



U.S. DEPARTMENT OF
ENERGY

Office of
ENERGY EFFICIENCY &
RENEWABLE ENERGY

FAST Forward: The FAST PSH Commissioning Prize Winning Concepts

A WPTO R&D Deep Dive Webinar

Welcome!

WPTO R&D Deep Dive Webinar Series

A look into the ongoing work of WPTO sponsored projects and program areas

November R&D Deep Dive Webinar:

Highlights of the Hydropower Licensing Report

Thursday, November 18, 1 – 2 p.m. ET

Logistics & Format

- Three FAST Prize winners will present
- Each presentation will be followed up with questions from the panelists
- This webinar will be recorded and made available to registrants
- Attendees' microphones are muted and attendees are not visible on video
- If you have technical issues, contact Megan Lennox

Thank you for participating!

Pumped-Storage Hydropower FAST Prize

PSH provides:

- large-scale electrical system reserve capacity,
- contributes to grid reliability, and
- supports supply-demand balancing with quick response capabilities and

New PSH development has stalled due to:

- *Difficulty* associated with benefit quantification
- *Significant* upfront capital costs and long commissioning times

DOE WPTO initiated the **Pumped-Storage Hydropower FAST Commissioning** solutions for reducing the cost, risk, and timeline associated with PSH development.

The **FAST Prize** culminated in Fall 2019 with a shark-tank style pitch contest share of the \$550k cash and in-kind pool.



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& RENEWABLE ENERGY
WATER POWER TECHNOLOGIES OFFICE

NREL
Transforming ENERGY



Hydropower Prize Request for Information

Help shape future hydropower prizes!

The National Renewable Energy Laboratory is seeking feedback from members of the hydropower industry, academia, research laboratories, and government agencies, as well as other stakeholders, to help identify opportunities for refining future hydropower prizes.

Please respond to the request for information at this link:

<https://www.nrel.gov/water/market-acceleration.html>





Jay Anders, Chief Operating
Officer, EPC Projects at Rye
Development



Carl Borgquist, CEO and President,
Absaroka Energy



Erin Foraker, Hydropower and
Renewable Energy Research
Coordinator, Bureau of Reclamation



Michael Manwaring, Executive
Vice President, McMillen Jacobs
Associates



Debbie Mursch,
Director Business
Development,
GE Renewable Energy

Tom Elderedge and Hector Medina

Liberty University

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WATER POWER TECHNOLOGIES OFFICE



Hybrid Modular Closed-Loop Scalable Pumped Storage (hydroelectric & solar)

Progress on Analysis, Modeling and Experimentation

Dr. Hector Medina and Dr. Thomas Eldredge

Speakers and Introduction



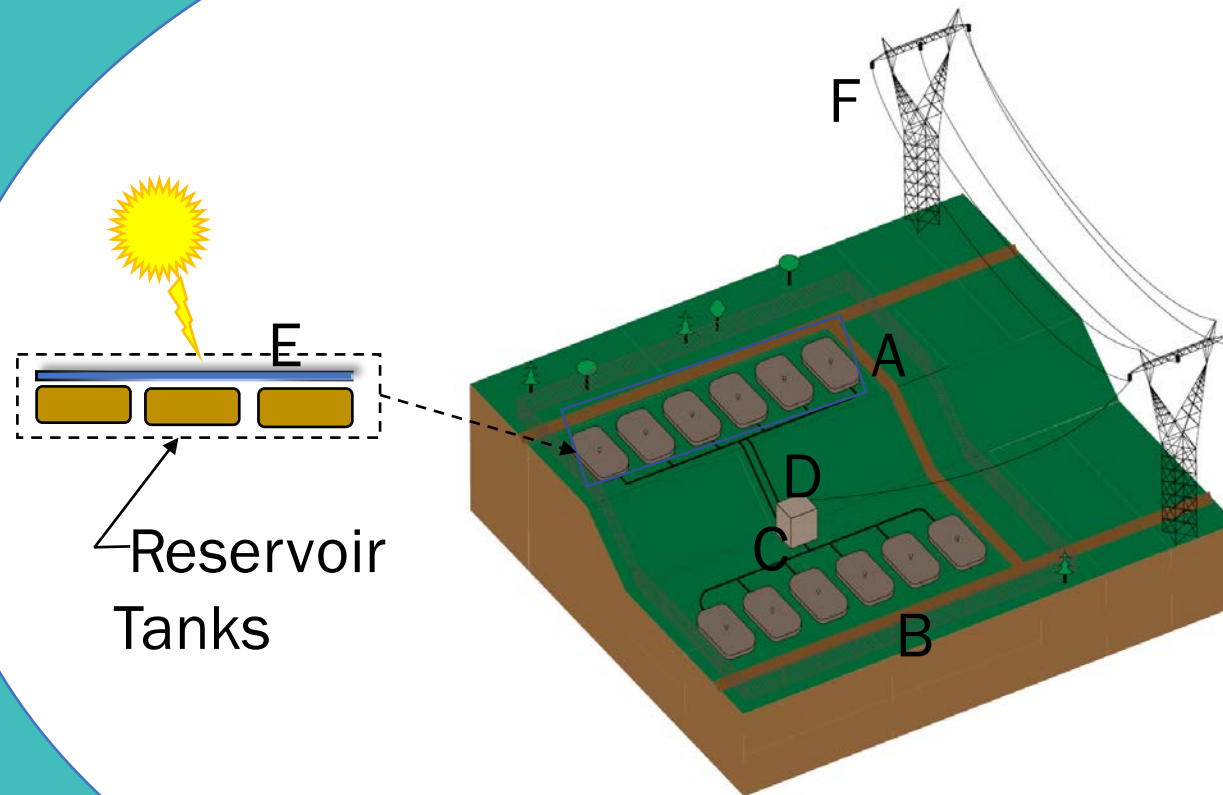
Dr. Hector Medina is a Professor and Director of the Mechanical Engineering Program in the School of Engineering at Liberty University. He teaches Mechatronics and Dynamic System Modeling. His research interests include energy systems, controls of intelligent systems, bio-inspired multi-functional materials, and surface engineering. Prior to working at LU, he worked in LWD/MWD systems in the oil industry as well as RF radio systems and high school teaching.



Dr. Tom Eldredge has a Ph.D. degree in mechanical engineering from the University of Tennessee. He is a licensed professional engineer in Connecticut. He has over 25 years of experience in various aspects of the power generation industry. Presently he is an Associate Professor of mechanical engineering at Liberty University.

Overview of the technology

- *Hybrid PSH-Solar: combined renewable energy with innovative PSH system*
- *Modular components*
- *Closed Loop: does not rely on natural bodies of water*
- *Scalable (1- 10+ MW)*

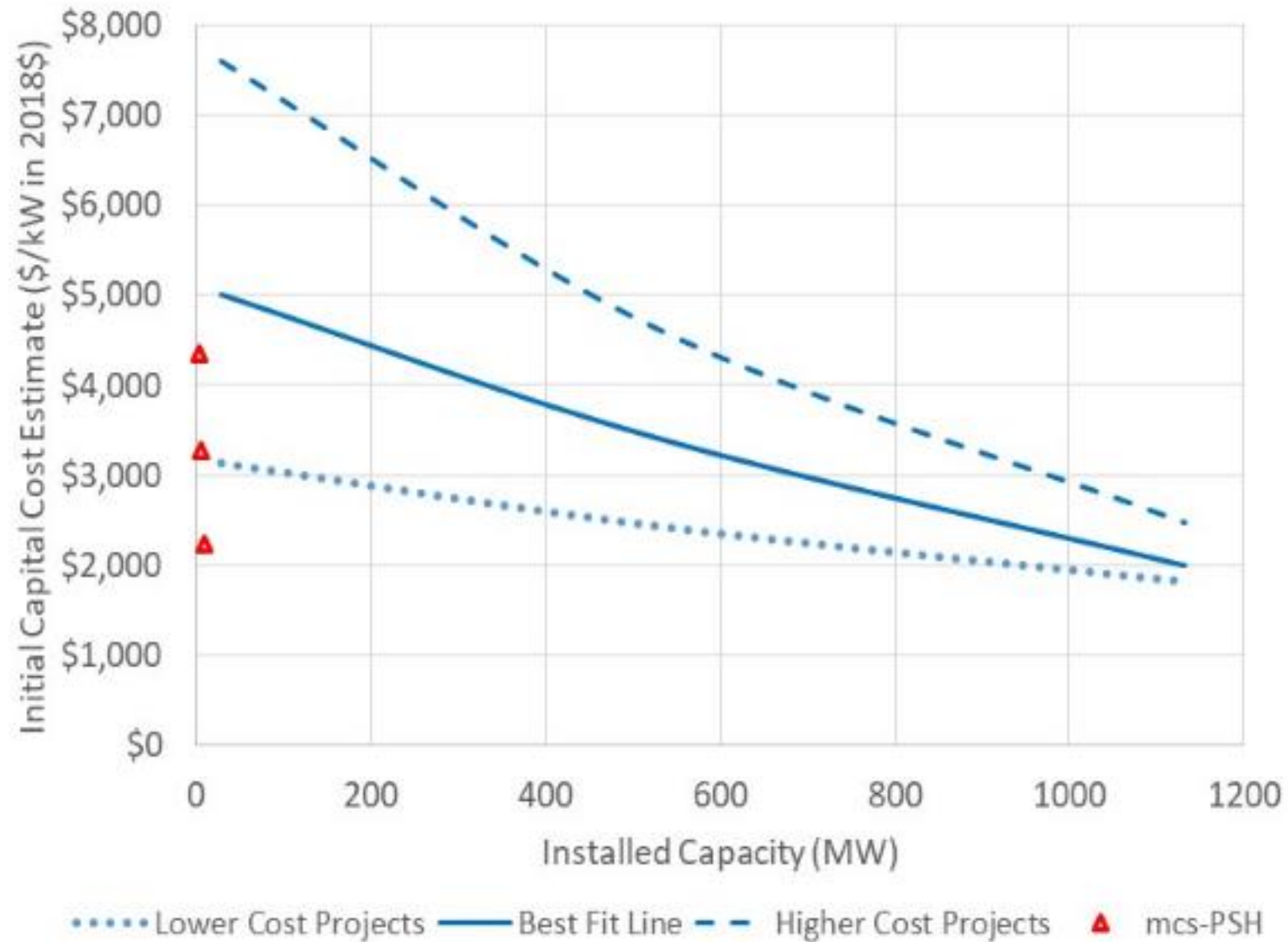


A= Upper reservoir
B = Lower reservoir
C= Powerhouse (well pump)
D = Penstock
E = Solar panels
F = Transmission lines



Cost and Market Analyses

Comparison of initial capital cost estimate (\$/kW) of current versus traditional PSH projects

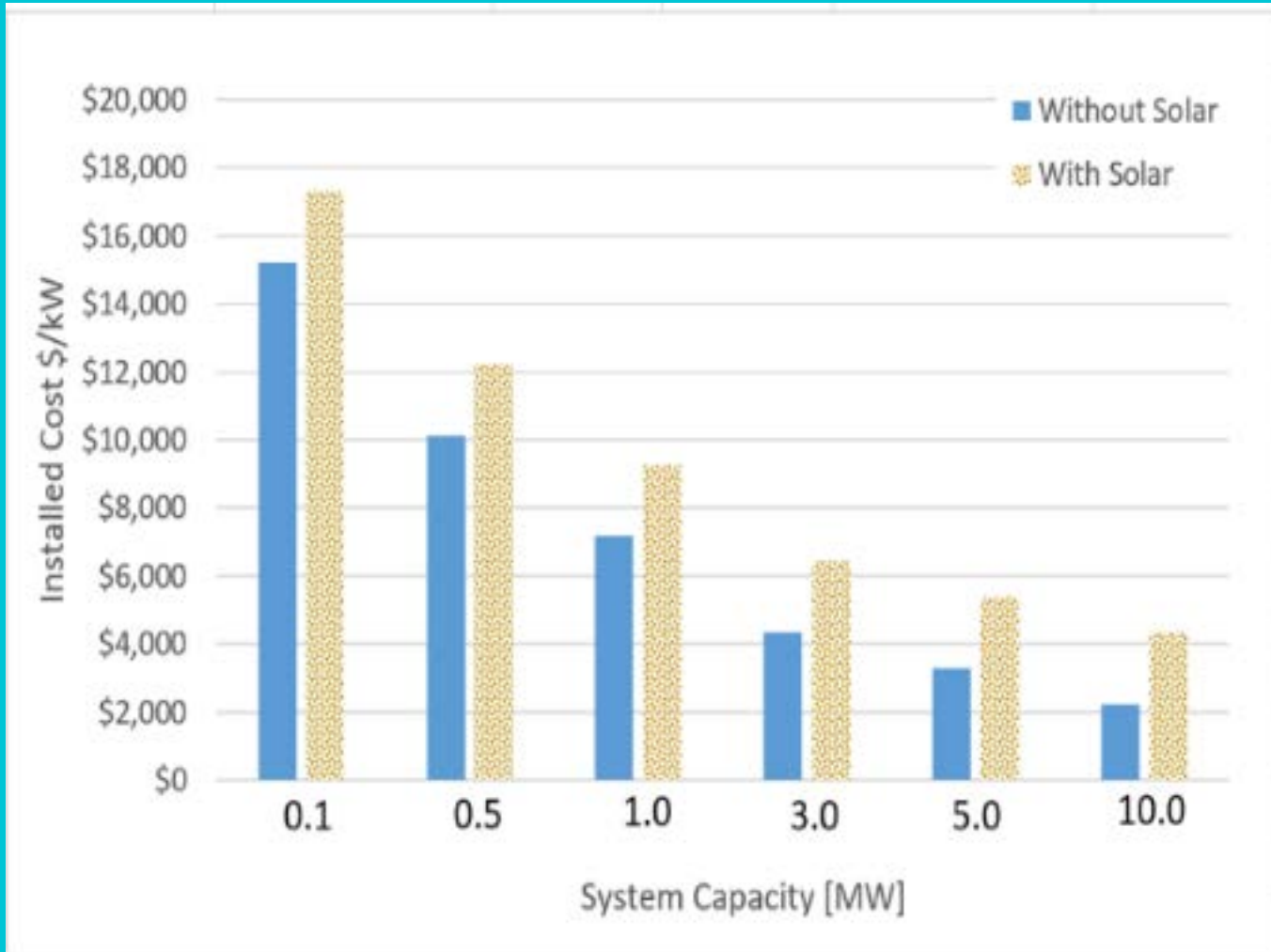


*Dollar value is based on year 2018.
Source: A. Witt, B. Hadjerioua, N. Bishop, and R. Uria, "Evaluation of the Feasibility and Viability of Modular Pumped Storage Hydro (m-PSH) in the United States" Oak Ridge National Laboratory, Oak Ridge, Tennessee, September 2015.*

