A3. Interim Cover

Standard Proctor Test Results Summary

Lift Approval Summary

Lift Approval Package

Buyoff Surveys

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A3. Interim Cover Standard Proctor Test Results Summary

Set	Proctor ID#	Date Sampled	Date Approved	Maximum Dry Density (lb/ft³)	Optimum Moisture Content (%)	Soils Description
	Interim Cover #1	04/21/10	06/08/10	124.5	12.0	Brown (10YR5/3) clay with abundant very fine to fine, subround to subangular, moderate to well sorted, sand
Set #1	Interim Cover #2	04/21/10	06/08/10	123.9	12.2	Brown (10YR5/3) clay with abundant very fine to fine, subround to subangular, moderate to well sorted, sand
	Interim Cover #3	04/21/10	06/08/10	123.7	12.2	Brown (10YR5/3) clay with abundant very fine to fine, subround to subangular, moderate to well sorted, sand
	Interim Cover #1 (2011)	03/21/11	03/28/11	119.7	11.0	Grayish in color and consists mostly fines
	Interim Cover #2 (2011)	08/05/11	08/11/11	115.6	13.5	Grayish in color and consists mostly fines
	Interim Cover #3 (2011)	09/20/11	10/04/11	115.0	14.5	Tannish in color and consists of mostly fines
	Interim Cover #4 (2011)	11/30/11	12/19/11	114.8	15.3	Tannish in color and consists of mostly fines
				Interim Co	over Top S	Soil
	Top Soil #1	01/04/10	02/08/10	115.6	12.3	Gray in color consist of mostly fines
	Top Soil #2	01/15/10	02/08/10	116.6	13.9	Grayish-red in color
	Top Soil #3	01/21/10	02/08/10	113.5	13.9	Grayish in color consist of mostly fines
	Top Soil #4	02/12/10	02/18/10	110.3	14.5	Grayish in color consist of mostly fines
	Top Soil #5	03/12/10	03/30/10	114.1	13.5	Grayish in color consist of mostly fines
	Top Soil #6	03/25/10	03/30/10	116.7	13.0	Grayish in color consist of mostly fines
	Top Soil #7	04/01/10	06/08/10	117.2	12.3	Brownish-gray in color consists mostly fines
	Top Soil #8	04/07/10	06/08/10	117.3	12.9	Brownish-gray in color consists mostly fines
	Top Soil #9	04/15/10	06/08/10	118.4	11.9	Brownish-gray in color consists mostly fines
	Top Soil #10	04/20/10	06/08/10	119.9	11.7	Material contains a small amount of shale and is gray in color
	Top Soil #11	04/27/10	06/08/10	118.2	12.2	Material contains a small amount of shale and is gray in color
	Top Soil #12	05/03/10	06/08/10	117.8	13.1	Gray in color consist of mostly fines
	Top Soil #13	05/06/10	06/08/10	115.7	13.8	Gray in color consist of mostly fines
	Top Soil #14	05/12/10	06/08/10	116.1	12.6	Gray in color consist of mostly fines
	Top Soil #15	05/18/10	06/08/10	115.0	13.9	Gray in color consist of mostly fines
	Top Soil #16	05/24/10	06/08/10	118.2	12.0	Gray in color consist of mostly fines
	Top Soil #17	05/27/10	06/08/10	120.3	10.8	Gray in color consist of mostly fines
	Top Soil #18	06/03/10	06/14/10	116.1	11.0	Grayish-yellow in color consist of mostly fines
	Top Soil #19	06/08/10	06/14/10	120.2	11.4	Grayish-yellow in color consist of mostly fines
	Top Soil #20	06/14/10	06/30/10	117.6	13.0	Gray in color consist of mostly fines
	Top Soil #21	06/17/10	06/30/10	119.7	13.1	Gray in color consist of mostly fines
	Top Soil #22	06/23/10	06/30/10	119.5	12.3	Gray in color consist of mostly fines
	Top Soil #23	07/07/10	07/29/10	115.0	11.2	Gray in color consist of mostly fines
	Top Soil #24	07/19/10	07/29/10	117.0	10.8	Grayish-yellow in color consist of mostly fines
	Top Soil #25	07/26/10	07/29/10	117.3	10.9	Gray in color consist of mostly fines
	Top Soil #26	08/02/10	08/26/10	115.7	11.7	Gray in color consist of mostly fines
	Top Soil #27	08/12/10	08/26/10	117.1	11.8	Gray in color consist of mostly fines
	Top Soil #28	08/24/10	09/07/10	119.4	11.4	Gray in color consist of mostly fines
	Top Soil #29	08/30/10	09/07/10	118.8	10.7	Gray in color consist of mostly fines
	Top Soil #30	09/09/10	09/24/10	119.6	11.2	Gray in color consist of mostly fines
	Top Soil #31	09/13/10	10/04/10	119.4	11.3	Gray in color consist of mostly fines
	Top Soil #32	09/15/10	10/04/10	118.0	11.4	Gray in color consist of mostly fines

A3. Interim Cover Standard Proctor Test Results Summary

Set	Proctor ID #	Date Sampled	Date Approved	Maximum Dry Density (lb/ft ³)	Optimum Moisture Content (%)	Soils Description
	Top Soil #33	09/16/10	10/04/10	119.6	11.3	Gray in color consist of mostly fines
	Top Soil #34	09/20/10	10/04/10	118.0	11.9	Gray in color consist of mostly fines
	Top Soil #35	09/21/10	10/04/10	116.8	12.4	Reddish in color consist of mostly fines
	Top Soil #36	09/23/10	10/05/10	117.8	12.0	Grayish in color consist of mostly fines
	Top Soil #37	09/27/10	10/05/10	118.7	11.9	Grayish in color consist of mostly fines
	Top Soil #38	09/29/10	10/06/10	119.7	11.6	Grayish in color consist of mostly fines
	Top Soil #39	10/04/10	10/15/10	118.1	12.0	Grayish in color consist of mostly fines
	Top Soil #40	10/07/10	10/15/10	118.8	11.8	Grayish in color consist of mostly fines
	Top Soil #41	10/12/10	11/01/10	118.1	11.7	Grayish in color consist of mostly fines
	Top Soil #42	10/14/10	11/01/10	116.7	11.7	Grayish in color consist of mostly fines

A3. Interim Cover Lift Approval Summary

Date	Lift ID #	# of Passing Moisture Tests	Quantity Approved (yd^3)	Cumulative Quantity Approved (yd³)	Average Thickness (ft.)	Northing	Easting	# of Nuclear Density Gauge Verifications	# of Sandcone Verifications
07/09/10	UIF27100709-00	0	156	156	0.1	6794574	2122394	1	0
07/21/10	UIB18100721-00	1	9,391	9,547	1.0	6795037	2122151	4	1
07/26/10	UIA18100726-00	0	1,096	10,643	0.9	6795027	2122117	0	0
08/05/10	UIA02100805-00	0	6,898	17,541	0.8	6795839	2122044	0	0
09/07/10	UIA01100907-00	0	1,403	18,944	1.0	6795943	2122062	0	0
11/30/10	UIE01101129-00	1	2,646	21,590	1.0	6795942	2122340	0	0
03/21/11	UII12110321-00	3	2,677	24,267	0.9	6795685	2122344	2	0
03/21/11	UIJ21110321-00	2	1,610	25,877	0.8	6795205	2122358	1	0
03/22/11	UIM12110322-00	1	2,307	28,184	1.0	6795690	2122512	0	0
03/22/11	UIK28110322-00	1	1,748	29,932	1.0	6794440	2122467	0	0
03/22/11	UII24110322-00	1	2,418	32,350	0.8	6794868	2122406	0	0
03/29/11	UII12110329-00	0	297	32,647	0.1	6795685	2122343	0	0
03/29/11	UIK28110329-00	1	175	32,822	0.1	6794436	2122467	0	0
03/29/11	UIM12110329-00	1	461	33,283	0.2	6795690	2122512	0	0
03/30/11	UIJ21110330-00	1	604	33,887	0.3	6795205	2122358	0	0
03/30/11	UII24110330-00	0	537	34,424	0.2	6794869	2122406	0	0
04/06/11	UIJ12110406-00	2	3,640	38,064	0.6	6795350	2122545	0	0
04/11/11	UIJ35110411-00	1	62	38,126	0.8	6794164	2122572	1	0
04/12/11	UIJ12110411-00	1	1,820	39,946	0.3	6795350	2122545	0	0
08/08/11	UIM18110805-00	1	2,988	42,934	0.7	6795069	2122708	2	0
08/09/11	UIM30110809-00	1	2,881	45,815	1.0	6794498	2122724	2	0
08/10/11	UIM18110809-00	1	2,376	48,191	0.3	6795067	2122691	2	0
08/10/11	UIN35110810-00	0	150	48,341	0.9	6794198	2122754	1	0
08/10/11	UIN35110810-01	1	83	48,424	0.5	6794198	2122754	1	1
09/21/11	UIR28110921-00	1	2,669	51,093	0.8	6794560	2122953	2	0
09/22/11	UIR28110922-00	1	1,501	52,594	0.4	6794560	2122934	2	0
09/26/11	UIQ23110926-00	1	1,784	54,378	0.8	6794806	2122939	2	0
09/23/11	UIS35110926-00	0	88	54,466	0.7	6794216	2123001	1	0
09/27/11	UIQ23110927-00	1	939	55,405	0.4	6794807	2122920	2	0
10/14/11	UIQ18111014-00	1	1,429	56,834	0.9	6795025	2122940	2	0
10/14/11	UIQ18111017-00	1	493	57,327	0.3	6795023	2122940	2	0
11/30/11	UIM10111130-00	1	4,880	62,207	1.0	6795440	2122710	3	0
12/01/11	UIM10111201-00	1	1,464	63,671	0.3	6795440	2122710	2	0
03/15/12	UIM01120313-00	1	5,643	69,314	0.8	6795994	2122773	4	0
03/16/12	UIM01120315-00	1	2,551	71,865	0.3	6796069	2122774	2	0

Total Quantity Approved (yd³) = 71,865
Total # of Nuclear Density Gauge Tests = 41

ai # of Naoical Delisity Gaage 105ts = 41

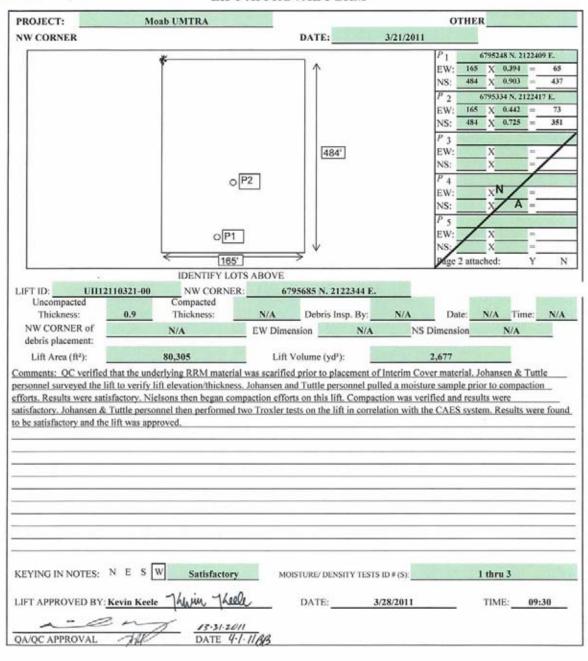
Total # of Moisture Tests = 31

Quantity per Moisture Test $(yd^3) = 2,318$

Total Average Thickness (ft.) = 0.63



LIFT APPROVAL FORM



Density Testing DOE-EM/GJRAC1783 Rev. 0

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Slope Elevation Survey

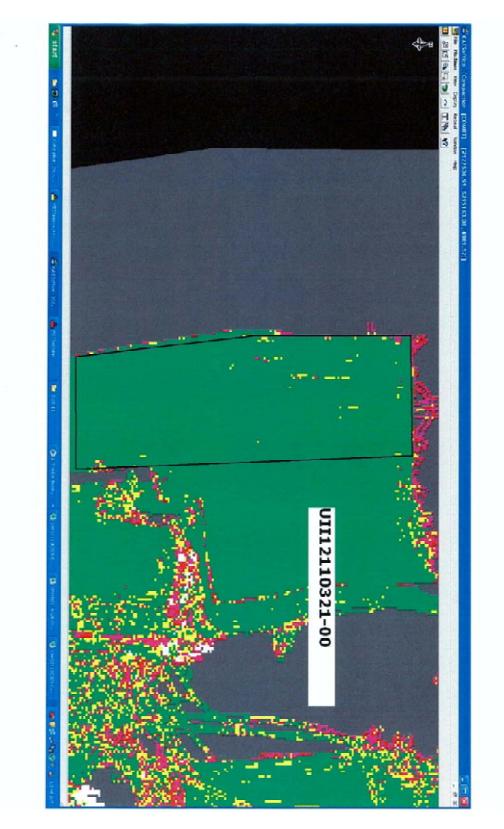
	Average lift	thickness=	0.9	Bounding Box	Northing	Easting	
	Grid Size=	Grid Size= 50'		Lower Left			
Lift ID:	· ·	1112110321-0	0	Upper Right		A	
Las	t Lift Elevat	tions	Lif	t Approval El	evations	Lift Thickness	
Northing	Easting	Elevation	Northing	Easting	Elevation	Thickness	
6795311	2122399	4993.0	6795311	2122399	4993.9	0.9	
6795461	2122399	4995.1	6795461	2122399	4996.0	0.9	
6795511	2122399	4994.2	6795511	2122399	4995.1	0.9	
6795261	2122449	4992.1	6795261	2122449	4992.8	0.7	
6795461	2122449	4995.2	6795461	2122449	4996.2	1.0	
6795211	2122499	4990.7	6795211	2122499	4991.5	0.8	
6795361	2122499	4994.3	6795361	2122499	4995.3	1.0	П
6795411	2122499	4995.6	6795411	2122499	4996.6	1.0	
6795561	2122499	4993.8	6795561	2122499	4994.8	1,0	
6795361	2122549	4994.6	6795361	2122549	4995.4	0.8	
6795511	2122599	4995.7	6795511	2122599	4996.3	0.6	
6795561	2122599	4994.6	6795561	2122599	4995.4	0.8	
						0.0	
						0.0	
						0.0	
				G11		0.0	
		10	_			0.0	
	2		A			0,0	
						0,0	_
						0.0	
			2			0.0	
						0.0	

EnergySolutions

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% =6	97.8%			-1.50		
Elevation Avg	4994.7	1	T T	2000		Minimum Number of Machine
Total =6	7222	1		Pass	Passes	
Total Lines	7385	1				3
		Lift ID:	UII12110321-00			
Northing	Easting		# of Passes	Passes =6	Count	ŀ
6795636	2122346	4993.6	4		1	Lift Height
6795682	2122346	4992.2	2		1	1' 0"
6795518	2122349	4994.7	6	- 1	1	
6795521	2122349	4994.7	6	1	1	Thick Lift Threshold
6795524	2122349	4994.6	6	1	1	2. 0
6795527	2122349	4994.5	6	1	1	
6795531	2122349	4994.4	6	1	1	Last Lift Elevation
6795534	2122349	4994.4	6	1	1	N/A
6795537	2122349	4994.4	6	1	1	
6795541	2122349	4994.3	6	1	1	Min. # of Wheel Passes
6795544	2122349	4994.3	6	1	1	6
6795547	2122349	4994.3	5		1	
6795550	2122349	4994.3	6	1	1	
6795554	2122349	4994.2	5		1	
6795557	2122349	4994.4	3		1	
6795560	2122349	4994.3	4		1	
6795564	2122349	4994.5	2		1	
6795567	2122349	4994.5	1		1	
6795593	2122349	4992.9	0		1	
6795626	2122349	4993.6	4		1	
6795629	2122349	4993.6	2		1	
6795632	2122349	4993.6	5		1	
6795636	2122349	4993.5	6	1	1	
6795639	2122349	4993.5	2		1	
6795642	2122349	4993.4	5		1	
6795646	2122349	4993.4	2		1	
6795652	2122349					
6795655	2122349	4993.1	4		1	
		4993.1	2	-	1	
6795662	2122349	4992.7	6	1	1	
6795668	2122349	4992.8	2		1	
6795672	2122349	4992.3	3		1	
6795675	2122349	4992.3	2		1	
6795678	2122349	4992.2	6	1	1	
6795682	2122349	4992.1	6	1	1	
6795685	2122349	4992.2	6	1	- 1	
6795403	2122352	4996.6	6	1	1	
6795406	2122352	4996.8	6	1	1	
6795409	2122352	4996.6	6	1	1	
6795413	2122352	4996.7	6	1	1	
6795416	2122352	4996.7	6	1	1	
6795419	2122352	4996.7	6	1	1	
6795422	2122352	4996.8	6	1	1	
6795426	2122352	4996.8	6	1	1	
6795429	2122352	4997.0	6	1	1	
6795432	2122352	4997.0	6	1	1	

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PROJECT: Moab UM	FRA Project		OTHER	
	2012 C C C C C C C C C C C C C C C C C C C	-00	DATE: 3/2	
TEST ID NUMBER(S): TEST LOCATION;				N/A DYGOLO
		_	TEST METHOD: N/A D1556	
ASTM D6938 (DENSITY DE		/	ASTM D1556 (DENSITY DE	/
Make/Model Gaug	e Serial#		Testing Apparatus Calibrates	
Last Calibration Date:	/		Bulk Density of sand (ρ ,) Mass of Sand to Fill Cone & Plate (i)	
Daily Standard Counts:			Mass of Sand to Fill Cone & Flate ("2)g
Density Mo	juire		Mass of bottle & cone before fi	lling
Method A (Direct Transmission or	Method B (Backsc	catter)	cone, plate &	
Depth Setting (inches) A Co	unt Time(minu	tes)	Mass of bottle & cone after fi cone, plate &	
Moisture Count	ensity Count		Mass of sand to fill o	
			plate, & hole (
Wet Density (1)(lbs/ft 3) Dr	y Density(lbs/ft3)	Mass of sand to file	hole g
			Mass of wet soil oonti	iner g
Moisture Density(lbs/ft ³) Me	oisture Fraction	(%)	Mass of Aonta	iner g
MOISTURE DETERMINATION			Mass of wet soil ()	M.) o
ASTM D464	3		Test Hole Vol	
Container ID 1263				/p; cm ³
Mass of container & wet specimen		_	/	
(M _{cmi})	1540.0	g	$M_A = 100 M_A / (w + 1)$	
Mass of container & dry specimen	10.1010	- 6	Wet Der	1001/17/1
(M ets)	1516.3	g		2.43 lbs/ft 3
Mass of water (M ,,)	2000		Dry De	nisty
$M_{w} = M_{cms} - M_{cds}$	23.7	g	$\rho_d = M$	/Vg/cm ³
M			Dry Unit We	eight
Mass of container (M _e) Mass of dry specimen (M _s)	1263.0	g		2.43lbs/ft ³
$M_x = M_{cdx} - M_c$	253.3	g	Soil Description: fine to fine, subre	
Moisture content (w)		T°	Proctor ID: Inte	
$w = (M_w / M_z) \times 100$	9.4	96	Standard Proctor (AST	
Dry Density $(\rho_{ab} = (100 \times \rho_{m}))$	1/(100 ± w)		Maximum Dry Density (7 amax)	134.5 (lbs/0 ³)
			Maximum Dry Density (72max)	124.5 (105/11)
pd = (100 x #####) ((100 + 9.3 Note: Wes Density from ASTM D 1 N (0 - 100) pr	0.0 //	bs/fi ³	Optimum Moisture (14 apr.)	12.0 (%)
		w.	Required Moisture: 7.0 %	to 17.0 %
Percent Compaction = Pa /	74 max x 100			1920 U - 1940 U - 1940 U
0.0 / 124.5 x 100 =	0.0 %		Required Percent Compaction	90.0 (%)
Comments:			TEST RESULTS:	320
dicrowave oven power setting on HIGH			X Pass	Date: 3/23/11
ninutes and subsequent incremental dry		ite until	Failed Moisture	
change of 0.1 % or less of the initial we	t mass of the soil.		Failed Compaction	Time: 09:00
			By: Kevin Keele / 1/4/	um Theele
			(print)	(signature)
~ on	03-31.2011			
QA/QC APPROVAL	DATE			



