

Gen3 CSP Summit 2021

Robust, High-Temperature, Chloride Salt Heat Exchanger Materials

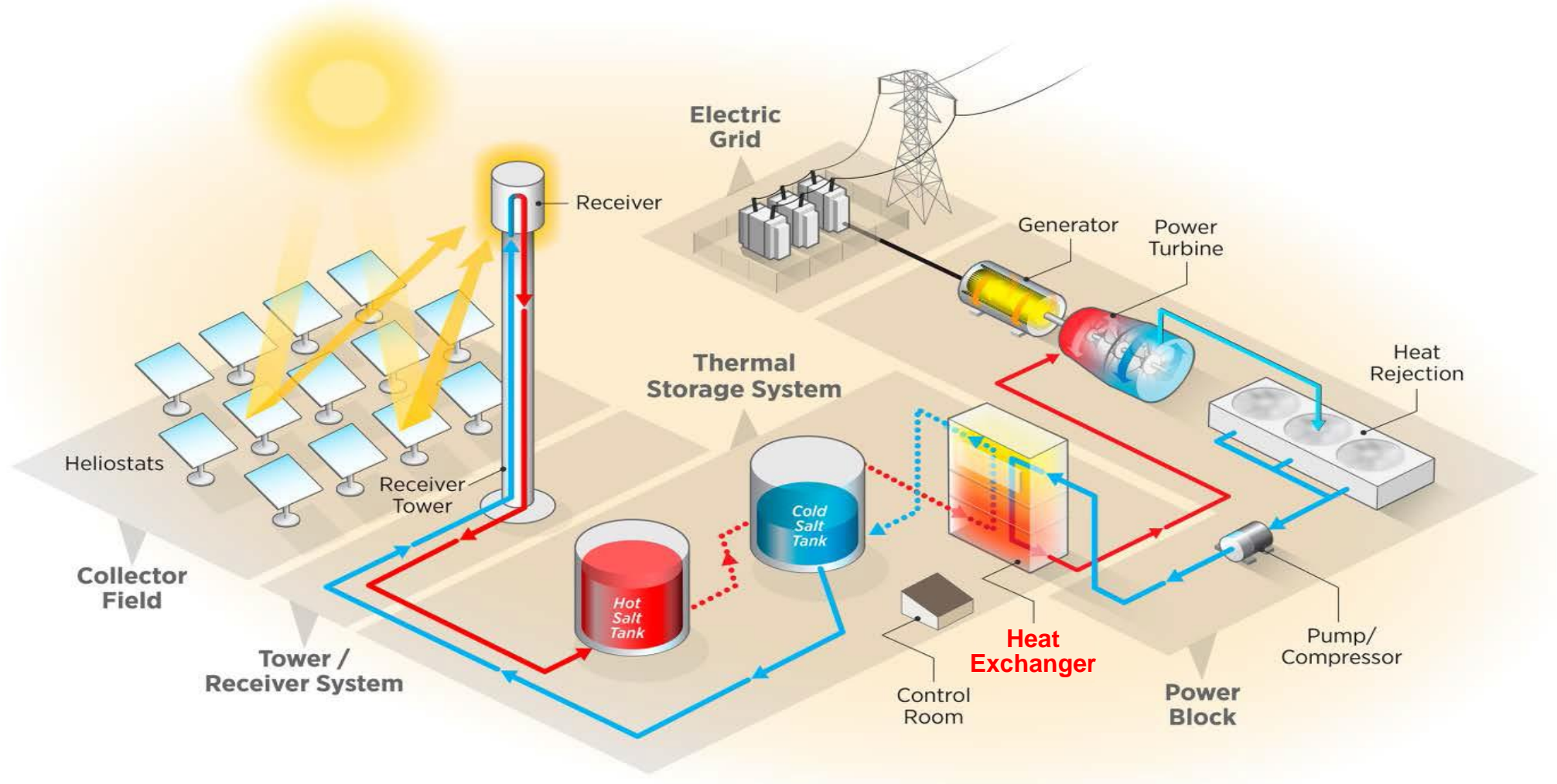
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Asegun Henry² (Co-PI), Aaron Wildberger³ (Co-PI)**