COMPARE OVERALL SYSTEM COSTS (with & without solar)

Key Points

- Incremental solar costs increase for higher system capacities
- The solar compensates for RTE losses.



Tracking vs fixed tilt solar PV

- Single axis tracking improves efficiency ~30% over a fixed tilt system.
- For utility scale (> 2MW) installations single axis tracking and fixed tilt installation costs appear to be within about 4%.
- Conclude that single axis tracking is economically feasible and recommended.

Market Analysis: Modular, Scalable, Hybrid Closed-Loop PSH System (h-mcs-PSH)

LIBERTY UNIV. FAST TEAM: MARKET/SWOT ANALYSIS

Strengths: Modular, scalable closed-loop PSH

- **Modular** design to construct in stages to meet new demand
- Small (1-10MW) plants for **urban & wind/solar co-locations**
- **Minimal water loss** using enclosed bladders as reservoirs
- **No dams needed**, limit excavation to level terrain for bladders
- Construction **cost/time savings** via standardized, prefab parts
- **Minimal environmental impacts** during construction/operation

Weaknesses: Lower economies of scale

- **Lower economies of scale** with smaller PSH plants
- **Capital cost** estimates ~\$7,160/kW(1MW) to \$2,235/kW(10 MW) vs. generic PSH (500MW) range of \$2,053-\$2,235/kW
- **Uncertain durability of bladders**, estimated plant life of 20 yrs. (2-3x shorter than conventional PSH plants, but longer than 13.7 yrs. estimate for lithium-ion batteries)

Modular, Scalable, Hybrid Closed-Loop PSH System (h-mcs-PSH)

Opportunities: Multiple locations & users

- **Build near** urban demand centers, industrial & renewable sites
- Use by paper, plastics & other **power-intensive** industries
- Contribute to **grid flexibility** as demand response solution
- Distributed energy storage resource for connected, multiple-building **campuses & small island/remote systems**

Threats: Delays & advances by competitors

- **Uncertain regulatory** response to using polymeric bladders
- **Need pilot plant** to determine costs, timing, commissioning
- Installed PSH costs for 10-hr duration storage is < batteries in 2020, but battery advances **lowers** PSH cost advantage by 2030



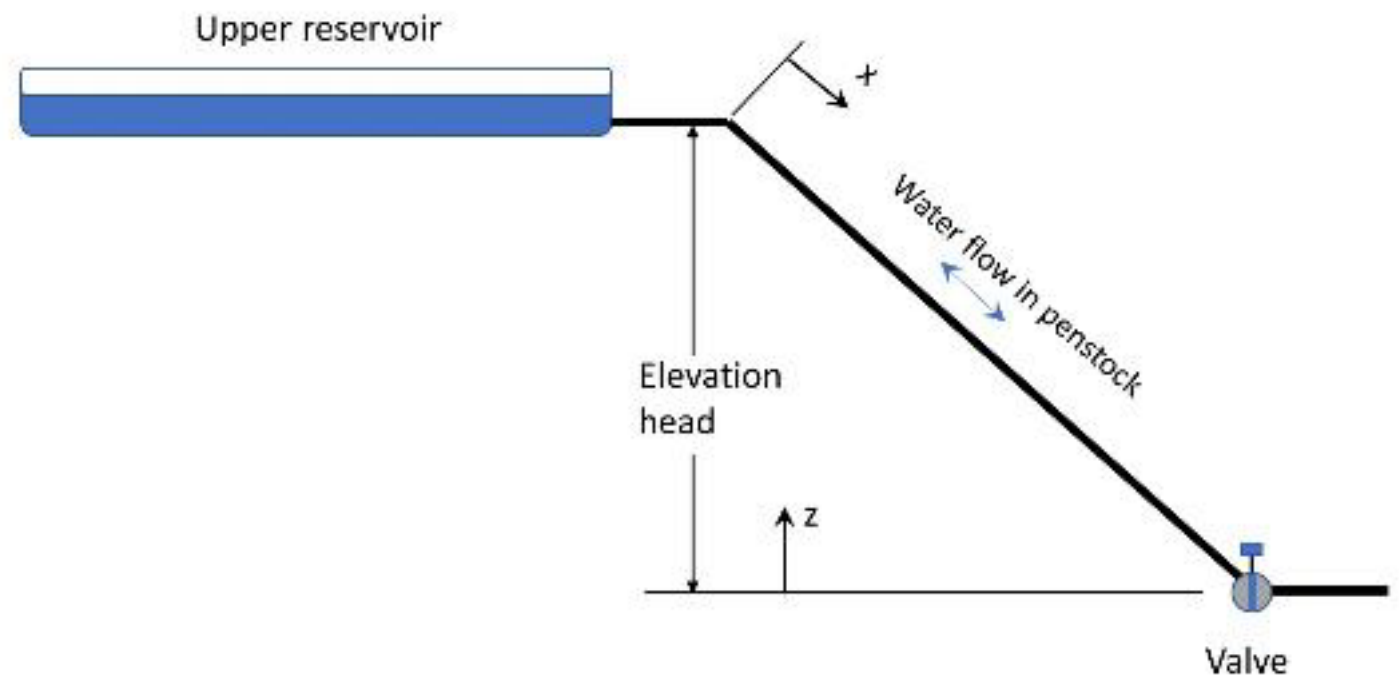
Penstock Analysis

Water Hammer Analysis

The 1D water hammer analysis was conducted by solving the Euler equation of motion and the continuity equation, as shown:

Continuity equation: $a^2 \frac{\partial v}{\partial x} + \frac{1}{\rho} \frac{\partial \rho}{\partial t} = 0$

Euler's equation of motion: $\frac{\partial v}{\partial t} + \frac{1}{\rho} \frac{\partial p}{\partial x} + g \frac{dz}{dx} + \frac{f}{2D} v|v| = 0$

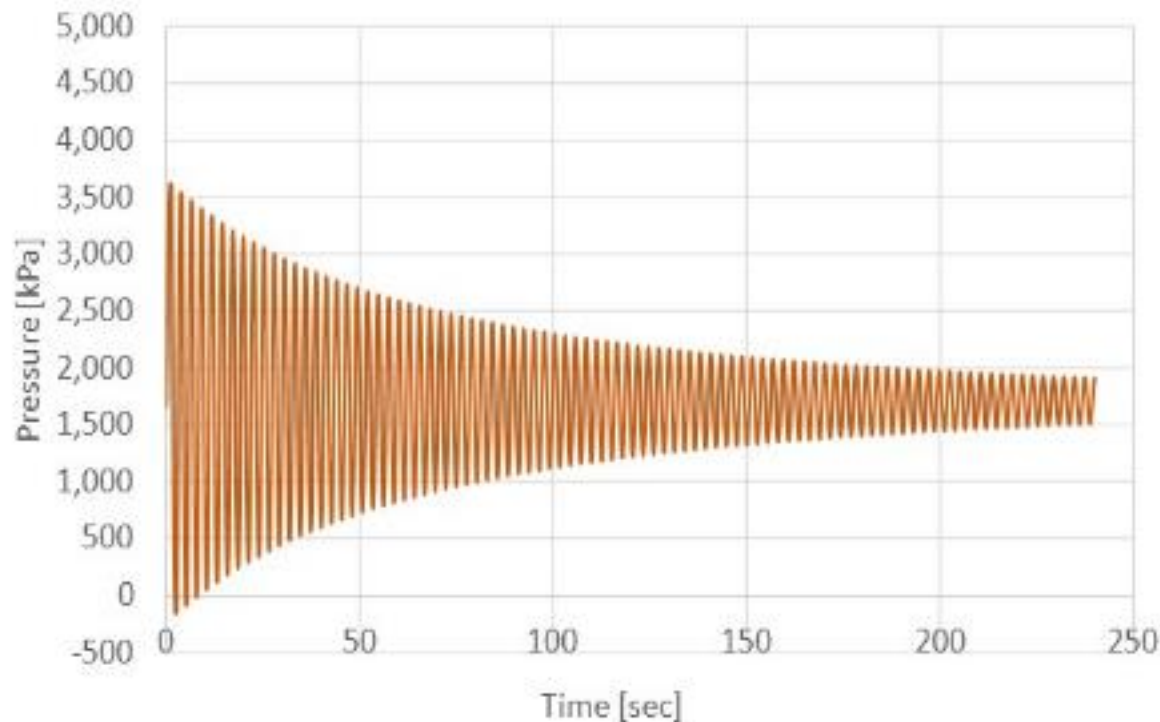


Water Hammer HDPE vs Steel

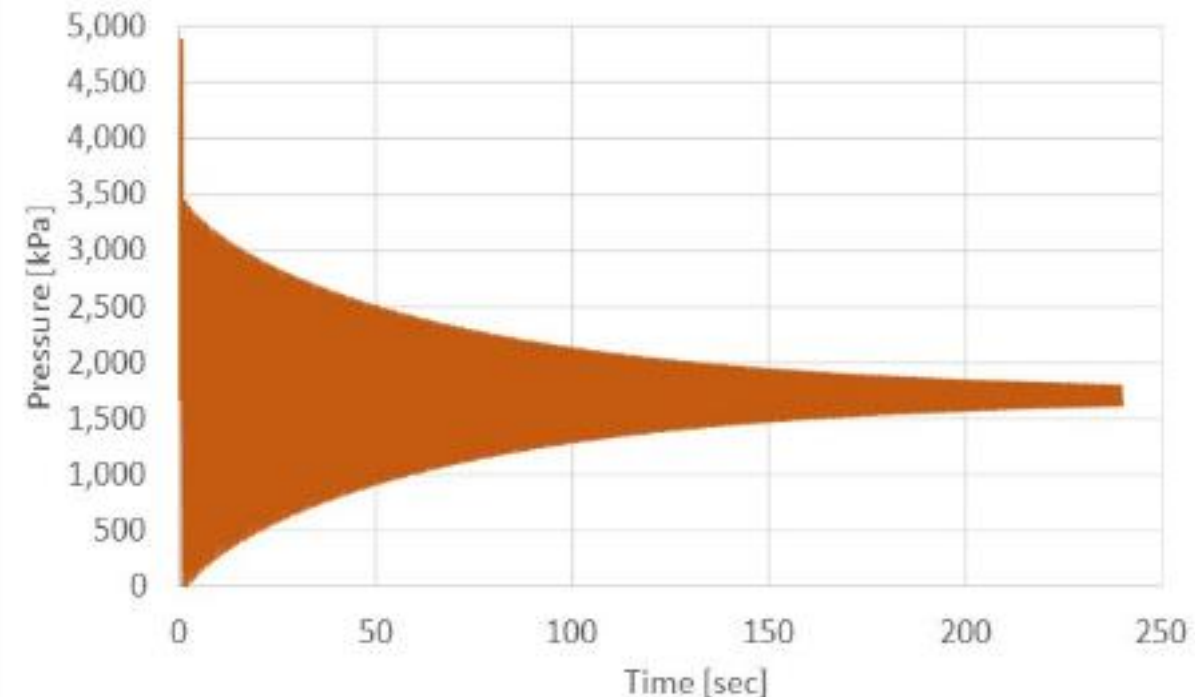
Key Points

- HDPE exhibits excellent fatigue characteristics.
- The HDPE pipe absorbs more energy than steel from cyclic loading.
- Pressure fluctuation frequency is ~3 times less than for steel.

x = 145 (HDPE)



x = 245 (Steel)



FEA and fatigue analysis on HDPE and steel near valve

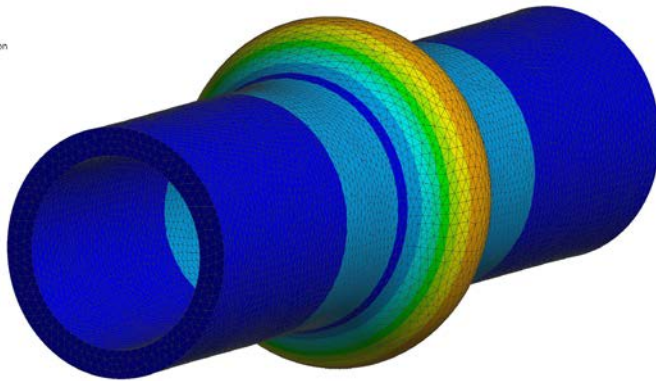
Key Point: HDPE it was found a theoretical infinite life for the cyclic loading assuming continuous opening/closing at 1 sec.

