2 Enclosure Ventilation System

Environmental Engineering/Evaluation Calculations

SPRU EEC-11-002 REVISION 2

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Separations Process Research Unit -
Disposition Project (SPRU-DP)

Radioactive Air Emissions Application for Approval
To Construct or Modify
H2 Enclosure Ventilation System

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Section A

Site Information

Separations Process Research Unit - Disposition Project (SPRU-DP)

Site Information

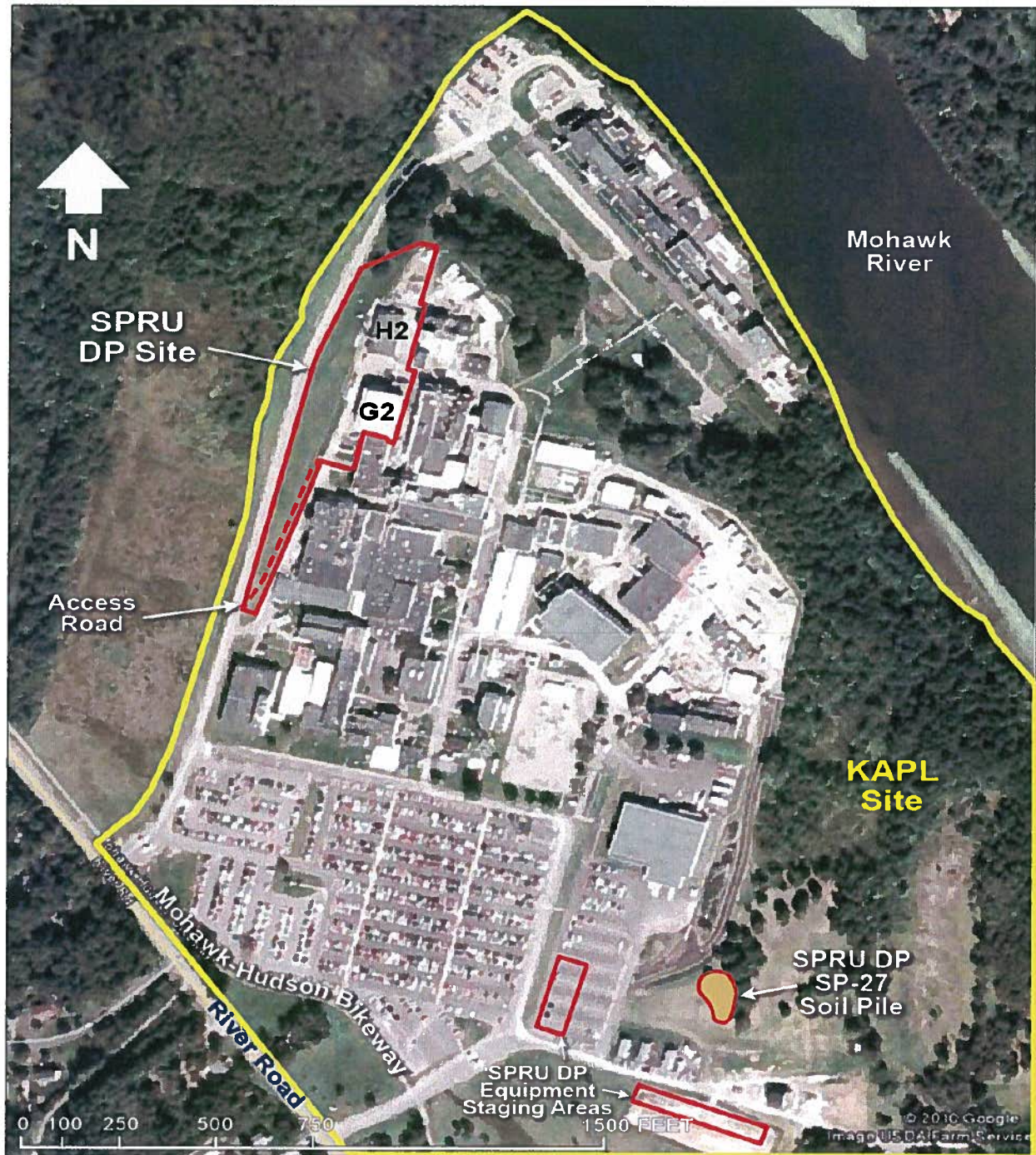
The Separations Process Research Unit (SPRU), located near Schenectady, New York, was operated from February 1950 to October 1953 for laboratory scale research and development on the REDOX (reduction/oxidation) and PUREX (plutonium-uranium extraction) processes. It supported operations at the Hanford Site (Washington State), and the Savannah River Site (South Carolina). The research was performed on a laboratory scale; SPRU never was a production plant. These activities left radioactive contamination inside the facilities.

- The main upper level SPRU Disposition Project facilities occupy approximately five acres on the 170-acre Knolls Atomic Power Laboratory (KAPL) site in Niskayuna, New York near the Mohawk River. KAPL is a U.S. Naval Nuclear Propulsion Program research and development facility operated under the auspices of the U.S. Department of Energy.

The SPRU facility (Figure A-1) consists primarily of two interconnected buildings (G2 and H2), portions of which lie underground:

- Building G2 – housed the laboratories, hot cells, separations process testing equipment, and the tunnel system beneath Building G2. Building G2 hot cells, equipment, ventilation/process piping systems, and tunnels contain residual radioactive contamination.
- Building H2 – used for liquid and solid waste processing. All areas of this building are contaminated or potentially contaminated.
- H2 Tank Farm (also known as the tank vaults) – a series of seven underground stainless steel tanks in concrete vaults along the eastern side of Building H2 used for storing liquid radioactive waste. The contents of these tanks have been consolidated into tank 509E.
- Pipe Tunnels – two concrete passageways. The first connecting Building H2 to Building G2; the second connecting Buildings G2, G1 and E1 (E1/G1 tunnels) which lie to the south and east of Building G2. The Pipe Tunnels contain radioactive piping and contaminated materials.

Figure A-1. Location of the SPRU Disposition Project (DP) Site



The facility is currently undergoing decontamination and decommissioning activities under the purview of the Department of Energy's (DOE) Office of Environmental Management (EM). In September 1992, the Department's Office of Nuclear Energy, (current organization is Office of Naval Reactors Laboratory Field Office [NRLFO]) and EM signed a Memorandum of Agreement (MOA) on decontaminating and decommissioning the SPRU facilities. The MOA was supplemented with the SPRU Functions, Assignments, and Responsibilities Agreement (FAR) in 2000, (current Revision 2, dated February 2009) establishing the roles and responsibilities of each Office regarding the decontamination and decommissioning of SPRU.

Upon the completion of the demolition and clean-up, and sampling to ensure the clean-up levels have been met, the land will be transferred back to the NRLFO for their continued mission use. EM and KAPL meet periodically to discuss mutual operations integration issues.

Environmental Restoration

The SPRU site process facilities and adjacent land areas are managed by the U.S. Department of Energy. The proposed action is the removal of Buildings G2 and H2, including the H2 and G2 tunnels, as well as the decontamination of the E1/G1 tunnels and the tank vaults, and removal of contaminated soils. By the end of 2010, a considerable amount of work to this end had been accomplished.

Section B

Technical Emission Point Information

I. Name & Address of Applicant

(Owner) US Department of Energy – Separations Process Research Unit- Disposition Project
Knolls Atomic Power Laboratory
Knolls Site
2425 River Road
Niskayuna, NY 12309

(Project Contractor) URS (previously Washington Group International [WGI])
Separations Process Research Unit – Disposition Project Office
2345 Nott Street East, Suite 201
Niskayuna, NY 12309

II. Name & Location of Proposed Source

H2 Enclosure Ventilation System

Separations Process Research Unit Disposition Project
Knolls Atomic Power Laboratory
Knolls Site
2425 River Road
Niskayuna, NY 12309

Facility Coordinates:

| | |
|-----------------------------|-----------------------------|
| Latitude | 42 Degrees 49 Minutes North |
| Longitude | 73 Degrees 52 Minutes West |
| Estimated Date of Shutdown: | To Be Determined |

III. Release Point Information – Emission Point ID: H2 Enclosure Ventilation Exhaust

Ground Elevation - 330 ft MSL (approximate),
Stack Height –6 ft (approximate, to centerline of horizontal stack),
Height above Structure – Not applicable. Horizontal stack approx. 6 ft above grade
Exhaust Duct Inside Dimensions - 60 inches dia. (nominal),
Exhaust Exit Temperature - 20-95°F, (ambient air),
Exhaust Exit Velocity - 30-45 ft/sec, (nominal)
Exhaust Exit Flow Rate -48,000 actual cubic feet per minute (ACFM) nominal
Monitoring Category – PIC 2 (ANSI/HPS N13.1-1999, Table 2)

IV. Technical Information About Source

Ventilation Unit Nature (typical unit)

- Modular HEPA filtration unit capable of providing High Efficiency Particulate Air (HEPA) filtration
- HEPA filters are each tested by the manufacturer to 99.97% efficiency with 0.3 μm AD aerosol
- Installed system has three parallel filtration trains
- Each train has a pre-filter and two banks of HEPA filters in series
- Each HEPA filter bank is tested in place to 99.95% efficiency with 0.7 μm AD aerosol

Size

- Three trains with 24"W X 24"H X 11.5"D HEPA filters in banks of 12 filters (3 x 4 array), two banks (stages) in series (double HEPA)
- HEPAs and pre-filter rated at train module design flow capacity of 16,000 ACFM
- One (1) air mover on each train
- Overall dimensions of each of three (3) filter train modules – 30 ft L x 10 ft W x 8 ft H
- Overall dimensions of the exhaust air mixer (approximate) – 25 ft L x 10 ft W x 8 ft H

Design

- Centrifugal fan air mover, with conventional bag-in/bag-out HEPA filter housing on each bank.
- Alarmed differential pressure gage across each filter bank and flow indicators mounted in a modular horizontally-placed housing.

Design Operating Capacity (nominal)

- 48,000 ACFM @ 15" w.g. (system capacity)

Representative Sample Withdrawal

- Three (3) modular HEPA filter trains discharge through a common generic air mixing device. A shrouded probe mounted in a representative sampling location has been qualified in accordance with ANSI/HPS N13.1-1999 [Ref.1]
- 20-100 liter per minute (LPM) adjustable sample rate
- 47 mm dia. particulate sample filter
- Integrated sample volume indication
- Exhaust air flow rate indication

V. Method of Source Operation and Description of Emission Controls

This application is for installation and operation of a HEPA-filtered ventilation exhaust system for an enclosure to be constructed over the H2 Building, debris pile, and the tank vaults. The ventilation system will exhaust the H2 enclosure by discharging HEPA-filtered air to the environment through an integrated mixing and sampling system. A source term that includes the estimated radioactive material inventory of Building H2, Tank Farm, G2/H2 tunnel, and sludge is the basis source term for this

application. Use of this ventilation system will result in actual emissions of lesser magnitude than modeled because the modeled filtration efficiency for each stage (99%) is conservative with respect to the actual tested efficiency for each bank (99.95%). Each train with the dual HEPA filtration is tested to be 99.999975% efficient. The optional use of PVUs inside the enclosure for work in the more contaminated areas adds another expected abatement factor which is not included in the H2 Building enclosure abatement calculation. The type of work supported by this enclosure ventilation system includes, but is not limited to, decontamination of the G2/H2 tunnel, packaging and removal of the H2 Building debris pile, removal of components from and decontamination of rooms and cells/pipe tunnels in Building H2, sludge equipment maintenance, sludge solidification, removal of the sludge tanks, decontamination of tank vaults, and other similar activities within the H2 Building and tank vault area covered by the enclosure.

Portable HEPA ventilation units operating on localized contaminated areas within the enclosure will also discharge to the H2 enclosure exhaust system. PVU operation inside the enclosure does not change the overall enclosure exhaust ventilation rate, monitoring requirements, or estimated emission rates.

The H2 enclosure ventilation system has three trains of equipment in parallel. Each train will be equipped with a spark arrestor, pre-filter, and two HEPA filter stages in series. The HEPA filters are tested and operated according to DOE regulations and guidance, and in accordance with Project procedures. These procedures include preoperational and annual in-place testing, annual calibrations of flow meters, and frequent monitoring by technicians for dose rate buildup, filter loading, and filter breaches. The H2 enclosure ventilation emissions are monitored for radioactivity with a continuous air particulate sampler at the point of discharge. Differential pressure across each HEPA filter bank is monitored, alarmed and interlocked to automatically place the system in a safe condition if the differential pressure is outside the acceptable operating range. Both sample volume and ventilation duct flow rate are measured and displayed using calibrated instruments.

It is important to note that this system consists of three (3) dual-HEPA-filtered exhaust trains operating singly or in combination, but discharging to the environment through a single mixing chamber and continuously sampled exhaust duct. (See Attachment D, Equipment Sketches and Specification Details.) Depending upon the configuration required to maintain enclosure negative air pressure, one, two, or three trains may be in operation at a given time.

Radioactive Emission Estimates

The source terms herein have been derived from analytical data, empirical measurements, and estimates of contaminant distribution based upon historical documentation and process knowledge. The dose to the maximally exposed offsite individual (MEOSI) was calculated using an EPA-approved dispersion code, CAP88-PC Version 3.0. [Ref. 2] Due to the density and close proximity of residences to several sector boundaries, the location of the MEOSI may shift year-to-year if annual dispersion results change slightly in relation to the 1989-2004 base period used in this analysis.

The source term that is used to calculate the effective dose equivalent (EDE) to the MEOSI is the entire source term of the H2 Building (which includes the G2/H2 tunnel), the sludge, and the tank vaults. Dose estimates are based on releases of H2 enclosure emissions at a two-meter elevation with no plume rise. The abated dose to the MEOSI based on processing the entire source inventory of the H2 Building and sumps, sludge, and tank vaults, is calculated to be $1.3\text{E-}04$ mrem/year, as shown in Attachment A.

Technical Information About Sampling

The sampler unit for collecting airborne particulate from the H2 enclosure ventilation exhaust ducting will be a stand-alone unit consisting of a filter assembly and a vacuum pump of sufficient capacity to withdraw a sample continuously through a 47 mm diameter filter for up to ten days without unacceptable filter loadup. Based upon the graded approach in Table 2 of ANSI/HPS N13.1-1999, this sampler will be continuously operated as a PIC 2 emission point sampler. Typically, samples will be changed weekly for units in continuous operation. Sampler system maintenance, filter handling, operation, calibration, and documentation will be specified in Project procedures. The sampling will be in compliance with the quality assurance project plan [Ref. 3] specific to SPRU's radiological NESHAP-related activities, and with ANSI/HPS N13.1-1999.

The sample withdrawal point will be within the center of area of the duct, and will be a shrouded probe design as described in ANSI/HPS N13.1-1999. The use of a mixing box that is scaled from a tested stack design and has successfully passed proof testing per Section 5.2.2.2 of ANSI/HPS N13.1-1999 will ensure collection of a representative sample.

Sample filters will generally be changed and assayed for gross radioactivity weekly. The filters will be composited in quarterly batches and analyzed for the major radionuclides of concern shown in Table A-4 in Attachment A, using 40 CFR 61 Appendix B, Method 114, EPA-approved measurement techniques. [Ref. 4; also see the Quality Assurance Project Plan, Ref.3.]

Analytical detection levels allow monitoring sample activity at levels that would indicate a chronic increase before it became a cause for operational concern. Detection of radioactivity above normal operational levels on a given sample will be cause for management notification, verification testing, and evaluation of a potential release greater than normally expected variations.

Summary

In summary, the management of H2 enclosure emissions presented here shows that, under normal operating conditions, the H2 enclosure ventilation unit operated at SPRU-DP will, through a combination of engineered controls and operational limitations, limit environmental releases of radioactivity to levels below well below the 40 CFR 61 Subpart H dose limits.

Section C

H2 Enclosure Ventilation Exhaust Monitoring for Radioactivity

H2 Enclosure Ventilation Exhaust Monitoring for Radioactivity

Purpose

The H2 enclosure ventilation exhaust monitoring at the Separations Process Research Unit (SPRU) Disposition Project (SPRU-DP) has two major purposes:

- Provide accurate assessment of normal operations
- Provide accurate and rapid assessment of upset radioactivity releases.

To properly quantify and assess the impacts of radioactivity potentially present in effluent air, a continuous integrated sample is withdrawn and measured offline. This provides accurate and quality-controlled laboratory measurement of radionuclides present in the discharge stream. Radiological screening of the particulate radioactivity on the sample filters is conducted using on-site gas proportional alpha-beta counters. The screening data are used to assess weekly and cumulative emissions for radioactivity trends. The filters are composited quarterly and sent to a laboratory offsite for isotopic analysis.

Upon identification of elevated gross particulate radioactivity in either workspace airborne monitoring or upon H2 enclosure exhaust filter screening, further filter analysis and area surveys will provide information required for rapid dose assessment purposes. Additional off-normal processes are described in the SPRU-DP NESHAPs Quality Assurance Project Plan. [Ref. 3]

Scope

The sampling pump is sized to provide the sample flow rate required for the shrouded probe. The shrouded probe is tested and qualified for specific combinations of exhaust flow velocity and nozzle inlet velocity. The sample pump installed on the exhaust duct sample train is sized to the nozzle's operating requirements with the design sampling range of 30 - 70 LPM for an exhaust flow rate range of 16,000 - 48,000 CFM. The normal sampling rate is 55 - 60 LPM for an exhaust flow rate of 44,000 - 48,000 CFM. This design provides optimum sensitivity for the sampler by collecting suitably-sized volumes, consistent with the ANSI/HPS N13.1-1999 requirements. [Ref. 1] The analysis of the sample filters will provide documented radioactive airborne particulate emissions data when combined with the measured system exhaust flow rate and sample withdrawal rate.

System Design

The H2 enclosure ventilation sampling system is designed to meet the applicable criteria in ANSI/HPS N13.1-1999, as referenced by 40 CFR 61 Subpart H. [Ref. 4] The shrouded withdrawal probe is specifically sized and ported to withdraw a sample from a single representative point, a well-characterized measurement location with uniform velocity and particulate distributions within the effluent duct, and the sample line and nozzle are designed to meet the Standard's requirements for

aspiration and transport efficiency of 10 μm aerodynamic diameter (AD) particles. (See Attachment D for nozzle specifications.)

The measured exhaust flow rate is used to adjust the sampling rate if the ventilation flow changes. Sample transport lines to the collection devices are sized to provide nonrestrictive turbulent flow under normal conditions. The sample line provides a long-radius bend for ninety-degree turns. Joints in the sample withdrawal section use butt-joined connectors that allow easy maintenance and component replacement as well as internally smooth surfaces critical to ensuring adequate particle penetration. Materials used in sample transport lines and connectors are corrosion resistant metals non-reactive to the intended sample stream (e.g., stainless steel) in order to maintain stable internal pipe wall conditions and prevent line loss due to static electricity buildup. Heat tracing will be used if needed to maintain sample line temperatures well above dew point for the sample stream being sampled, although for typical ambient air use this is not expected to be necessary.

The accurate quantification of radionuclide emission relies on several variables, including precise unbiased measurement of sample volume. This critical factor is controlled by utilizing air flow measuring devices calibrated by traceable instruments corrected for temperature, vacuum, and intrinsic instrument bias to initially qualify the sampling system and periodically verify accuracy. Installed calibrated air flow indicators provide system performance stability verification and total sample volume for routine sample collection.

