

### Investigation of Superluminescent Diodes for Smart-Lighting Systems

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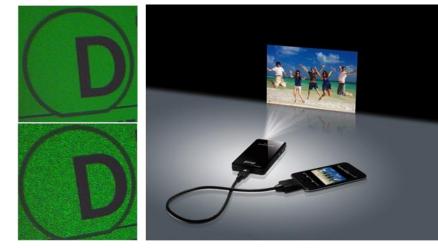
## Motivation

### **Applications of visible SLDs**

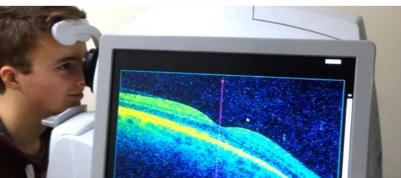


Automotive lighting (Droop-free)

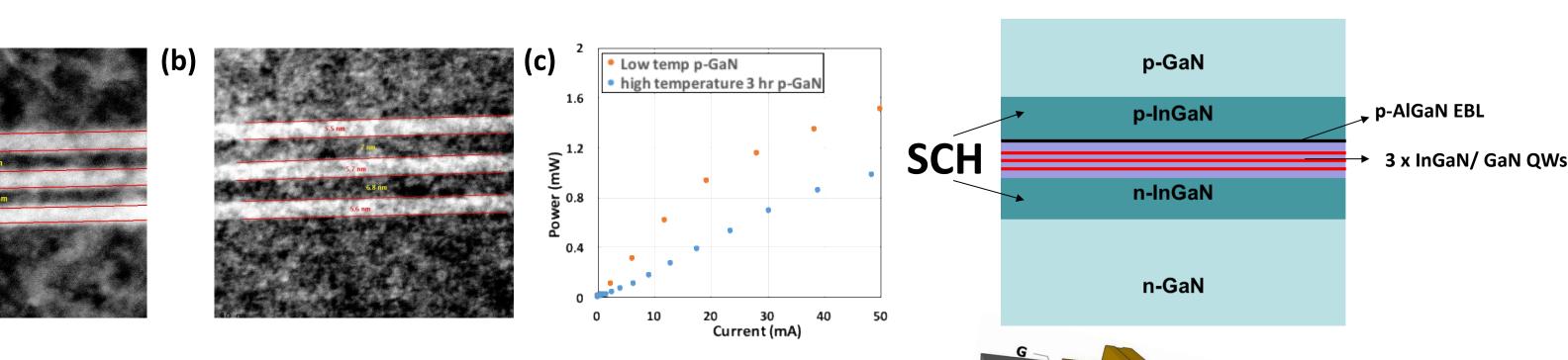




Pico-projection (Speckle-free)



# **SLD Epitaxial Growth and Fabrication**

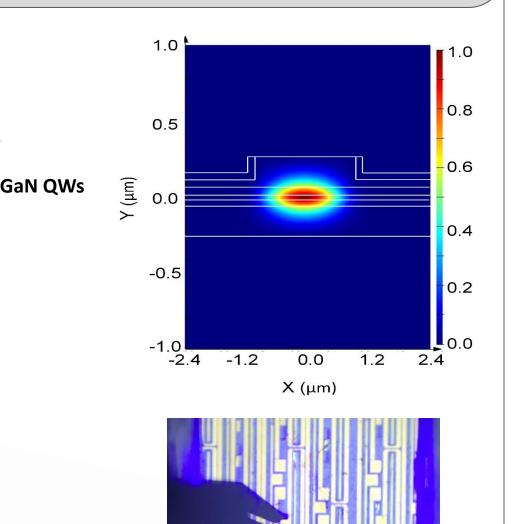


Comparison of active region area of planar *m*-plane LEDs with (a) 3 hr long p-GaN growth and (b) 45 min long p-GaN growth. The active region quality is improved considerably in the shorter p-GaN growth, confirmed by improved optical output power at a given current (c).