Deformation

HDPE

Dr: Polymer 1 1ft
Total Deformation
Type: Total Deformation
Unit: m
Time: 1
9/14/2019 2:49 PM

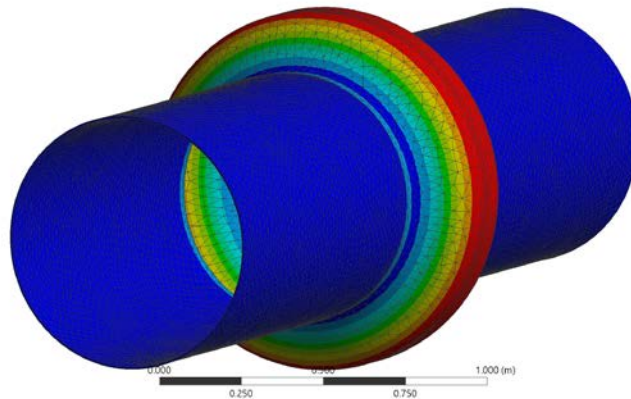
0.0042425 Max
0.0037711
0.0032997
0.0028283
0.002357
0.0018856
0.0014142
0.00094278
0.00047139
0 Min



Steel

A: Steel 1ft
Total Deformation
Type: Total Deformation
Unit: m
Time: 1
9/14/2019 2:41 PM

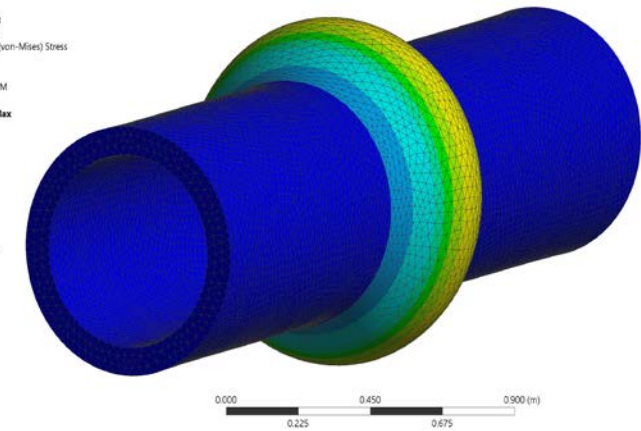
0.00060113 Max
0.00053433
0.00046754
0.00040075
0.00033396
0.00026717
0.00020038
0.00013358
6.6792e-5
0 Min



Stress

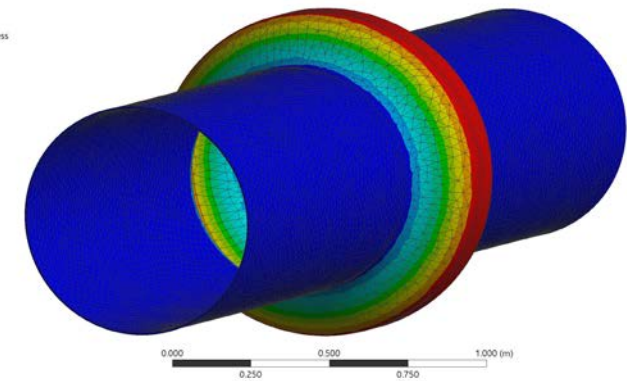
Dr: Polymer 1 1ft
Equivalent Stress
Type: Equivalent (von-Mises) Stress
Unit: Pa
Time: 1
9/14/2019 2:48 PM

1.4667e7 Max
1.3043e7
1.142e7
9.7961e6
8.1724e6
6.5487e6
4.9251e6
3.3014e6
1.6777e6
54068 Min



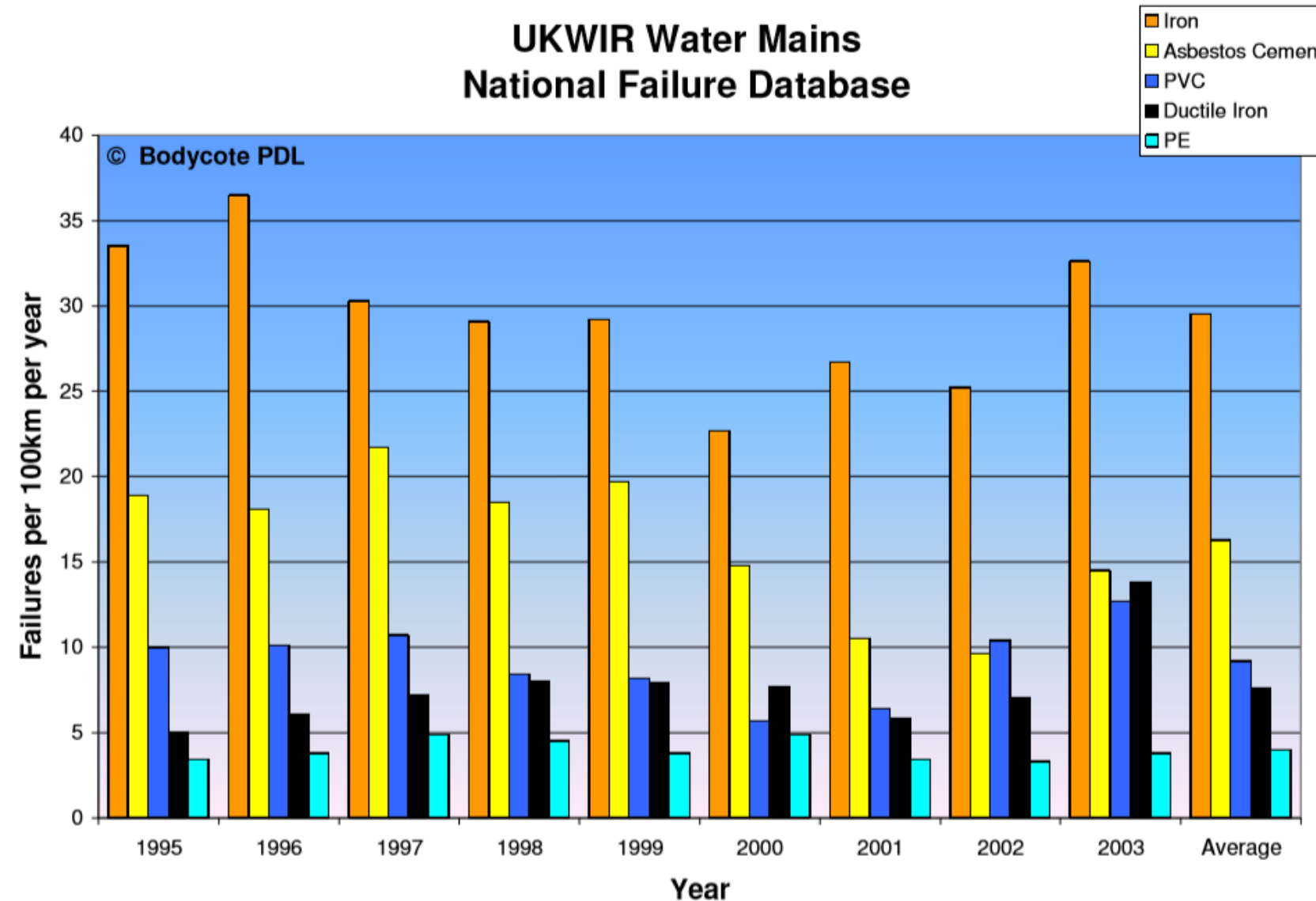
A: Steel 1ft
Equivalent Stress
Type: Equivalent (von-Mises) Stress
Unit: Pa
Time: 1
9/14/2019 2:42 PM

3.3406e8 Max
2.9718e8
2.603e8
2.2343e8
1.8655e8
1.4967e8
1.129e8
7.5918e7
3.9041e7
2.1647e6 Min



Benefits of HDPE Pipe

Figure from: MacKellar and Bodycote 2006



- *Lower pipe material cost than for steel and ductile iron.*
- *Installation costs lower than for steel and ductile iron.*
- *Data shows that installation is a safer process (fewer injuries)*
- *Connections less problematic*
 - *50 ft pipe lengths*
 - *Heat fusion joints (strong as pipe)*
- *HDPE has excellent fatigue characteristics*
- *Excellent hydraulic characteristics (low Manning coefficient)*
- *Not subject to corrosion or bio-fouling*

Extended FSI (fluid structure interaction) modeling of the penstock is being conducted with ORNL

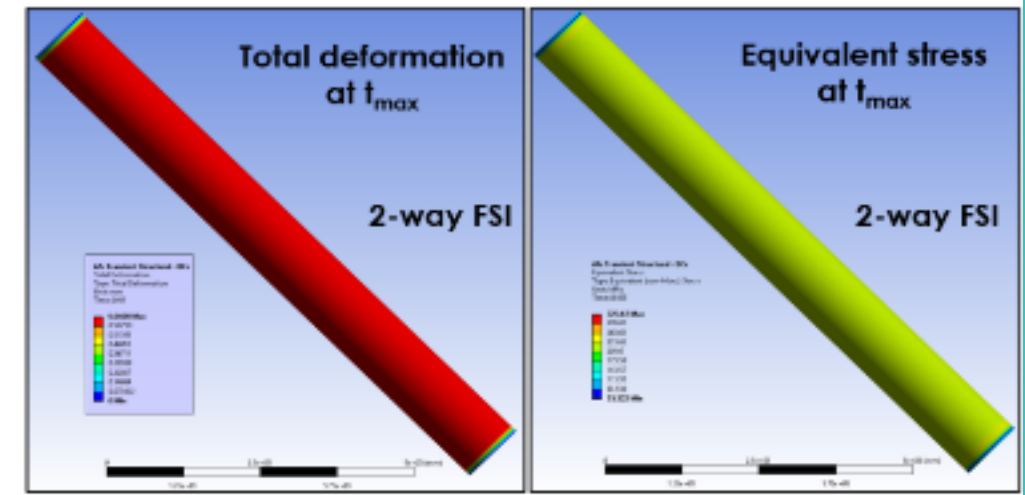
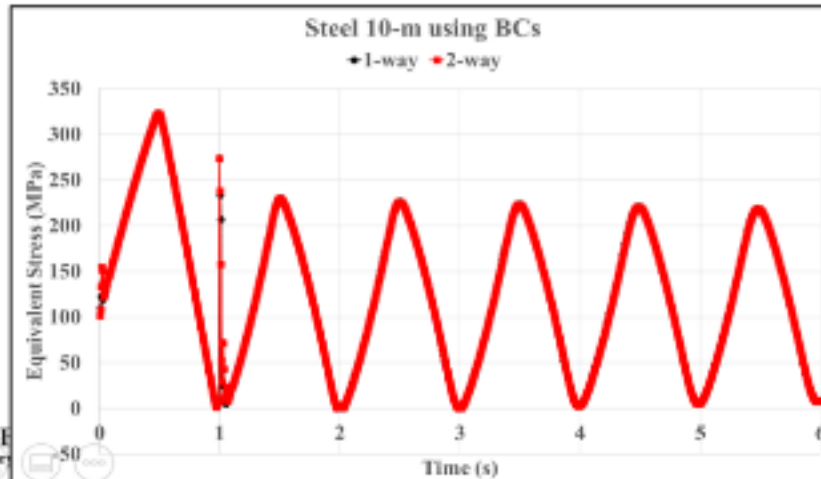
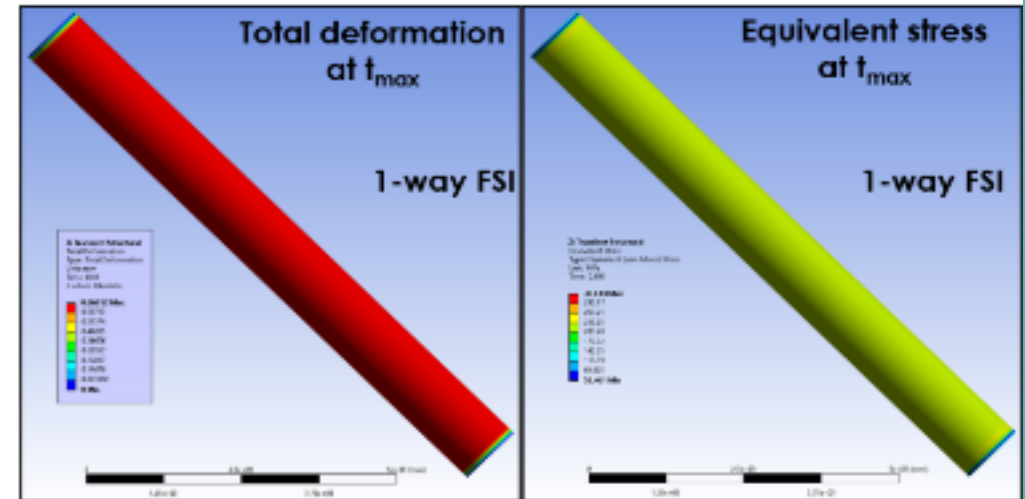
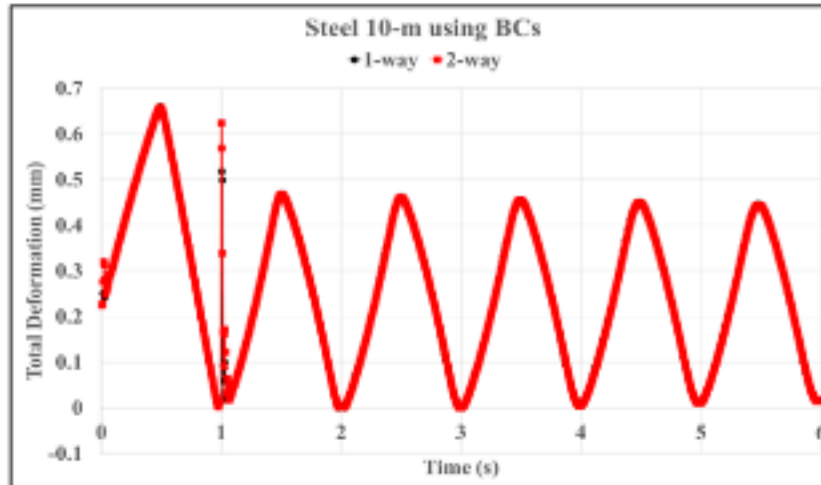
1. **Modal analysis of the pipes** with different lengths, ($L = 10\text{ m}$, 15 m , and 25 m), and different materials (available in Ansys materials database)
 - Steel
 - Cast iron and Gray Cast iron
 - HDPE
 - PVC
2. **One-way FSI** for different lengths $L = 10\text{ m}$, 15 m , and 25 m and materials
 - Steel
 - Cast iron and Gray Cast iron
 - HDPE
 - PVC
3. **Two-way FSI** for different lengths $L = 10\text{ m}$, 15 m , and 25 m and materials
 - Steel
 - Cast iron and Gray Cast iron
 - HDPE
 - PVC
4. **Refined transient analysis.**
 - Transient fluid calculations and structure analysis using inputs of pressure/velocity from 1D simulations of LU to better simulation the water hammer effect to the pipe.