The exhaust flow from the ventilation system will initially be tested for velocity, temperature, humidity, and flow direction in accordance with Methods 1 and 2 of 40 CFR 60, Appendix A. [Ref. 5] Testing and inspection will be performed and documented for the operational life of each system, as applicable, per ANSI/HPS N13.1-1999. The full qualification and maintenance requirements will be applied as applicable under the ANSI/HPS Standard graded approach recommendations.

Ventilation system sampling and filtration equipment, flow measurements, sampling system operation, sample media controls, system parameter data management, and attendant data reduction and calculations are subject to an overall site quality assurance plan. In addition, a NESHAPs-specific quality requirements document, SPRU-ENV-012, Quality Assurance Project Plan for Measurements of Radionuclide Air Concentrations for Rad NESHAP Compliance at the SPRU-DP, consistent with Method 114 of Appendix B in 40 CFR 61 and ANSI/HPS N13.1-1999, is specifically directed to radioactive airborne emissions-related monitoring.

System Operation

The 47 mm diameter filter sample media are changed on a weekly schedule, at which time any minor adjustments to flow rate or sample line temperature are made and recorded. Sample media are counted upon removal and after a holding period (for natural isotope decay) on a laboratory instrument for gross radioactivity, and filter composites are analyzed quarterly for Sr-90, gamma emitters (Cs-137), and alpha isotopic (Pu-238/239/240, Am-241) parameters.

The sample flow and exhaust flow will be determined empirically and documented for the H2 enclosure ventilation system. The radioactivity release quantity will be calculated based upon the relative flow rates and the radionuclide analytical values in a given sample composite or individual filter.

System Performance

For a sampler operating at 60 LPM, the sensitivity is typically 5E-18 $\mu\text{Ci/mL}$ for alpha isotopes, 5E-17 $\mu\text{Ci/mL}$ for Sr-90, and 5E-17 $\mu\text{Ci/mL}$ for Cs-137 in a quarterly composite. Actual flow rates will be measured and emission calculations will be based upon the empirical measurement.

Section D

Ventilation Exhaust Filtration Efficiency Testing and Acceptance Criteria

H2 Enclosure Ventilation Exhaust Filtration Efficiency Testing and Acceptance Criteria

H2 Enclosure Ventilation Exhaust Filtration Efficiency Testing

Ventilation is filtered through three (3) HEPA filter trains. Each train at minimum has a pre-filter, and two (2) HEPA filter banks (stages) in series that meet nuclear air cleaning efficiency standards and have been tested to demonstrate compliance with those standards. In addition, a filter differential pressure indicator allows an objective measurement of filter resistance (loading) for maintaining adequate design filtration within equipment specifications, and feedback for limit controls. Periodic (annual) challenge testing of each bank (stage) of the in-place HEPA filters is documented.

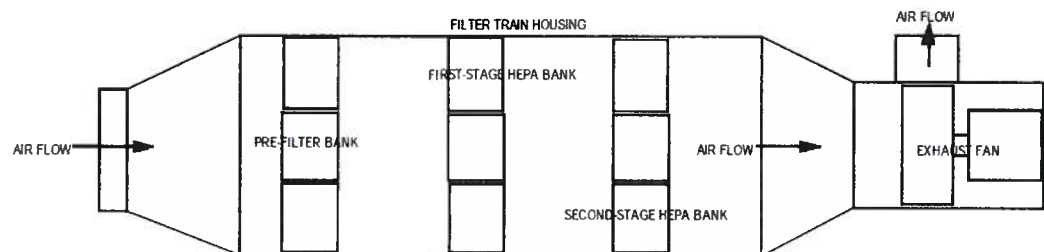
Filter differential pressures are checked to be within the unit recommended operating range (per the manufacturer's recommendations) prior to startup in a radiological application. An alarm indicates if the filter's differential pressure exceeds high or low set point limits during operation.

H2 Enclosure Ventilation System Aerosol Test Procedures and Acceptance Criteria

HEPA filters are used at the SPRU-DP in forced air ventilation systems to remove radioactive particulates from ventilation exhaust streams. These filters are individually tested by the manufacturer to be 99.97% efficient or greater for removal of particles of 0.3 μm aerodynamic diameter (AD). To assure that these filters are installed and functioning properly, a dioctyl phthalate (DOP), or approved equivalent aerosol challenge test is performed on each bank (stage) of the HEPA filter train prior to initial operation and after filter replacement. The test is conducted on each as-installed bank of HEPA filters in the ventilation system. For HEPA filters in series, each bank (stage) is separately tested. HEPA filter systems operating at the SPRU-DP are tested annually. Systems tested in place, including the H2 enclosure ventilation system module HEPA banks, must demonstrate a removal efficiency of at least 99.95% (0.0005 penetration) for 0.7 μm AD aerosols per DOE standards. A double HEPA filter train (filter banks in series) would have a tested efficiency of 0.0005 times 0.0005 (0.00000025 penetration, or 99.999975% removal efficiency) for 0.7 μm AD aerosols. [Ref. 6] Pre-filters are installed per manufacturer's instructions, and are not given an efficiency rating.

The H2 enclosure ventilation system will consist of three (3) parallel filter trains each containing a pre-filter (non-tested), a first-stage HEPA filter bank (tested), a second-stage HEPA filter bank (tested), and an exhaust fan.

Figure D-1. System Filter Train



Section E

References

References

1. American National Standards Institute, *Sampling and Monitoring Releases of Airborne Radioactive Substances from the Stacks and Ducts of Nuclear Facilities*, ANSI/HPS N13.1-1999
2. CAP88-PC Version 3.0 User Guide, USEPA Office of Radiation and Indoor Air, Washington, DC. December 09, 2007
3. Quality Assurance Project Plan for Measurements of Radionuclide Air Concentrations for Rad NESHAP Compliance at the SPRU-DP, SPRU-ENV-012, May 2011
4. 40 CFR 61 Subpart H, National Emission Standards for Emissions of Radionuclides Other Than Radon From Department of Energy Facilities
5. 40 CFR 60, Standards of Performance for New Stationary Sources, Appendix A, Test Method 1, Sample and Velocity Traverses for Stationary Sources; and Method 2, Determination of Gas Velocity and Volumetric Flow Rate
6. DOE HDBK-1169-2003, Nuclear Air Cleaning Handbook, 2003

Supporting References:

1. Andrew R. McFarland et al. *A Generic Mixing System for Achieving Conditions Suitable for Single Point Representative Effluent Air Sampling*, Health Physics 76(1)17-26, January 1999
2. Mark L. Maiello and Mark D. Hoover, *Radioactive Air Sampling Methods*, CRC Press, 2011

Attachment A

Source Term and Radiological Impact Modeling

Source Term and Radiological Impact Modeling

Introduction

Section B, "Technical Emission Point Information," and Section C, "H2 Enclosure Ventilation Exhaust Monitoring for Radioactivity," provide a description of the H2 enclosure ventilation system and associated sampler unit. These sections also provide the methodology for monitoring and managing the emissions from the H2 Building enclosure ventilation system. This section (Attachment A) provides the source terms, calculated emissions, and the resulting effective dose equivalent (EDE) to the maximally exposed off-site individual (MEOSI).

Source Term Identification

The source term is derived from the entire radioactive inventory associated with the H2 Building process equipment, sumps, rooms, and the debris pile, including the radioactive contamination in the G2/H2 tunnel; contaminated surfaces and equipment in the tank vaults; and the sludge.

The H2 Building and tank farm structures will be covered with an enclosure that maintains a negative internal pressure. The enclosure will be exhausted through a ventilation system equipped with pre-filters and dual HEPA filters, which consist of two banks in series. The removal of the H2 Building contents, the decontamination of the remaining structural shell, and the removal of contaminated floors and underlying soil will be conducted within the enclosure. Sludge solidification, tank vault equipment removal, and vault decontamination will also be conducted under this enclosure.

The prospective dose assessment related to work activities inside the H2 enclosure is based on the following assumptions:

- All emissions from the work activities are exhausted through the H2 enclosure ventilation system
- All emissions are released from the H2 enclosure exhaust duct. Prospective doses to offsite receptors are calculated from a location in the center of the SPRU DP work area and occur within a single calendar year. Note that retrospective doses that are included in compliance reports would typically be calculated based on a single emission point in the center of the KAPL site, which also is consistent with the location specified in Section B II.
- The doses for the nearby businesses and residents were determined using CAP88-PC Version 3.0 [Ref. A-1] with KAPL meteorological data from 1989 to 2004 and calculated emissions.
- The abated point source emission is based on the physical state factor in Appendix D of 40 CFR 61, [Ref. A-2] and the abatement provided by air filtration systems (0.01 for each of two HEPA filters in series)

- The emissions are modeled as point sources from a two-meter high horizontal stack with an assigned discharge momentum of zero. Because the momentum is assumed to be zero (no direct upward direction, i.e. zero velocity), the calculated dose is conservative. The diameter of the duct at the point of discharge does not affect the calculated doses within the calculation uncertainty range. If the velocity is set to 0.001 m/s, as is the practice in some models, there is no difference in the reported dose.
- For receptor locations, the rural food option in CAP88-PC was selected. The doses reported by CAP88 at the business locations are each divided by three to obtain the receptor doses at business locations
- The analysis includes all radionuclides that are expected to be in the process source term as well as all radionuclides that were detected in analyzed characterization samples. Four radionuclides (Cs-137, Sr-90, Pu-239 and Am-241) accounted for 99% of the dose to an offsite receptor.

Background of Calculation

CALCULATION METHODS

The radioactive material inventory from Building H2 (which also includes the G2/H2 tunnel inventory), and the tank vaults (including the sludge) is used to determine the source term for the EDE calculation. Appendix D factors are used in both the abated and unabated calculations to determine the emissions amount in curies:

$$E = (ST)(PS)(CF) \quad (A-1)$$

Where:

- E = Emissions, curies
- ST = Source Term or source inventory, curies
- PS = Physical State factor, dimensionless
- CF = Effluent Control Factor adjustment, dimensionless

And:

The Physical State factor (PS) for particulates is given in Appendix D of 40 CFR 61 (for materials below 100 degrees C):

$$PS_{\text{particulate}} = 1E-03$$

The PS for C-14 is one.

And:

The Effluent Control Adjustment Factors (CF) are those given in Table 1 of Appendix D.

For emission estimates:

$$CF_{\text{unabated}} = 1$$

$$CF_{\text{HEPA}} = 0.01 \text{ (for each of two HEPA filters)}$$

Radioactive Material Inventory

The radioactivity inventory estimates for the material inside the H2 Building enclosure are tabulated in Table A-1. The relative abundance of each minor radionuclide was proportioned to Pu-239 for plutonium and alpha emitters, or to the total Cs-137 plus Sr-90 inventory for beta-gamma emitters, based on laboratory analysis of characterization samples. Note that Sr-90 and Cs-137 progeny are included.

Table A-1. H2 Building Enclosure Radioactive Material Inventory (Ci)

| Radionuclide | H2 Building Inventory (Ci) |
|--------------|----------------------------|
| Pu-239 | 3.8 |
| Am-241 | 0.54 |
| Pu-241 | 0.51 |
| Sr-90 | 11 |
| Y-90 | 11 |
| Cs-137 | 34 |
| Ba-137m | 34 |
| U-233 | 3.2E-03 |
| U-234 | 2.4E-02 |
| U-235 | 9.9E-04 |
| U-238 | 1.6E-02 |
| C-14 | 2.7E-03 |
| Fe-55 | 1.5E-03 |
| Ni-63 | 2.1E-03 |
| Pu-238 | 5.0E-02 |
| Tc-99 | 3.6E-03 |
| Th-228 | 1.8E-04 |
| Th-230 | 1.6E-05 |
| Th-232 | 1.5E-04 |
| Pm-147 | 1.4E-01 |
| TOTAL | 95.09 |

Unabated Source Term Calculation

Using the Physical State factors from Appendix D, an unabated source term, which is the emissions potential without engineered controls, was developed from the radioactive material inventory, using equation A-1. The estimated emissions using Equation A-1 for Cs-137 for the H2 enclosure are:

$$E = (ST)(PS)(CF)$$

$$E = (34)(1.00E-03)(1)$$

$$E = 3.4E-02 \text{ Ci}$$

The unabated emissions results for the H2 Building enclosure radionuclide inventory are provided in Table A-2.

Table A-2. H2 Building Enclosure Unabated Source Term

| Radionuclide | H2 Building Inventory (Ci) | Physical State Factor (PS) | Control Factor (CF) | Source Term in Curies (E) |
|--------------|----------------------------|----------------------------|---------------------|---------------------------|
| Pu-239 | 3.8 | 1E-03 | 1 | 3.8E-03 |
| Am-241 | 0.54 | 1E-03 | 1 | 5.4E-04 |
| Pu-241 | 0.51 | 1E-03 | 1 | 5.1E-04 |
| Sr-90 | 11 | 1E-03 | 1 | 1.1E-02 |
| Y-90 | 11 | 1E-03 | 1 | 1.1E-02 |
| Cs-137 | 34 | 1E-03 | 1 | 3.4E-02 |
| Ba-137m | 34 | 1E-03 | 1 | 3.4E-02 |
| U-233 | 3.2E-03 | 1E-03 | 1 | 3.2E-06 |
| U-234 | 2.4E-02 | 1E-03 | 1 | 2.4E-05 |
| U-235 | 9.9E-04 | 1E-03 | 1 | 9.9E-07 |
| U-238 | 1.6E-02 | 1E-03 | 1 | 1.6E-05 |
| C-14 | 2.7E-03 | 1 | 1 | 2.7E-03 |
| Fe-55 | 1.5E-03 | 1E-03 | 1 | 1.5E-06 |
| Ni-63 | 2.1E-03 | 1E-03 | 1 | 2.1E-06 |
| Pu-238 | 5.0E-02 | 1E-03 | 1 | 5.0E-05 |
| Tc-99 | 3.6E-03 | 1E-03 | 1 | 3.6E-06 |
| Th-228 | 1.8E-04 | 1E-03 | 1 | 1.8E-07 |
| Th-230 | 1.6E-05 | 1E-03 | 1 | 1.6E-08 |
| Th-232 | 1.5E-04 | 1E-03 | 1 | 1.5E-07 |
| Pm-147 | 1.4E-01 | 1E-03 | 1 | 1.4E-04 |

Abated Source Term Calculation

The emissions potential that includes engineered controls was developed from the radioactive material inventory, using equation A-1. The estimated abated emissions using Equation A-1 for Cs-137 are:

$$E = (ST)(PS)(CF)$$

$$E = (34)(1.00E-03)(0.01)(0.01)$$

$$E = 3.4E-06 \text{ Ci}$$

The abated emissions results for the H2 Building enclosure radionuclide inventory are provided in Table A-3.

Table A-3. H2 Building Enclosure Abated Source Term

| Radionuclide | H2 Building Inventory (Ci) | Physical State Factor (PS) | Control Factor (CF) | Source Term in Curies (E) |
|--------------|----------------------------|----------------------------|---------------------|---------------------------|
| Pu-239 | 3.8 | 1E-03 | 1E-04 | 3.8E-07 |
| Am-241 | 0.54 | 1E-03 | 1E-04 | 5.4E-08 |
| Pu-241 | 0.51 | 1E-03 | 1E-04 | 5.1E-08 |
| Sr-90 | 11 | 1E-03 | 1E-04 | 1.1E-06 |
| Y-90 | 11 | 1E-03 | 1E-04 | 1.1E-06 |
| Cs-137 | 34 | 1E-03 | 1E-04 | 3.4E-06 |
| Ba-137m | 34 | 1E-03 | 1E-04 | 3.4E-06 |
| U-233 | 3.2E-03 | 1E-03 | 1E-04 | 3.2E-10 |
| U-234 | 2.4E-02 | 1E-03 | 1E-04 | 2.4E-09 |
| U-235 | 9.9E-04 | 1E-03 | 1E-04 | 9.9E-11 |
| U-238 | 1.6E-02 | 1E-03 | 1E-04 | 1.6E-09 |
| C-14 | 2.7E-03 | 1 | 1E-04 | 2.7E-07 |
| Fe-55 | 1.5E-03 | 1E-03 | 1E-04 | 1.5E-10 |
| Ni-63 | 2.1E-03 | 1E-03 | 1E-04 | 2.1E-10 |
| Pu-238 | 5.0E-02 | 1E-03 | 1E-04 | 5.0E-09 |
| Tc-99 | 3.6E-03 | 1E-03 | 1E-04 | 3.6E-10 |
| Th-228 | 1.8E-04 | 1E-03 | 1E-04 | 1.8E-11 |
| Th-230 | 1.6E-05 | 1E-03 | 1E-04 | 1.6E-12 |
| Th-232 | 1.5E-04 | 1E-03 | 1E-04 | 1.5E-11 |
| Pm-147 | 1.4E-01 | 1E-03 | 1E-04 | 1.4E-08 |

MEOSI Dose Calculation

The estimated dose to the MEOSI residing at a location 540 meters from the center of the SPRU-DP work area in the south-southwest sector has been calculated for the activities that could occur during the identified scope of work within the ventilated H2 enclosure. [See Figure B-2]

The unabated dose was calculated using CAP88-PC Version 3.0. The resulting CAP88 dose reports demonstrate that four major radionuclides (Cs-137, Sr-90, Pu-239, and Am-241) account for 99% of the dose to an offsite individual. Table A-4 (from Attachment C-2, Abated CAP88-PC Dose Runs) shows the relative percentage of doses attributed to the radionuclides (including daughters) within the H2 Building enclosure. Therefore monitoring of other radionuclides in the point source effluent is not required.

Table A-4. H2 Enclosure Dose Summary by Key Radionuclide

| Nuclide | Dose to MEOSI (mrem/yr) | % of Dose |
|----------------|--------------------------------|------------------------------|
| Pu-239 | 5.42E-05 | 42.1% |
| U-235 | 0.00E+00 | 0.0% |
| Th-231 | 0.00E+00 | 0.0% |
| Pa-231 | 0.00E+00 | 0.0% |
| Sr-90 | 1.99E-05 | 15.5% |
| Y-90 | 6.98E-08 | 0.1% [Sr-90 progeny] |
| Cs-137 | 3.34E-05 | 25.9% |
| Ba-137m | 8.66E-07 | 0.7% [Cs-137 progeny] |
| U-234 | 1.91E-07 | 0.1% |
| Th-230 | 0.00E+00 | 0.0% |
| Ra-226 | 0.00E+00 | 0.0% |
| Rn-222 | 0.00E+00 | 0.0% |
| U-235 | 0.00E+00 | 0.0% |
| U-238 | 1.09E-07 | 0.1% |
| Th-234 | 0.00E+00 | 0.0% |
| C-14 | 1.84E-08 | 0.0% |
| Fe-55 | 0.00E+00 | 0.0% |
| Ni-63 | 0.00E+00 | 0.0% |
| U-233 | 0.00E+00 | 0.0% |
| Th-229 | 0.00E+00 | 0.0% |
| Pu-238 | 6.80E-07 | 0.5% |
| U-234 | 0.00E+00 | 0.0% |
| Pu-241 | 7.54E-08 | 0.1% |
| Am-241 | 1.92E-05 | 14.9% |
| Np-237 | 0.00E+00 | 0.0% |
| U-237 | 0.00E+00 | 0.0% |
| Tc-99 | 0.00E+00 | 0.0% |

| Nuclide | Dose to MEOSI (mrem/yr) | % of Dose |
|--------------|-------------------------|---------------|
| Th-228 | 0.00E+00 | 0.0% |
| Ra-224 | 0.00E+00 | 0.0% |
| Th-232 | 0.00E+00 | 0.0% |
| Ra-228 | 0.00E+00 | 0.0% |
| Pm-147 | 5.85E-10 | 0.0% |
| Sm-147 | 0.00E+00 | 0.0% |
| TOTAL | 1.29E-04 | 100.0% |

Table A-5 presents a source term development summary for these four key radionuclides identified in Table A-4. Note that the unabated emissions were used as input for the CAP88-PC run represented in Attachment C-1, and abated emissions for the CAP88-PC run represented in Attachment C-2.