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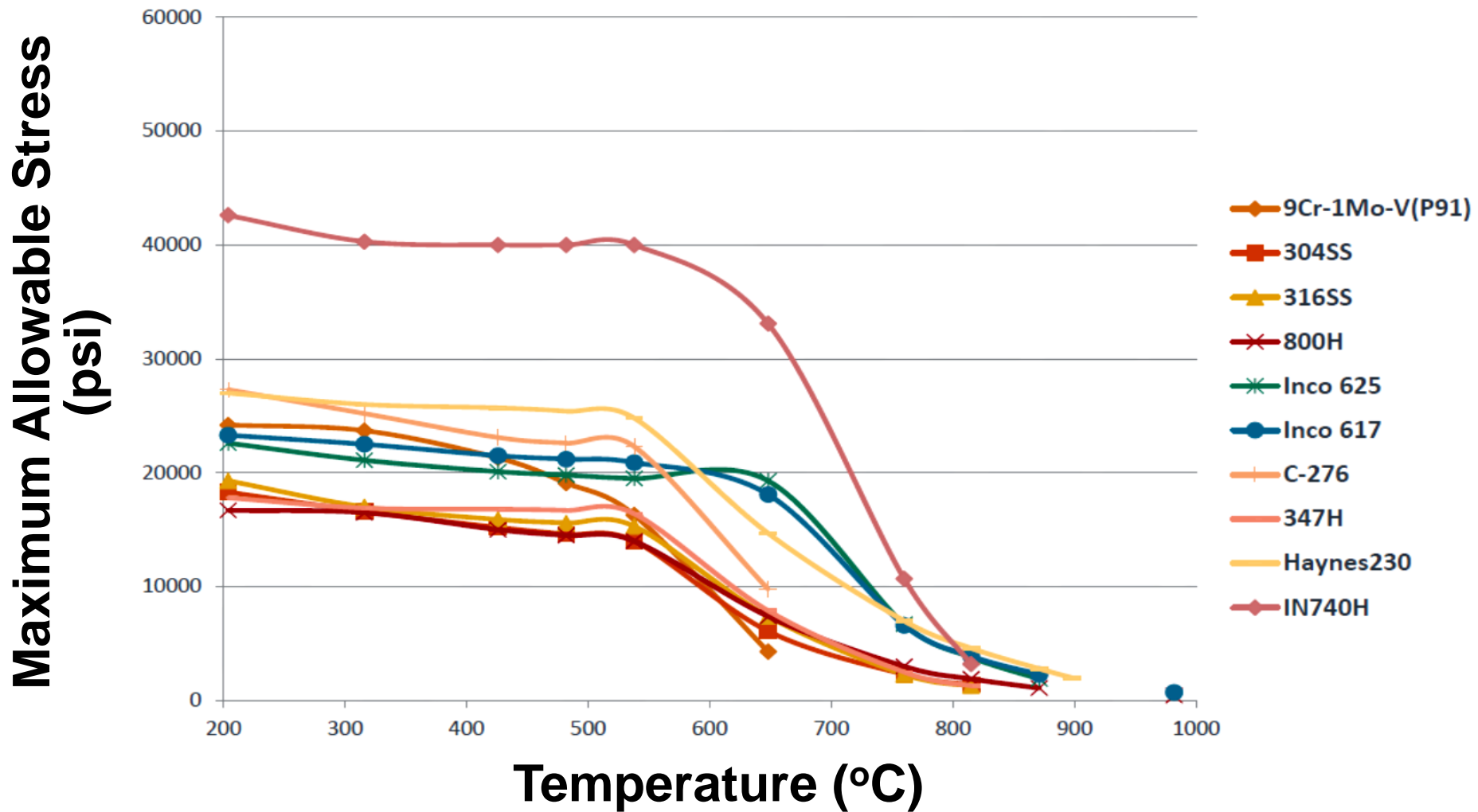
³Vacuum Process Engineering, Inc.