Work is on-going

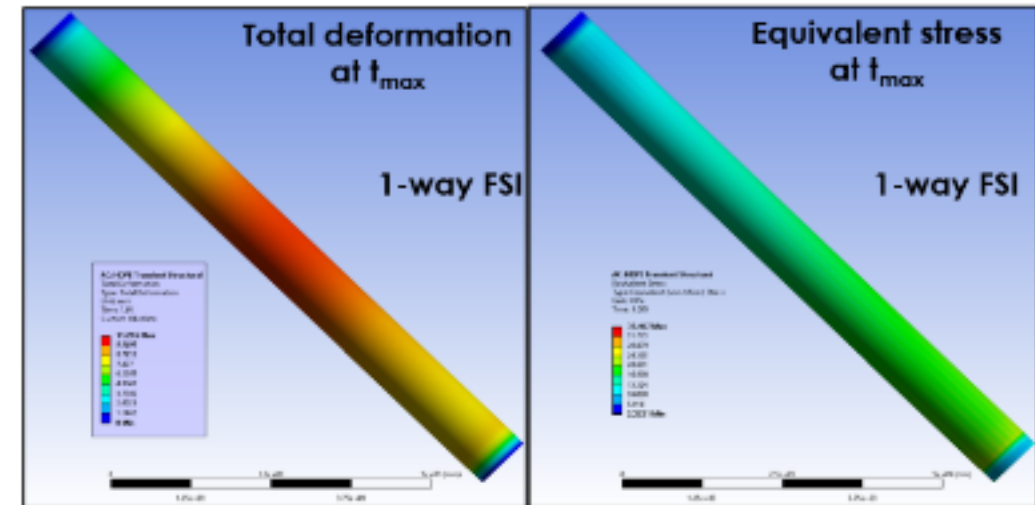
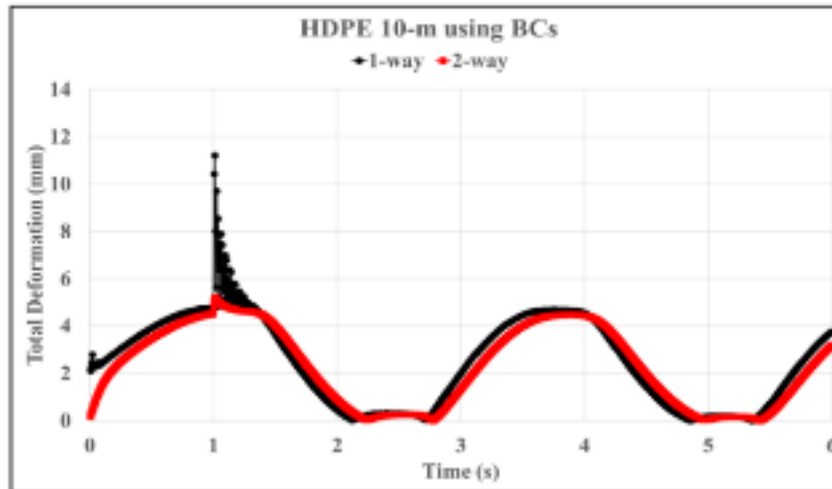
FSI calculations for 10m steel pipe showing equivalent stress and total deformation using 1D inputs for boundary condition

Case 1: 10 m, Structural Steel – Water hammer FSI using Pressure Inputs from 1D code



FSI calculations for 10m HDPE pipe showing equivalent stress and total deformation using 1D inputs for boundary condition

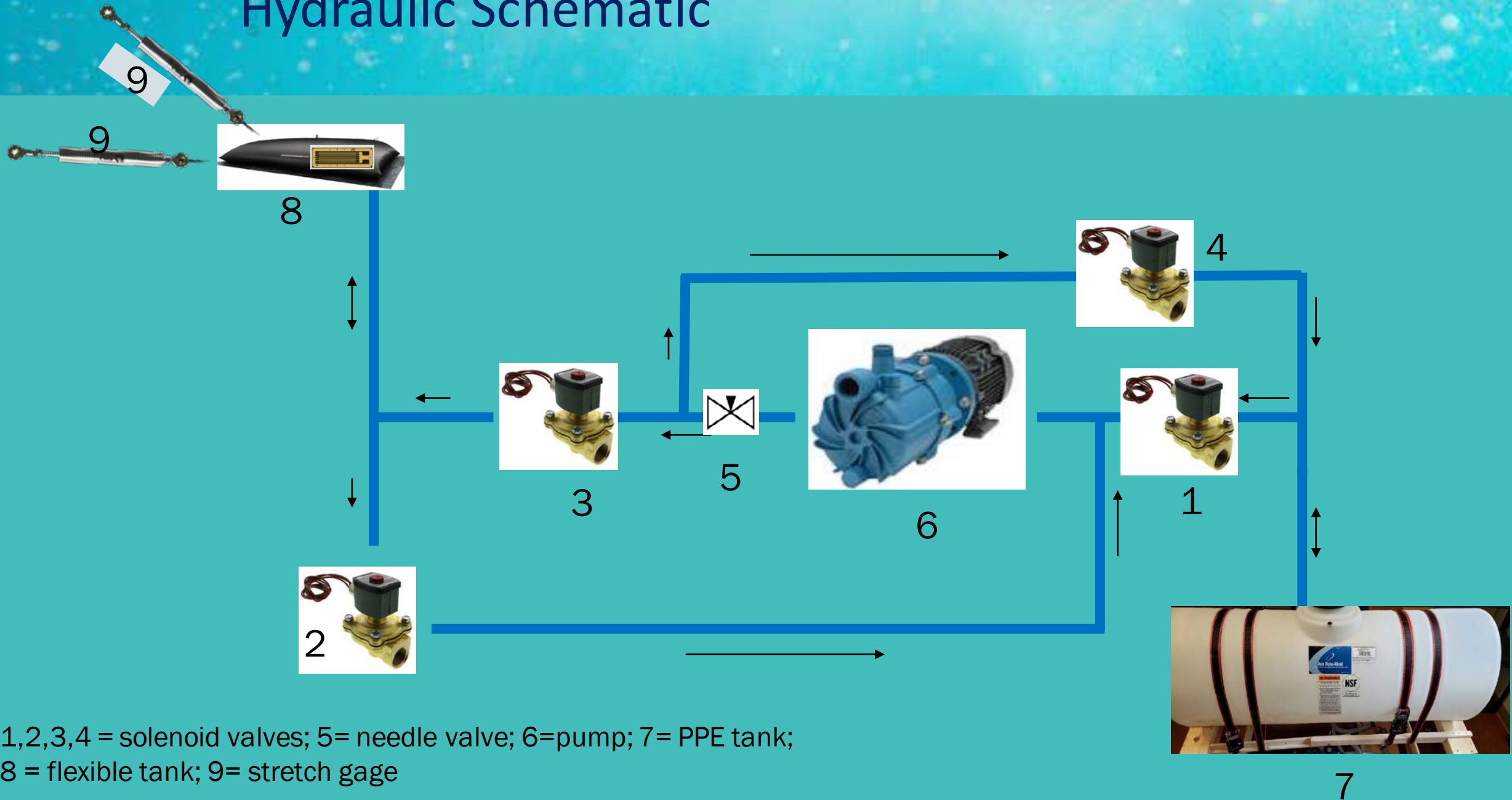
Case 1: 10 m, HDPE – Water hammer FSI using Pressure Inputs from 1D code





Small-scale testing setup

Hydraulic Schematic





Experiment Overview

- Upper reservoir consists of two polyurethane-coated nylon-based bladder tanks
- Lower reservoir is a PPE tank with a SP10 Series Self-Priming pump to pump the water to the bladder tanks
- Cyclic testing will be performed to see durability and efficiency of the system



Scaffolding used to create hydraulic head

- Load capacity to withstand at least 2 times the weight of full bladder tanks.
- Scaffolding assembled to a height of 30 ft.
- Six platforms utilized for safety and to hold the bladders
 - Bladder will be placed on the top level atop three platforms



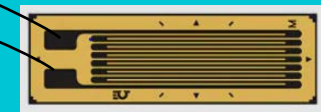
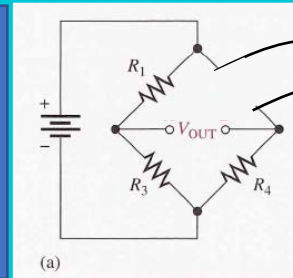
Electrical/Sensor Diagram



Solartron Orbit Network
for Displacement
Transducers

NI 9235 – Strain
Gauge Unit

Bridge
Completion
Module

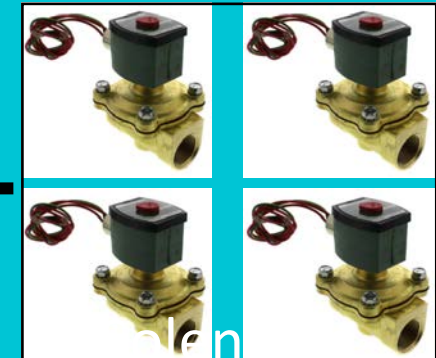


Strain Gauges on
Bladder Tank

cDAQ
General
Purpose
Data
Acquisition
Unit

NI 9428 –
Electromechanical
Relays

Switching 120
VAC to activate
solenoid valves



Controlling Flow
Direction

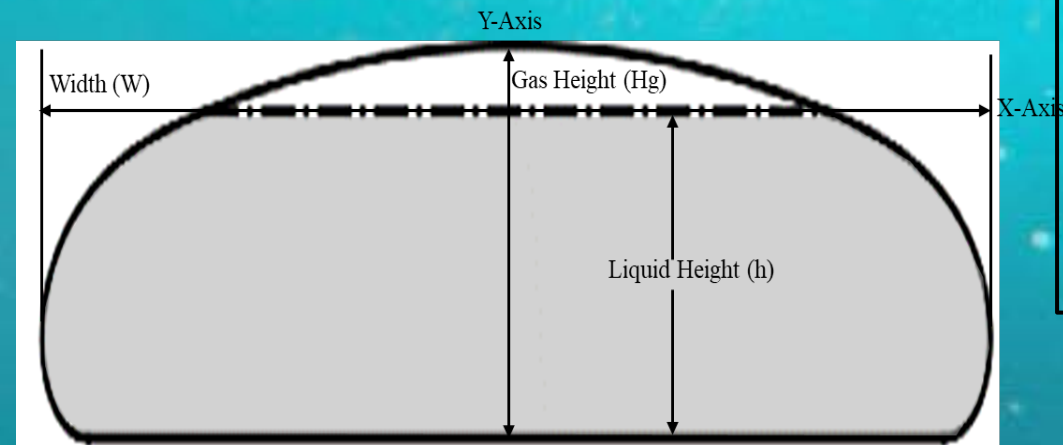


Bladder Tank Membrane Material Analysis

Membrane Stress Modeling(I)