FIELD DENSITY TEST

PROJECT: Moab U	MTRA Project	OTHER	
LIFT IDENTIFICATION:	UII12110321-00	DATE:	3/28/2011
TEST ID NUMBER(S):		2	
TEST LOCATION:	P1	TEST METHOD: N/A D	D1556 X D6938
ASTM D6938 (DENSITY I		ASTM D1556 (DENS	SITY DETERMINATION)
Make/Model Troxler 3430 Ga	uge Serial # 25142	Testing Apparatus C	Calibrated Vol. (lbs/ft 1)
Last Calibration Date: 3/	7/11	Bulk Density of sand (p1)	g/cm ³ y/s
Daily Standard Counts: On-Cell Standard		Mass of Sand to Fill Cone &	
Density 2396	Moisture 647	Mass of bottle & cone	hafara filling
Method A (Direct Tr	ansmission)		, plate & hole g
Depth Setting 8" (inches)		Mass of bottle & con-	e after filling
74.400000000000000000000000000000000000			, plate & hole g
Moisture Count 106	Density Count 1394		& hole (M)
Vet Density (pm) 123.8 (lbs/ft ³)	Dry Density 115.0 (lbs/ft ³)		nd to fill hole
		Mass of wet soi	/ —
Moisture Density 8.8 (lbs/ft ³)	Moisture Fraction 7.6 (%)		sof Antainer g
IOISTURE DETERMINATION		1	vet soil (M ₂)
ASTM D4	643	/	Hole Volume
Container ID 137:	5		$I_1 - M_2 / \rho_1$ cm ³
Mass of container & wet specimen		/	y Mass of soil
(M _{cmi})	1640.4 g		g /(w + 100)g
Mass of container & dry specimen		/ /	Wet Denisty
(M ctc)	1619.1 g	$\rho_m = (M)$	/V) x 62.43 lbs/ft
Mass of water (M ,,)	2.0		Dry Denisty
$M_{sc} = M_{cons} - M_{cds}$	21.3 g	/	$\rho_d = M_d / V g/cm^2$
100 4 100 100		Dry.	Unit Weight
Mass of container (M_c)	1375.0 g	V	= ρ _d x 62.43lbs/ft ²
Mass of dry specimen (M,)		Brown (10	YR5/3) Clay w/abundant ver
$M_s = M_{cdr} - M_c$ Moisture content (w)	244.1 g		ne, subround to subangular,
$w = (M_w / M_s) \times 100$	8.7 %		Interim Cover # 1 ctor (ASTM D698)
. (8.7		
Dry Density $(\rho_{i0} = (100 x)$	$(a_m)/(100 + w)$	Maximum Dry Density	(7 amax) 124.5 (lbs/ft
pd = (100 x 123.8)/(100+	8.7 = 113.9 /bs/ft 1	Optimum Moistu	re (w _{ept}) 12.0 (%)
Note: Wet Density from ASTM D 1556 (pm) take		10-12/2004 01 2 1 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	
Percent Compaction = p _d	/ v.mav v 100	Required Moisture:	0_% to17.0_%
113.9 / 124.5 x 100 =		Required Percent Cor	mpaction: 90.0 (%)
omments:	2.000		70.0 (70)
licrowave oven power setting on HIG	H. Initial time setting of 3	TEST RESULTS:	Date: 100/11
inutes and subsequent incremental d		X Pass	Date: 3/28/11
change of 0.1 % or less of the initial	기구에 가면한 구점 가장이 가장 이 경험에 되었다.	Failed Moisture Failed Compact	
			/ 141.141 160lg
		By: Kevin Keele	(signature)
Bun		the may	1. Spannery
	03312011		
QA/QC APPROVAL	DATE		

PROJECT: Moab UM	TRA Project		OTH	IER
LIFT IDENTIFICATION:	UII1211032	21-00		
TEST ID NUMBER(S):			3	
TEST LOCATION:				A D1556 X D6938
ASTM D6938 (DENSITY DE				ENSITY DETERMINATION)
Moisture Count 114	1	nutes)	Testing Apparatus Bulk Density of sand (p , Mass of Sand to Fill Co Mass of bottle & cc Mass of bottle & cc Mass of bottle & cc Mass of pli	Calibrated Vol. (lbs/ft³) g/cm³ ps/ft³ ne & Plate (M₂) g one before filling one, plate & hole cone after filling one, plate & hole sand to fill cone ate, & hole (M₁) g
Wet Density (ρ_m) 128.5 (lbs/ft^3) Dr Moisture Density 9.6 (lbs/ft^3) M		• C.C. 105-01-100	Mass of wer	f sand to filt hole g soil to container g wass of Anntainer g
MOISTURE DETERMINATION ASTM D464 Container ID 1263	3	Mass	of wet soil (M_3) g lest Hole Volume $(M_1 - M_2)/\rho_1 \qquad cm^3$	
Mass of container & wet specimen (M _{cms}) Mass of container & dry specimen	1536.0	g		Dry Mass of soil 9 M 1/(w + 100)g Wet Denisty
(M _{cds}) Mass of water (M _w)	1513.6	g	P	(M ₃ /V) x 62.43lbs/ft ³ Dry Denisty
$M_w = M_{cons} - M_{cds}$	22.4	g		$\rho_d = M_d / V$ g/cm^3 Dry Unit Weight
Mass of container (M _c) Mass of dry specimen (M _c)	1263.0	g		$\gamma_d = \rho_d \times 62.43$ lbs/ft ³ (10YRS/3) Clay w/abundant very
$M_x = M_{cds} - M_c$	250.6	g	Soil Description: fine t	o fine, subround to subangular, Sau
Moisture content (w) $w = (M_w / M_s) \times 100$	8.9	96	Proctor ID:	Interim Cover # 1 Proctor (ASTM D698)
Dry Density $(p_{ab} = (100 \times p_{ab}))$)/(100 + w)		Maximum Dry Den	sity (7 max) 124.5 (lbs/ft ³)
pd = (100 x 128.5)/(100 + 8.5 Note: Wet Density from ASTM D 1556 (ρ_w) soler percent Compaction = ρ_d /	vsidence over ASTM D 6938	lbs/ft ³	AT COMPANY OF THE PARTY OF THE	isture (w _{opt})(%) 7.0 _% to%
118.0 / 124.5 x 100 =	94.7 %		Required Percent	Compaction: 90.0 (%)
Comments: Microwave oven power setting on HIGH ninutes and subsequent incremental dry a change of 0.1 % or less of the initial we	ing periods of 1 mir		TEST RESULTS: X Pass Failed Moist Failed Comp By: Kevin Keele (print)	
~ our	03:31-2011			
QA/QC APPROVAL	DATE			



		In	terim Cover	LIT	TID: UIBIS	
Point#	Northing	Easting			Difference in feet	Difference in inch
	6794150		4964.7	4964.7	0.0	Difference in inches
	6794142		4964.6	4964.6	0.1	0
-	6794165		4965.3	4965.2	0.1	
	6794168	2122322	4965.3	4965.2	0.1	0
	6794173	2122372	4965.5	4965.4	0.1	0
	6794176	2122422	4965.5	4965.5	0.0	0
	6794170	2122477	4965.5	4965.5	0.0	0
	6794178	2122470	4965.7	4965.7	0.1	0
	6794171	2122515	4965.4	4965.4	0.0	0
	6794200	2122550	4966.2	4966.1	0.0	0
	6794200	2122500	4966.2	4966.1	0.0	0
	6794200	2122450	4966.2	4966.1	0.1	0
	6794200	2122400	4966.1	4966.1	0.0	0
	6794200	2122350	4966.1	4966.0	0.0	0
	6794192	2122315	4965.9	4965.8	0.1	0
	6794200	2122300	4966.1	4966.0	. 0.1	0
	6794242	2122266 2122265	4965.9	4965.8	0.0	0.
	6794242	2122250	4967.1	4967.1	0.0	0.
	6794242	2122315	4967.3	4967.2	0.0	0.
	6794242	2122315	4967.1 4967.3	4967.1	0.0	0.
	6794250	2122350	4967.3	4967.3	0.0	0.
	6794227	2122370	4967.0	4967.3 4967.0	0.0	0.
	6794227	2122420	4966.8		0.0	0.
	6794227	-2122471	4966.8	4966.8 4966.8	0.0	0.
-	6794220	2122507	4966.7	4966.7	0.0	0.
	6794219	2122548	4966.7	4966.7	0.0	0.
	6794250	2122550	4967.4	4967.4	0.0	0.:
	6794250	2122500	4967.4	4967.4	0.0	0.0
	6794250	2122450	4967.4	4967.4	0.0	0.
	6794250	2122400	4967.3	4967.3	0.0	0.
	6794269	2122486	4967.9	4967.9	0.0	0.:
	6794270	2122537	4968.0	4968.0	0.0	0.
	6794300	2122500	4968.7	4968.6	0.0	0.
	6794300	2122450	4968.6	4968.6	0.0	0.3
	6794283	2122440	4968.2	4968.2	0.0	0.3
	6794277	2122420	4968.1	4968.1	0.0	0.5
	6794311	2122426	4968.9	4968.9	0.0	0.3
	6794310	2122420	4968.9	4968.9	0.0	0.1
	6794300	2122400	4968.6	4968.6	0.0	0.1
	6794310	2122371	4969.0	4968.9	0.0	0.4
	6794300	2122350	4968.6	4968.6	0.1	0.7
	6794277	2122317	4968.0	4968.0	0.0	0.3
	6794292	2122316	4968.4	4968.4	0.0	0.3
	6794310	2122321	4968.8	4968.8	0.0	0.4
	6794316	2122315	4969.0	4969.0	0.0	0.3
	6794333	2122338	4969.4	4969.4	0.0	0.4
	6794349	2122343	4969.9	4969.9	0.0	0.1
	6794350	2122350	4969.8	4969.8	0.0	0.1
	6794344	2122401	4969.8	4969.8	0.0	0.0
	6794354	2122404	4970.1	4970.1	0.0	0.1
	6794350	2122450	4969.9	4969.9	0.0	0.1
	6794350	2122500	4970.0	4969.9	0.0	0.6
_	6794337	2122368	4969.6	4969.5	0.0	0.4
	6794359	2122320	4970.1 4969.9	4970.1	0.0	0.1

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67943		4970.4	4970.4	0.0	0
67941		4965.9	4965.9	0.0	0
67942		4967.1	4967.1	0.0	0
67943		4968.5	4968.5	0.0	0
679429 679429		4968.4	4968.4	0.0	0
679430		4968.4	4968.4	0.0	0
679430		4968.5 4968.6	4968.5	0.0	0
67943		4968.9	4968.5	0.1	1.
679427		4968.1	4968.9 4968.1	0.0	0.
679437		4970.7	4970.7	0.0	0.
679439		4971.0	4971.0	0.0	0.
679440		4971.2	4971.2	0.0	0.
679441		4971.5	4971.5	0.0	0.
679440		4971.2	4971.1	0.0	0.
679441		4971.4	4971.4	0.0	0
679440	0 2122400	4971.1	4971.1	0.0	0.:
679438	3 2122389	4970.7	4970.7	0.0	0.:
679439	9 2122384	4971.1	4971.1	0.0	0.4
679442		4971.7	4971.6	0.0	0.3
679441		4971.4	4971.4	0.0	0.3
679443		4972.0	4972.0	0.0	0.3
679440		4971.1	4971.1	0.0	0.0
679441		4971.5	4971.5	0.0	0.3
679442		4971.7	4971.7	0.0	0.1
679437		4970.5	4970.5	0.0	0.0
679436		4970.4	4970.3	0.0	0.3
679435		4969.8	4969.8	. 0.0	0.1
679436 679439		4970.0	4970.0	0.0	0.3
679440		4970.8 4971.2	4970.8	0.0	0.5
679439		4970.9	4971.2 4970.9	0.0	0.1
679439		4971.1	4971.1	0.0	0.1
6794389		4970.9	4970.8	0.0	0.0
6794410		4971.4	4971.3	0.0	0.5
6794420		4971.6	4971.6	0.0	0.3
6794450		4972.3	4972.3	0.0	0.1
6794460		4972.7	4972.6	0.0	0.1
6794460		4972.7	4972.7	0.0	0.1
6794450	2122350	4972.4	4972.3	0.0	0.1
6794459	2122371	4972.7	4972.7	0.0	0.4
6794450	2122400	4972.4	4972.4	0.0	0.2
6794450		4972.4	4972.4	0.0	0.2
6794450		4972.5	4972.4	0.1	0.7
6794450		4972.4	4972.4	0.0	0.1
6794460		4972.8	4972.8	0.0	0.3
6794511		4974.0	4974.0	0.0	0.5
6794500		4973.7	4973.7	0.0	0.0
6794510		4974.0	4973.9	0.1	0.8
6794510		4973.9	4973.9	0.0	0.4
6794500		4973.7	4973.6	0.0	0.1
6794511		4974.0	4974.0	0.0	0.1
6794500		4973.6	4973.6	0.0	0.1
6794510		4974.0	4973.9	0.0	0.4
6794500 6794510		4973.6	4973.6	0.0	0.4
6794510	2122275	4973.9	4973.9	0.0	0.2
6794560	2122300	4974.9	4974.8	0.0	0.3
6794550	2122325 2122350	4975.2 4974.9	4975.1	0.0	0.3
6794561	2122371	4975.2	4974.9 4975.2	0.0	0.1
0/34301	41440111	49/0.21	49/0 /	0.0	0.1

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	794561	2122411	4975.2	4975.2	0.0	0.
	794550	2122450	4975.0	4974.9	0.0	0.:
	794561	2122461	4975.3	4975.3	0.0	0.
	794600	2122450	4976.2	4976.2	0.0	. 0.:
	794611	2122430	4976.6	4976.6	0.0	0.3
	794623	2122418	4976.8	4976.8	0.0	0.:
	794630	2122400	4977.0	4977.0	0.0	0.0
	794600	2122400	4976.2	4976.2	0.0	0.2
	794610 794620	2122381	4976.5	4976.5	0.0	0.0
	794620		4976.8	4976.8	0.0	0.1
	794600	2122368	4976.5	4976.5	0.0	0.0
	794630	2122350	4976.2	4976.1	0.0	0.3
	794610	2122302	4977.0 4976.5	4977.0	0.0	0.1
	794650	2122300	4977.4	4976.4	0.0	0.5
	794600	2122300	4976.1	4977.4	0.0	0.4
	794660	2122302	4977.7	4976.1	0.0	0.2
	794650	2122350	4977.4	4977.7 4977.4	0.0	0.0
	794650	2122400	4977.4	4977.4	0.0	0.3
	794680	2122400	4978.2	4978.2	0.0	0.2
	94700	2122400	4978.7	4978.7	0.0	0.3
	94700	2122350	4978.7	4978.7		0.2
	94680	2122350	4978.2	4978.2	0.0	0.4
	94678	2122298	4978.2	4978.2	0.0	0.5
	94700	2122300	4978.7	4978.6	0.0	0.2
67	94730	2122300	4979.5	4979.5	0.0	0.4
67	94730	2122400	4979.5	4979.5	0.0	0.5
67	94750	2122400	4980.0	4980.0	0.0	0.6
	94780	2122400	4980.9	4980.8	0.0	0.5
	94800	2122400	4981.3	4981.2	0.1	0.6
	94830	2122400	4982.1	4982.1	0.0	0.2
	94850	2122400	4982.5	4982.5	0.0	0.3
	94880	2122400	4983.4	4983.3	0.0	0.6
	94900	2122400	4983.8	4983.8	0.1	0.6
	94930	2122400	4984.6	4984.6	0.0	0.3
	94950	2122400	4985.0	4985.0	0.0	0.2
	94980	2122400	4985.9	4985.9	0.0	0.3
	95000	2122400	4986.3	4986.3	0.0	0.3
	95030	2122350	4987.1	4987.1	0.0	0.6
	95000	2122350	4986.3	4986.2	0.0	0.6
	94980	2122350	4985.8	4985.8	0.0	0.4
	94950	2122350	4985.0	4985.0	0.0	0.2
	94930 94900	2122350	4984.6	4984.5	0.0	0.5
	94900	2122350 2122350	4983.8	4983.7	0.0	0.6
	94850	2122350	4983.3	4983.3	0.0	0.3
	94800	2122350	4982.5 4981.2	4982.5	0.0	0.6
	94730	2122350	4981.2	4981.2	0.1	0.6
	94750	2122350	4979.5	4979.5	0.0	0.6
	94780	2122350	4980.8	4979.9 4980.8	0.0	0.4
	4750	2122300	4979.9	4979.9	0.0	0.1
	4780	2122300	4979.9	4979.9	0.0	0.3
	4800	2122300	4981.2	4981.2	0.0	0.4
	94830	2122300	4982.1	4982.0	0.0	0.4
	4850	2122300	4982.5	4982.4	0.0	0.5
	4866	2122323	4982.9	4982.9	0.0	0.3
	4880	2122300	4983.3	4983.2	0.0	0.6
	4900	2122300	4983.7	4983.7	0.0	0.6
	4909	2122323	4984.0	4984.0	0.0	0.4
	4950	2122300	4985.0	4985.0	0.0	0.1
	4960	2122323	4985.3	4985.3	0.0	0.6

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	50		P		Dave Steward	
ate:	7/21/2010 C	QC signature: E	Beachem Bosh		eviewed by: Dave Stewar	t
	6795000	2122150	4986.2	4986.1	0.0	0.
	6795009	2122173	4986.4	4986.4	0.0	0.
	6795000	2122200	4986.2	4986.2	0.0	0.
	6795000	2122250	4986.2	4986.2	0.0	0
	6794959	2122223	4985.2	4985.2	0.0	0
	6794950	2122200	4984.9	4984.9	0.0	0
	6794959	2122173	4985.2	4985.2	0.0	
	6794909	2122173	4983.9	4983.9	0.0	
	6794909	2122223	4983.9	4983.6 4983.9	0.0	(
-	6794900	2122200	4983.7	4982.6	0.0	(
	6794859	2122173	4982.6	4982.7	0.0	
	6794859	2122223	4982.4 4982.7	4982.4	0.0	
	6794850	2122200	4981.2	4981.1	0.0	
-	6794750	2122200	4979.9	4979.8	0.0	
	6794696 6794750	2122200 2122200	4978.6	4978.6	0.0	
		2122200	4978.6	4978.6	0.1	
	6794660 6794700	2122202	4977.6	4977.6	0.0	
	6794650	2122200	4977.4	4977.3	0.0	
	6794400	2122300	4971.1	4971.1	0.0	
	6794309	2122242	4968.8	4968.8	0.0	2015)
	6794350	2122250	4969.8	4969.8	0.0	
	6794390	2122235	4970.8	4970.8	0.0	
	6794400	2122250	4971.0	4971.0	0.0	
	6794416	2122232	4971.4	4971.4	0.0	
	6794460	2122274	4972.6	4972.6	0.0	
	6794450	2122250	4972.3	4972.3	- 0.0	
732-7	6794462	2122225	4972.6	4972.6	0.0	
	6794500	2122250	4973.6	4973.6	0.0	
Santa	6794510	2122224	4973.9	4973.9	0.0	
2.52-535-1-	6794561	2122226	4975.2	4975.2	0.0	
	6794550	2122250	4974.9	4974.8	0.0	
- Assessment	6794559	2122274	4975.2	4975.2	0.0	
	6794600	2122250	4976.1	4976.1	0.1	
	6794610	2122252	4976.6	4976.4	0.0	
	6794650	2122250	4977.4	4977.7 4977.3	0.0	
	6794660	2122252	4977.7	4978.4	0.0	
	6794689	2122250	4978.6 4978.5	4978.6	0.0	
	6794700	2122250	4979.9	4979.9	0.0	
	6794781 6794750	2122250 2122250	4980.7	4980.7	0.0	
	6794800		4981.2	4981.1	0.0	
	6794830		4982.0	4981.9	0.0	
	6794850		4982.4	4982.4	0.0	
	6794859		4982.7	4982.7	0.0	
	6794900		4983.7	4983.7	0.0	
	6794909		4983.9	4983.9	0.0	
	6794950		4985.0	4984.9	0.0	-
	6794959	2122273	4985.2	4985.2	0.0	
	6795009	2122273	4987.0 4986.5	4987.0 4986.5	0.0	