Table A-5. H2 Enclosure Source Term Development Summary by Key Radionuclide

| | Cs-137 | Sr-90 | Pu-239 | Am-241 |
|---|-------------|-------------|-------------|-------------|
| Radioactive Material Inventory (Ci) | 3.4E+01 | 1.1E+01 | 3.8E+00 | 5.4E-01 |
| Physical State (PS) Factor | 1E-03 | 1E-03 | 1E-03 | 1E-03 |
| Unabated Source Term (CAP88-PC Input) (Ci) | 3.4E-02 | 1.1E-02 | 3.8E-03 | 5.4E-04 |
| Control Factor for Two(2) HEPA Filters in Series | (0.01*0.01) | (0.01*0.01) | (0.01*0.01) | (0.01*0.01) |
| Abated Source Term (CAP88-PC Input) (Ci) | 3.4E-06 | 1.1E-06 | 3.8E-07 | 5.4E-08 |

These calculations overestimate likely releases because each bank of the filtration systems is tested to 99.9+% efficiency performance. Table A-6 summarizes the doses estimated using the above emissions.

Table A-6. H2 Building Enclosure MEOSI Dose Summary (mrem/yr)

| Source Area | Cs-137 | Sr-90 | Pu-239 | Am-241 | TOTAL |
|--|---------|---------|---------|---------|---------|
| H2 Enclosure - Unabated Dose (see Attachment C-1) | 3.4E-01 | 2.0E-01 | 5.4E-01 | 1.9E-01 | 1.3E+00 |
| H2 Enclosure - Abated Dose (see Attachment C-2) | 3.4E-05 | 2.0E-05 | 5.4E-05 | 1.9E-05 | 1.3E-04 |

Summary

A summary tabulation of source terms, calculated emissions, and calculated abated EDE is provided in Table A-7. Given the unabated dose (EDE) of 1.3 mrem to the MEOSI, per 40 CFR 61.93(e) and 40 CFR 61(f), the monitoring category required (in accordance with ANSI/HPS N13.1-1999 graded approach) is Potential Impact Category 2, requiring continuous sampling for record of emissions with retrospective offline periodic analysis. [Ref. A-3]

Table A-7. Summary of Source Inventories and Doses for H2 Building Enclosure Ventilation

| SPRU-DP Area | Radioactive Material Inventory (Ci) | Estimated Abated Source Term (Ci/yr) | EDE Abated (mrem/yr) |
|------------------------------|-------------------------------------|--------------------------------------|----------------------|
| H2 Building Enclosure Totals | 95 | 9.8E-06* | 1.3E-04 |

*C-14 Physical State factor is assumed to be 1, not 1E-03 as for other radionuclides present

The calculated EDE to the MEOSI is 1.3E-04 mrem/yr for the abated emissions. This dose is based on the source terms, adjustment factors and abatement factors from 40 CFR 61 Appendix D, and the activities that could occur during the identified scope of work. It is a conservative dose calculation that overestimates the actual dose because the HEPA filters are more effective than modeled, and because the Project ALARA program will further reduce actual emissions.

To verify operations as expected, the H2 Building enclosure ventilation exhaust will be monitored with an ANSI/HPS N13.1-1999 compliant continuous sampler operating under PIC 2 requirements. (See Attachment D)

References

A-1. CAP88-PC Version 3.0 User Guide, USEPA Office of Radiation and Indoor Air, Washington, DC. December 09, 2007

A-2. 40 CFR 61, Appendix D, Methods for Estimating Radionuclide Emissions, December 1989

A-3. American National Standards Institute, Sampling and Monitoring Release of Airborne Radioactive Substances from the Stacks and Ducts of Nuclear Facilities, ANSI/HPS N13.1-1999

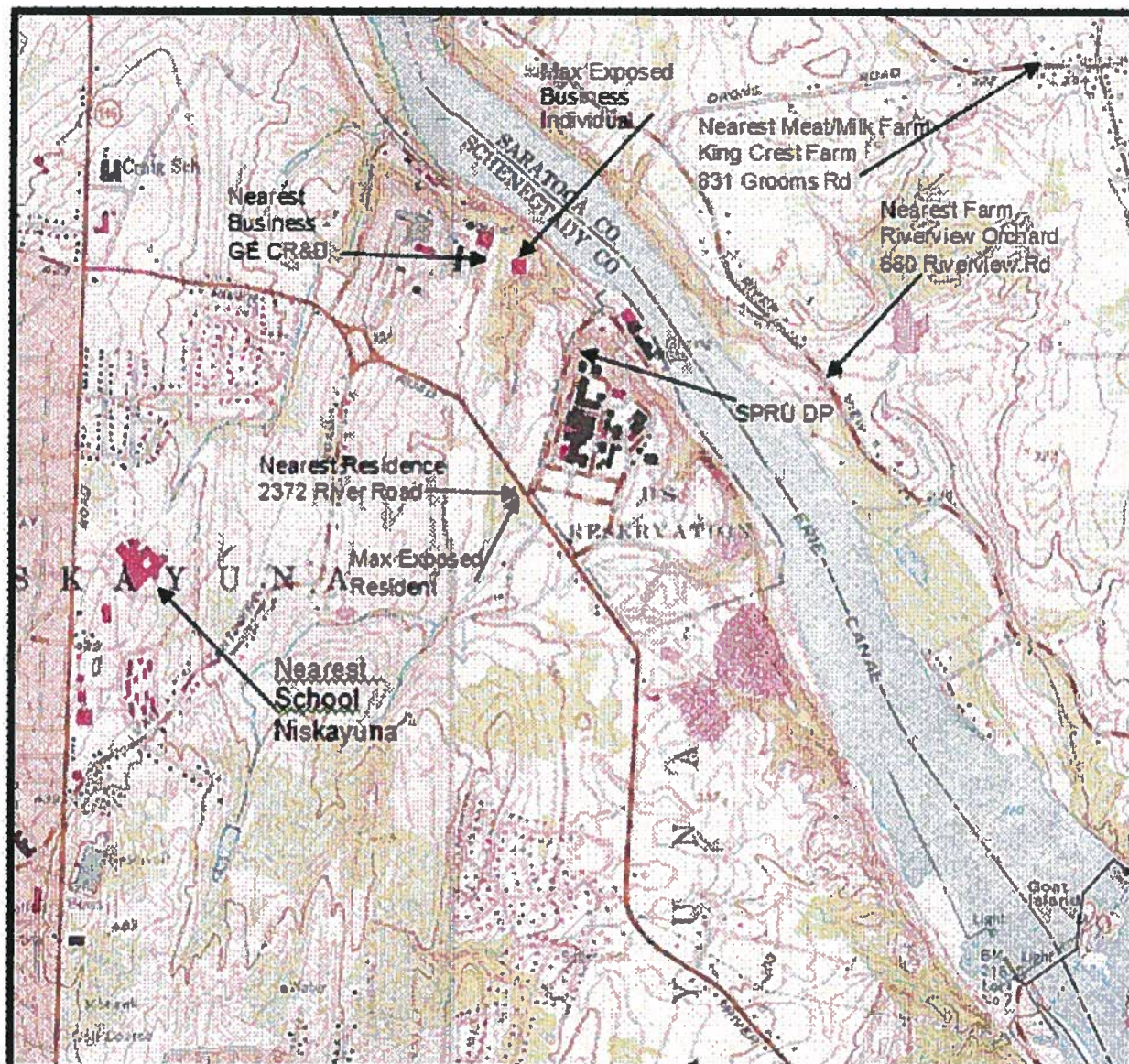
Attachment B

Meteorological Monitoring and Airborne Radionuclide Dispersion Modeling at SPRU-DP

Meteorological Monitoring and Airborne Radionuclide Dispersion Modeling at SPRU

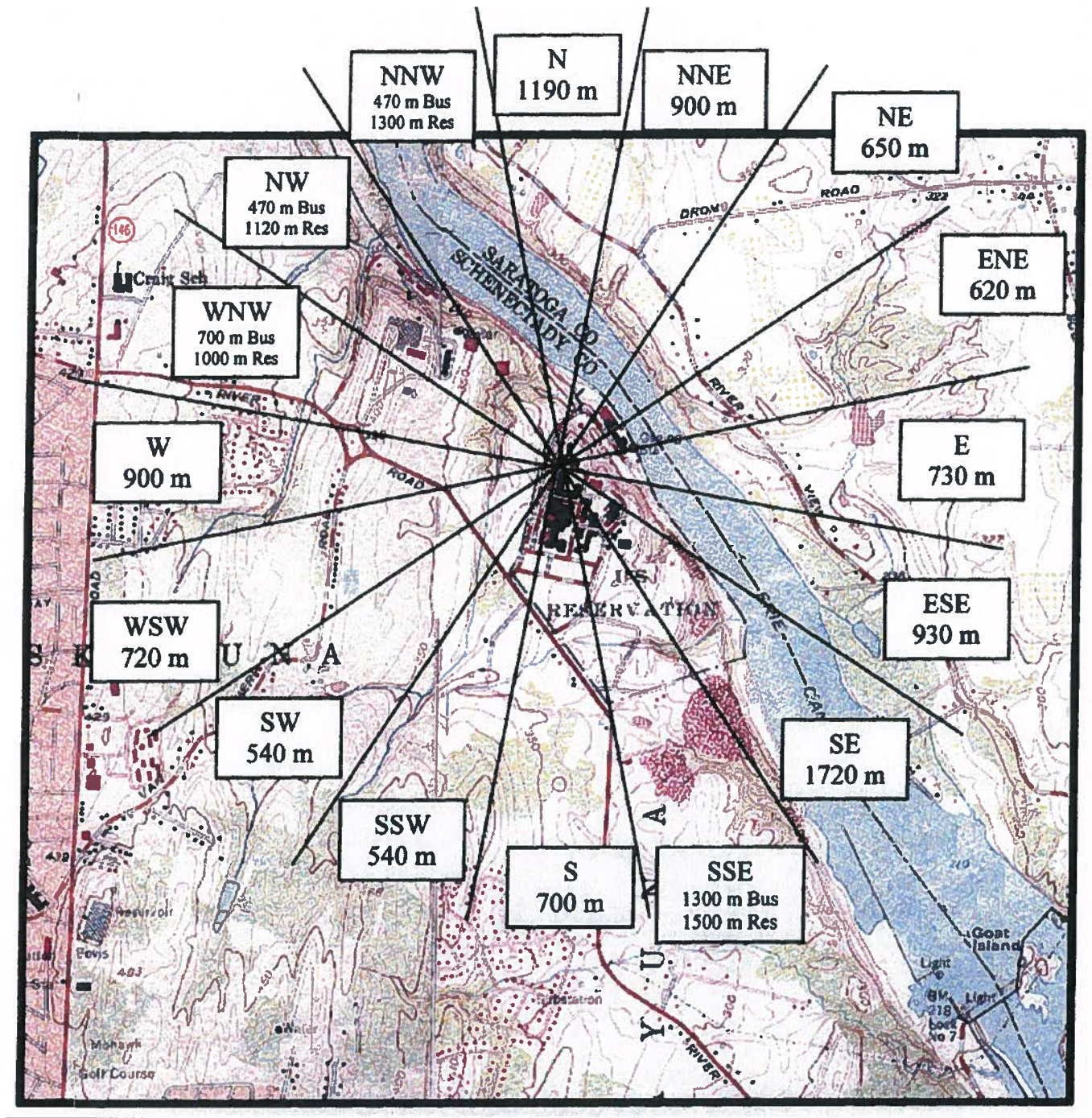
All meteorological data are derived from the Knolls Atomic Power Laboratory (KAPL). The environs and key receptor locations are shown below in Figure B-1. Figure B-2 lists the locations of receptors in each of 16 sectors around the center of the SPRU-DP work area.

Figure B-1. Location of the SPRU-DP Relative to Adjacent Sites and Key Receptors



The KAPL meteorological program data from 1989-2004 were used to prepare prospective dose estimates for the planned activities associated with PVU operation. Appropriate annual meteorological datasets will be used for retrospective compliance reporting.

Figure B-2. Location of the SPRU-DP Relative to Nearest Sector Receptors



ATTACHMENT C

CAP88-PC Dose Runs for SPRU-DP H2 Building Enclosure Ventilation System

ATTACHMENT C-1

CAP88-PC Dose Runs Using SPRU-DP Source Term for H2 Building, Sludge, & Tank Vaults

Unabated

CAP88 - PC

Version 3.0

Clean Air Act Assessment Package - 1988

SYNOPSIS REPORT

Non-Radon Individual Assessment

Jun 8, 2011 02:10 pm

Facility: SPRU DP
Address: 2425 River Road
City: Niskayuna
State: NY Zip: 12309

Source Category: H2 enclosure
Source Type: Stack
Emission Year: 2011

Comments: DnD of H2 building
89-2004 wind data rural food path

Effective Dose Equivalent
(mrem/year)

1.29E+00

At This Location: 540 Meters South Southwest

Dataset Name: H2 Point Source
Dataset Date: 6/8/2011 2:09:00 PM
Wind File: C:\Program Files\CAP88-PC30\WndFiles\knol890

Jun 8, 2011 02:10 pm

SYNOPSIS
Page 1

MAXIMALLY EXPOSED INDIVIDUAL

| | |
|-----------------------------|----------------------------|
| Location Of The Individual: | 540 Meters South Southwest |
| Lifetime Fatal Cancer Risk: | 6.04E-07 |

Jun 8, 2011 02:10 pm

SYNOPSIS
Page 2

RADIONUCLIDE EMISSIONS DURING THE YEAR 2004

| Nuclide | Type | Size | Source | TOTAL |
|---------|------|------|------------|---------|
| | | | #1 Ci/y | Ci/y |
| Pu-239 | S | 1 | 3.8E-03 | 3.8E-03 |
| Am-241 | M | 1 | 5.4E-04 | 5.4E-04 |
| Sr-90 | M | 1 | 1.1E-02 | 1.1E-02 |
| Y-90 | M | 1 | 1.1E-02 | 1.1E-02 |
| Cs-137 | F | 1 | 3.4E-02 | 3.4E-02 |
| Ba-137m | M | 1 | 3.4E-02 | 3.4E-02 |
| U-234 | S | 1 | 2.4E-05 | 2.4E-05 |
| U-235 | S | 1 | 9.9E-07 | 9.9E-07 |
| U-238 | S | 1 | 1.6E-05 | 1.6E-05 |
| C-14 | M | 1 | 2.7E-03 | 2.7E-03 |
| Fe-55 | M | 1 | 1.5E-06 | 1.5E-06 |
| Ni-63 | M | 1 | 2.1E-06 | 2.1E-06 |
| U-233 | S | 1 | 3.2E-06 | 3.2E-06 |
| Pu-238 | S | 1 | 5.0E-05 | 5.0E-05 |
| Pu-241 | S | 1 | 5.1E-04 | 5.1E-04 |
| Tc-99 | M | 1 | 3.6E-06 | 3.6E-06 |
| Th-228 | S | 1 | 1.8E-07 | 1.8E-07 |
| Th-230 | S | 1 | 1.6E-08 | 1.6E-08 |
| Th-232 | S | 1 | 1.5E-07 | 1.5E-07 |
| Pm-147 | M | 1 | 1.4E-04 | 1.4E-04 |

SITE INFORMATION

Temperature: 10 degrees C
Precipitation: 100 cm/y
Humidity: 8 g/cu m
Mixing Height: 1000 m

User specified location of max exposed individual.
(ILOC, JLOC): 8, 2

Jun 8, 2011 02:10 pm

SYNOPSIS
Page 3

SOURCE INFORMATION

Source Number: 1

Stack Height (m): 1.83
Diameter (m): 1.52

Plume Rise
Momentum (m/s): 0.00
(Exit Velocity)

AGRICULTURAL DATA

| | Vegetable | Milk | Meat |
|--------------------------------|-----------|-------|-------|
| Fraction Home Produced: | 0.700 | 0.400 | 0.440 |
| Fraction From Assessment Area: | 0.300 | 0.600 | 0.560 |
| Fraction Imported: | 0.000 | 0.000 | 0.000 |

Food Arrays were not generated for this run.
Default Values used.