Constituent Equations

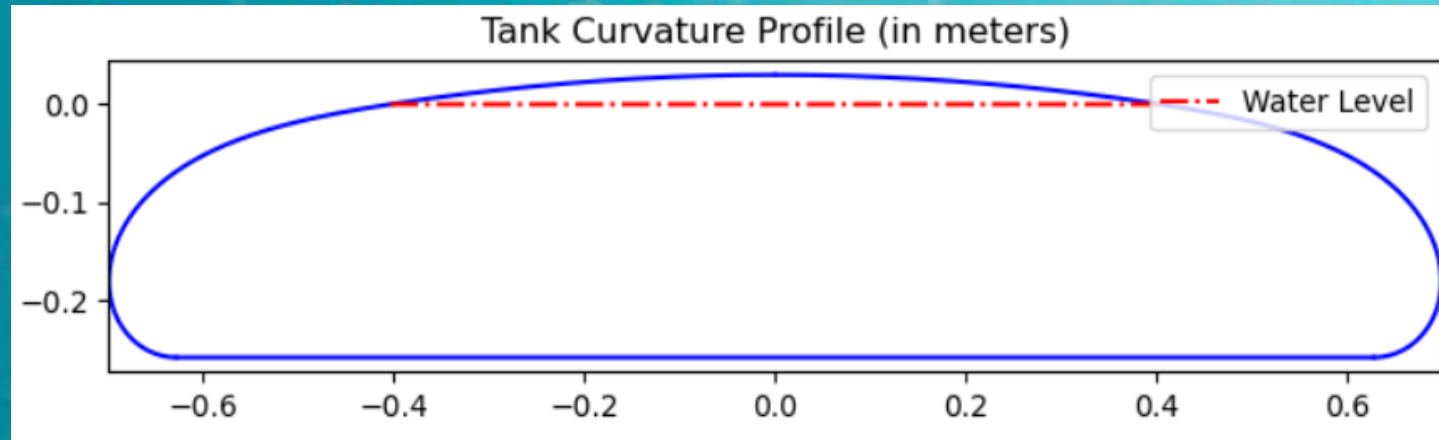
- The numerical model was implemented using MATLAB
 - MATLAB code was altered and converted to Python for use with our membrane bladder tanks
- Nomenclature
 - k- Curvature
 - s- Arc length
 - P_0 - Static pressure above liquid
 - h- y_{liquid} height
 - H_g - Gas height
 - T- Membrane stress force or tension per unit length
 - W- Width of collapsible tank
 - L- Length of collapsible tank



Collapsible tank schematic. The origin is the horizontal surface of the tank on the water surface. (Osadolor et al.)

$$k = \frac{P_0 - y \cdot g \rho}{T}$$
$$y_- = \begin{cases} y, & y \leq 0 \\ 0, & y > 0 \end{cases}$$
$$\begin{cases} \frac{d^2 x}{ds^2} = k \frac{dy}{ds} \\ \frac{d^2 y}{ds^2} = -k \frac{dx}{ds} \end{cases}$$

Membrane Stress Modeling(II)



Flexible Tank PSH

Input tank volume in cubic meters: 0.38

Input tank length in meters: 1.5

Input tank width in meters: 1.4

Input air height in millimeters: 30

Input liquid type: ☒ Water ☐ Gasoline

Calculate

Volume (m³): 0.38

Length (m): 1.5

Width (m): 1.397

Tension per unit length (N/m): 171.88

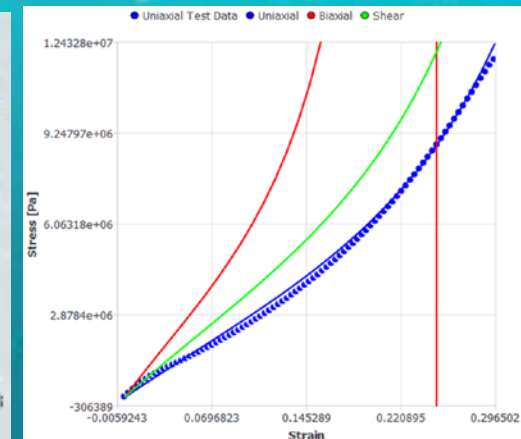
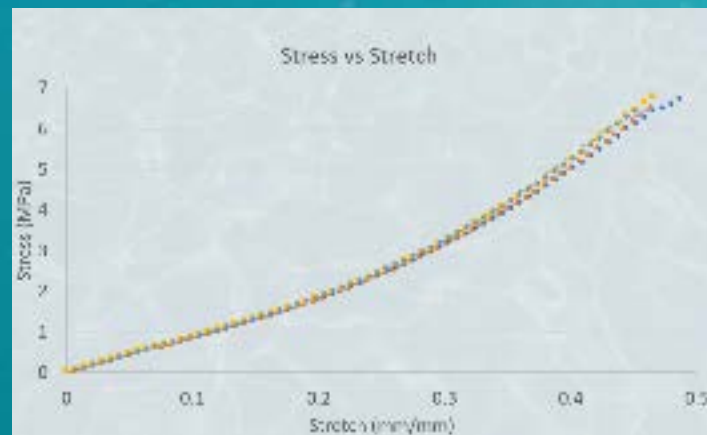
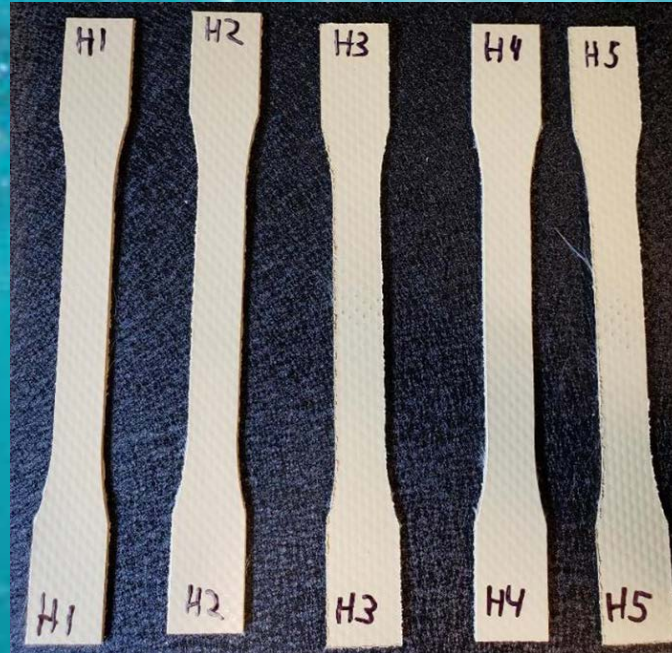
Static pressure (Pa): 62.97

Runtime (s): 15.218

Plot Shape

Membrane Mechanical Testing

- Monotonic
- Creep
- Fatigue
- Hydrolis
- UV-degradation



Panel Questions

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WATER POWER TECHNOLOGIES OFFICE



Doug Spaulding

Nelson Energy and Golder Associates

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& RENEWABLE ENERGY**
WATER POWER TECHNOLOGIES OFFICE

UNDERGROUND PUMPED STORAGE HYDROPOWER (UPSH)