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CRJ 000746

	The same of the sa		Intovino Com	. D. 6#	LIFT ID:	UIA02
Point#	Northing	Easting	Interim Cov			
1364	6795100	2122150			erence in feet Di	fference in inches
1363	6795100	2122200	4988.670	4988.661	0.0	
1362	6795100	2122250	4988.693	4988.690	0.0	
1361			4988.744	4988.718	0.0	
1360	6795100	2122300	4988.785	4988.747	0.0	
1339	6795100	2122350	4988.792	4988.776	0.0	
	6795150	2122350	4990.050	4990.039	0.0	
1340	6795150	2122300	4990.020	4990.010	0.0	0
1341	6795150	2122250	4989.986	4989.982	0.0	. 0
1342	6795150	2122200	4989.982	4989.953	0.0	0
1343	6795150	2122150	4989.943	4989.924	0.0	0
1322	6795200	2122150	4991.218	4991.188	0.0	0
1321	6795200	2122200	4991.245	4991.217	0.0	0
1320	6795200	2122250	4991.255	4991.245	0.0	
1319	6795200	2122300	4991.280	4991.274	0.0	0
1318	6795200	2122350	4991.345	4991.303	0.0	0
1297	6795250	2122350	4992.571	4992.566	0.0	0
1298	6795250	2122300	4992.542	4992.537	0.0	
1299	6795250	2122250	4992.520	4992.509	0.0	0.
1300	6795250	2122200	4992.507	4992.480	0.0	
1301	6795250	2122150	4992.452	4992.451	0.0	0.
1280	6795300	2122150	4993.763	4993.715		0.
1279	6795300	2122200	4993.776	4993.743	0.0	0.
1278	6795300	2122250	4993.784		0.0	0.
1277	6795300	2122300		4993.772	0.0	0.
1276	6795300	2122350	4993.811	4993.801	0.0	0.
1255			4993.831	4993.830	0.0	0.
	6795350	2122350	4995.101	4995.093	0.0	0.
1256	6795350	2122300	4995.061	4995.064	0.0	0.
1257	6795350	2122250	4995.037	4995.035	0.0	0.
1258	6795350	2122200	4995.025	4995.007	0.0	0,
1259	6795350	2122150	4994.985	4994.978	0.0	0.
1238	6795400	2122150	4995.817	4995.811	0.0	0.
1237	6795400	2122200	4996.142	4996.120	0.0	0.:
1236	6795400	2122250	4996.315	4996.299	0.0	0,:
1235	6795400	2122300	4996.331	4996.328	0.0	0.0
1234	6795400	2122350	4996.390	4996.356	0.0	0.4
1215	6795450	2122300	4995.774	4995.770	0.0	0.0
1216	6795450	2122250	4995.497	4995.461	0.0	0.4
1217	6795450	2122200	4995.183	4995.151	0.0	. 0.4
1218	6795450	2122150	4994.855	4994.842	0.0	0.2
1198	6795500	2122150	4993.885	4993.873	0.0	0.2
1197	6795500	2122200	4994.220	4994.182	0.0	
1196	6795500	2122250	4994.495	4994.492	0.0	0.5
1195	6795500	2122300	4994.830	4994.801	0.0	0.0
1195	6795500	2122300	4994.799	4994.801	0.0	0.3
1175	6795550	2122300	4993.858	4993.832	0.0	0.0
1176	6795550	2122250	4993.533	4993.523		0.3
1177	6795550	2122200	4993.242		0.0	0.1
1178	6795550	2122150	4992.911	4993.213	0.0	0.3
1158	6795600	2122150		4992.904	0.0	0.1
1157			4991.961	4991.935	0.0	0.3
1156	6795600 6795600	2122200	4992.256	4992.244	0.0	0.1
		2122250	4992.554	4992.554	0.0	0.0
1155	6795600	2122300	4992.879	4992.863	0.0	0.2
1154	6795600	2122350	4993.174	4993.173	0.0	0.0
1134	6795650	2122350	4992.207	4992.204	0.0	0.0
1135	6795650	2122300	4991.911	4991.894	0.0	0.2
1136	6795650	2122250	4991.590	4991.585	0.0	0.1
1137	6795650	2122200	4991.306	4991.275	0.0	0.4
1138	6795650	2122150	4990.980	4990.966	0.0	0.2
1118	6795700	2122150	4990.002	4989.997	0.0	0.2
1117	6795700	2122200	4990.356	4990.307	0.0	0.6

EnergySolutions



Date:	8/9/2010	QC signature:D	ave Stewart 0	St R	eviewed by:Beachem	
1058	6795850	2122150	4987.112	4987.090	0.0	0.0
1057	6795850	2122200	4987.400	4987.400	0.0	0.0
1056	6795850	2122250	4987.714	4987.709	0.0	0.1
1055	6795850	2122300	4988.032	4988.018	0.0	0.2
1054	6795850		4988.330	4988:328	0.0	0.0
1074	6795800		4989.309	4989.297	0.0	0.1
1075	6795800		4988.995	4988.987	0.0	0.1
1076	6795800		4988.692	4988.678	0.0	0.2
1077	6795800		4988.380	4988.369	0.0	0.1
1078	6795800		4988.072	4988.059	0.0	0.3
1098			4989.049	4989.028	0.0	0.3
1097	6795750		4989.364	4989.338	0.0	0.3
1095	6795750		4989.692	4989.647	0.0	0.0
1095	6795750		4989.967	4989.956	0.0	0.
1094	6795750		4990.269	4990.266	0.0	0.0
1114			4991.237	4991.235	0.0	0.1
1115			4990.952	4990.925	0.0	0.
1116		m / mmer v	4990.652	4990.616	0.0	0.

Da: Nor 8-25-16

Energy Solutions

px 2 of 2



Interim Buy off ID:			UIA01100813-00		Date:	8/13/2010	
Point #	Northing			Design Elevation	Difference in feet	Difference in inches	
1036	6795900		4987.081	4987,049	0.0	0.	
1037	6795900	2122250	4986.766	4986.740	0.0	0.	
1038	6795900	2122200	4986.457	4986.431	0.0		
1039	6795900	2122150	4986.153	4986.121	0.0		
					0.0		
				(50 ====5)	0.0		

HOT 8-25-10

EnergySolutions

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	Northing 6795660.1 6795667.9 6795667.9 6795707.6 6795792.8 6795792.8 6795792.8 6795872.7 6795872.7 6795884.0 6795983.4 6795983.7 6795990.4 6795990.4 6795990.4 6795990.5 6795945.1	Buy off ID: Easting 2122367 2122418 2122502 2122613 2122619 2122619 2122440 2122356 2122472 2122674 2122674 2122674 2122663	Surveyed Elevation 4992.1 4992.3 4992.5 4992.8 4991.2 4990.6 4989.9 4989.0 4988.0 4988.1 4988.1	4992 542 4992 822 4991 205 4990 608 4989 961 4989 262 4988 046 4988 652	Difference in feet 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.1 0.0 0.0	Difference in inches 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
2 3 4 5 6 7 8 9 10 11 12 13 14	6795667.9 6795685.3 6795707.6 6795792.8 6795792.8 6795796.8 6795806.5 6795872.7 6795878.5 6795884.8 6795890.4 6795983.7 6795968.7	2122418 2122502 2122613 2122620 2122619 2122619 2122440 2122356 2122360 2122472 2122674 2122674 2122669	4992.3 4992.5 4992.8 4991.2 4990.6 4989.9 4988.0 4988.0 4988.6	4992 346 4992 542 4992 822 4991 205 4990 608 4980 961 4982 626 4988 652	0.0 0.0 0.0 0.1 0.0 0.0 0.0	0 0 0 0 0 0
3 4 5 6 7 8 9 10 11 12 13 14	6795685.3 6795707.6 6795792.5 6795792.8 6795796.8 6795806.5 6795872.7 6795878.5 6795884.8 6795890.4 6795983.7 6795983.7	2122502 2122613 2122620 2122519 2122440 2122350 2122472 2122571 2122674 2122669	4992.5 4992.8 4991.2 4990.6 4989.9 4988.0 4988.6 4988.6	4992 542 4992 822 4991 205 4990 608 4989 961 4989 262 4988 046 4988 652	0.0 0.0 0.0 0.1 0.0 0.0 0.0	0 0 0 0 0
4 5 6 7 8 9 10 11 12 13 14	6795707.6 6795792.5 6795792.8 6795796.8 6795796.8 6795806.5 6795872.7 6795878.5 6795884.8 6795890.4 6795980.4 6795997.5 6795970.5	2122613 2122620 2122519 2122440 2122356 2122360 2122472 2122571 2122674 2122669	4992.8 4991.2 4990.6 4989.9 4989.2 4988.6 4988.6	4992.822 4991.205 4990.608 4989.961 4989.262 4988.046 4988.652	0.0 0.0 0.1 0.0 0.0 0.0	0 0 0 0
6 7 8 9 10 11 12 13 14	6795792.8 6795796.8 6795806.5 6795872.7 6795878.5 6795884.8 6795890.4 6795990.5 6795970.5	2122519 2122440 2122356 2122360 2122472 2122571 2122674 2122669	4990.6 4989.9 4989.2 4988.0 4988.6 4989.1	4990 608 4989 961 4989 262 4988 046 4988 652	0.1 0.0 0.0 0.0	0 0 0
7 8 9 10 11 12 13 14	6795796.8 6795806.5 6795872.7 6795878.5 6795884.8 6795890.4 6795983.7 6795970.5 6795956.7	2122440 2122356 2122360 2122472 2122571 2122674 2122669	4989.9 4989.2 4988.0 4988.6 4989.1	4989.961 4989.262 4988.046 4988.652	0.0 0.0 0.0	0
8 9 10 11 12 13 14	6795806.5 6795872.7 6795878.5 6795884.8 6795890.4 6795983.7 6795970.5 6795956.7	2122356 2122360 2122472 2122571 2122674 2122669	4989.2 4988.0 4988.6 4989.1	4989.262 4988.046 4988.652	0.0	. 0
9 10 11 12 13 14 15	6795872.7 6795878.5 6795884.8 6795890.4 6795983.7 6795970.5 6795956.7	2122360 2122472 2122571 2122674 2122669	4988.6 4989.1	4988.046 4988.652	0.0	
10 11 12 13 14 15	6795878.5 6795884.8 6795890.4 6795983.7 6795970.5 6795956.7	2122472 2122571 2122674 2122669	4988.6 4989.1	4988.652		
11 12 13 14 15	6795884.8 6795890.4 6795983.7 6795970.5 6795956.7	2122571 2122674 2122669	4989.1		0.0	0
13 14 15	6795890.4 6795983.7 6795970.5 6795956.7	2122674 2122669		4989.114	0.0	0
14 15	6795970.5 6795956.7		4909.0	4989.584	0.0	0
15	6795956.7	2122563	4987.8	4987.827	0.1	0
			4987.4	4987.405	0.0	0
16	0795945.1	2122456 2122361	4987.0	4986.980	0.0	0
		2122361	4986.6	4986.639	0.0	
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nments: N	orth West	Corner: 6795	996 N. 2122325 E.		0.0	0
	roval Date:	aviolesci sas	The Participant	Total Square Feet:		

U.S. Department of Energy Revision 0 December 2012

EnergySolutions





CRJ 001027



Interim Cover Buyoff Form

Client: Department of Energy Project: Moab UMTRA Project

Date: 08-11-2011

In signing this document, the signatory agrees that the lift is complete and meets both the project specifications and RAIP requirements.

Lift Area	Lift Area
UIM18	

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I when house	00-11-2011
But Anh -	08-11-2011
MITTH HOLAN FOR BOWNEN BOTH	08-11-2011
adonterou / mw6.	08-11-2011

OP-F-011 Rev 0, August 2010

File Index No. 43-1-1 Page 1 of 1 G. 21-111 488 1.1

Moab UMTRA Crescent Junction Disposal Cell Interim Cover Survey Measured by Jason Knowlton Checked by Kevin Keele July Johansen & Tuttle Engineering, Inc August 10, 2011

Point #	Northing	Easting	Design Elevation	Measured Elevation	Difference (feet)	Difference (inches)
201	6795006.2	2122702.0	4986.61	4986.62	0.01	0.1
202	6795012.5	2122751.6	4986.79	4986.80	0.01	0.1
203	6795018.7	2122801.2	4986.98	4986.99	0.01	0.1
204	6794981.6	2122906.7	4986.10	4986.13	0.03	0.4
205	6794975.3	2122857.1	4985.92	4985.93	0.01	0.1
206	6794969.1	2122807.4	4985.73	4985.74	0.01	0.1
207	6794962.8	2122757.8	4985.54	4985.55	0.01	0.1
208	6794956.6		4985.36	4985.40	0.05	0.5
209	6794907.0	2122714.5	4984.11	4984.15	0.04	0.5
210	6794913.2	2122764.1	4984.29	4984.32	0.03	0.3
211	6794919.5	2122813.7	4984.48	4984.49	0.01	0.1
212	6794925.7	2122863.3	4984.67	4984.70	0.03	0.4
213	6794931.9	2122912.9	4984.85	4984.86	0.01	0.1
214	6794882.3	2122919.1	4983.60	4983.63	0.03	0.4
215	6794876.1	2122869.5	4983.42	4983.43	0.01	0.2
216	6794869.9	2122819.9	4983.23	4983.27	0.04	0.4
217	6794863.6	2122770.3	4983.04	4983.07	0.02	0.3
218	6794857.4	2122720.7	4982.86	4982.87	0.01	0.1
219	6794807.8	2122726.9	4981.61	4981.61	0.00	0.0
220	6794814.0	2122776.5	4981.79	4981.82	0.02	0.3
221	6794820.3	2122826.2	4981.98	4981.98	0.00	0.0
222	6794826.5	2122875.8	4982.17	4982.18	0.01	0.1
223	6794832.7	2122925.4	4982.35	4982.35	0.00	0.0
224	6794783.1	2122931.6	4981.10	4981.10	0.00	0.0
225	6794776.9	2122882.0	4980.92	4980.92	0.00	0.0
226	6794770.6	2122832.4	4980.73	4980.77	0.04	0.4
227	6794764.4	2122782.8	4980.54	4980.58	0.03	0.4
228	6794758.2	2122733.2	4980.36	4980.37	0.02	0.2
229	6794708.6	2122739.4	4979.11	4979.15	0.04	0.5
230	6794714.8	2122789.0	4979.29	4979.31	0.02	0.2
231	6794721.0	2122838.6	4979.48	4979.48	0.00	0.0
232	6794727.3	2122888.2	4979.67	4979.71	0.04	0.5
233	6794733.5	2122937.8	4979.85	4979.85	0.00	0.0
234	6794683.9	2122944.1	4978.60	4978.63	0.02	0.3
235	6794677.7	2122894.5	4978.42	4978.43	0.01	0.1
236	6794671.4	2122844.9	4978.23	4978.26	0.03	0.4
237	6794665.2	2122795.3	4978.04	4978.05	0.00	0.0
238	6794658.9	2122745.6	4977.86	4977.90	0.04	0.5
239	6794609.3	2122751.9	4976.61	4976.62	0.02	0.2
240	6794615.6	2122801.5	4976.79	4976.81	0.02	0.2
241	6794621.8	2122851.1	4976.98	4977.00	0.02	0.3
242	6794628.1	2122900.7	4977.17	4977.18	0.01	0.1
243	6794578.4	2122907.0	4975.92	4975.96	0.04	0.5
244	6794572.2	2122857.3	4975.73	4975.76	0.03	0.4
245	6794566.0	2122807.7	4975.54	4975.56	0.01	0.1
246	6794559.7	2122758.1	4975.38	4975.38	0.02	0.2
247	6794553.5	2122708.5	4975.17	4975.21	0.03	0.4

248	6704E02 0	2122714.8	4070.00			
249		2122714.6	4973.92	4973.97	0.05	0.6
251			4974.11	4974.14	0.03	0.4
252	6794522.6	2122814.0	4974.29	4974.32	0.02	0.3
			4974.48	4974.49	0.01	0.1
253	6794528.8		4974.67	4974.68	0.01	0.1
254	6794479.2		4973.42	4973.42	0.00	0.0
255	6794473.0		4973.23	4973.25	0.02	0.3
256	6794466.7		4973.04	4973.06	0.02	0.2
257	6794460.5		4972.86	4972.88	0.02	0.2
258	6794454.3		4972.67	4972.71	0.04	0.4
259	6794404.7		4971.42	4971.42	0.00	0.0
260		2122776.8	4971.61	4971.64	0.03	0.3
261	6794417.1	2122826.4	4971.79	4971.80	0.01	0.1
262	6794423.4		4971.98	4972.01	0.03	0.4
263	6794429.6		4972.17	4972.18	0.02	0.2
264		2122931.9	4970.92	4970.95	0.04	0.5
265	6794373.8		4970.73	4970.75	0.02	0.2
266	6794367.5		4970.54	4970.59	0.05	0.6
267	6794361.3		4970.36	4970.40	0.04	0.5
268		2122733.5	4970.17	4970.21	0.04	0.5
269	6794305.4		4968.92	4968.95	0.03	0.3
270		2122789.3	4969.11	4969.13	0.02	0.3
271	6794317.9		4969.29	4969.32	0.03	0.4
272		2122888.5	4969.48	4969.52	0.04	0.5
273	6794330.4	2122938.1	4969.67	4969.71	0.04	0.5
274	6794280.8	2122944.4	4968.42	4968.46	0.05	0.6
275	6794274.5	2122894.8	4968.23	4968.25	0.02	0.3
276	6794268.3	2122845.2	4968.04	4968.08	0.04	0.5
277	6794262.1	2122795.6	4967.86	4967.88	0.02	0.3
278	6794255.8	2122745.9	4967.67	4967.68	0.01	0.1
279	6794206.2	2122752.2	4966.42	4966.46	0.04	0.5
280	6794212.5	2122801.8	4966.61	4966.65	0.04	0.5
281	6794218.7	2122851.4	4966.79	4966.84	0.05	0.6
282	6794224.9	2122901.0	4966.98	4966.99	0.01	0.1
283	6794231.2	2122950.6	4967.17	4967.18	0.01	0.2
284	6794191.5	2122955.6	4966.17	4966.19	0.02	0.3
285	6794185.3	2122906.0	4965.98	4966.02	0.04	0.5
286	6794179.0	2122856.4	4965.79	4965.82	0.02	0.3
287	6794172.8	2122806.8	4965.61	4965.65	0.04	0.5
288	6794166.5	2122757.2	4965.42	4965.44	0.02	0.2



Interim Cover Buyoff Form



Client: Department of Energy Project: Moab UMTRA Project

Date: 09-27-2011

In signing this document, the signatory agrees that the lift is complete and meets both the project specifications and RAIP requirements.