Power Tower Concept for Concentrated Solar Power



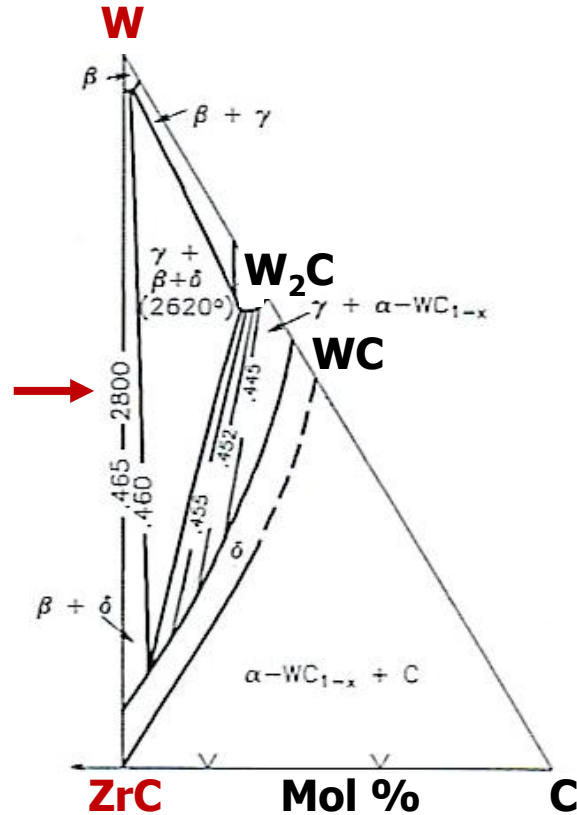
M. Mehos, C. Turchi, J. Vidal, M. Wagner, Z. Ma, C. Ho, W. Kolb, C. Andraka, A. Kruienza, "Concentrating Solar Power Gen3 Demonstration Roadmap," *Technical Report NREL/TP-5500-67464*, NREL, 2017

Temperature Limits of Metal Alloy Printed Circuit HEXs



Attributes of ZrC/W-based Composites

- ◆ Chemical compatibility at high temperatures
(No new compounds form between ZrC and W¹)



1. V. N. Eremenko, T. Y. Velikanova, L. V. Artyukh, G. M. Aksel'rod, A. S. Vishnevskii, *Phase Diagrams for Ceramists*, Vol. X, C-W-Zr System (Fig. 9034), Ed. A. E. McHale, The American Ceramic Society, 1994.

Attributes of ZrC/W-based Composites

- ◆ **Chemical compatibility at high temperatures**

(No new compounds form between ZrC and W)

- ◆ **Tailorable for corrosion resistance**

(ZrC/W cermets have been found to be resistant to corrosion in dry, oxygen-purified MgCl₂ (31.9 mol%)-KCl-based salt at 750°C in UHP Ar, with a projected recession of <12 μm/yr)

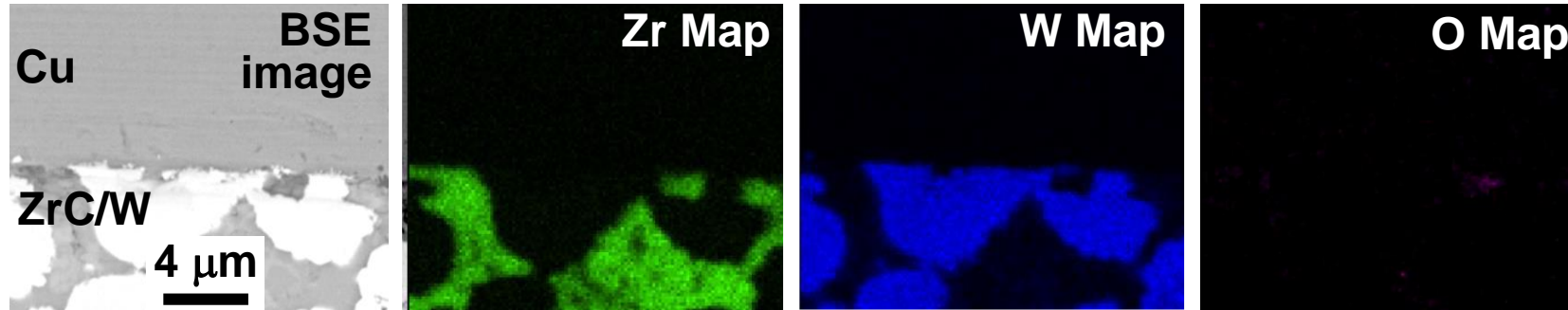
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Cu:ZrC/W interface
after 1000 h in
50 ppm CO in CO₂
at 750°C, 20 MPa²