ACKNOWLEDGEMENTS -

- FAST Sponsored Studies-



----- Market Analysis



----- Groundwater Evaluation

CONCEPT OVERVIEW – UPSH USING TBMS

COMPANY

PRODUCTS

SERVICES

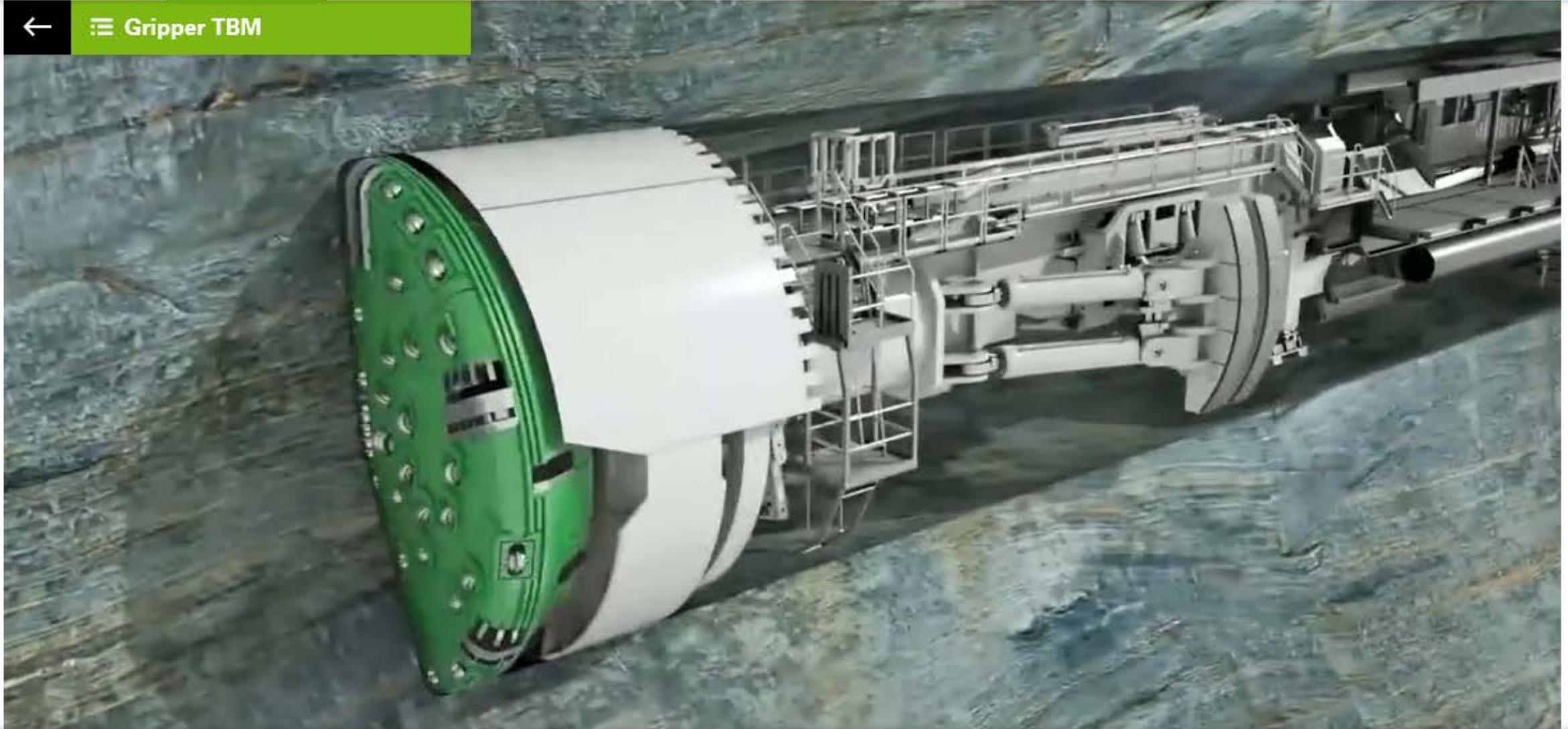
REFERENCES

NEWSROOM

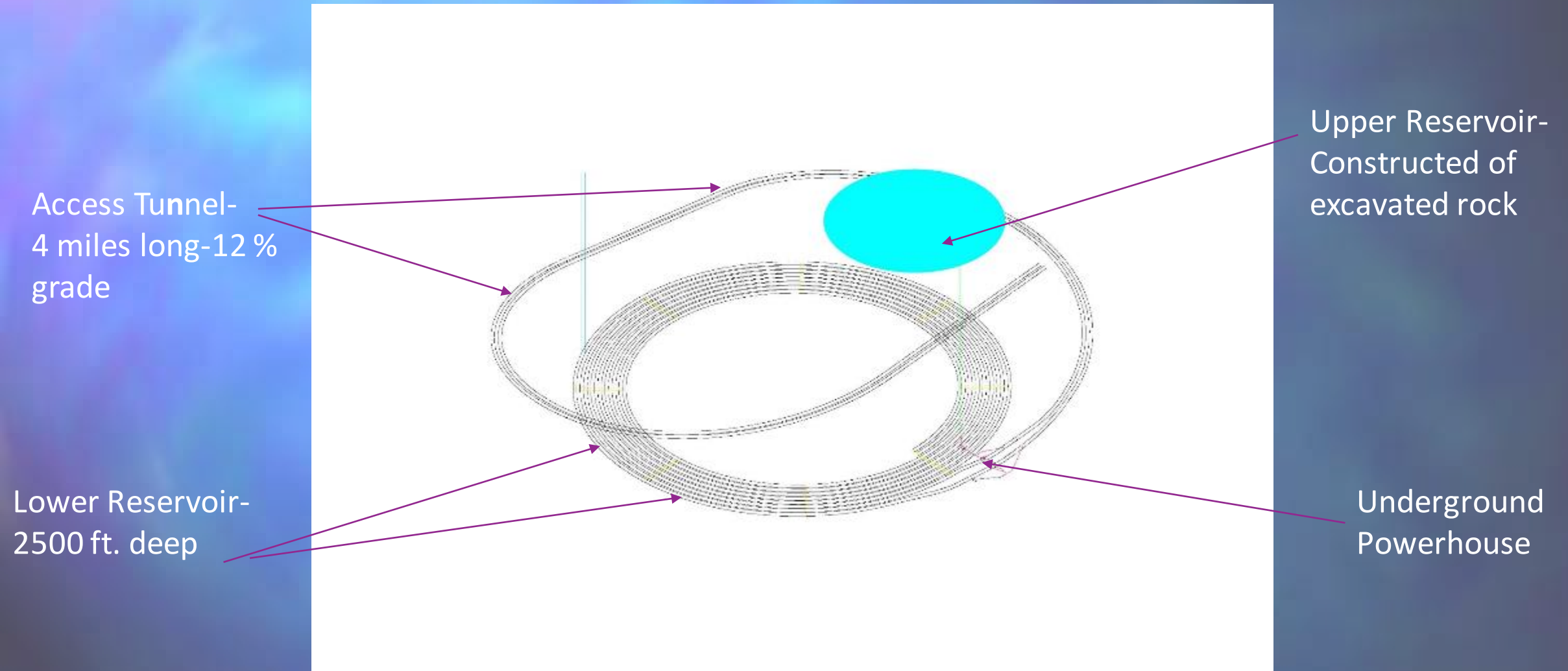
CAREERS



☰ Gripper TBM

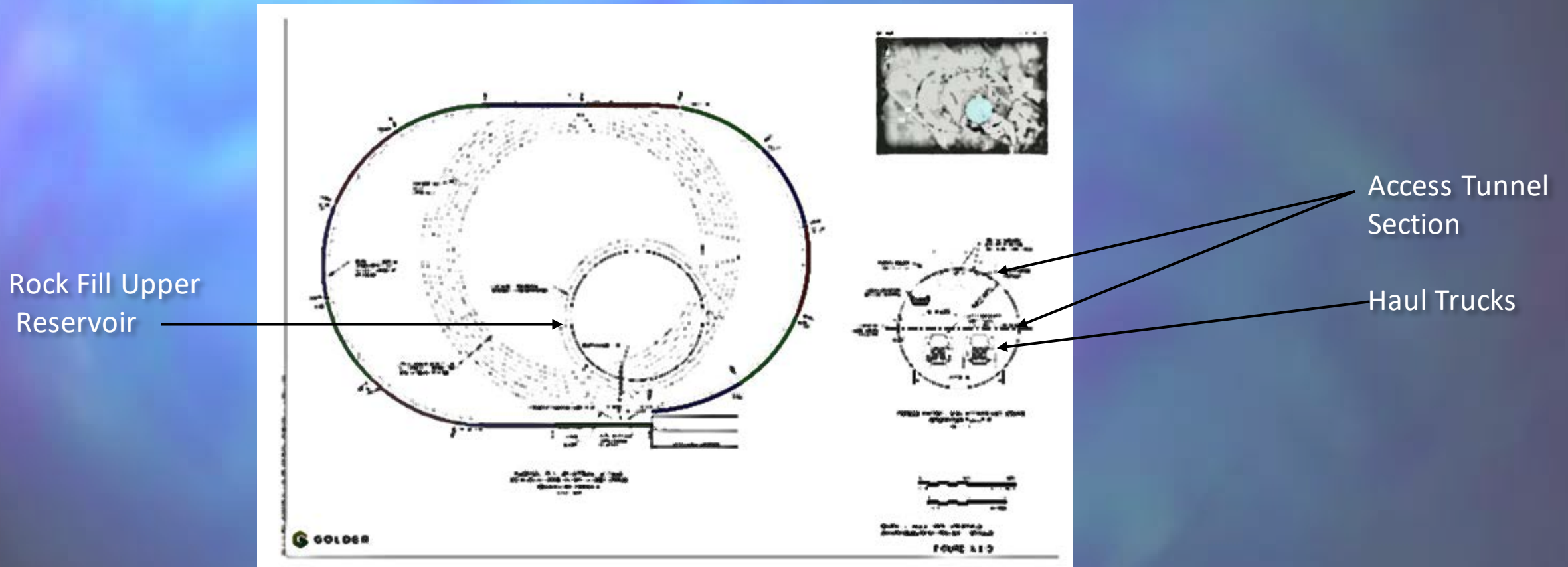


3-D Concept View-



Siting Requirements-

- High quality, strong, impermeable bedrock
- Close to existing Transmission
- Water Source, if groundwater a FERC license may not be required
- High Head (2500 ft.+/-) reduces costs



Note: Powerhouse can be accessed by vehicles –safety and constructibility advantage

ADVANCEMENT IN STATE OF THE ART-

- Use of TBMs drives down cost of UPSH
- UPSH Cost (\$/kWh) is comparable with conventional PHS
- Economical Projects can be sited in topographically challenged areas (ie.-the Midwest)
- Projects can be sited close to existing transmission
- As a closed system, UPHS has minimal impacts

TOTAL PROJECT COST*

Direct Construction Costs					
	2019-Estimated Cost				
Mobilization	20,000,000				
Upper Reservoir	78,722,530				
Powerhouse	241,983,690				
Underground Excavation	469,955,336				
Interconnection	29,116,504				
Make-up Water System	5,000,000				
Subtotal Direct Construction Costs	844,778,060				
Construction Indirect Costs-20%	168,955,612				
Total Construction Cost	1,013,733,672				
Construction Management-5%	50,686,684				
Design Engineering-4%	54,979,000				
Contingency 25% on non excavation items **	135,944,584				
	\$				
Total Direct Cost	1,255,343,940	1,885 \$/kW	157 \$/kWh		
Other Costs					
	\$				
Feasibility Study	2,000,000				
Licensing Permitting	2,000,000				
Owners Cost-Sales Tax , Insurance ,	\$				
Financing-3.2%*	40,171,006				
Interest During Construction -7.25% 86 months	\$				
	458,982,423				
Total Other Costs	503,153,429				
	\$				
TOTAL PROJECT COST	1,758,497,369	2,640 \$/kW	220 \$/kWh		
** 25 % contingency on non excavation items, -25% contingency is included in excavation cost					

Costs (\$2640/kW) and (\$220/kWh) for 12 hours of storage are based on prefeasibility study for Granite Falls Site. Cost for other sites with similar strong impermeable rock formations should be similar..

*AECOM & Golder Associates -W/ 25 % Contingency-

Cost Comparison Versus Conventional PHS (Licensed-Under Development)-

<u>Project</u>	<u>Size (MW)</u>	<u>Cost * (\$/kW)</u>	<u>Energy Storage Hours</u>	<u>Storage Cost (\$/kW-hr)</u>
Swan Lake North	600	2406	8.8	273
Eagle Mountain	1300	1920	10	192
Tazewell	850	2350	10	235
Goldendale	1200	2363	12.3	192
Granite Falls	666	2640	12	220
Lithium Batteries (3 Batteries)	3576		10	356

*From publicly Available Cost info.

Summary –UPSH -

- Has a much lower cost than batteries for long duration storage
- Cost competitive with conventional PHS
- Closed System (No fish, No water quality issues)
- **A UPSH site can be essentially environmentally benign**
- Using Groundwater- No FERC License may be required
- Can be sized for any amount of generation and storage
- Storage cost (\$/kWh)decrease with increasing amounts of energy storage

NEXT STEPS-

-Identify Potential Sites-

Nelson Energy has obtained FERC preliminary permits for sites in Minnesota (2), Wisconsin, South Dakota and Texas

- Engage a Sponsor

Nelson Energy has discussed the concept in detail with five utility groups and one federal agency- interest, but no sponsors to date

- Conduct a Site Specific Pre-feasibility study

- Sponsor Conducts a full feasibility study-including subsurface exploration

For Further Information-

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doug@nelsonenergy.us

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Panel Questions

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WATER POWER TECHNOLOGIES OFFICE

Gordon Wittmeyer and Biswajit Dasgupta

Southwest Research Institute

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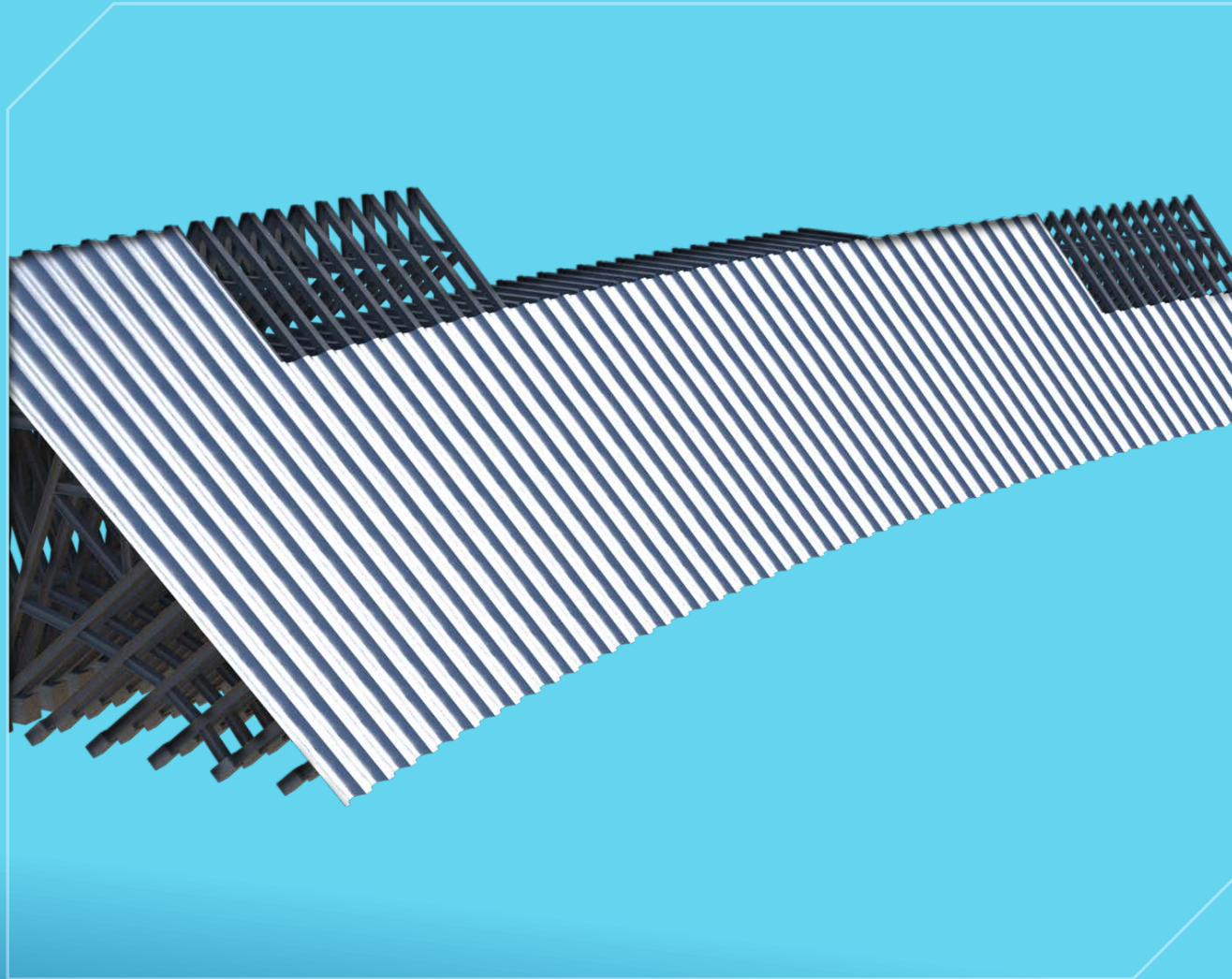
STEEL DAMS FOR ACCELERATING THE DEVELOPMENT OF NEW PSH PROJECTS