Lift Area		
23		
•		

Approver Name/Title	Signature	Sign Date
Brent Anderson - Construction Manager	R. FAM	09-27-2011
Beachem Bosh - QA/QC Representative	What was	09-27-2011
Adam Lucero - Nielson Construction	alan kun	09-27-2011
Kevin Keele - J&T QC Representative	Their Keole	09-27-2011
Comments		
Surface was visually inspected and found to be		
satisfactory. See attached map for area location		
satisfactory. See attached map for orea location and square footage. ** 9-27-11		
•		

OP-F-011 Rev 0. August 2010





Moab UMTRA Crescent Junction Disposal Cell Interim Cover Survey Measured by Jason Knowlton Checked by Kevin Keele July Johansen & Tuttle Engineering, Inc Sep. 27, 2011

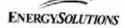


Point#	Northing	Easting	Design Elevation	Measured Elevation	Difference (feet)	Difference (inches)
295	6794789.36	2122981.22	4981.29	4981.33	0.05	0.6
296	6794795.60	2123030.83	4981.48	4981.49	0.01	0.1
297	6794801.83	2123080.44	4981.66	4981.67	0.01	0.1
298	6794758.46	2123136.29	4980.60	4980.60	0.00	0.0
299	6794752.22	2123086.68	4980.41	4980.44	0.02	0.3
300	6794745.99	2123037.07	4980.23	4980.25	0.03	0.3
301	6794739.75	2122987.46	4980.04	4980.07	0.03	0.3
302	6794690.14	2122993.70	4978.79	4978.82	0.03	0.3
303	6794696.38	2123043.31	4978.98	4979.01	0.03	0.4
304	6794702.61	2123092.92	4979.16	4979.19	0.03	0.3
305	6794708.85	2123142.53	4979.35	4979.37	0.02	0.3
306	6794659.24	2123148.76	4978.10	4978.12	0.02	0.2
307	6794653.01	2123099.15	4977.91	4977.92	0.01	0.1
308	6794646.77	2123049.55	4977.73	4977.74	0.01	0.2
309	6794640.53	2122999.94	4977.54	4977.56	0.02	0.3
310	6794634.29	2122950.33	4977.35	4977.36	0.01	0.1
311	6794584.68	2122956.56	4976.10	4976.14	0.03	0.4
312	6794590.92	2123006.17	4976.29	4976.31	0.03	0.3
313	6794597.16	2123055.78	4976.47	4976.48	0.00	0.0
314	6794603.40	2123105.39	4976.66	4976.66	0.00	0.0
315	6794609.63	2123155.00	4976.85	4976.85	0.00	0.0
316	6794560.02	2123161.24	4975.60	4975.61	0.01	0.1
317	6794553.79	2123111.63	4975.41	4975.43	0.02	0.3
318	6794547.55	2123062.02	4975.23	4975.24	0.01	0.2
319	6794541.31	2123012.41	4975.04	4975.06	0.02	0.3
320	6794535.07	2122962.80	4974.85	4974.88	0.02	0.3
321	6794485.46	2122969.04	4973.60	4973.61	0.01	0.1
322	6794491.70	2123018.65	4973.79	4973.81	0.02	0.2
323	6794497.94	2123068.26	4973.98	4973.99	0.01	0.1
324	6794504.18	2123117.87	4974.16	4974.19	0.03	0.3
325	6794510.42	2123167.48	4974.35	4974.39	0.04	0.5
326	6794460.81	2123173.72	4973.10	4973.12	0.02	0.2
327	6794454.57	2123124.11	4972.91	4972.92	0.01	0.1
328	6794448.33	2123074.50	4972.73	4972.73	0.00	0.0
329	6794442.09	2123024.89	4972.54	4972.58	0.04	0.5
330	6794435.85	2122975.28	4972.35	4972.38	0.02	0.3
331	6794386.24	2122981.52	4971.10	4971.11	0.01	0.1
332	6794392.48	2123031.13	4971.29	4971.31	0.02	0.3
333	6794398.72	2123080.74	4971.47	4971.51	0.03	0.4
334	6794404.96	2123130.34	4971.66	4971.68	0.02	0.2
335	6794411.20	2123179.95	4971.85	4971.85	0.00	0.0
336	6794361.59	2123186.19	4970.60	4970.60	0.00	0.0



337	6794355.35	2123136.58	4970.41	4970.42	0.01	0.1
338	6794349.11	2123086.97	4970.23	4970.23	0.00	0.0
339	6794342.87	2123037.36	4970.04	4970.04	0.00	0.0
340	6794336.64	2122987.75	4969.85	4969.88	0.02	0.3
341	6794287.03	2122993.99	4968.60	4968.61	0.01	0.1
342	6794293.26	2123043.60	4968.79	4968.80	0.01	0.1
343	6794299.50	2123093.21	4968.98	4969.00	0.03	0.3
344	6794305.74	2123142.82	4969.16	4969.19	0.03	0.3
345	6794311.98	2123192.43	4969.35	4969.38	0.03	0.4
346	6794262.37	2123198.67	4968.10	4968.12	0.02	0.3
347	6794256.13	2123149.06	4967.91	4967.92	0.00	0.0
348	6794249.89	2123099.45	4967.73	4967.75	0.03	0.3
349	6794243.65	2123049.84	4967.54	4967.54	0.00	0.0
350	6794237.42	2123000.23	4967.35	4967.39	0.04	0.5
351	6794197.73	2123005.22	4966.35	4966.37	0.01	0.2
352	6794203.97	2123054.83	4966.54	4966.55	0.02	0.2
353	6794210.20	2123104.44	4966.72	4966.74	0.01	0.2
354	6794216.44	2123154.05	4966.91	4966.91	0.00	0.0
355	6794222.68	2123203.66	4967.10	4967.11	0.02	0.2

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Interim Cover Buyoff Form

CRJ 000983

Client: Department of Energy Project: Moab UMTRA Project

Date: 10-19-2011

In signing this document, the signatory agrees that the lift is complete and meets both the project specifications and RAIP requirements.

Lift Area	1 if A		
UIQ18	Lift Area		

Approver Name/Title	Signature	Sign Date
Kevin Keele/ J&T Eng. QC Representative	Thuin Keele	10 - 18 - 11
Mitch Hogan/ ENERGYSOLUTIONS QA/QC Representative	· · ·	
Brent Anderson/ ENERGY SOLUTIONS Construction Manager	R+11	10.19.2011
Mark Greenhalgh/ Nielsons Construction Manager	mul Indias	10/18/11
Comments		1//
Lift area is approximately 42, 799 ft ²		
Surface was visually inspected and found to be satisfactory. See attached map for sea location. XX 10-18-11		

OP-F-011 Rev 0, August 2010 File Index No. 45-17
Page 1 of 1

Moab UMTRA Crescent Junction Disposal Cell Interim Cover Survey: UIQ18 Measured by Jason Knowlton Checked by Kevin Keele Junio Johansen & Tuttle Engineering, Inc Oct. 17, 2011

Point#	Northing	Easting	Design Elevation	Measured Elevation	Difference (feet)	Difference (inches)
361	6794987.8	2122956.3	4986.29	4986.29	0.00	0.0
362	6794994.0	2123005.9	4986.48	4986.48	0.00	0.0
363	6795000.3	2123055.5	4986.66	4986.68	0.02	0.3
364	6794956.9	2123111.3	4985.60	4985.62	0.02	0.2
365	6794950.7	2123061.7	4985.41	4985.42	0.01	0.1
366	6794944.4	2123012.1	4985.23	4985.25	0.02	0.3
367	6794938.2	2122962.5	4985.04	4985.09	0.05	0.6
368	6794888.6	2122968.7	4983.79	4983.82	0.03	0.3
369	6794894.8	2123018.4	4983.97	4984.02	0.04	0.5
370	6794901.1	2123068.0	4984.16	4984.18	0.02	0.3
371	6794907.3	2123117.6	4984.35	4984.37	0.03	0.3
372	6794857.7	2123123.8	4983.10	4983.12	0.02	0.3
373	6794851.4	2123074.2	4982.91	4982.92	0.01	0.2
374	6794845.2	2123024.6	4982.73	4982.76	0.03	0.4
375	6794839.0	2122975.0	4982.54	4982.56	0.02	0.2
376	6794808.1	2123130.0	4981.85	4981.86	0.01	0.1





Interim Cover Buyoff Form

Client: Department of Energy Project: Moab UMTRA Project

Date: 12-2-2011

In signing this document, the signatory agrees that the lift is complete and meets both the project specifications and RAIP requirements.

Lift Area	Lift Area
UIM10	Lift Area

Approver Name/Title	Signature	, Sign Date
Brent Anderson – EnergySolutions Construction Manager	B. + 11.	12-2-11
Mark Greenhalgh – Nielson Construction Manager	much Dr. h	12-2-11
Beachem Bosh - E.S. QA/QC Representative	The state of the s	12-2-11
Kevin Keele – J&T QC Representative	Their Theele	12-2-11
Comments		
Surface was inspected and found to be satisfactory. See attached map for area location and square footage.		
		1/10/10/10

OP-F-011 Rev 0, August 2010



QA Lavew: bracken book

Moab UMTRA Crescent Junction Disposal Cell Interim Cover Survey

Measured by Jason Knowlton Thin Kelle for JK 12-2-11 Checked by Kevin Keele Thin Theele Johansen & Tuttle Engineering, Inc Dec. 1, 2011

Point#	Northing	Easting	Design Elevation	Measured Elevation	Difference (feet)	Difference (inches)
383	6795409.33	2122701.69	4996.79	4996.94	0.14	1.7
384	6795415.57	2122751.30	4996.98	4997.11	0.13	1.5
385	6795359.72	2122707.93	4995.54	4995.63	0.09	1.1
386	6795365.96	2122757.54	4995.73	4995.73	0.00	0.0
387	6795372.19	2122807.15	4995.92	4995.95	0.03	0.3
388	6795378.43	2122856.76	4996.10	4996.15	0.04	0.5
389	6795384.67	2122906.37	4996.29	4996.38	0.09	1.1
390	6795390.91	2122955.98	4996.47	4996.53	0.06	0.7
391	6795397.15	2123005.58	4996.66	4996.73	0.07	0.9
392	6795347.54	2123011.82	4995.41	4995.45	0.03	0.4
393	6795341.30	2122962.21	4995.22	4995.28	0.06	0.7
394	6795335.06	2122912.60	4995.04	4995.05	0.01	0.1
395	6795328.82	2122862.99	4994.85	4994.88	0.02	0.3
396	6795322.58	2122813.39	4994.67	4994.70	0.03	0.4
397	6795316.35	2122763.78	4994.48	4994.56	0.08	0.9
398	6795310.11	2122714.17	4994.29	4994.39	0.10	1.2
399	6795260.50	2122720.40	4993.04	4993.08	0.03	0.4
400	6795266.74	2122770.01	4993.23	4993.25	0.02	0.3
401	6795272.97	2122819.62	4993.42	4993.45	0.03	0.4
402	6795279.21	2122869.23	4993.60	4993.65	0.04	0.5
403	6795285.45	2122918.84	4993.79	4993.86	0.07	0.8
404	6795291.69	2122968.45	4993.98	4994.02	0.05	0.6
405	6795297.93	2123018.06	4994.16	4994.24	0.07	0.9
406	6795248.32	2123024.30	4992.91	4992.97	0.06	0.7
407	6795242.08	2122974.69	4992.73	4992.79	0.06	0.7
408	6795235.84	2122925.08	4992.54	4992.58	0.04	0.5
409	6795229.60	2122875.47	4992.35	4992.36	0.00	0.0
410	6795223.37	2122825.86	4992.17	4992.21	0.04	0.5
411	6795217.13	2122776.25	4991.98	4992.00	0.02	0.3
412	6795210.89	2122726.64	4991,79	4991.83	0.03	0.4
413	6795161.28	2122732.88	4990.54	4990.57	0.02	0.3
414	6795167.52	2122782.49	4990.73	4990.78	0.05	0.6
415	6795173.76	2122832.10	4990.92	4990.94	0.03	0.3
416	6795179.99	2122881.71	4991.10	4991.12	0.02	0.2
417	6795186.23	2122931.32	4991.29	4991.29	0.01	0.1
418	6795192.47	2122980.93	4991.48	4991.55	0.08	0.9
419	6795198.71	2123030.54	4991.66	4991.66	0.00	0.0
420	6795149.10	2123036.77	4990.41	4990.48	0.06	0.8
421	6795142.86	2122987.17	4990.23	4990.24	0.02	0.2
422	6795136.62	2122937.56	4990.04	4990.05	0.01	0.1
423	6795130.38	2122887.95	4989.85	4989.88	0.03	0.3
424	6795124.15	2122838.34	4989.67	4989.73	0.06	0.7

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425	6795117.91	2122788.73	4989.48	4989.51	0.03	0.3
426	6795111.67	2122739.12	4989.29	4989.36	0.07	0.8
427	6795062.06	2122745.36	4988.04	4988.08	0.04	0.5
428	6795068.30	2122794.97	4988.23	4988.27	0.04	0.5
429	6795074.54	2122844.58	4988.42	4988.49	0.07	0.9
430	6795024.93	2122850.81	4987.17	4987.21	0.04	0.5
431	6795031.17	2122900.42	4987.35	4987.45	0.09	1.1
432	6795080.78	2122894.18	4988.60	4988.64	0.03	0.4
433	6795087.01	2122943.79	4988.79	4988.82	0.04	0.4
434	6795037.40	2122950.03	4987.54	4987.55	0.01	0.1
435	6795043.64	2122999.64	4987.72	4987.77	0.04	0.5
436	6795093.25	2122993.40	4988.97	4989.04	0.07	0.8
437	6795099.49	2123043.01	4989.16	4989.28	0.12	1.4
438	6795049.88	2123049.25	4987.91	4987.97	0.06	0.8

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	rea Buyof		UIM01		Date:	3/16/2012
		Easting	Surveyed Elevation	Design Elevation	Difference in feet	Difference in Inches
8723	6796025	2122977	4988.8	4988.8	0.0	0.:
8685	6796019 6796013	2122927		4988.6 4988.4	0.0	0,6
8609	67960013	2122828		4988.3	0.0	0.1
8610	6795980	2122831	4988.9	4988.8	0.1	1.3
8648	6795986	2122881	4989.1	4989.0	0.1	1.2
8686	6795992	2122931	4989.2	4989.2	0.0	0.3
8724	6795999	2122980		4969.4	0.0	0.3
8725 8687	6795949 6795943	2122987 2122937	4990.4 4990.2	4990.4 4990.2	0.1	0.6
8649	6795937	2122887	4990.0	4990.0	0.0	0.4
8611	6795930	2122838	4989.9	4989.8	0.1	3.0
0612	6795881	2122844	4990.9	4990.8	0.1	0.0
8650	6795887	2122894	4991.0	4991.0	0.0	0.2
688	6795893	2122943	4991.2	4991.2	0.1	9.0
3726 3727	6795899 6795850	2122993 2122999	4991.4 4992.4	4991.4 4992.4	0.1	3.0
6889	6795844	2122949	4992.2	4992.2	0.0	0.2
8651	6795837	2122900	4992.1	4992.0	0.1	1.1
3613	6795831	2122850	4991.8	4991.8	0.0	0,3
1614	6795782	2122857	4992.8	4992.8	0.0	0.2
652	6795788	2122906	4993.1 4993.2	4993.0 4993.2	0.1	1.1
690 691	6795794 6795744	2122956 2122962	4993.2	4993.2	0.0	0.1
653	6795738	2122912	4994.0	4994.0	0.0	0.3
615	6795732	2122863	4993.8	4993.8	0.0	0.1
616	6795682	2122869	4994.9	4994.8	0.1	0.8
654	6795689	2122919	4995.1	4995.0	0.1	1.0
692	6795895	2122968 2122974	4995.2 4996.3	4995.2 4996.2	0.0	0.5 1.2
693 655	6795645 6795639	2122974	4996.3 4996.0	4996.2	0.1	0.6
817	6795633	2122875	4995.8	4995.8	0.0	0.1
579	6795627	2122825	4995.6	4995.6	0.0	0.0
580	6795577	2122832	4996.7	4996.6	0.1	0.7
618	6795583	2122881	4996.8	4998.8	0.0	0.4
894	6795589 6795596	2122931 2122981	4997.1 4997.2	4997.0 4997.2	0.1	1.2
695	6795546	2122987	4998.2	4998.2	0.0	0.5
657	6795540	2122937	4996.0	4998.0	0.0	0.5
619	6795534	2122888	4997.8	4997.8	0.0	0.3
581	6795527	2122838	4997.7	4997.6	0.1	1.3
582	6795478	2122844	4998.6	4998.6	0.0	0.1
620 658	6795484 6795490	2122894 2122944	4998.8 4999.0	4998.8 4999.0	0.0	0.3
696	6795496	2122993	4999.2	4999.2	0.0	0.1
897	6795447	2122999	4997.9	4997.9	0.0	0.2
659	6795441	2122950	4997.7	4997.7	0.0	0.2
621	6795434	2122900	4997.6	4997.5	0.0	0.3
583 584	6795428	2122850	4997.4 4996.2	4997.4	0.0	0.2
622	6795378 6795385	2122857 2122906	4996.4	4996.1 - 4996.3	0.1	1.3
660	6795391	2122956	4996.5	4996.5	0.1	0.8
698	6795397	2123006	4996.7	4996.7	0.0	0.0
470	6795360	2122708	4995.6	4995.5	0.1	0.0
508	6795366	2122758	4995.8	4995.7	0.1	1.3
546	6795372	2122807	4996.0	4995.9	0.0	0.4
545 507	6795422 6795416	2122801 2122751	4997.2 4997.0	4997.2 4997.0	0.0	0.0
469	6795409	2122702	4998.9	4996.8	0.0	1.0
468	6795459	2122695	4998.1	4998.0	0.0	0.3
506	6795485	2122745	4998.2	4998.2	0.0	0.1
544	6795471	2122795	4998,4	4998.4	0.0	0.1
543	6795521	2122788	4997.5	4997.4	0.0	0.5 0.3

EnergySolutions

Approval Date: 3/16/2012 Total Square Feet: 229,596 orth West Corner: 6798089 N 2122774 E						
omments: QC performed a visual inspection of the final surface with satisfactory results. Visual inspection notes: The area was free of humping, thickened edges and defects. The layer uniform thickness was satisfactory see above survey results for layer thickness.						
					0.0	0.0
					0.0	0.0
					0.0	0.0
					0.0	0.0
					0.0	0.0
		3500250			0.0	0.0
					0.0	0.0
					0.0	0.0
					0.0	0.0
					0.0	0.4
					0.0	0.0
					0.0	0.0
					0.0	0.0
8533	6795994	2122729	4988.0	4987.9	0.1	1.0
8571	6796001	2122778	4988.1	4988.1	0.1	0.8
8572	6795974	2122782	4988.6	4988.6	0.0	0.0
8534	6795968	2122732	4988.5	4988.4	0.1	1.3
8497	6795912	2122689	4989.3	4989.2	0.1	1.
8535	6795918	2122738	4989.5	4969.4	0.1	1.
8573	6795924	2122788	4989.6	4969.6	0.0	0.
8574	6795875	2122794	4990.7	4990.6	0.1	1.3
8536	6795868	2122745	4990.5	4990.4	0.1	0.
8498	6795862	2122695	4990.3	4990.2	0.1	0.
8499	6795812	2122701	4991.3	4991.2	0.0	0.
8537	6795819	2122751	4991.5	4991.4	0.1	0.
8575	6795825	2122801	4991.6	4991.6	0.0	0.
8576	6795709	2122807	4992.7	4992.6	0.1	0.
8538	6795769	2122757	4992.4	4992.4	0.0	0.
8501 8500	6795713 6795763	2122714	4993.3	4992.2	0.1	1/2
8539	6795720	2122704	4993.5	4993.2	0.1	1.3
8577	6795726	2122813 2122764	4993.7 4993.5	4993.6 4993.4	0.1	1/
8578	6795676			4994.6	0.1	0.
8540	6795670	2122770	4994.5 4994.7	THE RESERVE THE PARTY OF THE PA	0.1	
8502	6795664	2122720		4994.4		1.3
8464	6795657	2122670	4994.2 4994.3	4994.1	0.1	1.
8465	6795608	2122677		4995.1	0.0	1.
	6795614		4995.3 4995.1	4995.2 4995.1	0.1	0.
8503		2122776	4995.3	4995.2	0.1	0.
8541	6795520	2122776	4995.4	4995.4	0.0	0.
8504 8542	6795564 6795571	2122733	4996.3 4996.5	4996.2	0.0	0.
8460	6795558	2122683	4996.1	4996.1 4996.2	0.0	0.
8467	8795509	2122689	4997.1	4997.1	0.1	0.