1. K. H. Sandhage, "Method for Enhancing Corrosion Resistance of Oxidizable Materials and Components Made Therefrom," *P.C.T./U.S. Patent Application*, 2017; *U.S. Provisional Patent Application*, 2016.
2. M. Caccia, M. Tabendeh-Khorshid, G. Itskos, A. R. Strayer, A. S. Caldwell, S. Pidaparti, S. Singnisai, A. D. Rohskopf, A. M. Schroeder, D. Jarrahbashi, T. Kang, S. Sahoo, N. R. Kadasala, A. Marquez-Rossy, M. H. Anderson, E. Lara-Curzio, D. Ranjan, A. Henry, K. H. Sandhage, "Ceramic/Metal Composites for Heat Exchangers in Concentrated Solar Power Plants," *Nature*, 562 (7727) 406-409 (2018).

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- ◆ **High thermal conductivity at 800°C**
($\kappa = 66.0 \text{ W/m}\cdot\text{K}^1$ vs. $22.1 \text{ W/m}\cdot\text{K}$ for IN740H² and $\leq 45 \text{ W/m}\cdot\text{K}$ for SiC³⁻⁵)

1. M. Caccia, M. Tabendeh-Khorshid, G. Itskos, A. R. Strayer, A. S. Caldwell, S. Pidaparti, S. Singnisai, A. D. Rohskopf, A. M. Schroeder, D. Jarrahbashi, T. Kang, S. Sahoo, N. R. Kadasala, A. Marquez-Rossy, M. H. Anderson, E. Lara-Curzio, D. Ranjan, A. Henry, K. H. Sandhage, "Ceramic/Metal Composites for Heat Exchangers in Concentrated Solar Power Plants," *Nature*, 562 (7727) 406-409 (2018).
2. <http://www.specialmetals.com/files/PCC%20EG%20740H%20White%20Paper.pdf>
3. A. Sommers, et al., "Ceramics and Ceramic Matrix Composites for Heat Exchangers in Advanced Thermal Systems – A Review," *Appl. Thermal Eng.*, 30, 1277-1291 (2010).
4. D.-M. Liu, B.-W. Lin, "Thermal Conductivity in Hot-Pressed Silicon Carbide," *Ceram. Int.*, 22, 407-414 (1996).
5. K. Watari, et al., "Effect of Grain Boundaries on Thermal Conductivity of Silicon Carbide Ceramic at 5 to 1300 K," *J. Am. Ceram. Soc.*, 86 (10) 1812-1814 (2003).

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(at RT: CTE W = $4.5 \times 10^{-6}/^{\circ}\text{C}$ and CTE ZrC = $4.0 \times 10^{-6}/^{\circ}\text{C}$; at 2700°C, CTE W = $9.2 \times 10^{-6}/^{\circ}\text{C}$ and CTE ZrC = $10.2 \times 10^{-6}/^{\circ}\text{C}$; No σ_f reduction after 10 cycles from RT - 750°C)