Gordon Wittmeyer and Biswajit Dasgupta
Southwest Research Institute

Michael Ingram and Vignesh Ramasamy
National Renewable Energy Laboratory

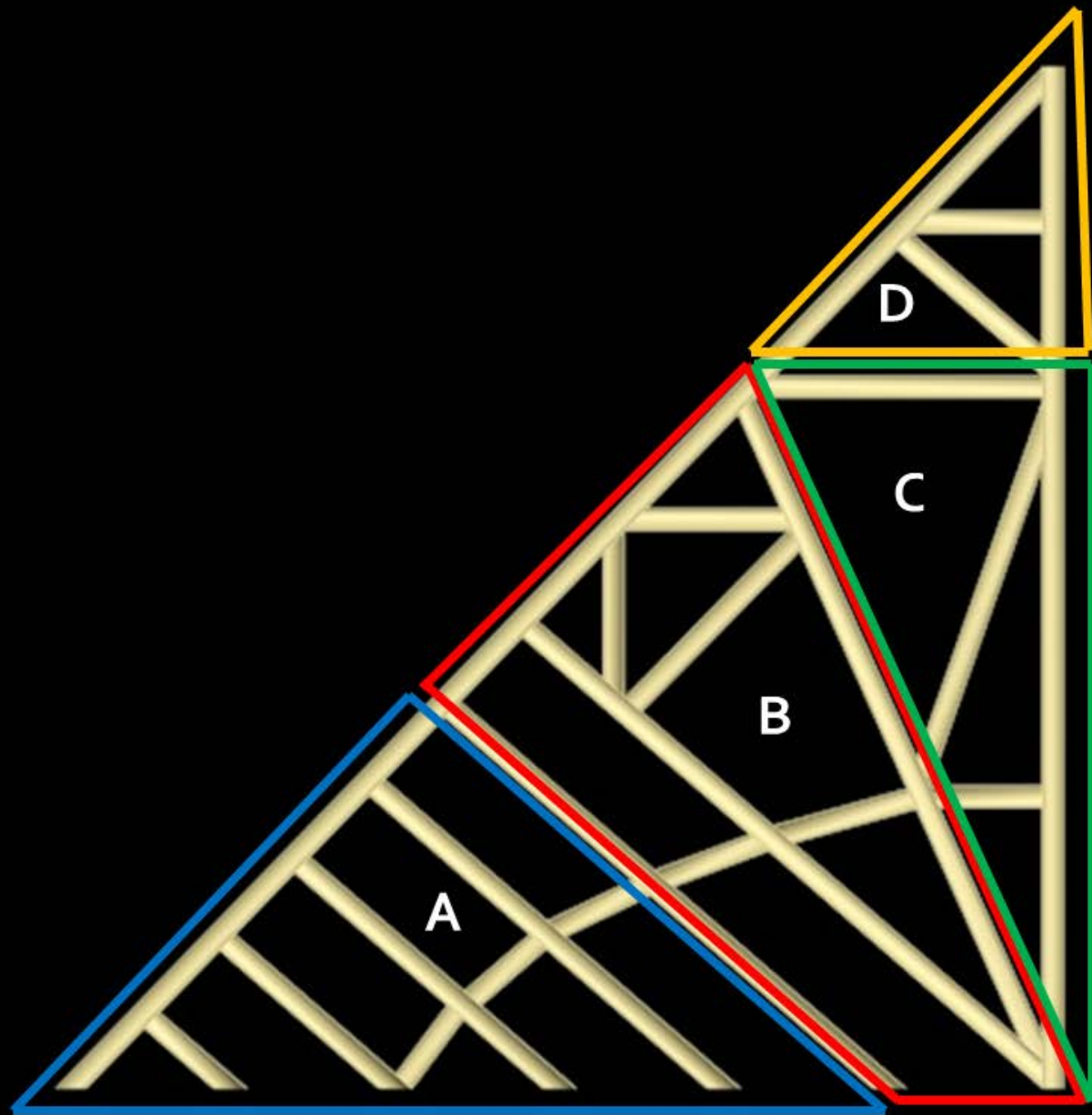
Vladimir Koritarov and Cathy Milostan
Argonne National Laboratory

October 27, 2021



MODULAR CONSTRUCTION OF RING-SHAPED MOUNTAIN TOP STEEL DAMS

- ▶ Right side advancing with placement of first steel frame modules
- ▶ Left side completed with all four frame modules and three water-tight plate modules





Kinzua, PA



Taum Sauk,
MO

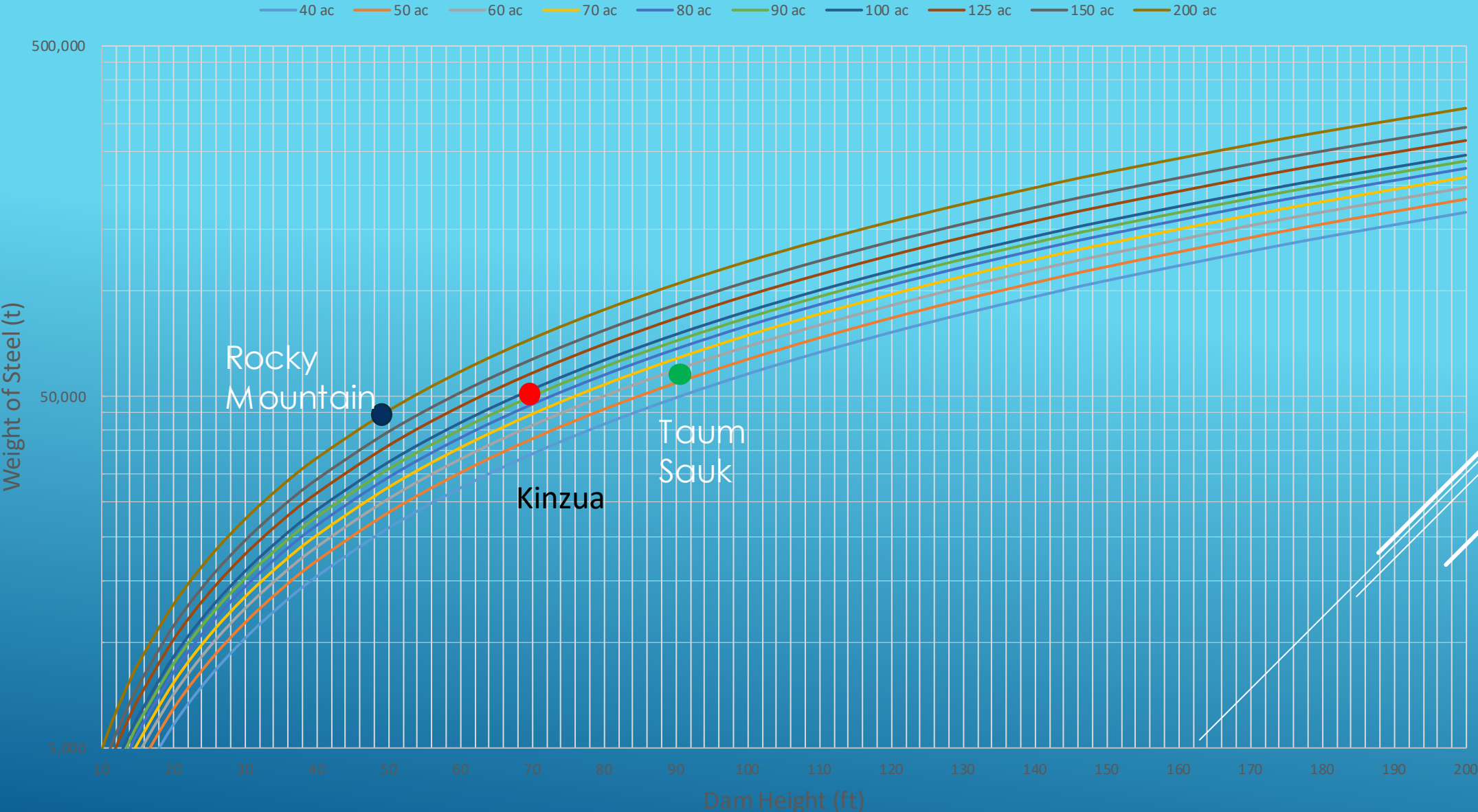


Rocky Mountain,
GA

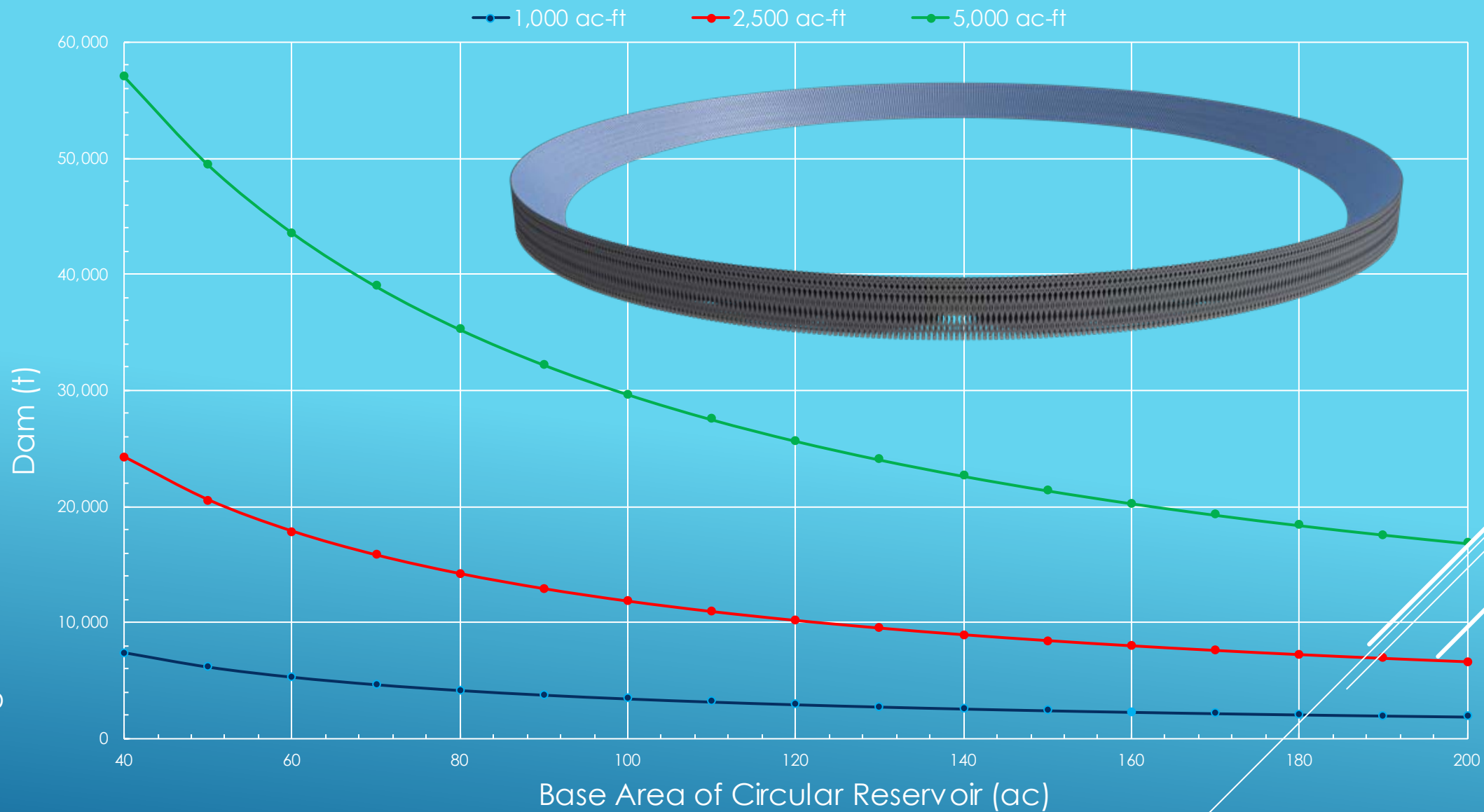


Ludington,
MI

Weight of Structural and Plate Steel vs Height for Circular Steel Dams with Base Areas Between 40 and 200 Acres



Weight of Structural and Plate Steel for Circular



Current PSH Dams Compared to Equivalent Steel Dams

	Rocky Mountain	Taum Sauk	Kinzua (Seneca)
Height (ft)	80	92	115
Length (ft)	12,800	6,660	7,800
Surface Area (ac)	210	55	110
Reservoir Volume (ac-ft)	10,200	4,350	5,756
Dam Material	Earthfill	RCC	Rockfill
Dam Volume (yd³)	10,738,000	3,750,000	268,000,000 (???)
Dam Cost (2020)	\$215 million	\$490 million	(???)
	Steel Dam	Steel Dam	Steel Dam
Height (ft)	50	92	70
Weight of Steel (t)	40,000	60,000	50,000
Dam Cost (2020)	\$80 million	\$120 million	\$100 million

Proposed Demonstration Project

PSH alternative to 10 to 100MW BESS units being installed in the ERCOT market

PSH should provide 4 to 8 hours duration instead of typical 1 to 3 hours from BESS

Target CAPEX of \$200 to \$250 per kWh to compete with utility-scale Li-Ion BESS
[Feldman et al. (2021): \$341/kWh and \$1,365/kW, \$2019]

Target sites that can accommodate larger diameter, shorter-height circular steel dams to take advantage of minimum impoundment expense per unit energy stored

Design steel dam supports and plate systems to be built at the fabricator, transported by truck on the interstate highway system, and assembled with low-capacity lifts on site.