Facet-etch indicating good

quality facets. Inset shows

cross-section at the ridge



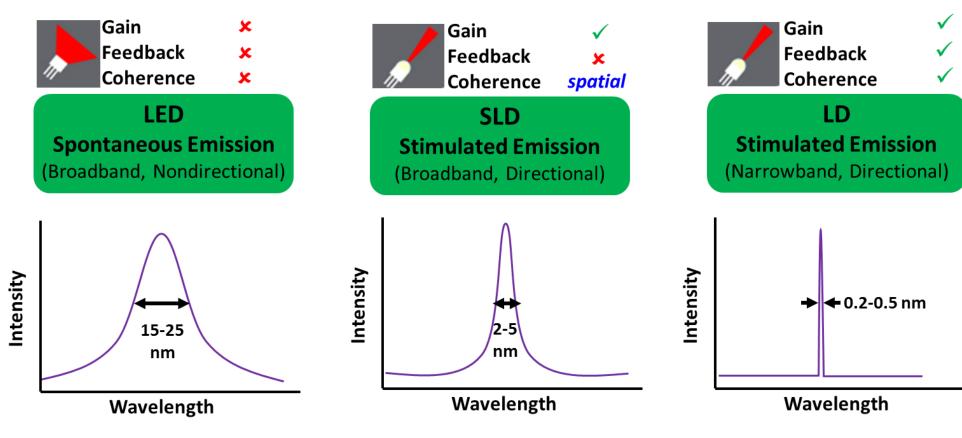


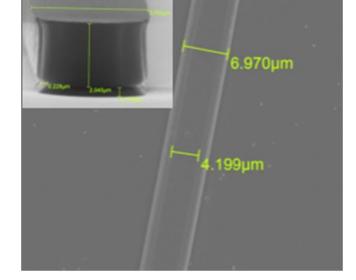


Visible-light Communication (VLC) (High modulation bandwidth)

**Optical Coherence Tomography** (High resolution imaging)

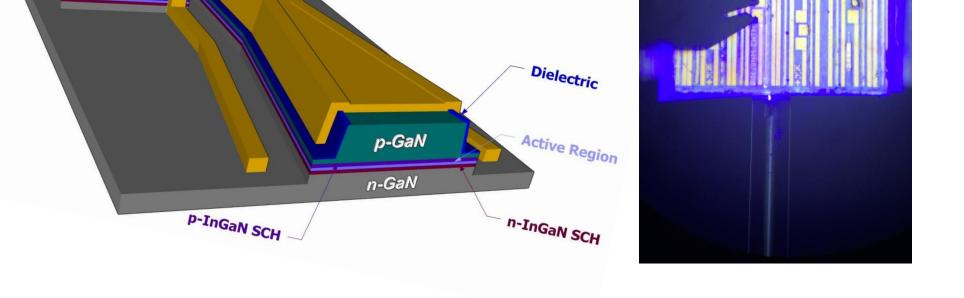
### Advantages of SLDs over LEDs and Lasers





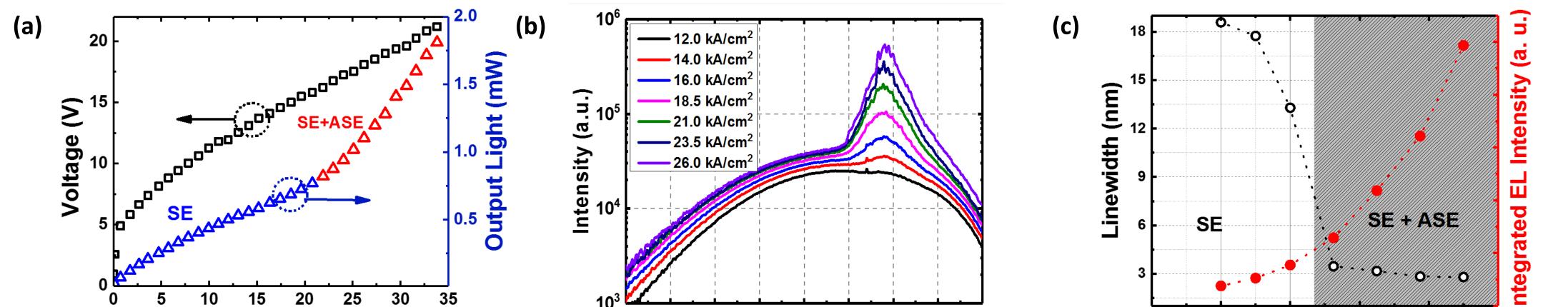
Self-aligned SiO<sub>2</sub> deposition. Inset shows the bilayer resist pattern used for achieving self-aligned dielectric

**Fabricated SLD and** laser arrays with pads for RF testing



(a) Epitaxial layer structure of the SLD indicating the separately-confined heterostructure guiding, whose simulated mode profile using Lumerical (FDTD) is shown in (b). (c) Pictographic illustration of a fabricated tapered waveguide SLD (TSLD). (d) A TSLD under electrical operation