EnergySolutions

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A4. Radon Barrier

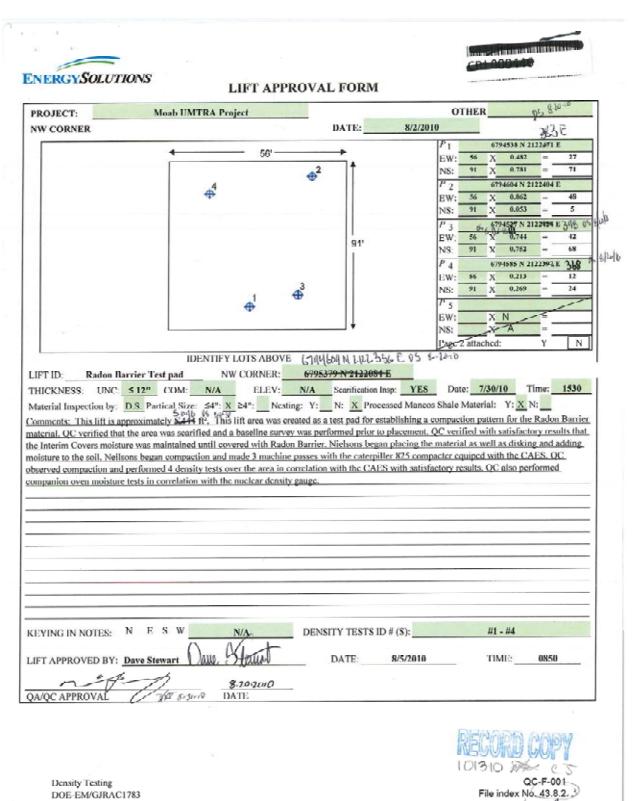
CAES Test Pad Lift Approval Package

Standard Proctor Test Results Summary

Lift Approval Summary

Lift Approval Package

U.S. Department of Energy	Moab UMTRA Project Crescent Junction Disposal Cell Interim Completion Report Addendum A
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U.S. Department of Energy Revision 0 December 2012

Rev. 0

DOE-EM/GJRAC1783



Slope Elevation Survey

	Average lift	thickness=	0.8	Bounding Box	Northing	Easting	
	Grid Size=	NA.	Mynn	Lower Left	N		
Lift ID:		rrier Test Pac		Upper Right		A	
	Lift Elevat			t Approval El		Lift Thickness	
Northing	Easting	Elevation	Northing	Easting	Elevation	Thickness	
			-	2122358	4976.4		_
6794582	2122358	4975.7	6794582	2122358		0.7	_
6794609	2122358	4976.4	6794609	2122356	4977.2 4975.0	0.7	_
6794527	2122361	4974.3	6794527	00 F 300 F 0 T			-
6794566	2122361	4975.3	6794566	2122361	4976.0	0.7	-
6794609	2122361	4976.5	6794609	2122361	4977.2	0.7	_
6794520	2122365	4974.1	6794520	2122365	4974.9	0.8	_
6794566	2122365	4975.3	6794566	2122365	4976.0	0.7	_
6794609	2122365	4976.5	6794609	2122365	4977.2	0.7	-
6794520	2122368	4974.2	6794520	2122368	4975.0	0.8	_
6794566	2122368	4975.4	6794566	2122368	4976.0	0.6	_
6794609	2122368	4976.5	6794609	2122368	4977.2	0.7	4
6794520	2122371	4974.2	6794520	2122371	4975.0	0.8	_
6794566	2122371	4975.3	6794566	2122371	4976.1	0.8	_
6794609	2122371	4976.5	6794609	2122371	4977.1	0.6	_
6794520	2122375	4974.1	6794520	2122375	4975.0	0.9	
6794566	2122375	4975.4	6794566	2122375	4976.0	0,7	
6794609	2122375	4976.5	6794609	2122375	4977.3	0.8	
6794520	2122378	4974.1	6794520	2122378	4974.9	0,8	
6794566	2122378	4975.3	6794566	2122378	4976.1	0.8	
6794609	2122378	4976.5	6794609	2122378	4977.2	0.7	П
6794523	2122381	4974.2	6794523	2122381	4975.1	0.9	\exists
6794566	2122381	4975.3	6794566	2122381	4976.2	1.0	\dashv
6794612	2122381	4976.6	6794612	2122381	4977.3	0.7	\dashv
6794523	2122384	4974.2	6794523	2122384	4975.2	1.0	\dashv
6794566	2122384	4975.2	6794566	2122384	4976.2	1.0	\dashv
6794612	2122384	4976.6	6794612	2122384	4977.4	0.8	\dashv
6794523	2122388	4974.2	6794523	2122388	4975.1	0.9	⊣
		4974.2	6794566	2122388	4976.2	1.0	\dashv
6794566	2122388		6794566	2122388	4977.4	0.8	\dashv
6794612	2122388	4976.6					\dashv
6794523	2122391	4974.2	6794523	2122391	4975.2	1.0	\dashv
6794566	2122391	4975.2	6794566	2122391	4976.2	1.0	\dashv
6794612	2122391	4976.6	6794612	2122391	4977.5	1.0	\dashv
6794523	2122394	4974.3	6794523	2122394	4975.2	0.9	4
6794566	2122394	4975.3	6794566	2122394	4976.2	0.9	-
6794612	2122394	4976.7	6794612	2122394	4977.5	0.8	_
6794523	2122398	4974.3	6794523	2122398	4975.2	0.9	\dashv
6794566	2122398	4975.3	6794566	2122398	4976.2	1.0	_
6794612	2122398	4976.8	6794612	2122398	4977.5	0.7	-
6794523	2122401	4974.3	6794523	2122401	4975.1	0.8	4
6794566	2122401	4975.3	6794566	2122401	4976.2	1.0	4
6794612	2122401	4976.7	6794612	2122401	4977.5	0.7	4
6794523	2122404	4974.3	6794523	2122404	4975.1	0.8	4
6794566	2122404	4975.4	6794566	2122404	4976.3	0,9	4
6794612	2122404	4976.7	6794612	2122404	4977.5	0.8	4
6794523	2122407	4974.3	6794523	2122407	4975.1	0.8	4
6794566	2122407	4975.4	6794566	2122407	4975.9	0.6	4
6794612	2122407	4976.7	6794612	2122407	4977.4	0.7	4
6794523	2122411	4974.3	6794523	2122411	4975.1	008	4
6794566	2122411	4975.3	6794566	2122411	4975.9	0.6	- 10

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6794523	2122414	4974.4	6794523	2122414	4975.1	0.7	
6794566	2122414	4975.3	6794566	2122414	4976.1	0.8	
6794602	2122414	4976.5	6794602	2122414	4977.3	0.8	
6794527	2122417	4974.4	6794527	2122417	4975.3	0.9	
6794566	2122417	4975.4	6794566	2122417	4975.9	0.6	
6794576	2122417	4975.7	6794576	2122417	4976.3	0.6	
6794527	2122420	4974.5	6794527	2122420	4975.4	1.0	
6794530	2122420	4974.6	6794530	2122420	4975.5	0.9	
6794563	2122420	4975.0	6794553	2122420	4975.6	0.6	
						0.0	
						0.0	
						0.0	
						0.0	
						0.0	
			1			0,0	
			1			0.0	
			1			0.0	
			13			0.0	
			- 220			0.0	
						0.0	
						0.0	
						0.0	
/						0.0	
						0.0	

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% =6	95.8%
Elevation Avg	4976.2
Total =6	485
Total Lines	506

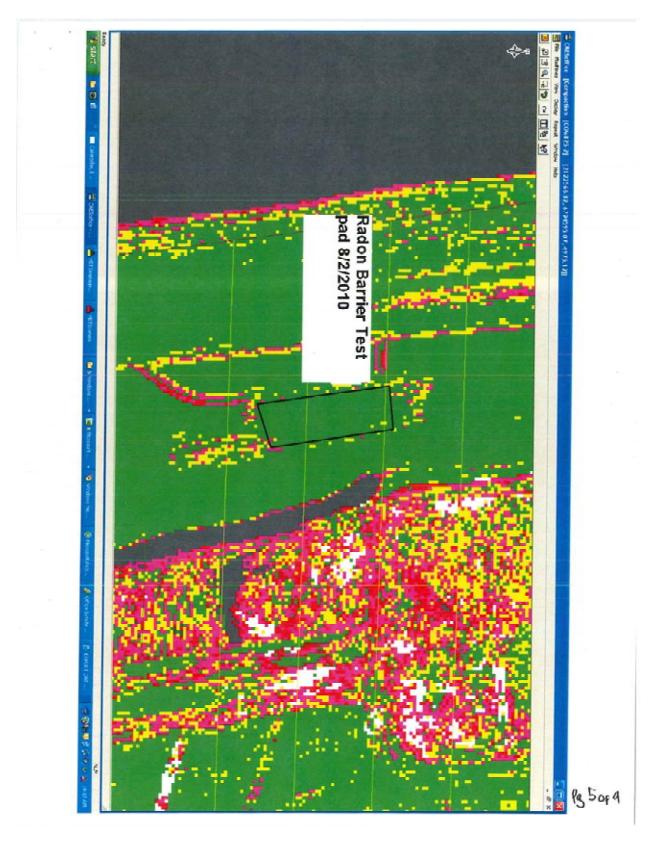
Pass

Minimum Number of Machine Passes

Lift ID:	Radon	Barrier	Test	pad	8/2/10	
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		est pad 8/2/10	Radon Barrier Te	Lift ID:		
	Count	Passes =6	# of Passes	Elevation	Easting	Northing
Lift Height	- 1		5	4976.7	2122358	6794582
1' 0"	1		5	4976.9	2122358	6794586
	1		5	4977.0	2122358	6794589
Thick Lift Threshold	1		5	4977.2	2122358	6794592
2' 0"	1		5	4977.3	2122358	6794595
	1		5	4977.5	2122358	6794599
Last Lift Elevation	1	1	6	4977.3	2122358	6794602
N/A	1	1	6	4977.4	2122358	6794605
	1	1	6	4977.5	2122358	6794609
Min. # of Wheel Passes	1	1	6	4974.8	2122361	6794527
6	1	1	6	4975.0	2122361	6794530
	1	1	6	4975.1	2122361	6794533
	1	1	6	4975.2	2122361	6794536
	1	1	6	4975.3	2122361	6794540
	1	1	6	4975.3	2122361	6794543
	1	1	6	4975.4	2122361	6794546
	1	1	6	4975.5	2122361	6794550
	1	1	6	4975.5	2122361	6794553
	1	i	6	4975.6	2122361	6794556
	1	i	6	4975.8	2122361	6794559
	1		5	4976.2	2122361	6794563
	1		5	4976.4	2122361	6794566
	1	1	6	4976.3	2122361	6794569
	1	1	6	4976.5	2122361	6794572
	1	1	6	4976.6	2122361	6794576
	1	1	6	4976.7	2122361	6794579
	1	1	6	4976.8	2122361	6794582
	1	- '	5	4976.9	2122361	6794586
	1	1	6	4977.1	2122361	6794589
	1	1	6	4977.2	2122361	6794592
	1	1	6			
	1	1	6	4977.3 4977.5	2122361	6794595 6794599
		1				
	1		4	4977.5	2122361	6794602
	1		3	4977.6	2122361	6794605
	1	1	6	4977.2	2122361	6794609
	1	1	6	4974.9	2122365	6794520
	1	1	6	4974.9	2122365	6794523
	1	1	6	4975.0	2122365	6794527
	1	1	6	4975.1	2122365	6794530
	1	1	6	4975.2	2122365	3794533
	1	1	6	4975.3	2122365	3794536
	1	1.	6	4975.4	2122365	3794540
	1		4	4975.8	2122365	3794543
	1	1	6	4975.8	2122365	3794546
	1	1	6	4975.9	2122365	3794550

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ENERGYSOLUTIONS	FIELD DENS	SITY TEST		
PROJECT: Moab UMTRA I	Project	ОТН	IER	
LIFT IDENTIFICATION: Rador	Barrier Test Pad 8/2/			
TEST ID NUMBER(S):	ALS MANO	1		
TEST LOCATION: 6794538 N	2122471 E	TEST METHOD:	D1556x	D6938
ASTM D6938 (DENSITY DETERM	(INATION)	ASTM D1556 (DI	ENSITY DETERM	INATION)
Make/Model Troxler 3430 Gauge Serie	al #31674	Testing Apparatus	Calibrated Vol. (I	bs/ft ³)
Last Calibration Date: 3/4/10		Bulk Density of sand (p	g/cm^3	USS/fi 3
Daily Standard Counts: Off-Cell Standard		Mass of Sand to Fill Co	ne & Plate (M ₂)	
Density 2495 Moisture	706	Mass of bottle & co	one before filling	
Method A (Direct Transmissio	n)	c	one, plate & hole	g
Depth Setting 8 (inches) Count Ti	me 1 (minutes)	Mass of bottle &		
Moisture Count 153 Density	Count 1576	Mass of	one, plate & hole sand to fill cone	g
			ate, & hole (M/1)	g
Wet Density (ρ _m) 126.1 (lbs/ft ³) Dry Dens	ity 114.1 (lbs/ft ³)		f sand to fill hole	g
		Mass of wet	soil No container	g
Moisture Density 12.0 (lbs/ft ³) Moisture	Fraction	N	Mass of Antainer	g
MOISTURE DETERMINATION		Mass	wet soil (M ₃)	g
ASTM D4643			est Hole Volume	
Container ID D-2		\/V=	$(M_1 - M_2)/\rho_1$	cm³
Mass of container & wet specimen			Dry Mass of soil	
(M _{cms})	400.8 g	$M_4 = 100$	M 3 / (w + 100)	g
Mass of container & dry specimen			Wet Denisty	3
(M_{cds}) Mass of water (M_w)	377.7 g	$\rho_m = 0$	M ₃ / V) x 62.43 Dry Denisty	lbs/ft
$M_{w} = M_{cms} - M_{cds}$	23.1 g		$\rho_d = M_4/V$	g/cm ³
W - CHS - Cus			Dry Unit Weight	8
Mass of container (Mc)	163.6 g		$y_d = p_d \times 62.43$	lbs/ft 3
Mass of dry specimen (M _s)			sh in color and cons	sists of mostly
$M_s = M_{cds} - M_c$	214.1 g	Soil Description:	fines.	
Moisture content (w) $w = (M_w / M_s) \times 100$			Radon Barri	
$w = (M_w / M_s) \times 100$	10.8	Standard F	Proctor (ASTM D698	5)
Dry Density $(\rho_{dj} = (100 \times \rho_m)/(100$	+ w)	Maximum Dry Dens	ity (γ _d max)118	8.4 (lbs/ft ³)
$\rho d = (100 \text{ x} 126.1)/(100 + 10.8) = $	113.8 lbs/ft ³	Optimum Moi	sture (w opt)13.	.2 (%)

Density Testing DOE-EM/GJRAC1783 Rev. 0

QA/QC APPROVAL

Comments:

Percent Compaction = ρ_d / $\gamma_d max x 100$

Microwave oven power setting on HIGH. Initial time setting of 3

a change of 0.1 % or less of the initial wet mass of the soil.

minutes and subsequent incremental drying periods of 1 minute until

113.8 / 118.4 x 100 =

QC-F-002 File Index No. 43.8.2 Page ____ of ____

to __16.2_ %

Date: 8/4/10

(%)

0845

95.0

Required Moisture: 10.2 %

TEST RESULTS:

Pass

Required Percent Compaction:

Failed Moisture

David Stewart
(print)

Failed Compaction

PROJECT: Monb UMTRA Project	OTHER
LIFT IDENTIFICATION: Radon Barrier Test F	ad 8/2/2010 DATE: 8/2/2010
TEST ID NUMBER(S):	2
TEST LOCATION: 6794604 N 2122404 E	TEST METHOD: D1556X D6938
ASTM D6938 (DENSITY DETERMINATION)	ASTM D1556 (DENSITY DETERMINATION)
Make/Model Troxler 3430 Gauge Serial # 31674	Testing Apparatus Calibrated Vol. (lbs/fr³)
Last Calibration Date: 3/4/10	Bulk Density of sand (ρ ₁) g/cm ³ g/s
Daily Standard Counts: Off-Cell Standard	Mass of Sand to Fill Cone & Plate (M ₂)
Density 2495 Moisture 706	Mass of bottle & cone before filling
Method A (Direct Transmission)	conc, plate & hole g
Depth Setting 8 (inches) Count Time 1 (minus	·
Moisture Count 152 Density Count 1602	Mass of sand to fill cone
	plate, & hole (M1)
Vet Density (p _m) 125.4 (lbs/ft ³) Dry Density 113.5 (l	
Moisture Density 11.9 (lbs/ft) Moisture Fraction 10.5	
	- Wassor-Container
IOISTURE DETERMINATION	Mass of wet soil (M ₃)
ASTM D4643	Test Hole Volume
Container ID D-3 Mass of container & wet specimen	$V = (M_1 - M_2)/p_1 \underline{\hspace{1cm}} cm^3$
(M _{cm}) 445.8	Bry Mass of soil $M_{+} = 100 M_{J} / (w + 100) $ g
Mass of container & dry specimen	Wet Denisty
(M eds) 419.2	$p_m = (M_s/V) \times 62.43$
Mass of water (M _w)	Dry Denisty
$M_{w} = M_{com} - M_{cds} $ 26.6	$p_d - M_d / V$ g/cm^3 Dry Unit Weight
Mass of container (M _c) 164.5	g $\gamma_d = \rho_d \times 62.43$ lbs/ft ³
Mass of dry specimen (M _s)	Yellowish in color and consists of mostly
$M_{\tau} = M_{cdr} - M_c \qquad 254.7$	g Soil Description: fines.
Moisture content (w) $w = (M_w / M_s) \times 100$ 10.4	Proctor ID: Radon Barrier #3 Standard Proctor (ASTM D698)
1917	,
Dry Density $(\rho_{a0} = (100 \times \rho_m)/(100 + w)$	Maximum Dry Density (γ₄max) 118.4 (lbs/ft)
$pd = (100 \times 125.4) / (100 + 10.4) = 113.5$ Ibs. Note: Wet Density from ASTM D 1556 (p.,) takes presidence over ASTM D 6938 (p.,	/ft ³ Optimum Moisture (w _{apt})13.2(%)
Note: Wet Density from ASTM D 1336 (g _m) takes presidence over ASTM D 6938 (g _m	Required Moisture: 10.2 % to 16.2 %
Percent Compaction = ρ _d / γ _d max x 100	
113.5 / 118.4 x 100 = 95.9 %	Required Percent Compaction: 95.0 (%)
omments:	TEST RESULTS:
icrowave oven power setting on HIGH. Initial time setting o nutes and subsequent incremental drying periods of 1 minut	A . and
change of 0.1 % or less of the initial wet mass of the soil.	Failed Moisture Failed Compaction Tide: 0900
	By: David Stewart /) Janua Livertan (signature)
242016	
QA/QC APPROVAL DATE	