DISTANCES (M) USED FOR MAXIMUM INDIVIDUAL ASSESSMENT

| | | | | | | |
|------|-----|------|------|------|------|------|
| 470 | 540 | 620 | 650 | 700 | 720 | 730 |
| 900 | 930 | 1000 | 1120 | 1190 | 1300 | 1500 |
| 1720 | | | | | | |

C A P 8 8 - P C

Version 3.0

Clean Air Act Assessment Package - 1988

D O S E A N D R I S K E Q U I V A L E N T S U M M A R I E S

Non-Radon Individual Assessment

Jun 8, 2011 02:10 pm

Facility: SPRU DP
 Address: 2425 River Road
 City: Niskayuna
 State: NY Zip: 12309

Source Category: H2 enclosure
 Source Type: Stack
 Emission Year: 2011

Comments: DnD of H2 building
 89-2004 wind data rural food path

Dataset Name: H2 Point Source
 Dataset Date: 6/8/2011 2:09:00 PM
 Wind File: C:\Program Files\CAP88-
 PC30\WndFiles\kno18904.WND

Jun 8, 2011 02:10 pm

SUMMARY
Page 1

PATHWAY EFFECTIVE DOSE EQUIVALENT SUMMARY

| Pathway | Selected Individual (mrem/y) |
|----------------|------------------------------------|
| INGESTION | 5.59E-01 |
| INHALATION | 7.22E-01 |
| AIR IMMERSION | 2.93E-05 |
| GROUND SURFACE | 9.25E-03 |
| INTERNAL | 1.28E+00 |
| EXTERNAL | 9.28E-03 |
| TOTAL | 1.29E+00 |

Jun 8, 2011 02:10 pm

SUMMARY
Page 2

NUCLIDE EFFECTIVE DOSE EQUIVALENT SUMMARY

| Nuclide | Selected Individual (mrem/y) |
|---------|------------------------------------|
| Pu-239 | 5.42E-01 |
| U-235 | 0.00E+00 |
| Th-231 | 7.21E-09 |
| Pa-231 | 0.00E+00 |
| Sr-90 | 1.99E-01 |
| Y-90 | 6.98E-04 |
| Cs-137 | 3.34E-01 |
| Ba-137m | 8.66E-03 |
| U-234 | 1.95E-03 |
| Th-230 | 1.89E-06 |
| Ra-226 | 0.00E+00 |
| Rn-222 | 0.00E+00 |
| U-235 | 7.25E-05 |
| U-238 | 1.11E-03 |
| Th-234 | 6.53E-07 |
| C-14 | 1.84E-04 |
| Fe-55 | 5.22E-08 |
| Ni-63 | 1.11E-07 |
| U-233 | 2.65E-04 |
| Th-229 | 0.00E+00 |
| Pu-238 | 7.12E-03 |
| U-234 | 0.00E+00 |
| Pu-241 | 8.21E-04 |
| Am-241 | 1.94E-01 |
| Np-237 | 0.00E+00 |
| U-237 | 0.00E+00 |
| Tc-99 | 1.26E-05 |
| Th-228 | 6.07E-05 |
| Ra-224 | 3.83E-08 |
| Th-232 | 3.24E-05 |
| Ra-228 | 0.00E+00 |
| Pm-147 | 6.99E-06 |
| Sm-147 | 0.00E+00 |
| TOTAL | 1.29E+00 |

Jun 8, 2011 02:10 pm

SUMMARY
Page 3

CANCER RISK SUMMARY

| Cancer | Selected Individual Total Lifetime Fatal Cancer Risk |
|----------|--|
| Esophagu | 3.77E-09 |
| Stomach | 1.34E-08 |
| Colon | 5.25E-08 |
| Liver | 2.34E-08 |
| LUNG | 3.08E-07 |
| Bone | 1.23E-08 |
| Skin | 3.41E-10 |
| Breast | 1.12E-08 |
| Ovary | 6.42E-09 |
| Bladder | 9.76E-09 |
| Kidneys | 2.10E-09 |
| Thyroid | 9.21E-10 |
| Leukemia | 1.11E-07 |
| Residual | 4.87E-08 |
| Total | 6.04E-07 |
| TOTAL | 1.21E-06 |

PATHWAY RISK SUMMARY

| Pathway | Selected Individual Total Lifetime Fatal Cancer Risk |
|----------------|--|
| INGESTION | 2.88E-07 |
| INHALATION | 3.12E-07 |
| AIR IMMERSION | 1.59E-11 |
| GROUND SURFACE | 4.74E-09 |
| INTERNAL | 5.99E-07 |
| EXTERNAL | 4.75E-09 |
| TOTAL | 6.04E-07 |

Jun 8, 2011 02:10 pm

SUMMARY
Page 4

NUCLIDE RISK SUMMARY

| Nuclide | Selected Individual |
|---------|-------------------------------------|
| | Total Lifetime Fatal Cancer Risk |
| Pu-239 | 2.76E-07 |
| U-235 | 0.00E+00 |
| Th-231 | 3.26E-15 |
| Pa-231 | 0.00E+00 |
| Sr-90 | 1.17E-07 |
| Y-90 | 2.14E-10 |
| Cs-137 | 1.69E-07 |
| Ba-137m | 4.67E-09 |
| U-234 | 1.46E-09 |
| Th-230 | 9.79E-13 |
| Ra-226 | 0.00E+00 |
| Rn-222 | 0.00E+00 |
| U-235 | 5.43E-11 |
| U-238 | 8.29E-10 |
| Th-234 | 9.28E-13 |
| C-14 | 1.27E-10 |
| Fe-55 | 3.64E-14 |
| Ni-63 | 1.09E-13 |
| U-233 | 1.99E-10 |
| Th-229 | 0.00E+00 |
| Pu-238 | 3.88E-09 |
| U-234 | 0.00E+00 |
| Pu-241 | 1.59E-10 |
| Am-241 | 3.05E-08 |
| Np-237 | 0.00E+00 |
| U-237 | 0.00E+00 |
| Tc-99 | 1.21E-11 |
| Th-228 | 5.19E-11 |
| Ra-224 | 2.30E-14 |
| Th-232 | 1.41E-11 |
| Ra-228 | 0.00E+00 |
| Pm-147 | 5.06E-12 |
| Sm-147 | 0.00E+00 |
| TOTAL | 6.04E-07 |

Jun 8, 2011 02:10 pm

SUMMARY
Page 5INDIVIDUAL EFFECTIVE DOSE EQUIVALENT RATE (mrem/y)
(All Radionuclides and Pathways)

| Distance (m) | | | | | | | |
|--------------|---------|---------|---------|---------|---------|---------|---------|
| Direction | 470 | 540 | 620 | 650 | 700 | 720 | 730 |
| N | 1.5E+00 | 1.2E+00 | 9.7E-01 | 9.1E-01 | 8.1E-01 | 7.8E-01 | 7.6E-01 |
| NNW | 3.7E+00 | 2.9E+00 | 2.3E+00 | 2.1E+00 | 1.9E+00 | 1.8E+00 | 1.7E+00 |
| NW | 1.5E+00 | 1.2E+00 | 9.6E-01 | 8.9E-01 | 8.0E-01 | 7.7E-01 | 7.5E-01 |
| WNW | 1.0E+00 | 8.2E-01 | 6.7E-01 | 6.3E-01 | 5.7E-01 | 5.5E-01 | 5.4E-01 |
| W | 1.0E+00 | 8.4E-01 | 6.8E-01 | 6.4E-01 | 5.8E-01 | 5.6E-01 | 5.5E-01 |
| WSW | 1.0E+00 | 8.2E-01 | 6.7E-01 | 6.2E-01 | 5.6E-01 | 5.4E-01 | 5.3E-01 |
| SW | 1.1E+00 | 8.9E-01 | 7.2E-01 | 6.7E-01 | 6.1E-01 | 5.9E-01 | 5.8E-01 |
| SSW | 1.6E+00 | 1.3E+00 | 1.0E+00 | 9.6E-01 | 8.6E-01 | 8.2E-01 | 8.1E-01 |
| S | 2.1E+00 | 1.6E+00 | 1.3E+00 | 1.2E+00 | 1.1E+00 | 1.0E+00 | 9.9E-01 |
| SSE | 2.0E+00 | 1.6E+00 | 1.2E+00 | 1.2E+00 | 1.0E+00 | 9.8E-01 | 9.6E-01 |
| SE | 1.7E+00 | 1.4E+00 | 1.1E+00 | 1.0E+00 | 9.1E-01 | 8.7E-01 | 8.5E-01 |
| ESE | 2.1E+00 | 1.7E+00 | 1.3E+00 | 1.2E+00 | 1.1E+00 | 1.1E+00 | 1.0E+00 |
| E | 2.5E+00 | 2.0E+00 | 1.6E+00 | 1.5E+00 | 1.3E+00 | 1.2E+00 | 1.2E+00 |
| ENE | 1.5E+00 | 1.2E+00 | 9.3E-01 | 8.7E-01 | 7.8E-01 | 7.5E-01 | 7.3E-01 |
| NE | 1.3E+00 | 1.0E+00 | 8.2E-01 | 7.6E-01 | 6.8E-01 | 6.6E-01 | 6.4E-01 |
| NNE | 1.3E+00 | 1.0E+00 | 8.2E-01 | 7.6E-01 | 6.8E-01 | 6.6E-01 | 6.4E-01 |

| Distance (m) | | | | | | | |
|--------------|---------|---------|---------|---------|---------|---------|---------|
| Direction | 900 | 930 | 1000 | 1120 | 1190 | 1300 | 1500 |
| N | 5.7E-01 | 5.5E-01 | 5.0E-01 | 4.5E-01 | 4.2E-01 | 3.9E-01 | 3.4E-01 |
| NNW | 1.2E+00 | 1.2E+00 | 1.0E+00 | 8.9E-01 | 8.2E-01 | 7.3E-01 | 6.1E-01 |
| NW | 5.6E-01 | 5.4E-01 | 4.9E-01 | 4.4E-01 | 4.1E-01 | 3.8E-01 | 3.3E-01 |
| WNW | 4.2E-01 | 4.0E-01 | 3.7E-01 | 3.4E-01 | 3.2E-01 | 3.0E-01 | 2.7E-01 |
| W | 4.2E-01 | 4.1E-01 | 3.8E-01 | 3.4E-01 | 3.3E-01 | 3.0E-01 | 2.8E-01 |
| WSW | 4.2E-01 | 4.0E-01 | 3.7E-01 | 3.4E-01 | 3.2E-01 | 3.0E-01 | 2.7E-01 |
| SW | 4.4E-01 | 4.3E-01 | 4.0E-01 | 3.6E-01 | 3.4E-01 | 3.2E-01 | 2.9E-01 |
| SSW | 6.0E-01 | 5.7E-01 | 5.2E-01 | 4.6E-01 | 4.3E-01 | 4.0E-01 | 3.5E-01 |
| S | 7.2E-01 | 6.9E-01 | 6.2E-01 | 5.4E-01 | 5.1E-01 | 4.6E-01 | 4.0E-01 |
| SSE | 7.0E-01 | 6.7E-01 | 6.1E-01 | 5.3E-01 | 5.0E-01 | 4.5E-01 | 3.9E-01 |
| SE | 6.3E-01 | 6.0E-01 | 5.5E-01 | 4.8E-01 | 4.5E-01 | 4.1E-01 | 3.6E-01 |
| ESE | 7.6E-01 | 7.2E-01 | 6.5E-01 | 5.7E-01 | 5.3E-01 | 4.8E-01 | 4.2E-01 |
| E | 8.7E-01 | 8.3E-01 | 7.5E-01 | 6.5E-01 | 6.0E-01 | 5.4E-01 | 4.6E-01 |
| ENE | 5.5E-01 | 5.3E-01 | 4.8E-01 | 4.3E-01 | 4.0E-01 | 3.7E-01 | 3.3E-01 |
| NE | 4.9E-01 | 4.7E-01 | 4.3E-01 | 3.9E-01 | 3.7E-01 | 3.4E-01 | 3.0E-01 |
| NNE | 4.9E-01 | 4.7E-01 | 4.3E-01 | 3.9E-01 | 3.6E-01 | 3.4E-01 | 3.0E-01 |

Jun 8, 2011 02:10 pm

SUMMARY
Page 6INDIVIDUAL EFFECTIVE DOSE EQUIVALENT RATE (mrem/y)
(All Radionuclides and Pathways)

| Distance (m) | |
|--------------|---------|
| <hr/> | |
| Direction | 1720 |
| <hr/> | |
| N | 3.1E-01 |
| NNW | 5.2E-01 |
| NW | 3.0E-01 |
| WNW | 2.5E-01 |
| W | 2.5E-01 |
| WSW | 2.5E-01 |
| SW | 2.6E-01 |
| SSW | 3.1E-01 |
| S | 3.5E-01 |
| SSE | 3.5E-01 |
| SE | 3.2E-01 |
| ESE | 3.7E-01 |
| E | 4.0E-01 |
| ENE | 3.0E-01 |
| NE | 2.8E-01 |
| NNE | 2.8E-01 |

Jun 8, 2011 02:10 pm

SUMMARY
Page 7INDIVIDUAL LIFETIME RISK (deaths)
(All Radionuclides and Pathways)

| Distance (m) | | | | | | | |
|--------------|---------|---------|---------|---------|---------|---------|---------|
| Direction | 470 | 540 | 620 | 650 | 700 | 720 | 730 |
| N | 7.1E-07 | 5.7E-07 | 4.6E-07 | 4.3E-07 | 3.8E-07 | 3.7E-07 | 3.6E-07 |
| NNW | 1.7E-06 | 1.4E-06 | 1.1E-06 | 9.8E-07 | 8.7E-07 | 8.3E-07 | 8.1E-07 |
| NW | 7.0E-07 | 5.6E-07 | 4.5E-07 | 4.2E-07 | 3.8E-07 | 3.6E-07 | 3.6E-07 |
| WNW | 4.8E-07 | 3.9E-07 | 3.2E-07 | 3.0E-07 | 2.7E-07 | 2.6E-07 | 2.6E-07 |
| W | 4.9E-07 | 4.0E-07 | 3.3E-07 | 3.0E-07 | 2.8E-07 | 2.7E-07 | 2.6E-07 |
| WSW | 4.8E-07 | 3.9E-07 | 3.2E-07 | 3.0E-07 | 2.7E-07 | 2.6E-07 | 2.6E-07 |
| SW | 5.2E-07 | 4.2E-07 | 3.4E-07 | 3.2E-07 | 2.9E-07 | 2.8E-07 | 2.8E-07 |
| SSW | 7.6E-07 | 6.0E-07 | 4.9E-07 | 4.5E-07 | 4.1E-07 | 3.9E-07 | 3.8E-07 |
| S | 9.5E-07 | 7.5E-07 | 6.0E-07 | 5.6E-07 | 5.0E-07 | 4.8E-07 | 4.7E-07 |
| SSE | 9.2E-07 | 7.3E-07 | 5.8E-07 | 5.4E-07 | 4.8E-07 | 4.6E-07 | 4.5E-07 |
| SE | 8.1E-07 | 6.4E-07 | 5.1E-07 | 4.8E-07 | 4.3E-07 | 4.1E-07 | 4.0E-07 |
| ESE | 9.9E-07 | 7.8E-07 | 6.3E-07 | 5.8E-07 | 5.2E-07 | 5.0E-07 | 4.9E-07 |
| E | 1.2E-06 | 9.2E-07 | 7.3E-07 | 6.8E-07 | 6.0E-07 | 5.8E-07 | 5.6E-07 |
| ENE | 6.8E-07 | 5.5E-07 | 4.4E-07 | 4.1E-07 | 3.7E-07 | 3.5E-07 | 3.5E-07 |
| NE | 5.9E-07 | 4.8E-07 | 3.9E-07 | 3.6E-07 | 3.3E-07 | 3.1E-07 | 3.1E-07 |
| NNE | 5.9E-07 | 4.8E-07 | 3.9E-07 | 3.6E-07 | 3.2E-07 | 3.1E-07 | 3.1E-07 |

| Distance (m) | | | | | | | |
|--------------|---------|---------|---------|---------|---------|---------|---------|
| Direction | 900 | 930 | 1000 | 1120 | 1190 | 1300 | 1500 |
| N | 2.7E-07 | 2.6E-07 | 2.4E-07 | 2.2E-07 | 2.0E-07 | 1.9E-07 | 1.7E-07 |
| NNW | 5.8E-07 | 5.5E-07 | 4.9E-07 | 4.2E-07 | 3.9E-07 | 3.5E-07 | 2.9E-07 |
| NW | 2.7E-07 | 2.6E-07 | 2.4E-07 | 2.1E-07 | 2.0E-07 | 1.9E-07 | 1.7E-07 |
| WNW | 2.0E-07 | 2.0E-07 | 1.8E-07 | 1.7E-07 | 1.6E-07 | 1.5E-07 | 1.4E-07 |
| W | 2.1E-07 | 2.0E-07 | 1.8E-07 | 1.7E-07 | 1.6E-07 | 1.5E-07 | 1.4E-07 |
| WSW | 2.0E-07 | 2.0E-07 | 1.8E-07 | 1.7E-07 | 1.6E-07 | 1.5E-07 | 1.4E-07 |
| SW | 2.2E-07 | 2.1E-07 | 1.9E-07 | 1.8E-07 | 1.7E-07 | 1.6E-07 | 1.4E-07 |
| SSW | 2.9E-07 | 2.8E-07 | 2.5E-07 | 2.2E-07 | 2.1E-07 | 1.9E-07 | 1.7E-07 |
| S | 3.4E-07 | 3.3E-07 | 3.0E-07 | 2.6E-07 | 2.5E-07 | 2.2E-07 | 2.0E-07 |
| SSE | 3.3E-07 | 3.2E-07 | 2.9E-07 | 2.6E-07 | 2.4E-07 | 2.2E-07 | 1.9E-07 |
| SE | 3.0E-07 | 2.9E-07 | 2.6E-07 | 2.3E-07 | 2.2E-07 | 2.0E-07 | 1.8E-07 |
| ESE | 3.6E-07 | 3.4E-07 | 3.1E-07 | 2.7E-07 | 2.6E-07 | 2.3E-07 | 2.0E-07 |
| E | 4.1E-07 | 3.9E-07 | 3.5E-07 | 3.1E-07 | 2.9E-07 | 2.6E-07 | 2.2E-07 |
| ENE | 2.6E-07 | 2.5E-07 | 2.3E-07 | 2.1E-07 | 2.0E-07 | 1.8E-07 | 1.6E-07 |
| NE | 2.4E-07 | 2.3E-07 | 2.1E-07 | 1.9E-07 | 1.8E-07 | 1.7E-07 | 1.5E-07 |
| NNE | 2.4E-07 | 2.3E-07 | 2.1E-07 | 1.9E-07 | 1.8E-07 | 1.7E-07 | 1.5E-07 |

Jun 8, 2011 02:10 pm

SUMMARY
Page 8INDIVIDUAL LIFETIME RISK (deaths)
(All Radionuclides and Pathways)

Distance (m)

Direction 1720

| | |
|-----|---------|
| N | 1.5E-07 |
| NNW | 2.5E-07 |
| NW | 1.5E-07 |
| WNW | 1.3E-07 |
| W | 1.3E-07 |
| WSW | 1.3E-07 |
| SW | 1.3E-07 |
| SSW | 1.6E-07 |
| S | 1.7E-07 |
| SSE | 1.7E-07 |
| SE | 1.6E-07 |
| ESE | 1.8E-07 |
| E | 2.0E-07 |
| ENE | 1.5E-07 |
| NE | 1.4E-07 |
| NNE | 1.4E-07 |

CAP88 - PC

Version 3.0

Clean Air Act Assessment Package - 1988

WEATHER DATA

Non-Radon Individual Assessment

Jun 8, 2011 02:10 pm

Facility: SPRU DP
Address: 2425 River Road
City: Niskayuna
State: NY Zip: 12309

Source Category: H2 enclosure
Source Type: Stack
Emission Year: 2011

Comments: DnD of H2 building
89-2004 wind data rural food path

Dataset Name: H2 Point Source
Dataset Date: 6/8/2011 2:09:00 PM
Wind File: C:\Program Files\CAP88-PC30\WndFiles\knol8904.WND

Jun 8, 2011 02:10 pm

WEATHER
Page 1

HARMONIC AVERAGE WIND SPEEDS (WIND TOWARDS)

| Pasquill Stability Class | | | | | | | | |
|--------------------------|-------|-------|-------|-------|-------|-------|-------|-----------|
| Dir | A | B | C | D | E | F | G | Wind Freq |
| N | 1.428 | 1.768 | 1.898 | 1.971 | 1.042 | 0.663 | 0.000 | 0.097 |
| NNW | 1.539 | 1.808 | 2.332 | 2.139 | 1.073 | 0.711 | 0.000 | 0.130 |
| NW | 1.387 | 1.444 | 1.400 | 1.248 | 0.838 | 0.702 | 0.000 | 0.044 |
| WNW | 1.303 | 1.365 | 1.193 | 0.882 | 0.701 | 0.563 | 0.000 | 0.027 |
| W | 1.143 | 1.134 | 0.909 | 0.792 | 0.631 | 0.613 | 0.000 | 0.022 |
| WSW | 1.149 | 1.078 | 1.033 | 0.913 | 0.666 | 0.615 | 0.000 | 0.021 |
| SW | 1.297 | 1.372 | 1.445 | 1.322 | 0.938 | 0.660 | 0.000 | 0.038 |
| SSW | 1.380 | 1.712 | 1.779 | 1.961 | 1.135 | 0.820 | 0.000 | 0.068 |
| S | 1.297 | 1.420 | 1.398 | 1.357 | 1.035 | 0.782 | 0.000 | 0.057 |
| SSE | 1.433 | 1.539 | 1.555 | 1.374 | 0.981 | 0.715 | 0.000 | 0.050 |
| SE | 1.628 | 2.068 | 2.500 | 2.116 | 1.082 | 0.700 | 0.000 | 0.068 |
| ESE | 1.911 | 2.708 | 3.690 | 3.554 | 1.425 | 0.785 | 0.000 | 0.190 |
| E | 1.735 | 2.592 | 3.292 | 2.957 | 1.308 | 0.750 | 0.000 | 0.101 |
| ENE | 1.599 | 1.833 | 2.230 | 1.635 | 0.909 | 0.676 | 0.000 | 0.035 |
| NE | 1.459 | 1.806 | 1.810 | 1.199 | 0.918 | 0.643 | 0.000 | 0.026 |
| NNE | 1.425 | 1.590 | 1.218 | 1.003 | 0.820 | 0.615 | 0.000 | 0.027 |