1. Y. S. Touloukian, R. K. Kirby, R. K., R. E. Taylor, P. D. Desai, *Thermophysical Properties of Matter*. Vol. 12. Thermal Expansion of Metallic Elements and Alloys, Plenum Press, New York, NY, USA, 1975.
2. Y. S. Touloukian, R. K. Kirby, R. E. Taylor, T. Y. R. Lee, *Thermophysical Properties of Matter*. Vol. 13. Thermal Expansion of Nonmetallic Solids, Plenum Press, New York, NY, USA, 1977.
3. M. Caccia, M. Tabendeh-Khorshid, G. Itskos, A. R. Strayer, A. S. Caldwell, S. Pidaparti, S. Singnisai, A. D. Rohskopf, A. M. Schroeder, D. Jarrahbashi, T. Kang, S. Sahoo, N. R. Kadasala, A. Marquez-Rossy, M. H. Anderson, E. Lara-Curzio, D. Ranjan, A. Henry, K. H. Sandhage, "Ceramic/Metal Composites for Heat Exchangers in Concentrated Solar Power Plants," *Nature*, 562 (7727) 406-409 (2018)
4. M. B. Dickerson, P. J. Wurm, J. R. Schorr, W. P. Hoffman, E. Hunt, K. H. Sandhage, "Near net-shaped, ultra-high melting, recession-resistant ZrC/W-based rocket nozzle liners via the displacive compensation of porosity (DCP) method," *J. Mater. Sci.* 39, 6005-6015 (2004).

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- ◆ **Enhanced toughness w.r.t. conventional monolithic ceramics**
($K_{1C} = 9.4 \pm 2.4$ MPa·m^{1/2} vs. ≤ 0.8 MPa·m^{1/2} for Pyrex, ≤ 1.4 MPa·m^{1/2} for concrete, ≤ 4.8 MPa·m^{1/2} for Hexoloy SiC¹⁻³)

1. Y. W. Zhao, Y. J. Wang, X. Y. Jin, P. Jia, L. Chen, Y. Zhou, G. M. Song, J. P. Li, Z. H. Feng, "Microstructure and Properties of ZrC-W Composite Fabricated by Reactive Infiltration of Zr₂Cu into WC/W Preform," *Mater. Chem. Phys.*, 153, 17-22 (2015).
2. W. D. Callister, *Materials Science and Engineering - An Introduction*, 6th Edn., John Wiley & Sons, 2003.
3. <http://www.refractories.saint-gobain.com/hexoloy/hexoloy-grades>

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- ◆ **High stiffness and retention of strength at 800°C**
($E = 44 \pm 16 \times 10^3$ ksi/305 \pm 110 GPa; $\sigma_F = 87 \pm 7$ ksi/598 \pm 51 MPa at 800°C)

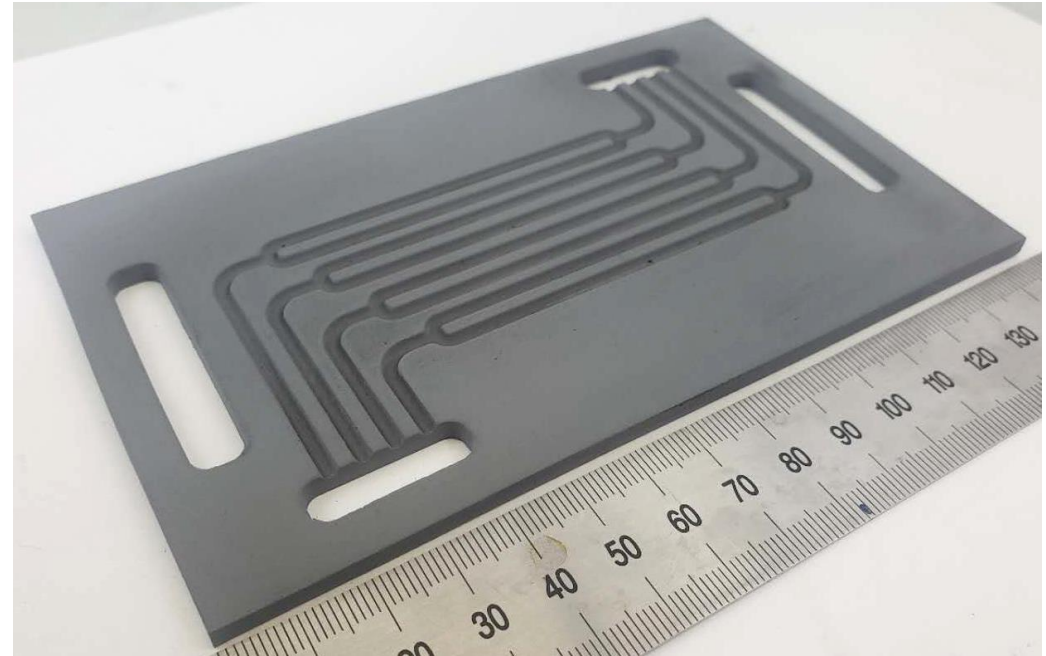
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- ◆ **Cost-effective fabrication of ZrC/W-based HEX plates**