Use commercial off-the-shelf centrifugal pumps as turbines (PATs) to reduce CAPEX and order times

Big Harkey Canyon PSH Project Specifications

Upper Reservoir

Diameter = 666 ft

Depth = 10 ft

Max volume = 320 ac-ft

Max water level = 3,025 ft amsl

Min water level = 3,015 ft amsl

Lower Reservoir

Diameter = 1,800 ft

Depth = 10 ft

Max volume = 580 ac-ft

Max water level = 2,381 ft amsl

Min water level = 2,371 ft amsl

Pump inlets at 2,311 ft amsl

Rated Head = 613 ft

Head race and surface conduit 4,700 ft

Vertical shaft 90 ft

Discharge (8.6 hr) 550 cfs; 4 x 5 MW = 20 MW

Fill time 11.8 hrs; 4 x 5 MW

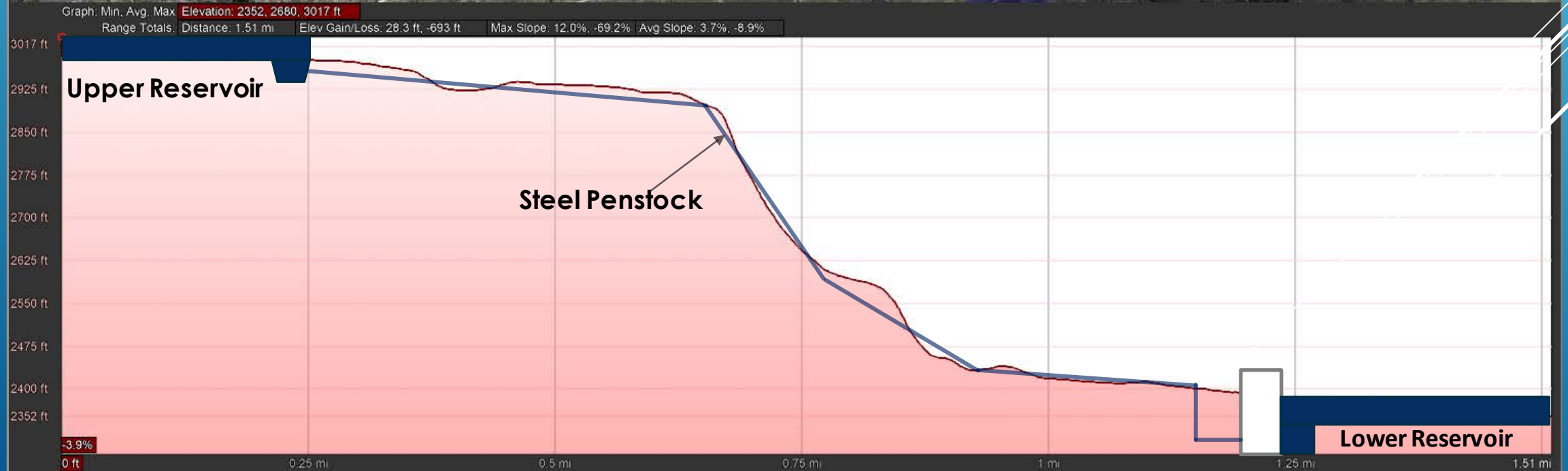
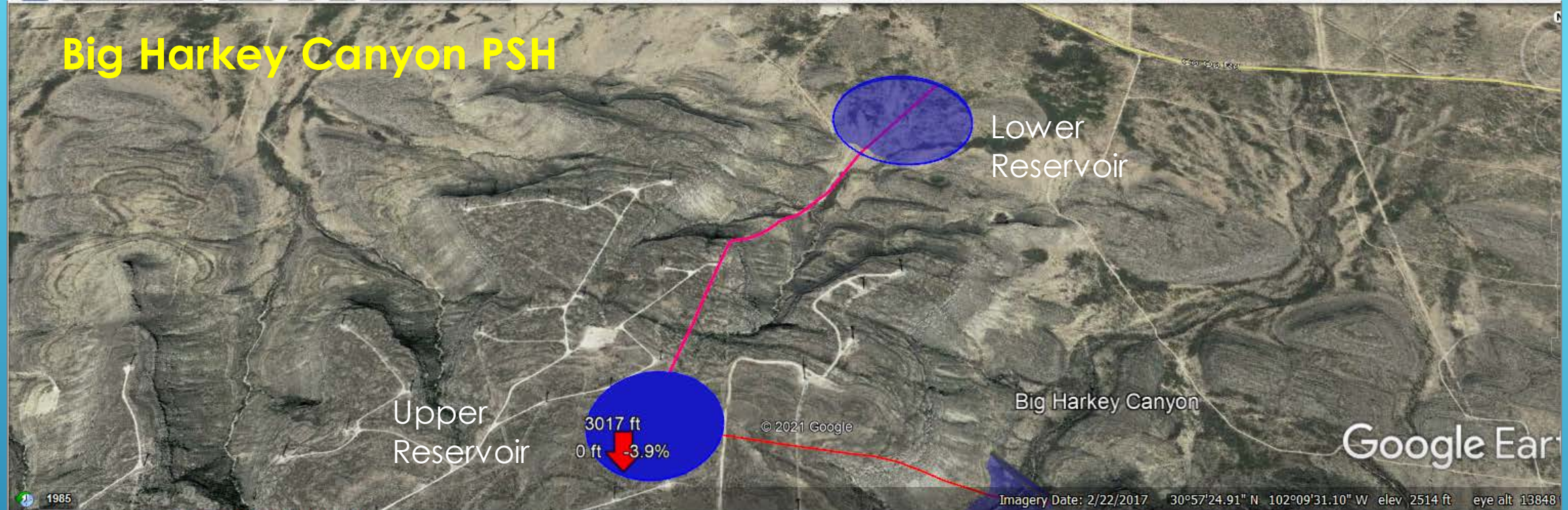
Energy required to fill = 235 MWh ($\eta=85\%$)

Energy recovered = 177 MWh ($\eta=85\%$)

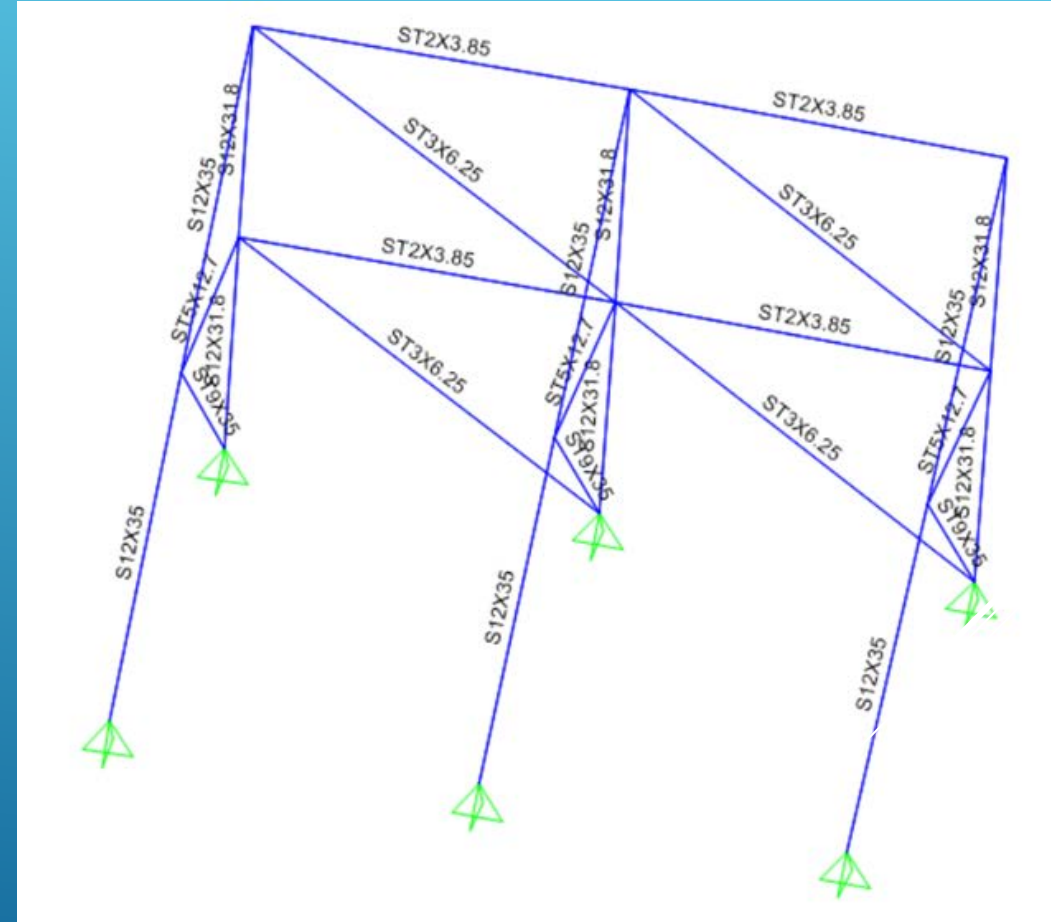
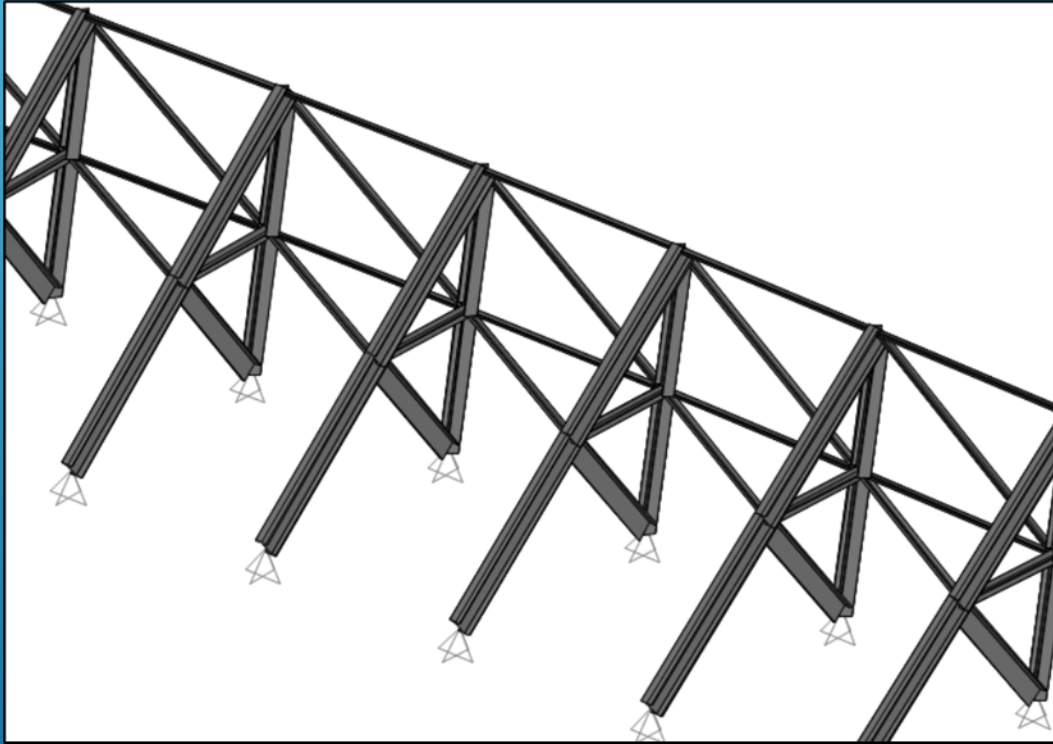
Round trip efficiency 72%

Conduit is 96 in diameter; Velocity of 11 fps

Big Harkey Canyon PSH



Design of Steel Structure and Concrete Foundations Optimized to Reduce Material Costs and Speed Assembly



General Bottom-Up Cost Model Developed to Estimate CAPEX for Big Harkey Canyon Demonstration PSH Project

Element	Cost (\$)
Site Staging and Preparation	\$2,287,015
Upper Reservoir	\$5,041,564
Lower Reservoir	\$5,464,176
Penstocks, Gates, Hoist, Trash Racks	\$3,283,449
Pumps, Electromechanical Controls, Substation	\$4,079,754
Transmission, Permitting and Interconnection	\$4,388,202
Sales Tax	\$1,006,715
Contingency (25%)	\$6,387,719
Developer Overhead (6%)	\$1,916,316
Profit (5%)	\$1,692,745
Total	\$35,547,655

Competitive PSH Facility with Relatively Low Capital Cost: Should be Competitive with Current BESS

PSH Plant Factors		Values
Rated Capacity		20MW
Energy Stored		177MWh
CAPEX/kWh/cycle		\$200
CAPEX/kW		\$1,726

PSH facility will still take longer to construct than a comparable BESS

Anticipate that the Levelized Cost of Energy Storage will be lower for this PSH project than an equivalent BESS

Panel Questions

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Thank you!

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