ARITHMETIC AVERAGE WIND SPEEDS (WIND TOWARDS)

| Pasquill Stability Class | | | | | | | |
|--------------------------|-------|-------|-------|-------|-------|-------|-------|
| Dir | A | B | C | D | E | F | G |
| N | 1.774 | 2.251 | 2.847 | 3.130 | 1.528 | 0.914 | 0.000 |
| NNW | 1.839 | 2.323 | 3.177 | 3.125 | 1.554 | 1.041 | 0.000 |
| NW | 1.660 | 1.934 | 2.060 | 2.160 | 1.306 | 1.019 | 0.000 |
| WNW | 1.540 | 1.674 | 1.659 | 1.606 | 1.167 | 0.812 | 0.000 |
| W | 1.341 | 1.436 | 1.368 | 1.404 | 1.009 | 0.861 | 0.000 |
| WSW | 1.356 | 1.451 | 1.653 | 1.896 | 1.049 | 0.842 | 0.000 |
| SW | 1.554 | 1.873 | 2.212 | 2.446 | 1.450 | 0.944 | 0.000 |
| SSW | 1.660 | 2.264 | 2.866 | 3.155 | 1.640 | 1.154 | 0.000 |
| S | 1.585 | 1.991 | 2.311 | 2.474 | 1.576 | 1.146 | 0.000 |
| SSE | 1.666 | 2.145 | 2.544 | 2.218 | 1.399 | 1.023 | 0.000 |
| SE | 1.912 | 2.639 | 3.548 | 3.315 | 1.506 | 0.980 | 0.000 |
| ESE | 2.130 | 3.077 | 4.303 | 4.520 | 1.921 | 1.146 | 0.000 |
| E | 2.026 | 2.952 | 4.182 | 4.253 | 1.831 | 1.125 | 0.000 |
| ENE | 1.913 | 2.527 | 3.687 | 3.035 | 1.430 | 0.981 | 0.000 |
| NE | 1.794 | 2.398 | 3.034 | 2.335 | 1.396 | 0.891 | 0.000 |
| NNE | 1.715 | 2.187 | 2.104 | 1.884 | 1.270 | 0.822 | 0.000 |

WEATHER
Page 2

| Pasquill Stability Class | | | | | | | |
|--------------------------|--------|--------|--------|--------|--------|--------|--------|
| Dir | A | B | C | D | E | F | G |
| N | 0.0166 | 0.0272 | 0.0957 | 0.3246 | 0.1128 | 0.0496 | 0.0000 |
| NNW | 0.0545 | 0.0977 | 0.3024 | 0.6829 | 0.1892 | 0.1114 | 0.0000 |
| NW | 0.1726 | 0.1982 | 0.2801 | 0.3102 | 0.1571 | 0.1343 | 0.0000 |
| WNW | 0.3168 | 0.2595 | 0.2241 | 0.1501 | 0.1260 | 0.1430 | 0.0000 |
| W | 0.3407 | 0.2808 | 0.1912 | 0.1379 | 0.1484 | 0.2055 | 0.0000 |
| WSW | 0.3033 | 0.2154 | 0.1907 | 0.1714 | 0.1769 | 0.2088 | 0.0000 |
| SW | 0.1651 | 0.1754 | 0.1730 | 0.1833 | 0.1429 | 0.1270 | 0.0000 |
| SSW | 0.0990 | 0.1235 | 0.1747 | 0.2745 | 0.1366 | 0.1343 | 0.0000 |
| S | 0.1012 | 0.1067 | 0.1444 | 0.3154 | 0.2270 | 0.2020 | 0.0000 |
| SSE | 0.0900 | 0.0926 | 0.1268 | 0.3648 | 0.2827 | 0.1904 | 0.0000 |
| SE | 0.0595 | 0.0805 | 0.1347 | 0.3520 | 0.1984 | 0.1184 | 0.0000 |
| ESE | 0.0221 | 0.0672 | 0.1973 | 0.4392 | 0.0981 | 0.0398 | 0.0000 |
| E | 0.0493 | 0.0984 | 0.3142 | 0.7300 | 0.1996 | 0.1051 | 0.0000 |
| ENE | 0.0573 | 0.0792 | 0.1773 | 0.3875 | 0.2655 | 0.1989 | 0.0000 |
| NE | 0.0593 | 0.0815 | 0.1454 | 0.2847 | 0.2817 | 0.2338 | 0.0000 |
| NNE | 0.0495 | 0.0546 | 0.0897 | 0.2538 | 0.2790 | 0.2020 | 0.0000 |
| TOTAL | 0.0798 | 0.1019 | 0.1989 | 0.4155 | 0.1711 | 0.1176 | 0.0000 |

```

Average Air Temperature: 10.0 degrees C
                        283.16 K
Precipitation: 100.0 cm/y
Humidity: 8.0 g/cu m
Lid Height: 1000 meters
Surface Roughness Length: 0.010 meters
Height Of Wind Measurements: 10.0 meters
Average Wind Speed: 2.660 m/s

Vertical Temperature Gradients:
STABILITY E 0.073 k/m
STABILITY F 0.109 k/m
STABILITY G 0.146 k/m

```

ATTACHMENT C-2

CAP88-PC Dose Runs Using SPRU-DP Source Term for H2 Building, Sludge, & Tank Vaults

Abated

CAP88 - PC

Version 3.0

Clean Air Act Assessment Package - 1988

SYNOPSIS REPORT

Non-Radon Individual Assessment
Jun 8, 2011 12:01 pm

Facility: SPRU DP
Address: 2425 River Road
City: Niskayuna
State: NY Zip: 12309

Source Category: H2 enclosure
Source Type: Stack
Emission Year: 2011

Comments: DnD of H2 building
89-2004 wind data rural food path

Effective Dose Equivalent
(mrem/year)

1.29E-04

At This Location: 540 Meters South Southwest

Dataset Name: H2 Point Source
Dataset Date: 6/8/2011 11:55:00 AM
Wind File: C:\Program Files\CAP88-PC30\WndFiles\kno1890

Jun 8, 2011 12:01 pm

SYNOPSIS
Page 1

MAXIMALLY EXPOSED INDIVIDUAL

| | |
|-----------------------------|----------------------------|
| Location Of The Individual: | 540 Meters South Southwest |
| Lifetime Fatal Cancer Risk: | 6.04E-11 |

Jun 8, 2011 12:01 pm

SYNOPSIS

Page 2

RADIONUCLIDE EMISSIONS DURING THE YEAR 2004

| Nuclide | Type | Size | Source | TOTAL |
|---------|------|------|------------|---------|
| | | | #1 Ci/y | |
| Pu-239 | S | 1 | 3.8E-07 | 3.8E-07 |
| Am-241 | M | 1 | 5.4E-08 | 5.4E-08 |
| Sr-90 | M | 1 | 1.1E-06 | 1.1E-06 |
| Y-90 | M | 1 | 1.1E-06 | 1.1E-06 |
| Cs-137 | F | 1 | 3.4E-06 | 3.4E-06 |
| Ba-137m | M | 1 | 3.4E-06 | 3.4E-06 |
| U-234 | S | 1 | 2.4E-09 | 2.4E-09 |
| U-235 | S | 1 | 9.9E-11 | 9.9E-11 |
| U-238 | S | 1 | 1.6E-09 | 1.6E-09 |
| C-14 | M | 1 | 2.7E-07 | 2.7E-07 |
| Fe-55 | M | 1 | 1.5E-10 | 1.5E-10 |
| Ni-63 | M | 1 | 2.1E-10 | 2.1E-10 |
| U-233 | S | 1 | 3.2E-10 | 3.2E-10 |
| Pu-238 | S | 1 | 5.0E-09 | 5.0E-09 |
| Pu-241 | S | 1 | 5.1E-08 | 5.1E-08 |
| Tc-99 | M | 1 | 3.6E-10 | 3.6E-10 |
| Th-228 | S | 1 | 1.8E-11 | 1.8E-11 |
| Th-230 | S | 1 | 1.6E-12 | 1.6E-12 |
| Th-232 | S | 1 | 1.5E-11 | 1.5E-11 |
| Pm-147 | M | 1 | 1.4E-08 | 1.4E-08 |

SITE INFORMATION

Temperature: 10 degrees C
 Precipitation: 100 cm/y
 Humidity: 8 g/cu m
 Mixing Height: 1000 m

User specified location of max exposed individual.
 (ILOC, JLOC): 8, 2

Jun 8, 2011 12:01 pm

SYNOPSIS
Page 3

SOURCE INFORMATION

Source Number: 1

Stack Height (m): 1.83
Diameter (m): 1.52

Plume Rise
Momentum (m/s): 0.00
(Exit Velocity)

AGRICULTURAL DATA

| | Vegetable | Milk | Meat |
|--------------------------------|-----------|-------|-------|
| | <hr/> | <hr/> | <hr/> |
| Fraction Home Produced: | 0.700 | 0.400 | 0.440 |
| Fraction From Assessment Area: | 0.300 | 0.600 | 0.560 |
| Fraction Imported: | 0.000 | 0.000 | 0.000 |

Food Arrays were not generated for this run.
Default Values used.

DISTANCES (M) USED FOR MAXIMUM INDIVIDUAL ASSESSMENT

| | | | | | | |
|------|-----|------|------|------|------|------|
| 470 | 540 | 620 | 650 | 700 | 720 | 730 |
| 900 | 930 | 1000 | 1120 | 1190 | 1300 | 1500 |
| 1720 | | | | | | |

CAP88 - PC

Version 3.0

Clean Air Act Assessment Package - 1988

DOSE AND RISK EQUIVALENT SUMMARIES

Non-Radon Individual Assessment

Jun 8, 2011 12:01 pm

Facility: SPRU DP
Address: 2425 River Road
City: Niskayuna
State: NY Zip: 12309

Source Category: H2 enclosure
Source Type: Stack
Emission Year: 2011

Comments: DnD of H2 building
89-2004 wind data rural food path

Dataset Name: H2 Point Source
Dataset Date: 6/8/2011 11:55:00 AM
Wind File: C:\Program Files\CAP88-
PC30\WndFiles\knol8904.WND

Jun 8, 2011 12:01 pm

SUMMARY
Page 1

PATHWAY EFFECTIVE DOSE EQUIVALENT SUMMARY

| Pathway | Selected Individual (mrem/y) |
|----------------|------------------------------------|
| INGESTION | 5.57E-05 |
| INHALATION | 7.21E-05 |
| AIR IMMERSION | 2.93E-09 |
| GROUND SURFACE | 9.25E-07 |
| INTERNAL | 1.28E-04 |
| EXTERNAL | 9.28E-07 |
| TOTAL | 1.29E-04 |

Jun 8, 2011 12:01 pm

SUMMARY
Page 2

NUCLIDE EFFECTIVE DOSE EQUIVALENT SUMMARY

| Nuclide | Selected Individual (mrem/y) |
|---------|------------------------------------|
| Pu-239 | 5.42E-05 |
| U-235 | 0.00E+00 |
| Th-231 | 0.00E+00 |
| Pa-231 | 0.00E+00 |
| Sr-90 | 1.99E-05 |
| Y-90 | 6.98E-08 |
| Cs-137 | 3.34E-05 |
| Ba-137m | 8.66E-07 |
| U-234 | 1.91E-07 |
| Th-230 | 0.00E+00 |
| Ra-226 | 0.00E+00 |
| Rn-222 | 0.00E+00 |
| U-235 | 0.00E+00 |
| U-238 | 1.09E-07 |
| Th-234 | 0.00E+00 |
| C-14 | 1.84E-08 |
| Fe-55 | 0.00E+00 |
| Ni-63 | 0.00E+00 |
| U-233 | 0.00E+00 |
| Th-229 | 0.00E+00 |
| Pu-238 | 6.80E-07 |
| U-234 | 0.00E+00 |
| Pu-241 | 7.54E-08 |
| Am-241 | 1.92E-05 |
| Np-237 | 0.00E+00 |
| U-237 | 0.00E+00 |
| Tc-99 | 0.00E+00 |
| Th-228 | 0.00E+00 |
| Ra-224 | 0.00E+00 |
| Th-232 | 0.00E+00 |
| Ra-228 | 0.00E+00 |
| Pm-147 | 5.85E-10 |
| Sm-147 | 0.00E+00 |
| TOTAL | 1.29E-04 |

Jun 8, 2011 12:01 pm

SUMMARY
Page 3

CANCER RISK SUMMARY

| Cancer | Selected Individual Total Lifetime Fatal Cancer Risk |
|----------|--|
| Esophagu | 3.77E-13 |
| Stomach | 1.34E-12 |
| Colon | 5.25E-12 |
| Liver | 2.33E-12 |
| LUNG | 3.08E-11 |
| Bone | 1.23E-12 |
| Skin | 3.41E-14 |
| Breast | 1.12E-12 |
| Ovary | 6.40E-13 |
| Bladder | 9.76E-13 |
| Kidneys | 2.10E-13 |
| Thyroid | 9.21E-14 |
| Leukemia | 1.11E-11 |
| Residual | 4.87E-12 |
| Total | 6.04E-11 |
| TOTAL | 1.21E-10 |

PATHWAY RISK SUMMARY

| Pathway | Selected Individual Total Lifetime Fatal Cancer Risk |
|----------------|--|
| INGESTION | 2.88E-11 |
| INHALATION | 3.11E-11 |
| AIR IMMERSION | 1.59E-15 |
| GROUND SURFACE | 4.73E-13 |
| INTERNAL | 5.99E-11 |
| EXTERNAL | 4.75E-13 |
| TOTAL | 6.04E-11 |

Jun 8, 2011 12:01 pm

SUMMARY

Page 4

NUCLIDE RISK SUMMARY

| Nuclide | Selected Individual |
|---------|-------------------------------------|
| | Total Lifetime Fatal Cancer Risk |
| Pu-239 | 2.76E-11 |
| U-235 | 0.00E+00 |
| Th-231 | 0.00E+00 |
| Pa-231 | 0.00E+00 |
| Sr-90 | 1.17E-11 |
| Y-90 | 2.14E-14 |
| Cs-137 | 1.69E-11 |
| Ba-137m | 4.67E-13 |
| U-234 | 1.45E-13 |
| Th-230 | 0.00E+00 |
| Ra-226 | 0.00E+00 |
| Rn-222 | 0.00E+00 |
| U-235 | 0.00E+00 |
| U-238 | 8.21E-14 |
| Th-234 | 0.00E+00 |
| C-14 | 1.27E-14 |
| Fe-55 | 0.00E+00 |
| Ni-63 | 0.00E+00 |
| U-233 | 0.00E+00 |
| Th-229 | 0.00E+00 |
| Pu-238 | 3.83E-13 |
| U-234 | 0.00E+00 |
| Pu-241 | 1.51E-14 |
| Am-241 | 3.03E-12 |
| Np-237 | 0.00E+00 |
| U-237 | 0.00E+00 |
| Tc-99 | 0.00E+00 |
| Th-228 | 0.00E+00 |
| Ra-224 | 0.00E+00 |
| Th-232 | 0.00E+00 |
| Ra-228 | 0.00E+00 |
| Pm-147 | 3.43E-16 |
| Sm-147 | 0.00E+00 |
| TOTAL | 6.04E-11 |

Jun 8, 2011 12:01 pm

SUMMARY
Page 5INDIVIDUAL EFFECTIVE DOSE EQUIVALENT RATE (mrem/y)
(All Radionuclides and Pathways)

| Direction | Distance (m) | | | | | | |
|-----------|--------------|---------|---------|---------|---------|---------|---------|
| | 470 | 540 | 620 | 650 | 700 | 720 | 730 |
| N | 1.5E-04 | 1.2E-04 | 9.7E-05 | 9.0E-05 | 8.1E-05 | 7.8E-05 | 7.6E-05 |
| NNW | 3.7E-04 | 2.9E-04 | 2.3E-04 | 2.1E-04 | 1.9E-04 | 1.8E-04 | 1.7E-04 |
| NW | 1.5E-04 | 1.2E-04 | 9.6E-05 | 8.9E-05 | 8.0E-05 | 7.7E-05 | 7.5E-05 |
| WNW | 1.0E-04 | 8.2E-05 | 6.7E-05 | 6.3E-05 | 5.7E-05 | 5.5E-05 | 5.4E-05 |
| W | 1.0E-04 | 8.4E-05 | 6.8E-05 | 6.4E-05 | 5.8E-05 | 5.5E-05 | 5.4E-05 |
| WSW | 1.0E-04 | 8.1E-05 | 6.7E-05 | 6.2E-05 | 5.6E-05 | 5.4E-05 | 5.3E-05 |
| SW | 1.1E-04 | 8.9E-05 | 7.2E-05 | 6.7E-05 | 6.1E-05 | 5.9E-05 | 5.7E-05 |
| SSW | 1.6E-04 | 1.3E-04 | 1.0E-04 | 9.6E-05 | 8.6E-05 | 8.2E-05 | 8.0E-05 |
| S | 2.0E-04 | 1.6E-04 | 1.3E-04 | 1.2E-04 | 1.1E-04 | 1.0E-04 | 9.9E-05 |
| SSE | 2.0E-04 | 1.6E-04 | 1.2E-04 | 1.1E-04 | 1.0E-04 | 9.8E-05 | 9.6E-05 |
| SE | 1.7E-04 | 1.4E-04 | 1.1E-04 | 1.0E-04 | 9.0E-05 | 8.7E-05 | 8.5E-05 |
| ESE | 2.1E-04 | 1.7E-04 | 1.3E-04 | 1.2E-04 | 1.1E-04 | 1.1E-04 | 1.0E-04 |
| E | 2.5E-04 | 2.0E-04 | 1.6E-04 | 1.4E-04 | 1.3E-04 | 1.2E-04 | 1.2E-04 |
| ENE | 1.5E-04 | 1.2E-04 | 9.3E-05 | 8.7E-05 | 7.8E-05 | 7.4E-05 | 7.3E-05 |
| NE | 1.3E-04 | 1.0E-04 | 8.2E-05 | 7.6E-05 | 6.8E-05 | 6.6E-05 | 6.4E-05 |
| NNE | 1.3E-04 | 1.0E-04 | 8.1E-05 | 7.6E-05 | 6.8E-05 | 6.5E-05 | 6.4E-05 |