Fabrication of ZrC/W HEX Plates

Channeled Porous WC Preform Plate

Fabricate porous, channeled WC preform plates

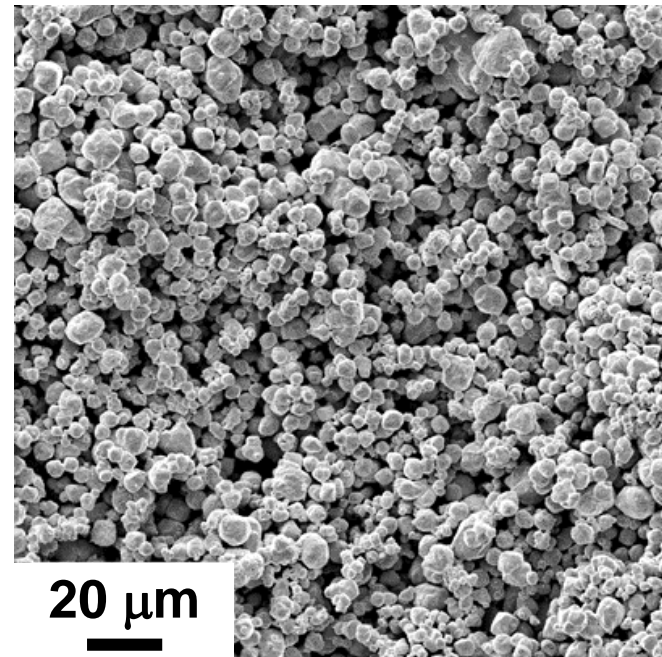


**Porous channeled WC preform plates (15 cm x 9 cm x 3 mm)
(pressing/stamping of WC/binder mixture, binder removal, light sintering)**

Fabrication of ZrC/W HEX Plates

Channeled Porous WC Preform Plate

Fabricate porous, channeled WC preform plates



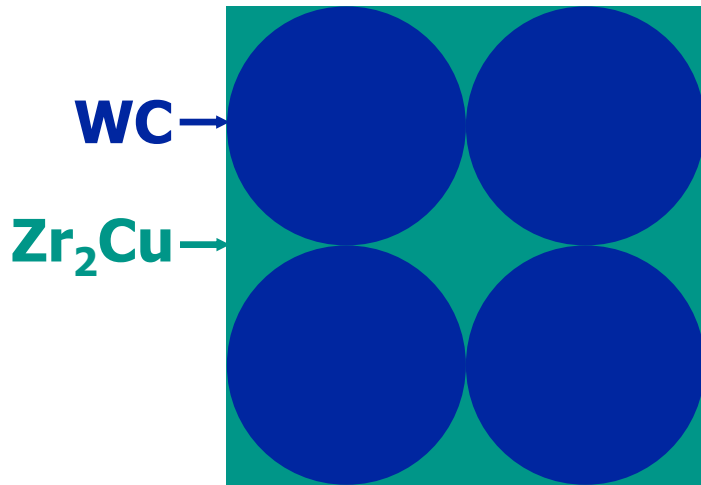
Secondary electron image of a fractured cross-section of a porous WC channeled preform plate

**Porous channeled WC preform plates (15 cm x 9 cm x 3 mm)
(pressing/stamping of WC/binder mixture, binder removal, light sintering)**