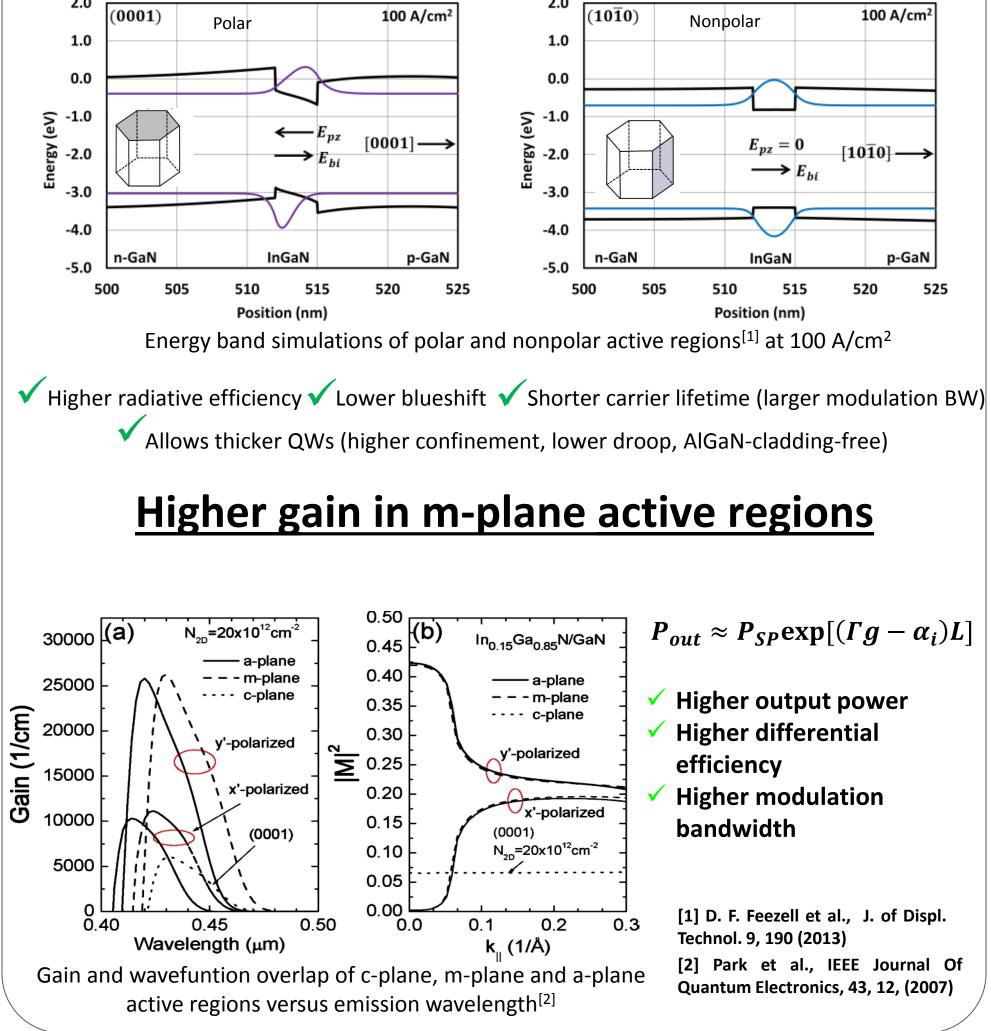


**Radiative Efficiency** λ~450 nm cient efficient LED Laser Above Threshold  $BN_{th}^2 + R_{st}$  $BN^2$  $\eta_r = \overline{AN + BN^2 + CN^3}$  $\frac{1}{AN_{th} + BN_{th}^2 + CN_{th}^3 + R_{st}}$ Valley of droop Independent of carrier Depends on carrier density  $\rightarrow$  no droop density  $\rightarrow$  droop 10 15 20 Input power density (kW/cm<sup>2</sup>)

Comparison of the expression for IQE using the ABC model for spontaneous emission dominated devices (LEDs) and stimulated emission dominated devices (SLDs and laser diodes)<sup>[J. J. Wierer et al., (2013)]</sup>