| Direction | Distance (m) | | | | | | |
|-----------|--------------|---------|---------|---------|---------|---------|---------|
| | 900 | 930 | 1000 | 1120 | 1190 | 1300 | 1500 |
| N | 5.7E-05 | 5.5E-05 | 5.0E-05 | 4.4E-05 | 4.2E-05 | 3.8E-05 | 3.4E-05 |
| NNW | 1.2E-04 | 1.2E-04 | 1.0E-04 | 8.9E-05 | 8.2E-05 | 7.3E-05 | 6.1E-05 |
| NW | 5.6E-05 | 5.4E-05 | 4.9E-05 | 4.4E-05 | 4.1E-05 | 3.8E-05 | 3.3E-05 |
| WNW | 4.2E-05 | 4.0E-05 | 3.7E-05 | 3.4E-05 | 3.2E-05 | 3.0E-05 | 2.7E-05 |
| W | 4.2E-05 | 4.1E-05 | 3.8E-05 | 3.4E-05 | 3.2E-05 | 3.0E-05 | 2.7E-05 |
| WSW | 4.1E-05 | 4.0E-05 | 3.7E-05 | 3.4E-05 | 3.2E-05 | 3.0E-05 | 2.7E-05 |
| SW | 4.4E-05 | 4.3E-05 | 3.9E-05 | 3.6E-05 | 3.4E-05 | 3.2E-05 | 2.8E-05 |
| SSW | 6.0E-05 | 5.7E-05 | 5.2E-05 | 4.6E-05 | 4.3E-05 | 4.0E-05 | 3.5E-05 |
| S | 7.2E-05 | 6.9E-05 | 6.2E-05 | 5.4E-05 | 5.1E-05 | 4.6E-05 | 4.0E-05 |
| SSE | 7.0E-05 | 6.7E-05 | 6.0E-05 | 5.3E-05 | 4.9E-05 | 4.5E-05 | 3.9E-05 |
| SE | 6.3E-05 | 6.0E-05 | 5.5E-05 | 4.8E-05 | 4.5E-05 | 4.1E-05 | 3.6E-05 |
| ESE | 7.6E-05 | 7.2E-05 | 6.5E-05 | 5.7E-05 | 5.3E-05 | 4.8E-05 | 4.2E-05 |
| E | 8.7E-05 | 8.3E-05 | 7.4E-05 | 6.5E-05 | 6.0E-05 | 5.4E-05 | 4.6E-05 |
| ENE | 5.5E-05 | 5.2E-05 | 4.8E-05 | 4.3E-05 | 4.0E-05 | 3.7E-05 | 3.3E-05 |
| NE | 4.9E-05 | 4.7E-05 | 4.3E-05 | 3.9E-05 | 3.6E-05 | 3.4E-05 | 3.0E-05 |
| NNE | 4.9E-05 | 4.7E-05 | 4.3E-05 | 3.8E-05 | 3.6E-05 | 3.4E-05 | 3.0E-05 |

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SUMMARY
Page 6INDIVIDUAL EFFECTIVE DOSE EQUIVALENT RATE (mrem/y)
(All Radionuclides and Pathways)

| Distance (m) | |
|--------------|--|
|--------------|--|

| | |
|-----------|------|
| Direction | 1720 |
|-----------|------|

| | |
|-----|---------|
| N | 3.1E-05 |
| NNW | 5.2E-05 |
| NW | 3.0E-05 |
| WNW | 2.5E-05 |
| W | 2.5E-05 |
| WSW | 2.5E-05 |
| SW | 2.6E-05 |
| SSW | 3.1E-05 |
| S | 3.5E-05 |
| SSE | 3.5E-05 |
| SE | 3.2E-05 |
| ESE | 3.7E-05 |
| E | 4.0E-05 |
| ENE | 3.0E-05 |
| NE | 2.8E-05 |
| NNE | 2.8E-05 |

Jun 8, 2011 12:01 pm

SUMMARY
Page 7INDIVIDUAL LIFETIME RISK (deaths)
(All Radionuclides and Pathways)

| Distance (m) | | | | | | | |
|--------------|---------|---------|---------|---------|---------|---------|---------|
| Direction | 470 | 540 | 620 | 650 | 700 | 720 | 730 |
| N | 7.1E-11 | 5.7E-11 | 4.6E-11 | 4.3E-11 | 3.8E-11 | 3.7E-11 | 3.6E-11 |
| NNW | 1.7E-10 | 1.4E-10 | 1.1E-10 | 9.8E-11 | 8.7E-11 | 8.3E-11 | 8.1E-11 |
| NW | 7.0E-11 | 5.6E-11 | 4.5E-11 | 4.2E-11 | 3.8E-11 | 3.6E-11 | 3.6E-11 |
| WNW | 4.8E-11 | 3.9E-11 | 3.2E-11 | 3.0E-11 | 2.7E-11 | 2.6E-11 | 2.6E-11 |
| W | 4.9E-11 | 4.0E-11 | 3.3E-11 | 3.0E-11 | 2.8E-11 | 2.7E-11 | 2.6E-11 |
| WSW | 4.8E-11 | 3.9E-11 | 3.2E-11 | 3.0E-11 | 2.7E-11 | 2.6E-11 | 2.6E-11 |
| SW | 5.2E-11 | 4.2E-11 | 3.4E-11 | 3.2E-11 | 2.9E-11 | 2.8E-11 | 2.8E-11 |
| SSW | 7.6E-11 | 6.0E-11 | 4.9E-11 | 4.5E-11 | 4.1E-11 | 3.9E-11 | 3.8E-11 |
| S | 9.5E-11 | 7.5E-11 | 6.0E-11 | 5.6E-11 | 5.0E-11 | 4.8E-11 | 4.7E-11 |
| SSE | 9.2E-11 | 7.3E-11 | 5.8E-11 | 5.4E-11 | 4.8E-11 | 4.6E-11 | 4.5E-11 |
| SE | 8.0E-11 | 6.4E-11 | 5.1E-11 | 4.8E-11 | 4.3E-11 | 4.1E-11 | 4.0E-11 |
| ESE | 9.9E-11 | 7.8E-11 | 6.3E-11 | 5.8E-11 | 5.2E-11 | 5.0E-11 | 4.9E-11 |
| E | 1.2E-10 | 9.2E-11 | 7.3E-11 | 6.8E-11 | 6.0E-11 | 5.8E-11 | 5.6E-11 |
| ENE | 6.8E-11 | 5.4E-11 | 4.4E-11 | 4.1E-11 | 3.7E-11 | 3.5E-11 | 3.5E-11 |
| NE | 5.9E-11 | 4.8E-11 | 3.9E-11 | 3.6E-11 | 3.2E-11 | 3.1E-11 | 3.1E-11 |
| NNE | 5.9E-11 | 4.7E-11 | 3.9E-11 | 3.6E-11 | 3.2E-11 | 3.1E-11 | 3.1E-11 |

| Distance (m) | | | | | | | |
|--------------|---------|---------|---------|---------|---------|---------|---------|
| Direction | 900 | 930 | 1000 | 1120 | 1190 | 1300 | 1500 |
| N | 2.7E-11 | 2.6E-11 | 2.4E-11 | 2.2E-11 | 2.0E-11 | 1.9E-11 | 1.7E-11 |
| NNW | 5.8E-11 | 5.5E-11 | 4.9E-11 | 4.2E-11 | 3.9E-11 | 3.5E-11 | 2.9E-11 |
| NW | 2.7E-11 | 2.6E-11 | 2.4E-11 | 2.1E-11 | 2.0E-11 | 1.9E-11 | 1.7E-11 |
| WNW | 2.0E-11 | 2.0E-11 | 1.8E-11 | 1.7E-11 | 1.6E-11 | 1.5E-11 | 1.4E-11 |
| W | 2.1E-11 | 2.0E-11 | 1.8E-11 | 1.7E-11 | 1.6E-11 | 1.5E-11 | 1.4E-11 |
| WSW | 2.0E-11 | 2.0E-11 | 1.8E-11 | 1.7E-11 | 1.6E-11 | 1.5E-11 | 1.4E-11 |
| SW | 2.2E-11 | 2.1E-11 | 1.9E-11 | 1.8E-11 | 1.7E-11 | 1.6E-11 | 1.4E-11 |
| SSW | 2.9E-11 | 2.8E-11 | 2.5E-11 | 2.2E-11 | 2.1E-11 | 1.9E-11 | 1.7E-11 |
| S | 3.4E-11 | 3.3E-11 | 3.0E-11 | 2.6E-11 | 2.4E-11 | 2.2E-11 | 1.9E-11 |
| SSE | 3.3E-11 | 3.2E-11 | 2.9E-11 | 2.5E-11 | 2.4E-11 | 2.2E-11 | 1.9E-11 |
| SE | 3.0E-11 | 2.9E-11 | 2.6E-11 | 2.3E-11 | 2.2E-11 | 2.0E-11 | 1.8E-11 |
| ESE | 3.6E-11 | 3.4E-11 | 3.1E-11 | 2.7E-11 | 2.6E-11 | 2.3E-11 | 2.0E-11 |
| E | 4.1E-11 | 3.9E-11 | 3.5E-11 | 3.1E-11 | 2.9E-11 | 2.6E-11 | 2.2E-11 |
| ENE | 2.6E-11 | 2.5E-11 | 2.3E-11 | 2.1E-11 | 2.0E-11 | 1.8E-11 | 1.6E-11 |
| NE | 2.4E-11 | 2.3E-11 | 2.1E-11 | 1.9E-11 | 1.8E-11 | 1.7E-11 | 1.5E-11 |
| NNE | 2.4E-11 | 2.3E-11 | 2.1E-11 | 1.9E-11 | 1.8E-11 | 1.7E-11 | 1.5E-11 |

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SUMMARY
Page 8

INDIVIDUAL LIFETIME RISK (deaths)
(All Radionuclides and Pathways)

| Distance (m) | |
|--------------|---------|
| <hr/> | |
| Direction | 1720 |
| <hr/> | |
| N | 1.5E-11 |
| NNW | 2.5E-11 |
| NW | 1.5E-11 |
| WNW | 1.3E-11 |
| W | 1.3E-11 |
| WSW | 1.3E-11 |
| SW | 1.3E-11 |
| SSW | 1.6E-11 |
| S | 1.7E-11 |
| SSE | 1.7E-11 |
| SE | 1.6E-11 |
| ESE | 1.8E-11 |
| E | 2.0E-11 |
| ENE | 1.5E-11 |
| NE | 1.4E-11 |
| NNE | 1.4E-11 |

CAP88 - PC

Version 3.0

Clean Air Act Assessment Package - 1988

WEATHER DATA

Non-Radon Individual Assessment
Jun 8, 2011 12:01 pm

Facility: SPRU DP
Address: 2425 River Road
City: Niskayuna
State: NY Zip: 12309

Source Category: H2 enclosure
Source Type: Stack
Emission Year: 2011

Comments: DnD of H2 building
89-2004 wind data rural food path

Dataset Name: H2 Point Source
Dataset Date: 6/8/2011 11:55:00 AM
Wind File: C:\Program Files\CAP88-PC30\WndFiles\knol8904.WND

Jun 8, 2011 12:01 pm

WEATHER
Page 1\

HARMONIC AVERAGE WIND SPEEDS (WIND TOWARDS)

| Pasquill Stability Class | | | | | | | | |
|--------------------------|-------|-------|-------|-------|-------|-------|-------|-----------|
| Dir | A | B | C | D | E | F | G | Wind Freq |
| N | 1.428 | 1.768 | 1.898 | 1.971 | 1.042 | 0.663 | 0.000 | 0.097 |
| NNW | 1.539 | 1.808 | 2.332 | 2.139 | 1.073 | 0.711 | 0.000 | 0.130 |
| NW | 1.387 | 1.444 | 1.400 | 1.248 | 0.838 | 0.702 | 0.000 | 0.044 |
| WNW | 1.303 | 1.365 | 1.193 | 0.882 | 0.701 | 0.563 | 0.000 | 0.027 |
| W | 1.143 | 1.134 | 0.909 | 0.792 | 0.631 | 0.613 | 0.000 | 0.022 |
| WSW | 1.149 | 1.078 | 1.033 | 0.913 | 0.666 | 0.615 | 0.000 | 0.021 |
| SW | 1.297 | 1.372 | 1.445 | 1.322 | 0.938 | 0.660 | 0.000 | 0.038 |
| SSW | 1.380 | 1.712 | 1.779 | 1.961 | 1.135 | 0.820 | 0.000 | 0.068 |
| S | 1.297 | 1.420 | 1.398 | 1.357 | 1.035 | 0.782 | 0.000 | 0.057 |
| SSE | 1.433 | 1.539 | 1.555 | 1.374 | 0.981 | 0.715 | 0.000 | 0.050 |
| SE | 1.628 | 2.068 | 2.500 | 2.116 | 1.082 | 0.700 | 0.000 | 0.068 |
| ESE | 1.911 | 2.708 | 3.690 | 3.554 | 1.425 | 0.785 | 0.000 | 0.190 |
| E | 1.735 | 2.592 | 3.292 | 2.957 | 1.308 | 0.750 | 0.000 | 0.101 |
| ENE | 1.599 | 1.833 | 2.230 | 1.635 | 0.909 | 0.676 | 0.000 | 0.035 |
| NE | 1.459 | 1.806 | 1.810 | 1.199 | 0.918 | 0.643 | 0.000 | 0.026 |
| NNE | 1.425 | 1.590 | 1.218 | 1.003 | 0.820 | 0.615 | 0.000 | 0.027 |

ARITHMETIC AVERAGE WIND SPEEDS (WIND TOWARDS)

| Pasquill Stability Class | | | | | | | |
|--------------------------|-------|-------|-------|-------|-------|-------|-------|
| Dir | A | B | C | D | E | F | G |
| N | 1.774 | 2.251 | 2.847 | 3.130 | 1.528 | 0.914 | 0.000 |
| NNW | 1.839 | 2.323 | 3.177 | 3.125 | 1.554 | 1.041 | 0.000 |
| NW | 1.660 | 1.934 | 2.060 | 2.160 | 1.306 | 1.019 | 0.000 |
| WNW | 1.540 | 1.674 | 1.659 | 1.606 | 1.167 | 0.812 | 0.000 |
| W | 1.341 | 1.436 | 1.368 | 1.404 | 1.009 | 0.861 | 0.000 |
| WSW | 1.356 | 1.451 | 1.653 | 1.896 | 1.049 | 0.842 | 0.000 |
| SW | 1.554 | 1.873 | 2.212 | 2.446 | 1.450 | 0.944 | 0.000 |
| SSW | 1.660 | 2.264 | 2.866 | 3.155 | 1.640 | 1.154 | 0.000 |
| S | 1.585 | 1.991 | 2.311 | 2.474 | 1.576 | 1.146 | 0.000 |
| SSE | 1.666 | 2.145 | 2.544 | 2.218 | 1.399 | 1.023 | 0.000 |
| SE | 1.912 | 2.639 | 3.548 | 3.315 | 1.506 | 0.980 | 0.000 |
| ESE | 2.130 | 3.077 | 4.303 | 4.520 | 1.921 | 1.146 | 0.000 |
| E | 2.026 | 2.952 | 4.182 | 4.253 | 1.831 | 1.125 | 0.000 |
| ENE | 1.913 | 2.527 | 3.687 | 3.035 | 1.430 | 0.981 | 0.000 |
| NE | 1.794 | 2.398 | 3.034 | 2.335 | 1.396 | 0.891 | 0.000 |
| NNE | 1.715 | 2.187 | 2.104 | 1.884 | 1.270 | 0.822 | 0.000 |

Jun 8, 2011 12:01 pm

WEATHER
Page 2

FREQUENCIES OF STABILITY CLASSES (WIND TOWARDS)

| Pasquill Stability Class | | | | | | | |
|--------------------------|--------|--------|--------|--------|--------|--------|--------|
| Dir | A | B | C | D | E | F | G |
| N | 0.0166 | 0.0272 | 0.0957 | 0.3246 | 0.1128 | 0.0496 | 0.0000 |
| NNW | 0.0545 | 0.0977 | 0.3024 | 0.6829 | 0.1892 | 0.1114 | 0.0000 |
| NW | 0.1726 | 0.1982 | 0.2801 | 0.3102 | 0.1571 | 0.1343 | 0.0000 |
| WNW | 0.3168 | 0.2595 | 0.2241 | 0.1501 | 0.1260 | 0.1430 | 0.0000 |
| W | 0.3407 | 0.2808 | 0.1912 | 0.1379 | 0.1484 | 0.2055 | 0.0000 |
| WSW | 0.3033 | 0.2154 | 0.1907 | 0.1714 | 0.1769 | 0.2088 | 0.0000 |
| SW | 0.1651 | 0.1754 | 0.1730 | 0.1833 | 0.1429 | 0.1270 | 0.0000 |
| SSW | 0.0990 | 0.1235 | 0.1747 | 0.2745 | 0.1366 | 0.1343 | 0.0000 |
| S | 0.1012 | 0.1067 | 0.1444 | 0.3154 | 0.2270 | 0.2020 | 0.0000 |
| SSE | 0.0900 | 0.0926 | 0.1268 | 0.3648 | 0.2827 | 0.1904 | 0.0000 |
| SE | 0.0595 | 0.0805 | 0.1347 | 0.3520 | 0.1984 | 0.1184 | 0.0000 |
| ESE | 0.0221 | 0.0672 | 0.1973 | 0.4392 | 0.0981 | 0.0398 | 0.0000 |
| E | 0.0493 | 0.0984 | 0.3142 | 0.7300 | 0.1996 | 0.1051 | 0.0000 |
| ENE | 0.0573 | 0.0792 | 0.1773 | 0.3875 | 0.2655 | 0.1989 | 0.0000 |
| NE | 0.0593 | 0.0815 | 0.1454 | 0.2847 | 0.2817 | 0.2338 | 0.0000 |
| NNE | 0.0495 | 0.0546 | 0.0897 | 0.2538 | 0.2790 | 0.2020 | 0.0000 |
| TOTAL | 0.0798 | 0.1019 | 0.1989 | 0.4155 | 0.1711 | 0.1176 | 0.0000 |

ADDITIONAL WEATHER INFORMATION

```

Average Air Temperature: 10.0 degrees C
                        283.16 K
Precipitation: 100.0 cm/y
Humidity: 8.0 g/cu m
Lid Height: 1000 meters
Surface Roughness Length: 0.010 meters
Height Of Wind Measurements: 10.0 meters
Average Wind Speed: 2.660 m/s

```

Vertical Temperature Gradients:

| | |
|-------------|-----------|
| STABILITY E | 0.073 k/m |
| STABILITY F | 0.109 k/m |
| STABILITY G | 0.146 k/m |

ATTACHMENT D

Equipment Sketches and Specification Details

(Typical)