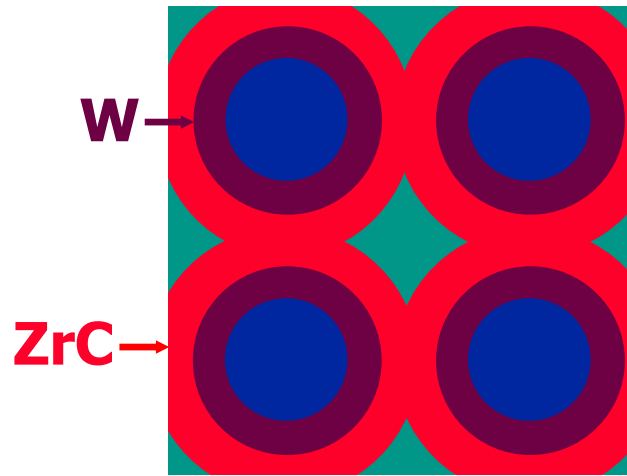
Displacive Compensation of Porosity (DCP) Process¹⁻³



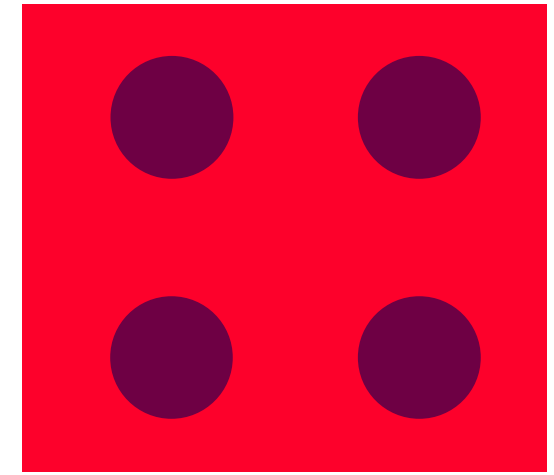
$$\text{where } V_m[\text{ZrC} + \text{W}] = 2.01V_m[\text{WC}]$$



Infiltrated



Partial Rxn



Complete Rxn

1. K. H. Sandhage, et al., *U.S. Patents* No. 6,833,337, 2004; No. 6,598,656, 2003; No. 6,407,022, 2002.
2. K. H. Sandhage, A. S. Henry, *U.S. Patent Appln.*, No. 16/094,262, 2017; *U.S. Provisional Patent Appln.*, 2016.
3. K. H. Sandhage, M. R. Caccia, *U.S. Patent Appln.*, No. 16/503,117, 2019; *U.S. Provisional Patent Appln.*, 2018.

Fabrication of ZrC/W HEX Plates

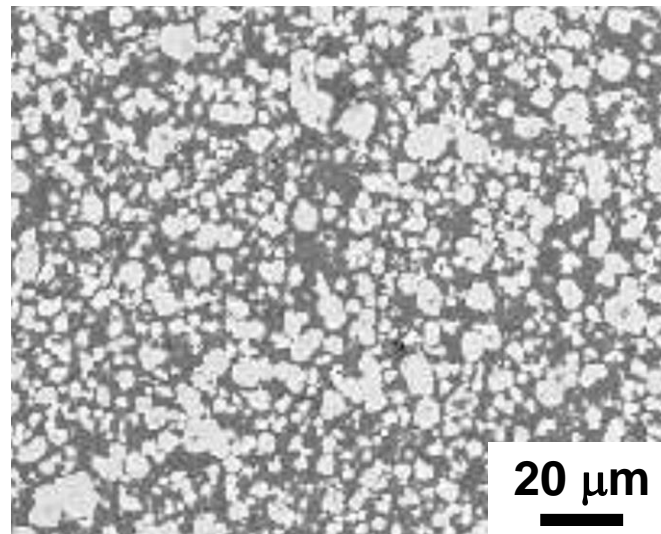
Channeled Porous WC Preform Plate

Fabricate porous, channeled WC preform plates

↓ Reactive Conversion

Channeled ZrC/W Plate

Generate dense, net-size channeled ZrC/W plates via the DCP process



Backscattered electron image of a polished cross-section of a dense, ZrC/W channeled plate