TEST ID NUMBER(S): d $E^{-} = 2P^{C} \cdot P^{C} \cdot P^$	
TEST LOCATION: 679453 PN 2122424 E ASTM D6938 (DENSITY DETERMINATION) Make/Model Troatler 3430. Gauge Scrial # 31674 Last Calibration Date: 34/10 Density 2495	2/2010
TEST LOCATION: 679453 PN 2122424 E ASTM D6938 (DENSITY DETERMINATION) Make/Model Troatler 3430. Gauge Scrial # 31674 Last Calibration Date: 34/10 Density 2495	
ASTM D6938 (DENSITY DETERMINATION) Make/Model Troxler 3430. Gauge Serial # 31674 Last Calibration Date: $3/410$ Density 2495	x D6938
Last Calibration Date: $3/4/10$ Daily Standard Counts: $O(f) Coll Standard$ Density 2495 Molsture 706 Method A (Direct Transmission) Depth Setting 8 (Inches) Count Time 1 (Infinites) Moisture Count 154 Density Count 1334 et Density (p_m) 132.4 ($f(bs/f)^3$) Dry Density 120.4 ($f(bs/f)^3$) Mass of sand to fill conce, plate & hold Mass of sand to fill conce, plate & hold Mass of sand to fill conce, plate & hold Mass of sand to fill conce, plate & hold Mass of sand to fill conce, plate & hold Mass of sand to fill conce, plate & hold Mass of sand to fill conce, plate & hold Mass of sand to fill conce, plate & hold Mass of sand to fill conce, plate & hold Mass of sand to fill conce, plate & hold Mass of sand to fill conce, plate & hold Mass of sand to fill conce, plate & hold Mass of sand to fill conce, plate & hold Mass of sand to fill conce, plate & hold Mass of sand to fill conce and the filling conce, plate & hold Mass of sand to fill conce and the filling conce, plate & hold Mass of sand to fill conce and the filling conce, plate & hold Mass of sand to fill conce and the filling conce, plate & hold Mass of sand to fill conce and the filling conce, plate & hold Mass of sand to fill fold Mass of sand to fill	TERMINATION)
Last Calibration Date: $3/4/10$ Daily Standard Counts: $O(f) Coll Standard$ Density 2495 Molsture 706 Method A (Direct Transmission) Depth Setting 8 (Inches) Count Time 1 (Infinites) Moisture Count 154 Density Count 1334 et Density (p_m) 132.4 ($f(bs/f)^3$) Dry Density 120.4 ($f(bs/f)^3$) Mass of sand to fill conce, plate & hold Mass of sand to fill conce, plate & hold Mass of sand to fill conce, plate & hold Mass of sand to fill conce, plate & hold Mass of sand to fill conce, plate & hold Mass of sand to fill conce, plate & hold Mass of sand to fill conce, plate & hold Mass of sand to fill conce, plate & hold Mass of sand to fill conce, plate & hold Mass of sand to fill conce, plate & hold Mass of sand to fill conce, plate & hold Mass of sand to fill conce, plate & hold Mass of sand to fill conce, plate & hold Mass of sand to fill conce, plate & hold Mass of sand to fill conce and the filling conce, plate & hold Mass of sand to fill conce and the filling conce, plate & hold Mass of sand to fill conce and the filling conce, plate & hold Mass of sand to fill conce and the filling conce, plate & hold Mass of sand to fill conce and the filling conce, plate & hold Mass of sand to fill fold Mass of sand to fill	Vol. (lbs/ft3)
Density 2495 Moisture 706 Mass of bottle & cone before filling cone, plate & bot Mass of bottle & cone after filling cone, plate & bot Mass of bottle & cone after filling cone, plate & bot Mass of bottle & cone after filling cone, plate & bot Mass of bottle & cone after filling cone, plate & bot Mass of bottle & cone after filling cone, plate & bot Mass of bottle & cone after filling cone, plate & bot Mass of bottle & cone after filling cone, plate & bot Mass of bottle & cone after filling cone, plate & bot Mass of bottle & cone after filling cone, plate & bot Mass of bottle & cone after filling cone, plate & bot Mass of bottle & cone after filling cone, plate & bot Mass of bottle & cone after filling cone, plate & bottle & cone after filling cone, plate & bot Mass of bottle & cone after filling cone, plate & bottle & cone before filling cone, plate	
Method A (Direct Transmission) Depth Setting 8 (inches) Count Time 1 (minutes) Moisture Count 154 Density Count 1334 et Density (p_{ub}) 132.4 ($lhsift^3$) Dry Density 120.4 ($lhsift^3$) Mass of sand to fill conplate, & hole (M_1) Mass of sand to fill conplate, & hole (M_2) Mass of sand to fill conplate, & hole (M_1) Mass of sand to fill conplate, & hole (M_2) Mass of sand to fill conplate, & hole (M_1) Mass of sand to fill conplate, & hole (M_2) Mass of sand to fill conplate, & hole (M_1) Mass of sand to fill conplate, & hole (M_2) Mass of sand to fill conplate, & hole (M_2) Mass of container Density 12.1 ($lhsift^3$) Moisture Fraction 10.2 (%) Mass of container & wet specimen (M_{col}) Mass of container & wet specimen (M_{col}) Mass of container & wet specimen (M_1) Mass of other wet soil (M_2) Dry Density (M_2) 164.5 g Mass of other wet soil (M_2) Mass of container (M_1) Mass of container (M_2) Mass of other & conce, plate & hol Mass of bottle & conc after filling conce, plate & hole (M_2) Mass of sand to fill conplate & hole (M_2) Mass of sand to fill conplate & hole (M_2) Mass of wet soil (M_2) Mass of container (M_2) M_2 100 M_1 /(M_2) M_2 100 M_2 /(M_2) M_2 100 M_3 /(M_2) M_2 100 M_3 /(M_2) M_3 100 M_4 1	(v)
Method A (Direct Transmission) Depth Settling 8 (inches) Count Time 1 (infinites) Moisture Count 154 Density Count 1334 Cone, plate & hol Mass of sand to fill conplate, & hole (M_1) Mass of sand to fill conplate, & hole (M_2) Mass of sand to fill conplate, & hole (M_1) Mass of sand to fill conplate, & hole (M_2) Mass of sand to fill conplate, & hole (M_1) Mass of sand to fill conplate, & hole (M_2) Mass of sand to fill conplate, & hole (M_1) Mass of sand to fill conplate, & hole (M_2) Mass of container ID D-3 Mass of container & wet specimen (M_1) Mass of container & wet specimen (M_2) All 12.9 g Mass of container & wet specimen (M_2) Mass of container & M_2 Mass of container (M_2)	line
Conce, plate & hold Mass of sand to fill complate, & hold Mass of sand to fill complate, & hold Mass of sand to fill complate, & hold (M_1) Mass of sand to fill complate, & hold (M_2) Mass of sand to fill complate, & hold (M_3) Mass of sand to fill complate, & hold (M_3) Mass of sand to fill complate, & hold (M_3) Mass of sand to fill complate, & hold (M_3) Mass of sand to fill complate, & hold (M_3) Mass of sand to fill complate, & hold (M_3) Mass of sand to fill complate, & hold (M_3) Mass of wet soil (M_3) Mass of wet soil (M_3) Mass of wet soil (M_3) Mass of container & wet specimen (M_{nm}) Mass of container & wet specimen (M_{nm}) Mass of container & dry specimen (M_{nm}) Mass of dry specimen (M_n) Mass of dry specimen $($	~ /
Moisture Count 154 Density Count 1334 Mass of sand to fill conplaint, & hole (M_f) and the fill count plate, & hole (M_f) and (M_f) and the fill count plate, & hole (M_f) and $($	~ /
tet Density $(p_m) = 132.4 - (lbs/ft^3)$ Dry Density $= 120.4 - (lbs/ft^3)$ Mass of sand to fill hold Mass of wet soil (butter Density $= 12.1 - (lbs/ft^3)$ Moisture Fraction $= 10.2 - (\%)$ Mass of wet soil (butter Density $= 12.1 - (lbs/ft^3)$ Moisture Fraction $= 10.2 - (\%)$ Mass of wet soil (butter Density $= 12.1 - (lbs/ft^3)$ Moisture Fraction $= 10.2 - (\%)$ Mass of wet soil (butter Density $= 12.1 - (lbs/ft^3)$ Moisture Density $= 12.1 - (lbs/ft^3)$ Mass of wet soil (butter Density $= 12.1 - (lbs/ft^3)$ Mass of wet soil (butter Density $= 12.1 - (lbs/ft^3)$ Mass of wet soil (butter Density $= 12.1 - (lbs/ft^3)$ Mass of wet soil (butter Density $= 12.1 - (lbs/ft^3)$ Mass of wet soil (butter Density $= 12.1 - (lbs/ft^3)$ Mass of wet soil (butter Density $= 12.1 - (lbs/ft^3)$ Mass of wet soil (butter Density $= 12.1 - (lbs/ft^3)$ Mass of wet soil (butter Density $= 12.1 - (lbs/ft^3)$ Mass of wet soil (butter Density $= 12.1 - (lbs/ft^3)$ Mass of wet soil (butter Density $= 12.1 - (lbs/ft^3)$ Mass of wet soil (butter Density $= 12.1 - (lbs/ft^3)$ Mass of wet soil (butter Density $= 12.1 - (lbs/ft^3)$ Mass of wet soil (butter Density $= 12.1 - (lbs/ft^3)$ Mass of wet soil (butter Density $= 12.1 - (lbs/ft^3)$ Mass of wet soil (butter Density $= 12.1 - (lbs/ft^3)$ Mass of container & wet specimen (butter Density $= 12.1 - (lbs/ft^3)$ Mass of container & wet specimen (butter Density	nc
Mass of wet soil ontainer Mass of wet soil on	
DISTURE DETERMINATION ASTM D4643 Container ID B-3 Mass of container & wet specimen (M_{cma}) Mass of container & wet specimen (M_{cmb}) Mass of container & dry specimen (M_{cmb}) Mass of water (M_{w}) Mass of water (M_{w}) Mass of container (M_{c}) Dry Density (M_{cmb}) Mass of container (M_{c}) Dry Unit Weighthough in color and Soil Description: Froctor ID: Radon F Standard Proctor (ASTM I) Standard Proctor (ASTM I) Maximum Dry Density (γ_{c}) Percent Compaction (γ_{c}) Maximum Dry Density (γ_{c}) Required Moisture: TEST RESULTS: X Pass Pass Pass Failed Moisture	
Container ID D-3 Mass of container & wet specimen (M_{cont}) Mass of container & dry specimen (M_{cont}) Mass of water (M_{ul}) Mass of container & dry specimen (M_{cont}) Mass of water (M_{ul}) Mass of container (M_{cont}) Mass of container (M_{cont}) Mass of water (M_{ul}) Mass of water (M_{ul}) Mass of container (M_{cl}) Pry Unit Welgh M_{cl} + M_{cl}	ner g
Container ID	
Container ID	
Mass of container & wet specimen (M_{cont}) 412.9 g $M_A = 100 M_A / (w + 100)$ Wet Denisty $M_B = M_{cont} + M_B = M_{cont} + M_B = M_{cont} + M_B = M_B$	
Mass of container & dry specimen (M_{cdd}) 388.4 g Mass of water (M_{iii}) 388.4 g Mass of water (M_{iii}) 24.5 g Mass of container (M_{ci}) 164.5 g Mass of container (M_{ci}) 164.5 g Mass of dry specimen (M_{ii}) 164.5 g Mass of container (M_{ci}) 164.5 g Proctor III 165. g Proctor ID: Radon II 165. g Standard Proctor (ASTM II 165. g Proctor ID: Radon II 165. g Maximum Dry Density $(\rho_{ii}) = (100 \times \rho_{iii})/(100 + 10.9 = 119.3)$ 165. fines. Proctor ID: Radon II 165. g Maximum Dry Density $(\rho_{ii}) = (100 \times \rho_{iii})/(100 + 10.9 = 119.3)$ 165. fines. Proctor ID: Radon II 165. g Maximum Dry Density $(\rho_{ii}) = (100 \times \rho_{iii})/(100 + 10.9 = 119.3)$ 165. fines. Proctor ID: Radon II 165. g Maximum Dry Density $(\rho_{ii}) = (100 \times \rho_{iii})/(100 + 10.9 = 119.3)$ 165. fines. Required Moisture: 10.2 % to pass of the process of	
Mass of water (M_{w}) $M_{w} = M_{cons} = M_{cole}$ $M_{w} = M_$	90)s
Mass of water (M_w) $M_w = M_{cms} - M_{cds}$ Mass of container (M_c) Mass of container (M_c) Mass of dry specimen (M_s) $M_s = M_{cds} - M_c$ Moisture content (w) $W = (M_w / M_s) \times 100$ Dry Density $(\rho_{s0} = (100 \times \rho_{sw})/(100 + w))$ Proceeding the first of the Domity from ASTM D 1936 (ρ_{s0}) and solve the Domity from ASTM D 1936 (ρ_{s0}) asker presidence over ASTM D 1938 (ρ_{s0}) Percent Compaction = ρ_d / $\gamma_d max \times 100$ Percent Compaction = ρ_d / $\gamma_d max \times 100$ Required Moisture: 10.2 % Required Percent Compaction: TEST RESULTS: Trowave oven power setting on HIGH. Initial time setting of 3 and subsequent incremental drying periods of 1 minute until	
$M_{w} = M_{cons} - M_{cds}$ $M_{ss} = M_{cons} - M_{cds}$ $M_{ss} = M_{cons} - M_{cds}$ $M_{ss} = M_{cds} - M_{c}$ $M_{ss} = M_{cds} - M_{c}$ $M_{ss} = M_{cds} - M_{c}$ $M_{s} = M_{cds} - M_{c}$ $M_{ss} = M_{ss} - M_{cds}$ $M_{ss} = M_{ss} - M_{ss}$ $M_$	
Mass of container (M_c) Mass of container (M_c) Mass of dry specimen (M_s) $M_s = M_{cab} - M_c$ Moisture content (w) $w = (M_w / M_d) \times 100$ Dry Density $(\rho_{ell} = (100 \times \rho_m)/(100 + w)$ $pl = (100 \times 132.4)/(100 + 10.9 = 119.3)/(100 + w)$ Maximum Dry Density $(\rho_{ell} = (100 \times \rho_m)/(100 + w))$ $pl = (100 \times 132.4)/(100 + 10.9 = 119.3)/(100 + w)$ Maximum Dry Density $(\rho_{ell} = (100 \times \rho_m)/(100 + w))/(100 + w)$ Percent Compaction $\rho_{ell} = (100 \times \rho_m)/(100 + w)/(100 + w)$ Percent Compaction $\rho_{ell} = (100 \times \rho_m)/(100 + w)/(100 + w)$ Required Moisture: $\rho_{ell} = (100 \times \rho_m)/(100 + w)/(100 + w)$ Required Percent Compaction: TEST RESULTS: Trowave oven power setting on HIGH. Initial time setting of 3 and subsequent incremental drying periods of 1 minute until	
Mass of dry specimen (M_a) $M_a = M_{cab} - M_c$ Moisture content (w) $w = (M_m / M_d) \times 100$ Dry Density $(\rho_{ab} = (100 \times \rho_m)/(100 + w)$ $pil = (100 \times 132.4)/(100 + 10.9 = 119.3)$ $pil = $	ght
M ₃ = M _{cds} - M _c Moisture content (w) $w = (M_w / M_b) \times 100$ Dry Density $(\rho_{s0} = (100 \times \rho_{s0})/(100 + w)$ $pd = (100 \times 132.4)/(100 + 10.9 = 119.3) \text{ fbs/ft}^2$ Percent Compaction = $\rho_d / \gamma_d max \times 100$ $119.3 / 118.4 \times 100 = 100.8$ Optimum Moisture (w _{opt}) Required Moisture: 10.2 % Required Percent Compaction: TEST RESULTS: Trowave oven power setting on HIGH. Initial time setting of 3 mutes and subsequent incremental drying periods of 1 minute until	
Moisture content (w) $w = (M_m / M_s) \times 100$ 10.9 % Proctor ID: Radon E Standard Proctor (ASTM I Dry Density $(\rho_{s0} = (100 \times \rho_{s0})/(100 + w))$ Maximum Dry Density $(r_{s0} = 100 \times 132.4)/(100 + 10.9 = 119.3)$ Ibs/ft Optimum Moisture (w_{opt}) Percent Compaction = ρ_{s0} / γ_{s0} max $\times 100$ Required Moisture: 10.2 % Required Percent Compaction: TEST RESULTS: Trowave oven power setting on HIGH. Initial time setting of 3 mutes and subsequent incremental drying periods of 1 minute until	
Dry Density $(\rho_{ab} = (100 \times \rho_{ab})/(100 + w)$ $pal = (100 \times 132.4)/(100 + 10.9 = 119.3) lbs/ft^2$ Percent Compaction = $\rho_d = (100.8) / (100$	
$pd = (100 \times 132.4) / (100 + 10.9 = 119.3) $	
Note: Wet Dentity from ASTM D 1936 (ρ_n) takes presidence over ASTM D 6938 (ρ_n) Percent Compaction = ρ_d / γ_d max x 100 119.3 / 118.4 x 100 = 100.8 % Required Moisture: 10.2 % Required Percent Compaction: TEST RESULTS: Trowave oven power setting on HIGH. Initial time setting of 3 total subsequent incremental drying periods of 1 minute until	118.4 (lbs/
Percent Compaction = \(\rho_d \) / \(\gamma_d max \) x \ 100 \\ \text{119.3} \) / \(\frac{118.4}{2} \) x \(\text{100} \) = \(\frac{100.8}{2} \) \(\frac{7}{6} \) The entropy of th	13.2 (%)
Percent Compaction = \(\rho_d \) / \(\gamma_d \) max \(x \) 100.8 \\ \text{7.60} = \text{100.8} \text{7.60} \) Required Percent Compaction: TEST RESULTS: Trowave oven power setting on HIGH. Initial time setting of 3 Total and subsequent incremental drying periods of 1 minute until Test Results: X Pass Failed Moisture	to 16.2 5
minents: TEST RESULTS: TEST RESULTS: X Pass utes and subsequent incremental drying periods of 1 minute until	
crowave oven power setting on HIGH. Initial time setting of 3 X Pass utes and subsequent incremental drying periods of 1 minute until	95.0 (%)
utes and subsequent incremental drying periods of 1 minute until	
Falled Moisture	Date: 8/4/10
range of 0.1 76 of 1988 Of the finital wet mass of the son.	Time: 0915
Failed Compaction By: David Stewart / David 4	66
By: David Stewart /1) out &	(signature)
2-17) 18-17.10	
QA/QC APPROVAL DATE	

PROJECT: Moab UM	ITRA Project	NSITY TEST OTHER
LIFT IDENTIFICATION:	Radon Barrier Test Pad	8/2/2010 DATE: 8/2/2010
TEST ID NUMBER(S):	65 1200	·4
TEST LOCATION: 679		TEST METHOD: D1556x D6938
ASTM D6938 (DENSITY DI	ETERMINATION)	ASTM D1556 (DENSITY DETERMINATIO
Make/Model Troxler 3430 Gau	ge Serial #_ 31674	Testing Apparatus Calibrated Vol. (lbs/ft s)
Last Calibration Date: 3/4/	10	Bulk Density of sand (p ₁)
Daily Standard Counts: Off Cell Standard		Mass of Sand to Fill Cone & Plate (M ₂)
Density 2495 Me	oisture 706	Mass of bottle & cone before filling
Method A (Direct Tra		cone, plate & hole
Depth Setting 8 (inches) C		Mass of bottle & cone after filling
		cone, plate & hole
Moisture Count181	Density Count 1424	Mass of sand to fill cone
Wet Density (ρ _m) 129.8 (lbs/ft ⁻¹) D	ny Daneity 116 3 //he/fi	plate, & hole (M/1) g Mass of sand to fil/ hole g
rece Delisity (par 125.0 (100))	iy Delisity 115.5 (1057)	Mass of sand to fill hole g Mass of wet soil to container g
Moisture Density 14.5 (lbs/ft ²) M	Loisture Fraction 12.6 A	
module beliaty 142 (103)1) in	Tacton 12.0 (Mass of Container g
MOISTURE DETERMINATION		Mass of wet soil (M ₃)
ASTM D464	13	Test Hole Volume
Container ID D-2		$V = (M_1 - M_2)/\rho_1 \underline{\hspace{1cm}} c$
Mass of container & wet specimen		Dry Mass of soil
(M cmr)	412.8 g	$M_4 = 100 M_3 / (w + 100) g$
Mass of container & dry specimen		Wet Denisty
(M _{cds}) Mass of water (M _w)	385.0 g	
$M_w = M_{con} - M_{cd}$	27.8	Dry Denisty $\rho_d = M_d/V \qquad g$
DE W - DE pare - DE pare	27.8 g	Dry Unit Weight
Mass of container (M,)	164.5 g	$\gamma_d = \rho_d \times 62.43 \qquad lb$
Mass of dry specimen (M,)	0	Yellowish in color and consists of m
$M_s = M_{ods} - M_c$	220.5 g	Soil Description: fines.
Moisture content (w)		Proctor ID: Radon Barrier #3
$w = (M_w / M_s) \times 100$	12.6	

Density Testing DOE-EM/GJRAC1783 Rcv. 0

Percent Compaction = ρ_d / $\gamma_d max \times 100$

Microwave oven power setting on HIGH. Initial time setting of 3

minutes and subsequent incremental drying periods of 1 minute until

97.4 %

115.3 / 118.4 x 100 =

Page QC-F-002 Page Q of

to 16.2 %

Date: 8/4/10

95.0

Required Moisture: 10.2 %

TEST RESULTS:

X Pass

Required Percent Compaction:

Failed Moisture

A4. Radon Barrier Standard Proctor Test Results Summary

Set	Proctor ID #	Date Sampled	Date Approved	Maximum Dry Density (lb/ft³)	Optimum Moisture Content (%)	Soils Description	Liquid Limit (%)	Plastic Limit (%)	Plasticity Index (%)
361	Radon Barrier #1	05/28/10	05/28/10	113.1	14.0	Gray in color some shale*	33.0	17.0	16.0
	Radon Barrier #2(A)	08/02/10	08/02/10	119.9	11.5	Yellowish in color and consists of mostly fines	33.4	15.0	18.4
Set #1	Radon Barrier #3(A)	08/02/10	08/02/10	118.4	13.2	Yellowish in color and consists of mostly fines	30.6	14.7	15.9
0,	Radon Barrier #4(A)	08/02/10	08/03/10	119.7	11.8	Yellowish in color and consists of mostly fines	33.2	16.6	16.6
0.	Radon Barrier #5(B)	08/04/10	08/04/10	116.2	13.2	Gray in color and consists of mostly fines	32.1	13.3	18.8
Set #2	Radon Barrier #6(B)	08/04/10	08/04/10	117.5	13.1	Gray in color and consists of mostly fines	30.8	13.9	16.9
	Radon Barrier #7(B)	08/04/10	08/04/10	118.6	12.7	Gray in color and consists of mostly fines	32.2	14.4	17.8
3	Radon Barrier #8(C)	08/12/10	08/12/10	118.2	13.3	Gray in color and consists of mostly fines	32.1	15.9	16.2
Set #3	Radon Barrier #9(C)	08/12/10	08/12/10	118.4	12.5	Gray in color and consists of mostly fines	33.0	16.8	16.2
•	Radon Barrier #10(C)	08/12/10	08/12/10	116.8	12.0	Gray in color and consists of mostly fines	32.6	15.7	17.0
	Radon Barrier #11(D)	08/17/10	08/17/10	118.8	12.6	Gray in color and consists of mostly fines	33.0	16.0	17.0
	Radon Barrier #12(E)	08/24/10	10/05/10	119.2	11.4	Gray in color and consists of mostly fines	33.0	18.0	15.0
	Radon Barrier #13(F)	08/27/10	10/05/10	119.8	11.0	Gray in color and consists of mostly fines	33.0	17.0	16.0
	Radon Barrier #14(G)								
N/A	Radon Barrier #15(G)	Proctor se	t rejected d	ue to proctor o	curves.				
	Radon Barrier #16(G)								
4	Radon Barrier #17(H)	09/10/10	10/05/10	120.0	11.1	Gray in color and consists of mostly fines	30.0	16.0	14.0
Set #4	Radon Barrier #18(H)	09/10/10	10/05/10	119.8	11.3	Gray in color and consists of mostly fines	30.0	16.0	14.0
	Radon Barrier #19(H)	09/10/10	10/05/10	119.4	11.7	Gray in color and consists of mostly fines	31.0	15.0	16.0
15	Radon Barrier #20(I)	09/10/10	10/05/10	120.8	11.4	Gray in color and consists of mostly fines	31.0	13.0	18.0
Set #5	Radon Barrier #21(I)	09/10/10	10/05/10	119.5	11.6	Gray in color and consists of mostly fines	31.0	16.0	16.0
	Radon Barrier #22(I)	09/10/10	10/05/10	118.7	11.7	Gray in color and consists of mostly fines	31.0	14.0	17.0
	Radon Barrier #23(J)	09/16/10	10/05/10	120.3	11.4	Gray in color and consists of mostly fines	32.0	16.0	16.0
6	Radon Barrier #1 (2011)	03/30/11	04/04/11	120.2	11.8	Gray in color and consist of mostly fines	33.0	16.0	17.0
Set #6	Radon Barrier #2 (2011)	03/30/11	04/04/11	120.9	11.1	Gray in color and consist of mostly fines	31.0	17.0	14.0
	Radon Barrier #3 (2011)	03/30/11	04/04/11	122.0	11.3	Gray in color and consist of mostly fines	31.0	16.0	15.0
	Radon Barrier #4 (2011)	04/04/11	04/06/11	121.0	11.0	Gray in color and consist of mostly fines	32.0	15.0	17.0
	Radon Barrier #5 (2011)	04/05/11	04/14/11	122.2	11.0	Gray in color and consist of mostly fines	30.0	17.0	13.0
	Radon Barrier #6 (2011)	04/12/11	04/18/11	122.0	10.8	Gray in color and consist of mostly fines	31.0	14.0	17.0
	Radon Barrier #7 (2011)	04/14/11	04/28/11	118.8	12.6	Gray in color and consists of mostly fines	32.0	15.0	17.0
	Radon Barrier #8 (2011)	04/20/11	04/28/11	120.5	11.5	Gray in color and consists of mostly fines	30.0	15.0	15.0

A4. Radon Barrier Standard Proctor Test Results Summary

Set	Proctor ID #	Date Sampled	Date Approved	Maximum Dry Density (lb/ft³)	Optimum Moisture Content (%)	Soils Description	Liquid Limit (%)	Plastic Limit (%)	Plasticity Index (%)
	Radon Barrier #9 (2011)	04/21/11	05/11/11	116.6	13.6	Gray in color and consists of mostly fines	35.0	19.0	16.0
	Radon Barrier #10 (2011)	04/27/11	05/11/11	118.2	12.4	Gray in color and consist of mostly fines	33.0	17.0	16.0
	Radon Barrier #11 (2011)	05/03/11	05/16/11	118.3	11.9	Gray in color and consists of mostly fines	35.0	17.0	18.0
	Radon Barrier #12 (2011)	05/09/11	05/16/11	115.7	14.7	Gray in color and consists of mostly fines	35.0	20.0	15.0
	Radon Barrier #13 (2011)	05/09/11	05/16/11	114.0	14.2	Gray in color and consists of mostly fines	35.0	19.0	16.0
	Radon Barrrier #14 (2011)	05/09/11	05/16/11	115.0	13.8	Gray in color and consists of mostly fines	34.0	17.0	17.0
	Radon Barrier #15 (2011)	05/16/11	05/27/11	115.9	14.4	Gray in color and consists of mostly fines	35.0	17.0	18.0
	Radon Barrier #16 (2011)	05/25/11	06/06/11	118.6	13.2	Tannish in color and consists mostly of fines	31.0	17.0	14.0
	Radon Barrier #17 (2011)	05/25/11	06/06/11	117.0	13.7	Tannish in color and consists mostly of fines	32.0	17.0	15.0
	Radon Barrier #18 (2011)	05/25/11	06/06/11	116.6	14.1	Tannish in color and consists mostly of fines	31.0	17.0	14.0
	Radon Barrier #19 (2011)	08/11/11	10/03/11	117.1	14.0	Grayish in color and consists mostly of fines	33.0	16.0	17.0
	Radon Barrier #20 (2011)	08/11/11	10/03/11	115.7	14.3	Grayish in color and consists mostly of fines	33.0	16.0	17.0
	Radon Barrier #21 (2011)	08/11/11	10/03/11	116.2	13.8	Grayish in color and consists mostly of fines	32.0	17.0	15.0
	Radon Barrier #22 (2011)	08/25/11	09/07/11	114.4	14.7	Tannish in color and consists mostly of fines	30.0	16.0	14.0
	Radon Barrier #23 (2011)	08/31/11	09/13/11	115.0	14.5	Tannish in color and consists mostly of fines	32.0	16.0	16.0
	Radon Barrier #24 (2011)	09/07/11	09/29/11	115.2	15.0	Tannish in color and consists mostly of fines	32.0	17.0	15.0
	Radon Barrier #25 (2011)	09/28/11	10/03/11	115.8	14.5	Tannish in color and consists mostly of fines	32.0	16.0	16.0
	Radon Barrier #26 (2011)	10/04/11	10/25/11	114.5	15.0	Tannish in color and consists mostly of fines	33.0	16.0	17.0
	Radon Barrier #27 (2011)	10/12/11	10/25/11	116.3	14.4	Tannish in color and consists mostly of fines	33.0	16.0	17.0

^{*}All shale breaks down when exposed to water. Approximately 97% of material passes the #200 sieve.

A4. Radon Barrier Lift Approval Summary

Date	Lift ID #	# of Passing Moisture Tests	Quantity Approved (yd³)	Cumulative Quantity Approved (yd³)	CAES Screen Passing Pixels (%)	Average Thickness (ft)	Proctor ID #	# of Nuclear Density Gauge Verifications	# of Sandcone Verifications	Verified Compaction (%)	Notes
08/02/10	Test Pad	4	N/A	0	95.8	0.8	RB-3	4	0	97.4	1,2
08/10/10	URB27100810-00	2	2,711	2,711	98.2	0.6	RB-3	2	1	97.9	
08/10/10	URA11100810-00	3	5,237	7,948	98.1	0.7	RB-3	3	1	100.1	
08/16/10	URA11100811-00	3	3,192	11,140	95.6	0.5	RB-8C	3	0	97.1	
08/17/10	URC11100811-00	6	3,293	14,433	98.9	0.6	RB-3 RB-8	0	0	N/A	
08/18/10	URC11100817-00	3	2,939	17,372	98.1	0.6	RB-8	0	0	N/A	
08/17/10	URA11100817-00	3	3,712	21,084	94.2	0.6	RB-8C	1	0	98.4	
08/20/10	URA11100819-00	6	4,328	25,412	92.9	0.7	RB-8	0	0	N/A	
08/24/10	URC11100823-00	6	2,002	27,414	93.7	0.4	RB-8 RB-11D	0	0	N/A	
08/25/10	URA11100824-00	3	4,328	31,742	92.4	0.7	RB-11D	0	0	N/A	
08/26/10	URC11100824-00	6	3,504	35,246	90.0	0.7	RB-11D	0	0	N/A	
09/07/10	URA01100907-00	5	2,340	37,586	96.2	0.4	RB-12E	0	0	N/A	
09/13/10	URA01100909-00	3	4,093	41,679	95.6	0.7	RB-18H	0	0	N/A	
09/14/10	URA01100914-00	3	3,938	45,617	97.9	0.7	RB-23I	0	0	N/A	
09/15/10	URA01100915-00	3	3,910	49,527	96.9	0.7	RB-23I	0	0	N/A	
09/20/10	URA01100916-00	3	3,910	53,437	95.3	0.7	RB-22I	0	0	N/A	
09/29/10	URA01100924-00	3	1,552	54,989	95.0	0.3	RB-12E	0	0	N/A	
09/29/10	URC11100827-00	3	1,478	56,467	99.1	0.3	RB-12E	0	0	N/A	
09/29/10	URA11100827-00	3	1,039	57,506	99.1	0.2	RB-12E	0	0	N/A	
03/31/11	URF15110331-00	2	2,671	60,177	99.8	0.5	RB-3(2011)	0	0	N/A	
03/31/11	URH01110330-00	4	3,053	63,230	99.5	0.7	RB-3(2011)	2	0	98.4	
03/31/11	URH01110331-00	2	3,391	66,621	98.9	0.7	RB-3(2011)	1	0	96.4	
04/04/11	URI35110404-00	1	49	66,670	N/A	0.8	RB-3(2011)	1	0	97.0	
04/04/11	URI35110404-01	1	52	66,722	N/A	0.8	RB-3(2011)	1	0	98.4	
04/06/11	URF01110406-00	2	2,617	69,339	97.9	0.6	RB-3(2011)	0	0	N/A	
04/07/11	URH01110407-00	4	3,118	72,457	97.7	0.7	RB-4(2011)	0	0	N/A	
04/11/11	URJ35110411-00	1	59	72,516	N/A	0.8	RB-4(2011)	1	0	96.3	
04/12/11	URF1510412-00	4	3,847	76,363	99.4	0.6	RB-4(2011)	0	0	N/A	П
04/13/11	URJ12110413-00	3	3,998	80,361	99.1	0.6	RB-4(2011)	0	0	N/A	
04/14/11	URF01110414-00	4	3,475	83,836	98.9	0.7	RB-6(2011)	0	0	N/A	
04/18/11	URJ12110418-00	4	3,998	87,834	99.4	0.6	RB-6(2011)	0	0	N/A	
04/21/11	URE14110421-00	3	4,278	92,112	99.3	0.7	RB-6(2011)	0	0	N/A	
04/25/11	URH01110425-00	5	3,582	95,694	99.2	0.7	RB-7(2011)	0	0	N/A	
04/26/11	URH14110426-00	5	3,479	99,173	97.5	0.6	RB-7(2011)	0	0	N/A	
04/28/11	URE01110428-00	4	3,038	102,211	99.2	0.6	RB-8(2011)	0	0	N/A	

A4. Radon Barrier Lift Approval Summary

Date	Lift ID #	# of Passing Moisture Tests	Quantity Approved (yd³)	Cumulative Quantity Approved (yd³)	CAES Screen Passing Pixels (%)	Average Thickness (ft)	Proctor ID #	# of Nuclear Density Gauge Verifications	# of Sandcone Verifications	Verified Compaction (%)	Notes
05/02/11	URE14110502-00	4	3,802	106,013	98.3	0.6	RB-8(2011)	0	0	N/A	
05/03/11	URH01110503-00	4	2,450	108,463	98.9	0.5	RB-9(2011)	0	0	N/A	
05/04/11	URH14110504-00	6	3,291	111,754	98.1	0.6	RB-9(2011)	0	0	N/A	
05/05/11	URE01110505-00	5	3,751	115,505	99.0	0.7	RB-9(2011)	0	0	N/A	
05/11/11	URE14110511-00	5	4,811	120,316	98.4	0.7	RB-10(2011)	0	0	N/A	
05/16/11	URH01110516-00	4	3,191	123,507	98.0	0.7	RB-12(2011)	0	0	N/A	
05/17/11	URH14110517-00	5	2,989	126,496	97.5	0.6	RB-12(2011)	0	0	N/A	
05/23/11	URE01110523-00	6	2,680	129,176	98.5	0.5	RB-12(2011)	0	0	N/A	
05/26/11	URE14110526-00	4	3,548	132,724	99.6	0.5	RB-17(2011)	0	0	N/A	
06/01/11	URH01110601-00	4	2,396	135,120	97.9	0.5	RB-17(2011)	0	0	N/A	
06/01/11	URH14110601-00	2	3,060	138,180	97.5	0.6	RB-17(2011)	0	0	N/A	
08/24/11	URM18110822-00	5	2,338	140,518	N/A	0.6	RB-21(2011)	2	0	97.1	
08/25/11	URO19110824-00	2	1,956	142,474	N/A	0.6	RN-21(2011)	2	0	98.6	
08/26/11	URM18110825-00	2	3,117	145,591	N/A	0.8	RB-21(2011)	2	0	97.3	
08/29/11	URO19110826-00	2	2,224	147,815	N/A	0.7	RB-21(2011)	2	0	95.7	
08/30/11	URM19110830.00	2	3,162	150,977	N/A	0.8	RB-21(2011)	2	0	96.4	
08/31/11	URO19110831-00	1	2,397	153,374	N/A	0.8	RB-22(2011)	2	0	98.6	
09/02/11	URO1910901-00	2	2,320	155,694	N/A	0.8	RB-22(2011)	2	0	99.0	
09/07/11	URM18110902-00	3	3,232	158,926	N/A	0.8	RB-22(2011)	2	1	100.4	
09/28/11	URQ23110928-00	1	1,826	160,752	N/A	0.7	RB-24(2011)	2	0	95.5	
09/29/11	URQ29110929-00	2	1,757	162,509	N/A	0.6	RB-24(2011)	2	1	100.8	
10/03/11	URQ231110929-00	1	2,095	164,604	N/A	0.8	RB-24(2011)	2	0	98.1	
10/03/11	URQ29111003-00	1	2,320	166,924	N/A	0.8	RB-24(2011)	2	0	97.1	
10/05/11	URQ23111004-00	2	2,105	169,029	N/A	0.8	RB-24(2011)	2	0	98.7	
10/10/11	URQ29111005-00	2	2,025	171,054	N/A	0.7	RB-25(2011)	2	0	99.5	
10/10/11	URQ23111007-00	2	1,588	172,642	N/A	0.6	RB-25(2011)	2	0	99.4	
10/11/11	URQ29111011-00	1	2,323	174,965	N/A	0.8	RB-25(2011)	2	0	100.1	
10/19/11	URQ18111019-00	1	948	175,913	N/A	0.6	RB-25(2011)	2	0	98.6	
10/20/11	URQ18111020-00	1	1,322	177,235	N/A	0.8	RB-25(2011)	2	0	97.7	
10/21/11	URQ18111021-00	1	1,169	178,404	N/A	0.7	RB-27(2011)	2	0	98.6	
10/24/11	URQ18111024-00	1	1,153	179,557	N/A	0.7	RB-27(2011)	2	0	97.5	
10/24/11	URQ18111024-01	1	1,267	180,824	N/A	0.8	RB-27(2011)	1	0	99.5	
10/31/11	URM18110909-00	3	3,396	184,220	N/A	0.8	RB-23(2011)	2	0	99.9	
10/31/11	URO19110907-00	3	2,267	186,487	N/A	0.8	RB-23(2011)	2	0	99.1	
10/31/11	URQ18111025-00	1	158	186,645	N/A	0.1	RB-27(2011)	2	0	99.1	
10/31/11	URQ23111012-00	2	2,080	188,725	N/A	0.8	RB-25(2011)	3	0	99.5	

A4. Radon Barrier Lift Approval Summary

Date	Lift ID #	# of Passing Moisture Tests	Quantity Approved (yd³)	Cumulative Quantity Approved (yd ³)	CAES Screen Passing Pixels (%)	Average Thickness (ft)	Proctor ID #	# of Nuclear Density Gauge Verifications	# of Sandcone Verifications	Verified Compaction (%)	Notes
10/31/11	URQ29111013-00	1	1,671	190,396	N/A	0.6	RB-25(2011)	2	0	100.0	

Average CAES Screen Passing Pixels (%) = 97.45

Total Quantity Approved (yd³) = 190,396

Total # of Nuclear Density Gauge Tests = 71

Total # of Moisture Tests = 215

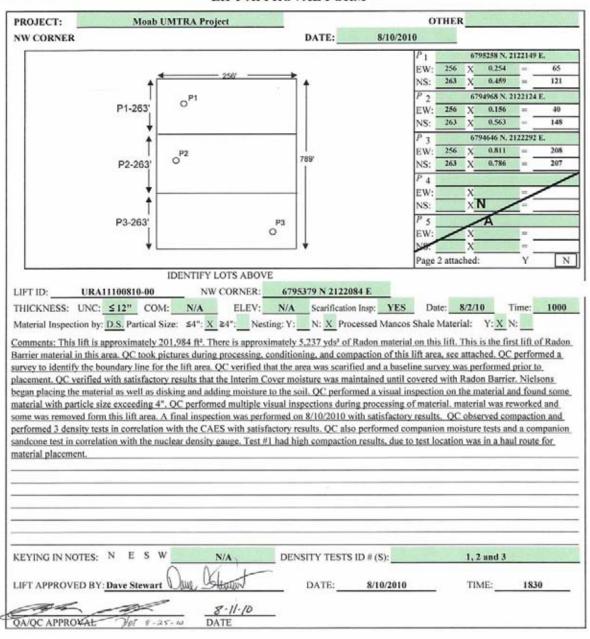
Quantity per Moisture Test (yd³) = 886

Total Average Thickness (ft.) = 0.6

- 1. Lift was created as a test pad to establish a compaction pattern for the Radon Barrier material.
- 2. Three passes were made with a Caterpillar 825 compacter equipped with the CAES; four density tests were performed to establish proof of compaction.