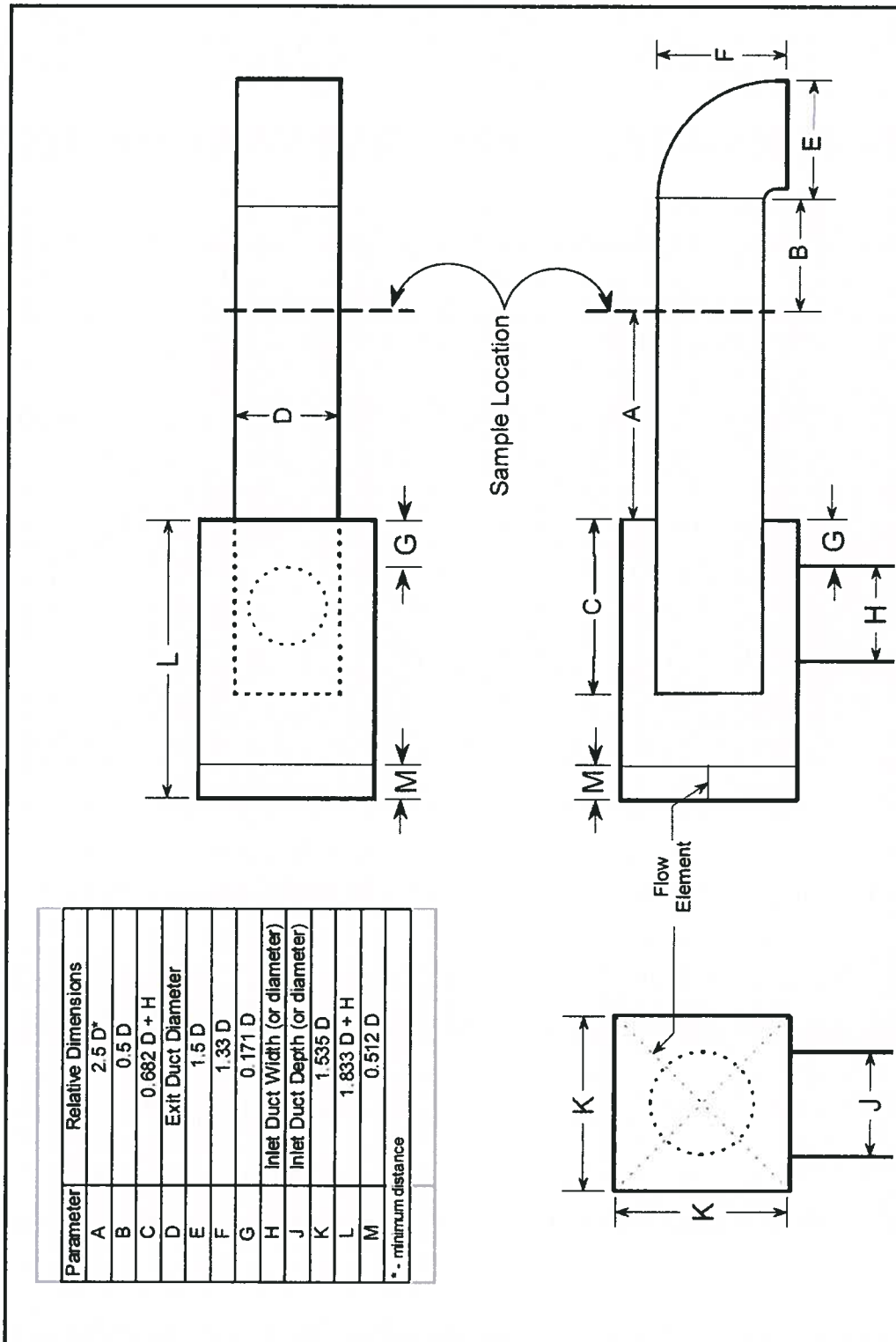
Ventilation Air Mover and Filtration System

Sampling Section and Sampler/Withdrawal Location

A mixing box and sampling duct apparatus according to Figure 15.11 K of Radioactive Air Sampling Methods by Maiello and Hoover (2011) will be provided. Off-the-shelf air sample pumps, filter holders, and an ANSI/HPS N13.1-1999 shrouded sample probe with custom designed air mixer and sample duct that matches the required flow rate range of the enclosure ventilation system will be installed. The sample probes are stainless steel. Nominal parameters for the mixer and sampling systems are:

1. For a HEPA filtered air handler rated at 48,000 ACFM (nominal):
 - a. Overall length, width and height – 25 feet L, 10 feet W, and 8 feet H
 - b. Sampling duct diameter - 60 inches (nominal)
 - c. Duct inlet connection - 60 inches (nominal)
 - d. Delta P at maximum flow rate - 15 inches H₂O
 - e. Mixer, duct, air sampler and protective “doghouse” mounted on a structural frame.
2. Vendor testing prior to delivery will certify the following:
 - a. A certificate of conformance for each air sampling system attesting that the sampling system has been tested and/or analyzed as required to satisfy ANSI/HPS N13.1-1999 Section 5.2.2.2. Testing of individual systems for gas or particulate COV is not required if suitable prototype testing is documented and the Vendor certifies that the item sold to buyer conforms to the tested unit and/or configuration.
 - b. The vendor will perform velocity COV testing on each unit.
 - c. Calibration certificates for the air sample pump and air flow instruments will be provided with each air monitoring system.

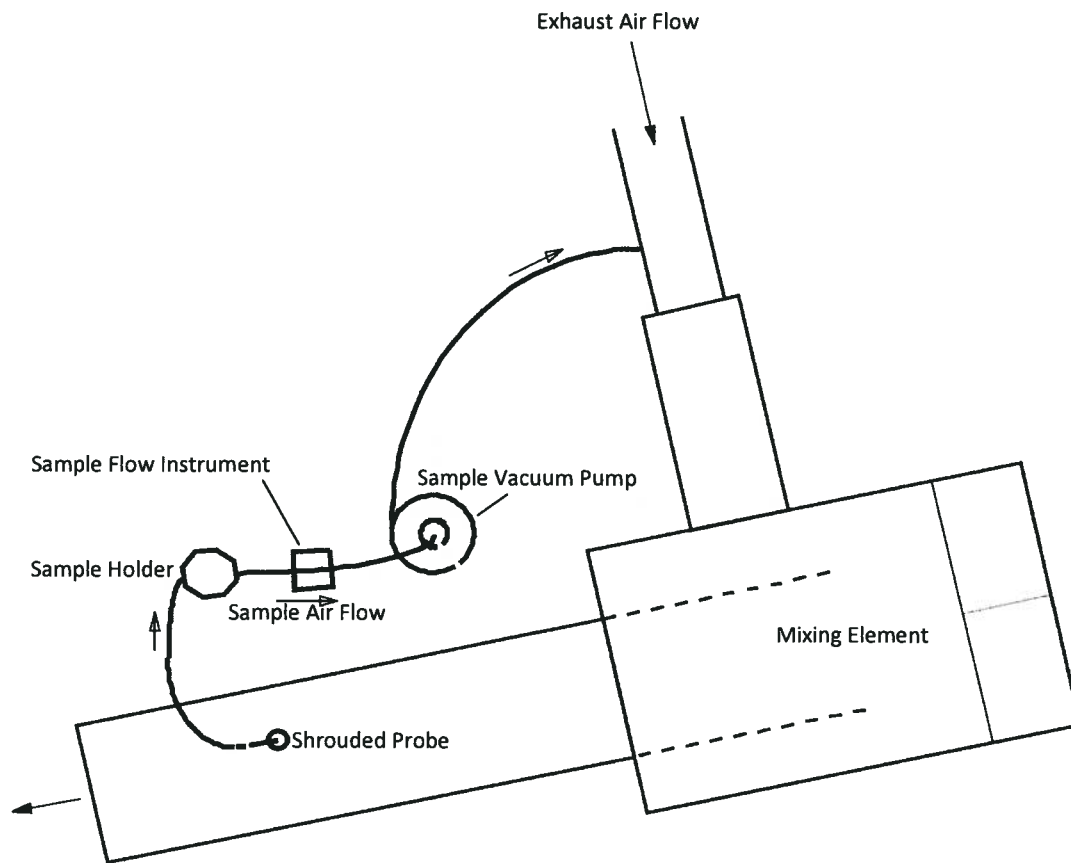
Generic Mixing System



Note: End elbow (E) not required unless wind will affect sample location flow profile

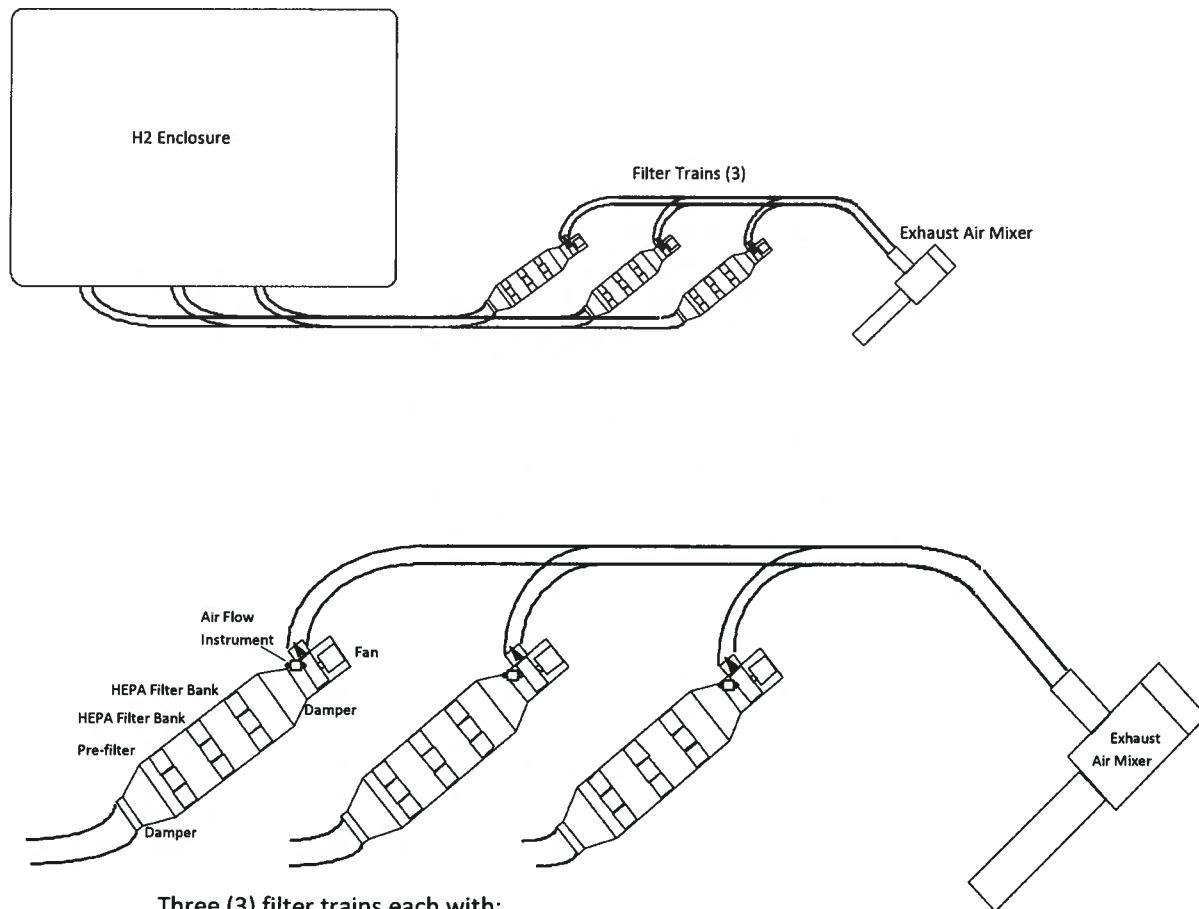
H₂ Enclosure Exhaust Air Mixer

General Arrangement (not to scale)



H2 Enclosure Ventilation System

Proposed General Arrangement (not to scale)



Three (3) filter trains each with:

- Inlet damper,
- Pre-filter,
- First-stage HEPA filter,
- Second-stage HEPA filter,
- Outlet damper,
- Flow measurement instrument, and
- Fan.

Exhaust air mixer with:

- Shrouded sample probe
- Sample flow measurement instrument
- Sample filter holder
- Sample vacuum pump

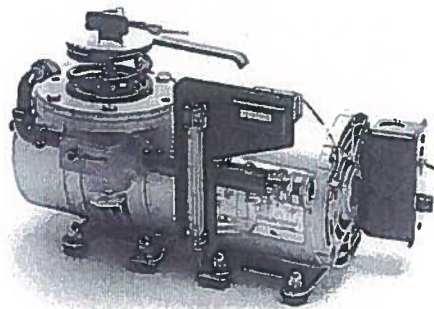
Typical Air Sample Pump

RADēCO

17 West Pkwy Plainfield, Ct. 06374
TEL: (860) 564-1220 FAX (860) 564-6631 www.radecoinc.com

PORTABLE CONSTANT FLOW AIR SAMPLER MODEL AVS-28A

- CONSTANT AIRFLOW MAINTAINED WITH ΔP ACROSS THE FILTER OF UP TO 17" Hg (FLOW RATE DEPENDENT)
- BALANCED, EASY TO CARRY COMPACT SYSTEM
- FLOW RATE INDICATION ON ROTOMETER, CFM OR LPM
- RATED FOR CONTINUOUS DUTY
- LOW NOISE LEVEL
- MINIMUM MAINTENANCE
- OPTIONAL ELAPSED TIME INDICATOR
- ALL UNITS INDIVIDUALLY CALIBRATED AND TRACEABLE TO NIST



Industry Workhorse Continues to Lead the Field

The Model AVS-28A Portable Constant Flow Air Sampler is a continuous duty, constant flow device. It can be used with filters and cartridges in the collection of airborne contaminants, or as a regulated, positive displacement vacuum supply for continuous air monitors and stack sampling systems.

The ability of the AVS-28A to maintain a preset sample flow rate is controlled by the unique side-mounted regulator valve. The RADēCO regulator valve is not a bypass design, and therefore the exhaust contains only sampled air. The AVS-28A has the superior ability to compensate for added ΔP across sampling media.

The sampling flow rate is read out on a side-mounted rotometer which measures the differential pressure across the in-line anodized aluminum venturi. All units are individually calibrated and traceable to NIST.

RADēCO

17 West Pkwy Plainfield, CT 06374

TEL: (860) 564-1220 FAX: (860) 564-6631, www.radecoinc.com

PORTABLE CONSTANT FLOW AIR SAMPLER MODEL AVS-28A

Specifications

Air Flow Rate: Adjustable from 0.5 to 3.5 CFM (10 to 100 LPM).

Air Flow Regulation: $\pm 5\%$ of set air flow rate up to maximum capability of pump.

Dimensions/Weight: 12" Long x 14" Wide 9" High, (30.5 cm x 35.6 cm x 22.9 cm), 38 lbs (17.27 kg).

Power Requirement/Cable: 115V, 60Hz, 4.6 Amps; 230V, 50hz, 2.3 Amps. Three wire, (6) six feet (10) Ten Amp rating; British and European available.

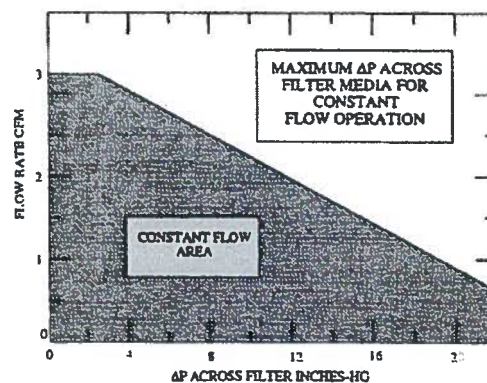
Air Flow Indicator: Venturi mounted rotometer.

Air Mover/Motor: Self-adjusting carbon vane type. Pump is designed for continuous operation at 26" Hg vacuum. Rated at 1/4 horsepower with thermal overload protection.

Input Connection: 3/8" Female Quick Disconnect.

Re-settable Elapsed Time Meter: 99999 hours and 59 minutes, pushbutton re-

| Sample Holders Available | |
|---|---|
| Model No. | Description |
| 2500-04 | 2" diameter filter, open face |
| 2500-42 | 47 mm diameter filter, open face |
| 2500-21 | 2" diameter filter/RADēCO cartridge, open face |
| 2500-46 | 47 mm diameter filter/RADēCO cartridge, open face |
| 2500-45 | 2" diameter filter/RADēCO cartridge, in-line |
| 2500-44 | 47 mm diameter filter/RADēCO cartridge, in-line |
| Other style holders available. Please call for selection information. | |



Typical Air Sample Flow Instrument

RADēCO

17 West Pkwy Plainfield, CT. 06374

TEL: (860) 564-1220 FAX: (860) 564-6631 Email: info@radecoinc.com www.radecoinc.com**CONTINUOUS AIR VOLUME TOTALIZER
MODEL AVT-100**

- EASILY ADAPTS TO MOST POSITIVE DISPLACEMENT PUMPS
- RUGGED TURBINE MONITORS FLOW
- LCD DISPLAYS:
 - Elapsed Sample Time
 - Flow Rate
 - Total Volume
- BATTERY-BACKED DATA MEMORY
- MICROPROCESSOR BASED
- CIRCUIT BREAKER
- EASE OF CALIBRATION



The **Model AVT-100** has been designed for use in continuous air sampling applications. This microprocessor based unit is a reliable alternative to the use of rotometers, venturi and mechanical time meters, simplifying air sampling procedures while adding significantly higher accuracy to air sampling data.

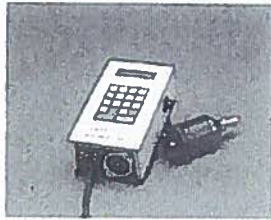
The **Model AVT-100** is composed of two assemblies—the display chassis assembly and the remote air turbine assembly. The two assemblies are interconnected by an 18" cable with locking connectors. The remote air turbine assembly can be attached to the exhaust of any non-lubricated positive displacement pump. The air turbine rotates at speeds proportional to the air velocity of the pump's inlet (sampled air). The turbine's rotation is sensed by a reflective sensor/breaker disc. The microprocessor converts the signal to volume and displays the FLOW RATE, TOTAL VOLUME, and ELAPSED TIME on the LCD readout.

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MODEL AVT-100 CONTINUOUS AIR VOLUME TOTALIZER



When the sampling pump is plugged into the **AVT-100**, the **AVT-100** will control the AC power applied to the pump, should the AC power be interrupted, the **AVT-100** will store all sampling data and restart the sampler when the AC power is restored

Specifications

| | |
|-------------------------------|---|
| Operational Range: | Up to 999,999 cubic feet or 999,999 cubic meters |
| Accuracy of Totalizer: | ± 5% FS |
| Timer Circuit: | Microprocessor-controlled crystal oscillator |
| Operational Voltage: | 95 to 135V, 50 to 60 Hz, 1 Phase, or 205—240V, 50 Hz, 1 Phase |
| Chassis Dimensions: | 8" Long x 4.75" Wide x 4" High 203mm x 121mm x 102mm |
| Turbine Dimensions: | 4" Long x 2" Diameter, with 18" Cable 102mm x 51mm, with 457mm Cable |
| Weight: | 3 Pounds (1.4 Kg) |
| Turbine Inlet: | 1/4" NPT (Female Thread) |
| Turbine outlet: | 1/8" NPT (Female Thread) |
| Readout of Totalizer: | LCD; Two lines 16 characters, backlit. Continuous display of cumulative volume + flowrate + elapsed time. Toggles between CFM and LPM |
| Controls: | ON/OFF Switch (circuit breaker) Keypad, 16 key controls function and calibration |

Air Sample Withdrawal Nozzle

SHROUDED SAMPLING PROBE



Information & specifications may change without notice

- Meets requirements for ANSI N13.1-1999 and ISO 2889 2008
- Available for 1.0 inch or 1.5 inch sample lines
- Improved transmission efficiency over range of flow velocities
- Improved transmission efficiency over range of flow angles
- Lower internal wall losses than isokinetic sample probes
- Less sensitive to flow turbulence
- Use in fixed or variable sample flow systems

The Shrouded Sampling Probe is anisokinetic probe manufactured by Lab Impex Systems (LIS) under licence from Texas A & M University. The probe is designed for high efficiency extraction of aerosols from ventilation stacks, and for the nuclear industry is most commonly used in radioactive effluent sampling and measurement systems.