20 μ m

Fabrication of ZrC/W HEX Plates

Channeled Porous WC Preform Plate

↓ Reactive Conversion

Channeled ZrC/W Plate

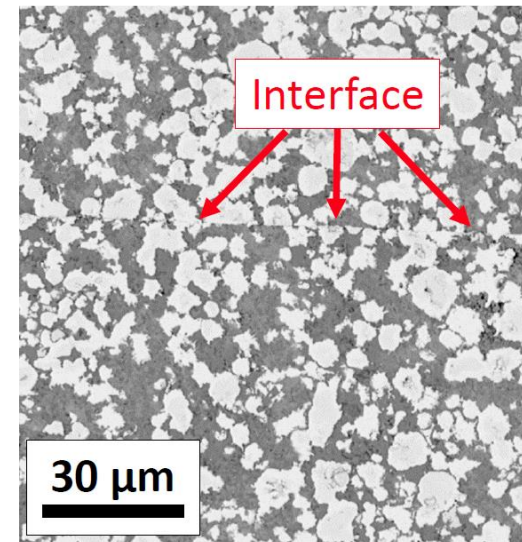
↓ Joining

Dense ZrC/W Plate

Channeled ZrC/W Plate

Fabricate porous, channeled WC preform plates

Generate dense, net-size channeled ZrC/W plates via the DCP process



BSE image of a diffusion-bonded ZrC/W plate pair (1600°C, 2 h, 10 MPa)

Summary and Ongoing Work

- ◆ ZrC/W-based cermets provide an unusual and attractive combination of high-temperature mechanical and thermal properties relative to Fe- and Ni-based alloys
- ◆ ZrC/W composites (and other oxidizable materials, including metal alloys) can be endowed with corrosion resistance in supercritical CO₂-based fluids via use of a new concept^{1,2}:
a supercritical buffered (reducing) CO/CO₂ fluid

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- ◆ **ZrC/W composites (and other oxidizable materials, including metal alloys) can be endowed with corrosion resistance in supercritical CO₂-based fluids via use of a new concept:**
 - a supercritical buffered (reducing) CO/CO₂ fluid*
- ◆ **Scalable, low-cost ceramic forming methods, coupled with a shape/size-preserving reactive melt infiltration (DCP) process, can be used to fabricate ZrC/W HEX plates with tailorable channel patterns**
- ◆ **Diffusion bonding of ZrC/W plates, and brazing of Cu to Ni alloy headers, can provide high-pressure seals for use with sCO/CO₂-bearing fluids at 720°C**

Attributes of Al_2O_3 /Cr-based Composites

- ◆ **Chemical compatibility at high temperatures**
(Al_2O_3 and Cr do not undergo a displacement rxn; $T_m[Al_2O_3] = 2054^\circ C$; $T_m[Cr] = 1863^\circ C$)
- ◆ **Creep resistance**
(Al_2O_3 is quite creep resistant at $750^\circ C$; cermets with a continuous Al_2O_3 matrix have exhibited negligible creep at $1000^\circ C$, 20 MPa)
- ◆ **Failure strength and toughness**
(Four-point-bend σ_F (64 vol% Al_2O_3 /36 vol% Cr) = 47×10^3 psi/320 MPa at $750^\circ C$; $K_{1C} = 7.2$ MPa·m^{1/2} at RT)
- ◆ **Thermal expansion match**
($100 \cdot \Delta L/L_0$ from $25^\circ C$ to $750^\circ C$: Cr = 0.71%, Al_2O_3 = 0.63%)
- ◆ **Thermal conductivity**
(ROM κ (64 vol% Al_2O_3 /36 vol% Cr) = 28 W/m-K at $750^\circ C$ vs. 23.4 W/m-K for H230)
- ◆ **Oxidation resistance**
(slow parabolic kinetics at $750^\circ C$ in CO_2 and air¹)

1. T. D. Nguyen, M. Caccia, C. K. McCormack, G. Itskos, K. H. Sandhage, "Corrosion of Al_2O_3 /Cr and Ti_2O_3 /Cr Composites in Flowing Air and CO_2 at $750^\circ C$," *Corros. Sci.*, 179, 109115-1 to 109115-12 (2021)

Acknowledgements

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- ◆ **Matching support has also been provided by Purdue University and the Massachusetts Institute of Technology**

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