LIFT APPROVAL FORM



Density Testing DOE-EM/GJRAC1783 Rev. 0 QC-F-001 File index No. 43.8.2 Page ___ of ___2



Slope Elevation Survey

- 5	THE RESERVE AND ADDRESS OF THE PERSON NAMED IN	thickness=			Northing	Easting	_
	Grid Size=	50	0'	Lower Left	N		4
Lift ID:	U	RA11100810-		Upper Right		A	_
Last	Lift Eleva	tions	Lif	t Approval El	evations	Lift Thickness	
Northing	Easting	Elevation	Northing	Easting	Elevation	Thickness	٦
6794794	2122165	4980.7	6794794	2122165	4981.7	1.0	\neg
6794844	2122165	4982.1	6794844	2122165	4983.1	1.0	
6794894	2122165	4983.5	6794894	2122165	4984.5	1.0	
6794944	2122165	4984.9	6794944	2122165	4985.8	0,9	
6794994	2122165	4986.2	6794994	2122165	4987.0	0.9	\neg
6795044	2122165	4987.2	6795044	2122165	4988.1	1.0	
6794644	2122215	4977.3	6794644	2122215	4978.2	0.9	
6794694	2122215	4978.6	6794694	2122215	4979.5	0.9	
6794744	2122215	4979.8	6794744	2122215	4980.8	0,9	
6794794	2122215	4981.1	6794794	2122215	4982.1	1.0	
6794844	2122215	4982.3	6794844	2122215	4983.3	1.0	
6794894	2122215	4983.6	6794894	2122215	4984.3	0.8	
6794944	2122215	4985.0	6794944	2122215	4985.7		
6794994	2122215	4986.1	6794994	2122215	4987.0	0.9	
6795044	2122215	4987.3	6795044	2122215	4988.2	0.9	
6794644	2122265	4977.4	6794644	2122265	4978.2	0.8	
6794694	2122265	4978.5	6794694	2122265	4979.5	0.9	
6794744	2122265	4979.9	6794744	2122265	4980.8	0.9	
6794794	2122265	4981.3	6794794	2122265	4982.1	0,9	
6794844	2122265	4982.3	6794844	2122265	4983.4	1.0	٦
6794894	2122265	4983.5	6794894	2122265	4984.4	1.0	П
6794944	2122265	4984.7	6794944	2122265	4985.7	1.0	┪
6794994	2122265	4986.1	6794994	2122265	4987.0	1.0	┪
6795044	2122265	4987.3	6795044	2122265	4988.3	1.0	┪
6794644	2122315	4977.3	6794644	2122315	4978.2	1.0	
6794694	2122315	4978.5	6794694	2122315	4979.4	0.9	┑
6794744	2122315	4979.9	6794744	2122315	4980.7	0.8	٦
6794794	2122315	4981.4	6794794	2122315	4982.1	0.8	٦
6794844	2122315	4982.5	6794844	2122315	4983.4	0.9	٦
6794894	2122315	4983.6	6794894	2122315	4984.7	1.0	٦
6794944	2122315	4984.9	6794944	2122315	4985.9	1.0	
6794994	2122315	4986.3	6794994	2122315	4987.2	0.9	
6795044	2122315	4987.6	6795044	2122315	4988.5	0.9	
6794644	2122365	4977.4	6794644	2122365	4978.0	0.7	
6794694	2122365	4978.7	6794694	2122365	4979.3	0,7	
6794744	2122365	4980.0	6794744	2122365	4980.9	0.9	
6794794	2122365	4981.4	6794794	2122365	4982.2	0.9	
6794844	2122365	4982.6	6794844	2122365	4983.4	0.8	
6794894	2122365	4983.7	6794894	2122365	4984.6	0,9	
6794944	2122365	4985.1	6794944	2122365	4985.9	0.8	
6794994	2122365	4986.4	6794994	2122365	4987.0		
6795044	2122365	4987.5	6795044	2122365	4988.0	0.6	_
6794644	2122415	4977.5	6794644	2122415	4977.8	0.3	_
6794694	2122415	4978.6	6794694	2122415	4978.9	0.3	
6794744	2122415	4980.0	6794744	2122415	4980.2	0.2	Ц
6794794	2122415	4981.3	6794794	2122415	4981.4	0.1	
6794844	2122415	4982.4	6794844	2122415	4982.4	0.0	4
6794894	2122415	4983.4	6794894	2122415	4983.4	0.0	4
6794944 6795052	2122415	4984.7 4987.6	6794944 6795052	2122415 2122119	4984.7 4988.1	0.0	\dashv

Energy Solutions

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\Box	0.6	4989.4	2122119	6795102	2122119 4988.7	6795102
	0.7	4990.5	2122119	6795152	2122119 4989.8	6795152
	0.6	4991.7	2122119	6795202	2122119 4991.1	6795202
	0.6	4993.1	2122119	6795252	2122119 4992.5	6795252
	0.8	4994.4	2122119	6795302	2122119 4993.7	6795302
	0.7	4995.6	2122119	6795352	2122119 4994.9	6795352
	0.5	4995.8	2122119	6795402	2122119 4995.4	6795402
	1.0	4988.3	2122169	6795052	2122169 4987.4	6795052
	0.9	4989.6	2122169	6795102	2122169 4988.7	6795102
	0.8	4990.9	2122169	6795152	2122169 4990.1	6795152
	0.7	4992.0	2122169	6795202	2122169 4991.3	6795202
	0.7	4993.2	2122169	6795252	2122169 4992.6	6795252
\neg	0.7	4994.4	2122169	6795302	2122169 4993.8	6795302
\neg	0.5	4995.5	2122169	6795352	2122169 4994.9	6795352
\Box	0.4	4996.1	2122169	6795402	2122169 4995.6	6795402
\Box	0.1	4995.1	2122169	6795452	2122169 4995.0	6795452
\neg	0.9	4989.7	2122219	6795102	2122219 4988.8	6795102
\neg	0.8	4990.9	2122219	6795152	2122219 4990.1	6795152
\neg	0.8	4992.0	2122219	6795202	2122219 4991.3	6795202
\neg	0.8	4993.4	2122219	6795252	2122219 4992.6	6795252
\neg	0.7	4994.6	2122219	6795302	2122219 4993.9	6795302
\neg	0.6	4995.6	2122219	6795352	2122219 4995.0	6795352
\neg	0.4	4996.2	2122219	6795402	2122219 4995.8	6795402
\neg	0.2	4995.6	2122219	6795452	2122219 4995.4	6795452
\neg	0.6	4990.7	2122269	6795152	2122269 4990.1	6795152
\neg	0.6	4992.0	2122269	6795202	2122269 4991.3	6795202
\neg	0.7	4993.4	2122269	6795252	2122269 4992.6	6795252
\neg	0.8	4994.6	2122269	6795302	2122269 4993.8	6795302
\neg	0.6	4995.6	2122269	6795352	2122269 4995.0	6795352
\neg	0.6	4996.4	2122269	6795402	2122269 4995.8	6795402
\neg	0.3	4995.6	2122269	6795452	2122269 4995.3	6795452
	0.8	4991.0	2122319	6795152	2122319 4990.1	6795152
□(0.9	4992.2	2122319	6795202	2122319 4991.4	6795202
\neg	0.8	4993.4	2122319	6795252	2122319 4992.6	6795252
□(0.8	4994.6	2122319	6795302	2122319 4993.8	6795302
\neg	0.7	4995.8	2122319	6795352	2122319 4995.1	6795352
\neg	0.5	4996.3	2122319	6795402	2122319 4995.8	6795402
\neg	0.2	4995.9	2122319	6795452	2122319 4995.7	6795452
\neg	0.3	4990.3	2122369	6795152	2122369 4990.0	6795152
\neg	0.2	4991.4	2122369	6795202	2122369 4991.2	6795202
\neg	0.1	4992.3	2122369	6795252	2122369 4992.2	6795252
\neg	0.0					

| Number of Data | Sum of Point | Thickness | 91 | 62.827956 |

of Thick Points 0.0

EnergySolutions

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% =6	98.1%
Elevation Avg	5987.5
Total =6	14714
Total Lines	14995

Pass

Minimum Number of Machine Passes

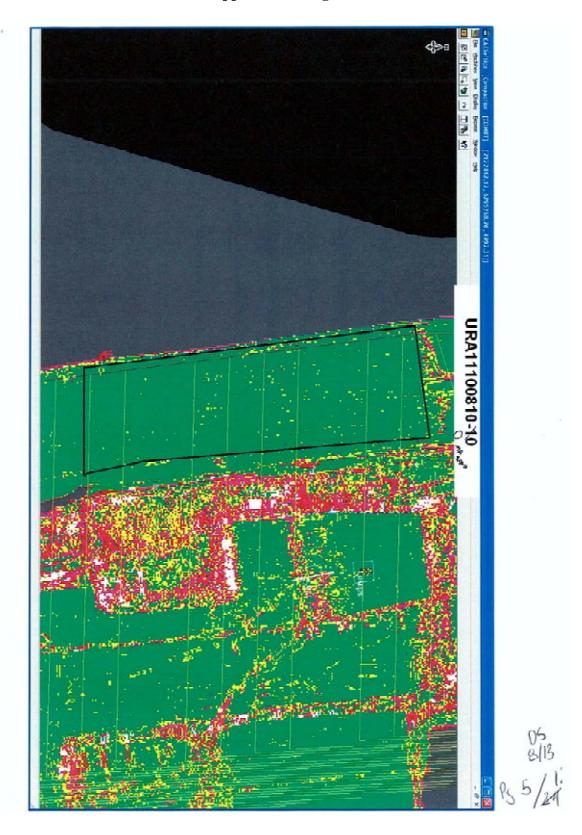
Total Lines	14995		10.5			3
	46	Lift ID:	URA11100810-00			
Northing	Easting	Elevation	# of Passes	Passes =6	Count	
6795366	2122087	4995.1	6	1	1	Lift Height
6795370	2122087	4995.1	6	1	1	1' 0"
6795373	2122087	4995.2	6	1	1	
6795376	2122087	4995.2	6	1	1	Thick Lift Threshold
6795337	2122090	4994.6	6	1	1	2. 0
6795340	2122090	4994.8	6	1	1	
6795343	2122090	4994.9	6	1	1	Last Lift Elevation
6795347	2122090	4995.0	6	1	1	N/A
6795350	2122090	4995.1	6	1	1	
6795353	2122090	4995.2	6	1	1	Min. # of Wheel Passes
6795357	2122090	4995.3	6	1	1	6
6795360	2122090	4995.4	6	1	1	
6795363	2122090	4995.4	6	1	1	
6795366	2122090	4995.4	6	1	1	
6795370	2122090	4995.5	6	1	1	
6795373	2122090	4995.6	6	1	1	
6795376	2122090	4995.6	6	1	1	
6795380	2122090	4995.7	6	1	1	
6795298	2122093	4993.7	6	1	1	
6795301	2122093	4993.8	6	1	1	
6795304	2122093	4993.9	6	1	1	
6795307	2122093	4994.1	6	1	1	
6795311	2122093	4994.2	6	1	1	
6795314	2122093	4994.3	6	1	1	
6795317	2122093	4994.4	6	1	1	
6795320	2122093	4994.5	6	1	1	
6795324	2122093	4994.6	6	1	1	
6795327	2122093	4994.6	6	1	1	
6795330	2122093	4994.7	6	1	1	
6795334	2122093	4994.8	6	1	1	
6795337	2122093	4994.9	6	1	1	
6795340	2122093	4995.0	6	1	1	
6795343	2122093	4995.1	6	1	1	
6795347	2122093	4995.1	6	1	1	
6795350	2122093	4995.3	6	1	1	
6795353	2122093	4995.4	6	1	1	
6795357	_		6	1	1	
6795360	2122093	4995.5 4995.6	6	1	1	
	2122093	4995.6	6	1	1	
6795363 6795366	2122093		6	1	1	
		4995.6				
6795370	2122093	4995.7	6	1	1	
6795373	2122093	4995.8	6	1	1	
6795376	2122093	4995.8	6	1	1	
D/505 3803	1 21221013	4995			7 1	

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6795380

4996.3

2122093





FIELD DENSITY TEST

PROJECT: Moab UN	ATRA Project	ОТ	HER
LIFT IDENTIFICATION:	URA11100810-00	DATE:	8/10/2010
TEST ID NUMBER(S):		#1	
TEST LOCATION: 679			D1556XD6938
ASTM D6938 (DENSITY D			DENSITY DETERMINATION)
Make/Model 3430 Gas	age Serial # 27523	Testing Apparatus	Calibrated Vol. (lbs/fi3)
Last Calibration Date: 8/2	NAME OF THE OWNER OWNER OF THE OWNER OWNE		g/cm ³
Daily Standard Counts: Off-Cell Standard			Cone & Plate (M ₂)
Density 2217 N	Anistone 666	100 CONTRACTOR	
		Mass of bottle &	cone before filling
Method A (Direct Tri Depth Setting 8 (inches)		Mass of bottle &	cone, plate & hole g
Depart Sering		300000000000000000000000000000000000000	cone, plate & hole g
Moisture Count 171	Density Count 935	7.6.59900	of sand to fill cone
Vet Density (p _m) 137.8 (lbs/ft ²) 1	Des Daneits 123.2 (he/fi	2.01	of sand to fill hole
131.8 (way)	717 LPCHSHY 123.2 (108/JI		et soil container g
Moisture Density 14.7 (lbs/fi ³)	Moisture Fraction 11.9 /5	127	/.
1700 (1707)	110 (Mass of Container g
IOISTURE DETERMINATION		Mas	s of wet soil (M ₃)
ASTM D46	543		Test Hole Volume
Container ID D3		/'	$V = (M_1 - M_2) / \rho_1 cm$
Mass of container & wet specimen			Dry Mass of soil
(M _{cms})	384.0 g	$M_4 = 1$	00 M ₃ / (w + 100)g
Mass of container & dry specimen			Wet Denisty
(M_{cds}) Mass of water (M_w)	358.3 g	/ Pm'	= (M ₃ /V) x 62.43lbs. Dry Denisty
$M_w = M_{cont} - M_{col}$	25.7		$\rho_d = M_d / V g/c$
			Dry Unit Weight
Mass of container (M_c)	164.4 g		$\gamma_{d} = \rho_{d} \times 62.43$ lbs.
Mass of dry specimen (M_s)		Vel	lowish in color, mostly consists o
$M_s = M_{cols} - M_c$	193.9 g	Soil Description:	fines.
Moisture content (w)	1,700		Radon Barrier # 3
$w = (M_w / M_s) \times 100$	13.3 %		d Proctor (ASTM D698)
Dry Density $(\rho_{ab} = (100 \text{ x}))$)_)/(100 + w)	Maximum Dry De	ensity (7 dmax) 118.4 (lbs
pd = (100 x 137.8)/(100 + 1) Note: Wet Density from ASTM D 1556 (p _n) takes	3.3 = 121.7 bs/ft*	Optimum N	foisture (w opt)13.2(%
The state of the s	**************************************	Required Moisture:	
Percent Compaction = p_d	/ γ _d max x 100	117777	
121.7 / 118.4 x 100 =	102.8 %	Required Percer	nt Compaction: 95.0 (%
omments:		TEST RESULTS:	
his test area had higher compaction r		s a X Pass	Date: 8/10/
ul route during placement. Microwa IGH. Initial time setting of 3 minutes		Failed Moi	isture
rying periods of 1 minute until a chan	[점점하기 : [1] 이 맛이 하면 되었다. [2] [2] [4] [4] [4] [4] [4] [4] [4] [4] [4] [4	Failed Con	npaction Time: 141
itial wet mass of the soil.		By: Kyler Edgehor	
25462		(print)	(itypethure)
	8-17-2010		
QA/QC APPROVAL	DATE		

U.S. Department of Energy Revision 0 December 2012



FIELD DENSITY TEST

PROJECT: Moab	UMTRA Project		o	THER		
LIFT IDENTIFICATION:	URA11100810-	00	DATE	1	8/10/2	:010
TEST ID NUMBER(S):			# 2	250-		75.00
TEST LOCATION:			TEST METHOD:	x D	556	X D6938
ASTM D6938 (DENSITY	DETERMINATION)		ASTM D1556	(DENSI	TY DETE	RMINATION)
Make/Model Troxler 3430 C Last Calibration Date: 8 Daily Standard Counts: Off-Cell Standard Density 2217 Method A (Direct Depth Setting 8 (inches)	27523 27523	-	Testing Apparatus Bulk Density of sand of Mass of Sand to Fill Mass of bottle & Mass of bottle Mass Mass	Ω Ca (p ₁) Cone & & cone, & cone, of soft and plate, & s of sand	1.57 g/ Plate (M ₂) efore filling plate & hol after filling plate & hol to fill cone to hole (M ₁), it to fill hole	ol. (lbs/ft ³) 0.04113 (cm ³ 97.8 bs/ft ³) 1824.6 g g c 6114.6 g g c 2418.7 g c 3695.9 g c 1871.3 g
Moisture Density 16.2 (lbs/ft ³)	Moistura Emotion 141	1961	Mass of	wet soil	& containe	r 2500.0 g
MOISTURE DETERMINATION ASTM D		-1.00		rest H	of containe et soil (M_3) lole Volum $(-M_2)/\rho$	2483.8 g
Mass of container & wet specimen	(2000)		-catecourt		Mass of so	
(M _{cms})		g	$M_d =$	200000000000000000000000000000000000000		2209.0 g
Mass of container & dry specimen (M_{ads})		g			Vet Denisty Vi x 62.4	3 129.8 bs/ft 3
Mass of water (M)		0	Pm		Dry Denist	
$M_w = M_{cone} - M_{cole}$	1	g				1.8 g/cm ³
14					Unit Weigh	
Mass of container (M_c) Mass of dry specimen (M_c)		g				3115.5 lbs/ft ³
$M_s = M_{cds} - M_c$		g	Soil Description:		is color , n	nostly consists of
Moisture content (w)		10				Barrier #3
$w = (M_w / M_z) \times 100$	1000000	96			or (ASTM	
Dry Density $(\rho_{a0} = (100)$	$(x \rho_m)/(100 + w)$		Maximum Dry E	Density (y ₄ max)	118.4 (lbs/ft ³)
$pd = (100 \times 129.8) / (100 + 100.8)$ Note: West Dennity from ASTM D 1536 (p_n) is Percent Compaction = p_n 115.5 / 118.4 x 100 =	12.4 = 115.5 lbs/ aks presidence wer ASTM D 6938 (p _a) / γ _d max x 100	Ji ³		Moisture :: 10.2	: (w _{opt}) _ !_%	13.2 (%)
Comments: dicrowave oven power setting on H ninutes and subsequent incremental change of 0.1 % or less of the initia	drying periods of 1 minute	3081	TEST RESULTS: X Pass Failed Me Failed Co By: Kyler Edgehe (print)	ompactio	Jel.	Date: 8/10/10 Time: 1425 (xigntlive)
not my	8.17.2010					
QA/QC APPROVAL	DATE					
Density Testing DOE-EM/GJRAC1783 Rev. 0						QC-F-002 le Index No. 43.8.2 Page of 24 12

U.S. Department of Energy Revision 0 December 2012



FIELD DENSITY TEST

PROJECT: Moab UMT	RA Project		U.		
LIFT IDENTIFICATION:	URA111008	10-00	DATE	8/1	0/2010
TEST ID NUMBER(S):			#3		
TEST LOCATION: 67946			TEST METHOD:	D1556	X D6938
ASTM D6938 (DENSITY DET		_	ASTM D1556 (DENSITY DE	TERMINATION)
Make/Model Troxler 3430 Gauge	Serial # 27523		Testing Apparatus	Calibrated	Vol. (lbs/ft 3)
Last Calibration Date: 8/21/1		_	Bulk Density of sand		
Daily Standard Counts: Off-Cell Standard		- 1	Mass of Sand to Fill (AND RESIDENCE OF THE PARTY OF T	
Section 18 1 Control of the Section Control o		- 1			
Density 2217 Moi			Mass of bottle &		
Method A (Direct Trans		utre)	Mass of bottle	cone, plate & & cone after fi	
Depth Setting 8 (inches) Co	ant time_1_(min	utes)		cone, plate &	hole g
Moisture Count 190 D	ensity Count1062	2		of sand to fill c	
	D	m with		plate, & holo	
/et Density (ρ _m) 132.8 (lbs/ft ³) Dry	Density	(ibs/ji)		of sand to file vet soil & conta	A —
Moisture Density 16.5 (lbs/ft ³) Mo	dature Fraction 14	2 (96)	iviass of v	/	
violature Density 10.5 (10a)1 / 1010	and traction 14.	(70)		Mass of conta	iner g
IOISTURE DETERMINATION			Ma	ss of wet soil (1	(1 ₁) g
ASTM D4643				Test Hole Vol	
Container ID D-1			/	$V = (M_1 - M_2)$	/p1cm
Mass of container & wet specimen		\neg	/	Dry Mass of	soil
(M cms)	380.0	g	/M,-	$100 M_{\rm J}/(w + 1)$	100)g
Mass of container & dry specimen			/	Wet Der	
(M ch)	356.7	g	/ P-	$= (M_J/V) \times 6$	
Mass of water (M_w) $M_w = M_{cmr} - M_{cdr}$	23.3	g	/	Dry De	nisty , / Vg/c
M w M cmr M chr	2010	-8		Dry Unit We	
Mass of container (Mc)	164.4	g	/	$\gamma_d = \rho_d \times 6$	100000 NOON
Mass of dry specimen (M _s)	5000	7 f			r, mostly consists
$M_s = M_{cds} - M_c$	192.3	g	Soil Description:		
Moisture content (w) $w = (M_w / M_s) \times 100$					on Barrier #3
W - (M # / M 1) X 100	12.1	96	Standa	rd Proctor (AS)	M D698)
Dry Density $(\rho_{d0} = (100 \times \rho_{m0}))$)/(100 + w)		Maximum Dry D	ensity (7 amax)	118.4(lbs
pd = (100 x 132.8)/(100+ 12.1	/ = 118.4	lhe/ft ³	Ontinum 2	doisture (w.)	13.2 (%
Note: Wet Density from ASTM D 1556 (p.,) takes pro	ridance over ASIM D 6938 ((a.)	Opanium i	violature (in apr)	15.2
			Required Moisture	10.2 %	to 16.2
Percent Compaction = ρ_d /					
118.4 / 118.4 x 100 =	100.0 %		Required Perce	nt Compaction	95.0 (%
omments:	100000000000000000000000000000000000000		TEST RESULTS:		
licrowave oven power setting on HIGH. inutes and subsequent incremental dryi			X Puss	20010	Date: 8/10/
change of 0.1 % or less of the initial we		ute until	Failed Mo		
			Failed Co	N	Time: 145
			By: Kyler Edgeho	use /	(signethre)
2 = 4 4 - 1	1000000		grad)		in Staling at
QA/QC APPROVAL	8/7-2010 DATE				
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