This probe design has several advantages over non-shrouded probes (such as the traditional isokinetic variety): lower internal wall losses, better off-angle performance, lower sensitivity to flow stream turbulence, and the ability to operate in either a fixed flow or variable flow rate mode.

Another significant benefit is that a single probe design may be used for a range of stack velocities and geometries, thereby allowing a single shrouded sampling probe design to be used for a variety of different stack applications (diameters and flow rates). Shrouded probes are typically less expensive than a custom sampling rake designed for a single stack.

Optimal Efficiency

In a stack installation, the shrouded probe will be used with a transport system specifically designed to ensure that aerosol losses within the sample probe and transport lines are kept to a minimum. Typically a system will comprise a shrouded probe, an in-stack transport line, a mounting flange, and an external transport line that conveys the aerosol sample from the stack to the sampling or monitoring system.

Transport system design is an important step in optimizing overall sampling efficiency, and Lab Impex Systems can assist clients in the design process by using software modelling to determine the transmission efficiency of aerosol through the transport system.



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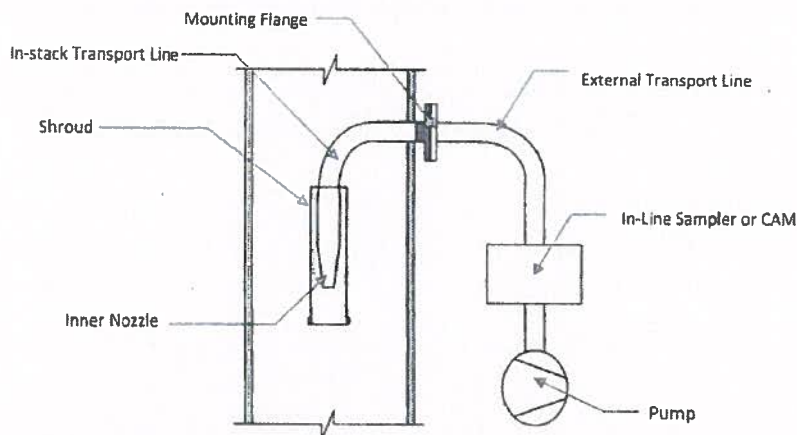
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SHROUDED SAMPLING PROBE

Principle of Operation

A vacuum pump (installed downstream of the sampling or monitoring system) will draw a continuous sample of stack gas through the probe and transport system.

At the entrance to the probe, the stack gas will be decelerated by the shroud to a velocity about one third that of the free stream in the stack. The inner nozzle will sample the central core of the gas stream which enters the shroud, while the remainder of the gas is exhausted at the rear of the shroud via the annular gap between the shroud and the inner nozzle.



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The Advantages of Using the Shrouded Probe

- 1) A single probe design is suitable for the majority of stacks. Custom probe design is not required for each stack.
- 2) The shrouded probe can sample over a range of stack velocities. Isokinetic sampling is only valid when the draw off velocity is equal to free-stream velocity.
- 3) In ventilation systems where the stack velocity does change, the variation of transmission with velocity is lower than a traditional isokinetic probe.
- 4) The shrouded probe allows representative sampling to be achieved through a single point measurement. A sampling rake is not required to achieve representative sampling.

Performance Characteristics

ANSI N13.1-1999 specifies that over the range of anticipated operating conditions (sampling flow rate and stack velocity) an acceptable aerosol sampling probe must have a transmission ratio * between 80% and 130% and an aspiration ratio** less than 150% for 10 μ m aerodynamic diameter aerosol particles.

*The transmission ratio is the concentration of aerosol at the exit plane of a probe divided by the concentration in the stack at the probe location.

**The aspiration ratio is the aerosol concentration at the probe entrance plane divided by the concentration in the stack at the probe location.



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SHROUDED SAMPLING PROBE

Shrouded Sampling Probe

PHYSICAL CHARACTERISTICS

The shrouded probes are manufactured to close tolerances using 304 stainless steel.

DIMENSIONS (Height x Depth x Width)

The shrouded probes use the same external shroud (and dimensions) but have different internal dimensions based on the application.

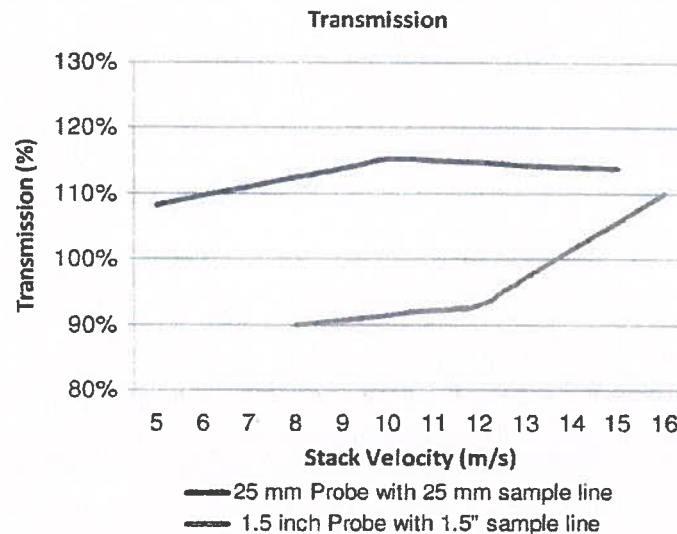
- Overall Length: 242 mm (probe only - without sample lines)
- Diameter: 60 mm diameter (at widest point, lip on inlet)
- Connection: 25 mm ID, 1.0-inch ID, or 1.5-inch ID depending on the model of probe selected

ISO-2889 2009 Requirements

While not a comprehensive list of requirements, the bullet points listed below summarize the primary requirements of ISO-2889 *Sampling Airborne Radioactive Materials from the Stacks and Ducts of Nuclear Facilities* as issued in 2009.

- Sampling location provides the ability to extract a representative sample.
- Determine the properties of the sampling location through a series of tests.
- Determine penetration of contaminants through the system.
- Penetration 10- μ m AD particles greater than 50%
- Actual penetration should be measured.
- Extract, deliver, and collect $\geq 50\%$ of gases or vapours etc.
- Demonstrate performance of multi-nozzle probes in the same way as a single nozzle.

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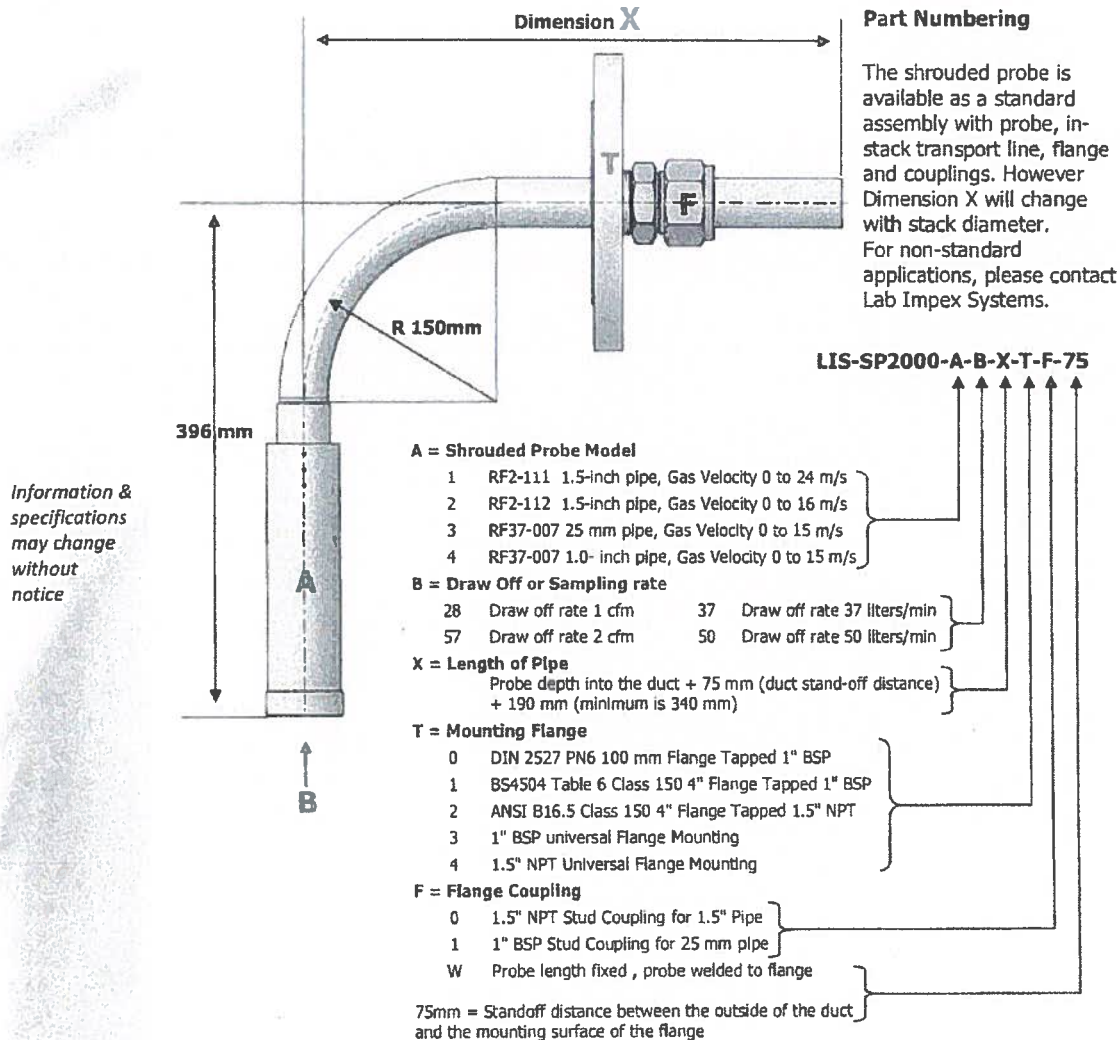


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SHROUDED SAMPLING PROBE



References:

- ANSI/HPS N13.1-1999 "Sampling and Monitoring Releases of Airborne Radioactive Substances from the Stacks and Ducts of Nuclear Facilities"
- ISO 2889 "Sampling Airborne Radioactive Materials from the Stacks and Ducts of Nuclear Facilities" issued in 2009
- Chandra, S.; McFarland, A. R. (1995) Comparison of aerosol sampling with shrouded probe and unshrouded probes. *Am. Ind. Hyg. Assoc. J.* 56:459-466
- Chandra, S.; McFarland, A. R. (1997) Shrouded probe performance: Variable flow operation and effect of free stream turbulence. *Aerosol Sci. Technol.* 26:111-126



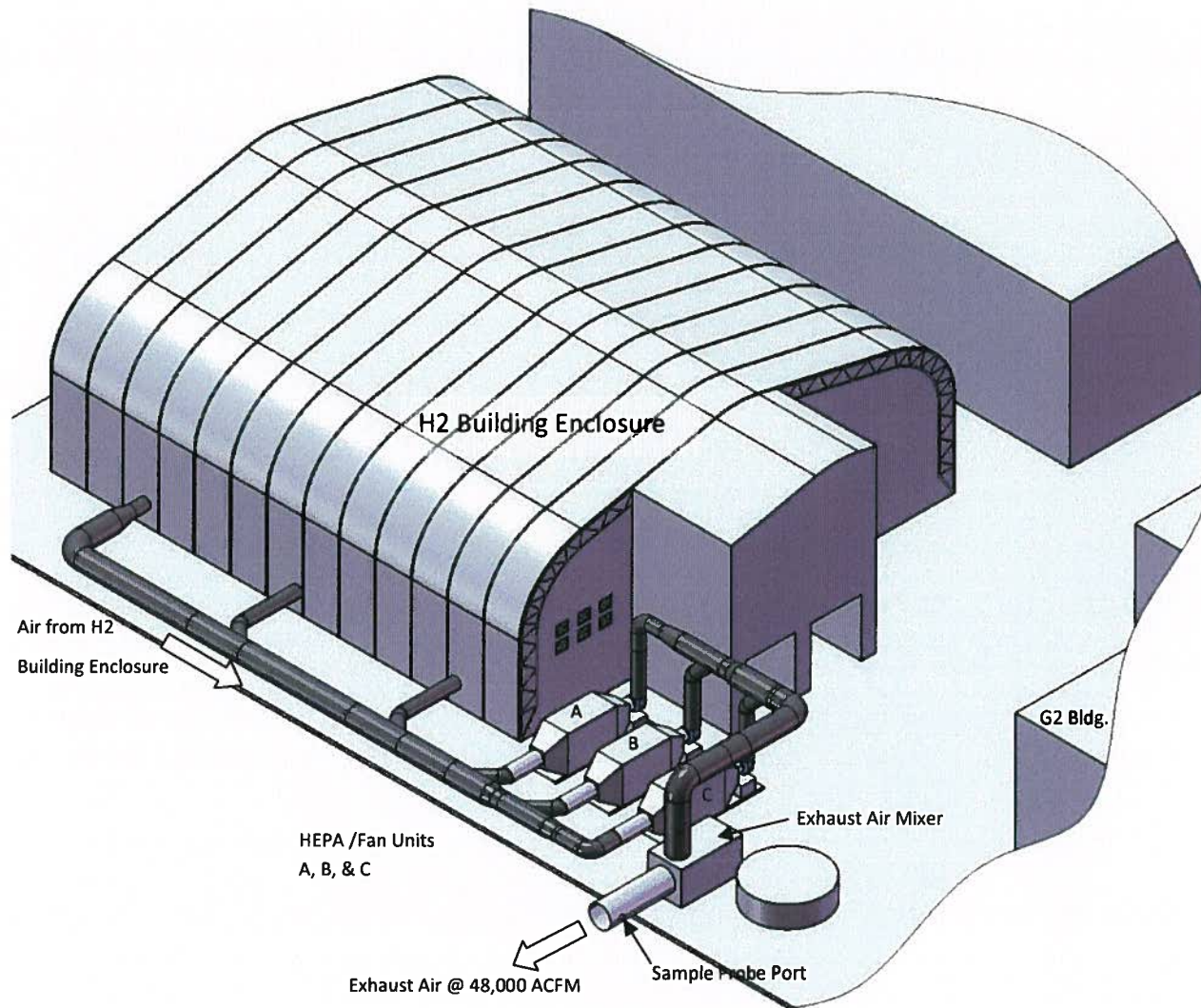
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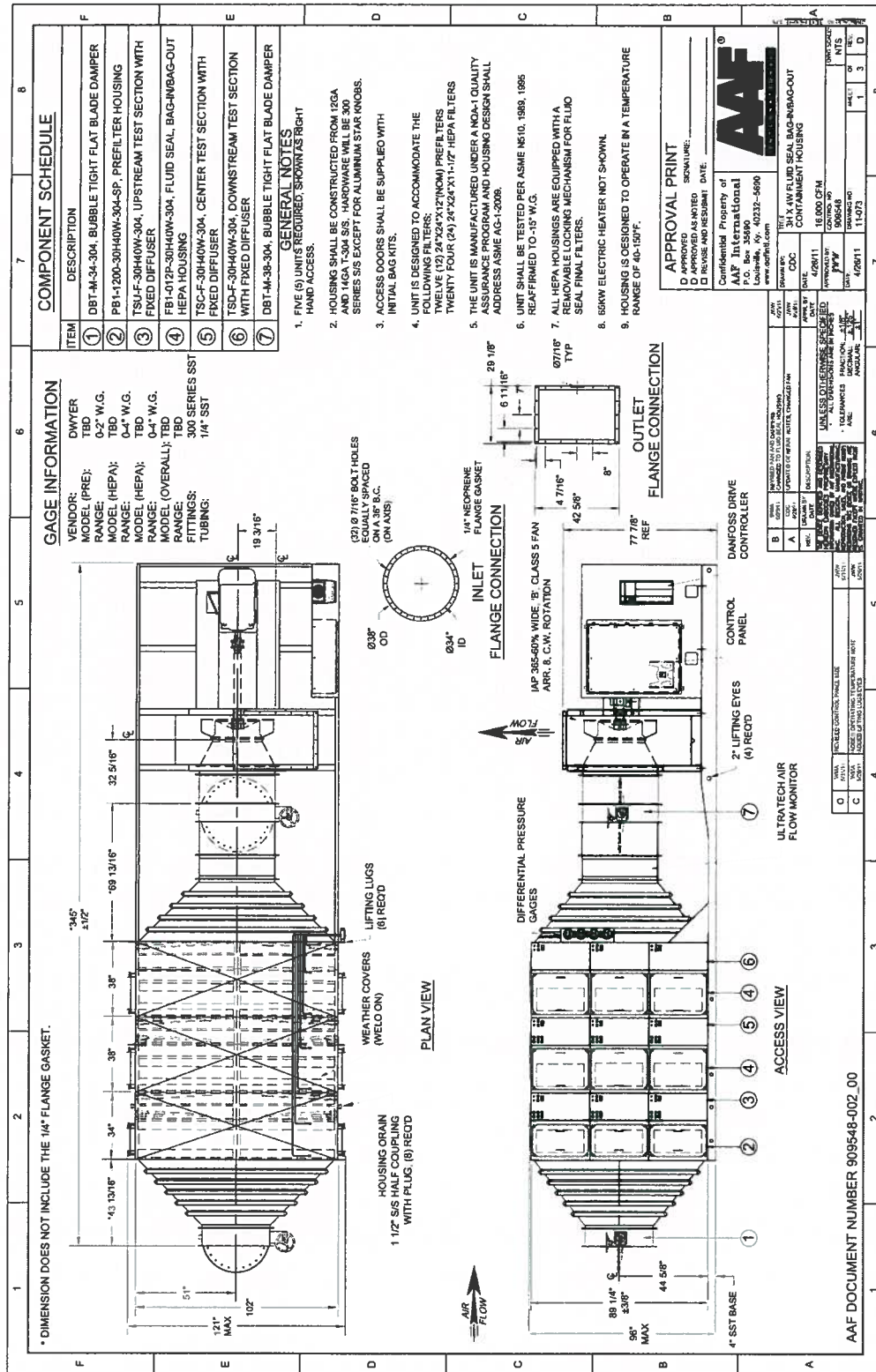
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H2 Enclosure Ventilation Exhaust System Component Arrangement (Preliminary Design)



H2 Enclosure Ventilation Exhaust HEPA /Fan Unit Assembly (Preliminary Design)



Re General Note 9. – The specification range has been modified to “ambient to 150° F.”