### Advantages of nonpolar SLDs over c-plane SLDs

20			20		
2.0 (0001)	Dolar	100 A/cm <sup>2</sup>	$(10\overline{1}0)$	Nonnolar	10

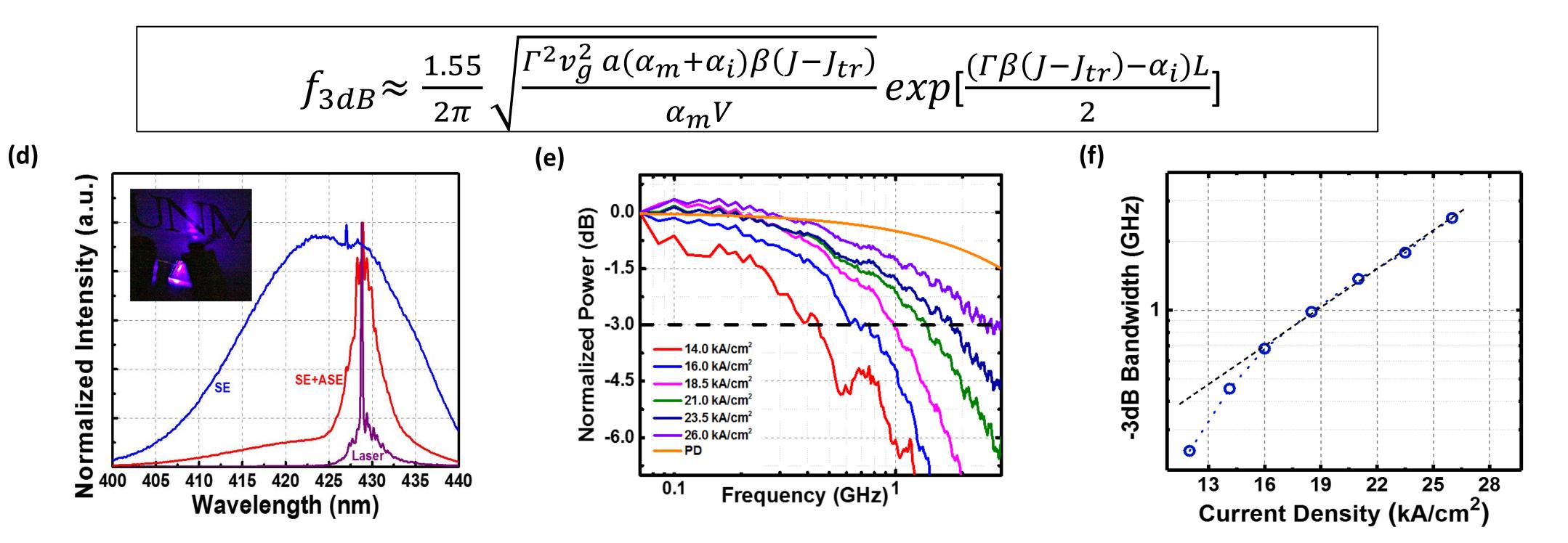


Current Density (kA/cm<sup>2</sup>)

#### 400 405 410 415 420 425 430 435 440 Wavelength (nm)

20 16 24 28 Current Density (kA/cm<sup>2</sup>)

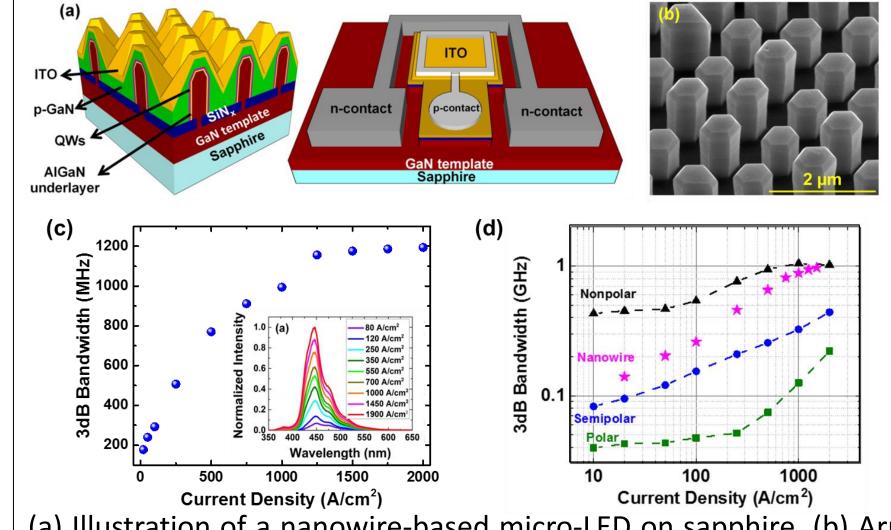
(a) L-J-V characteristics of TSLD. Spectral evolution is shown in (b). (c) Linewidth and total integrated power of the EL spectrum versus current density.

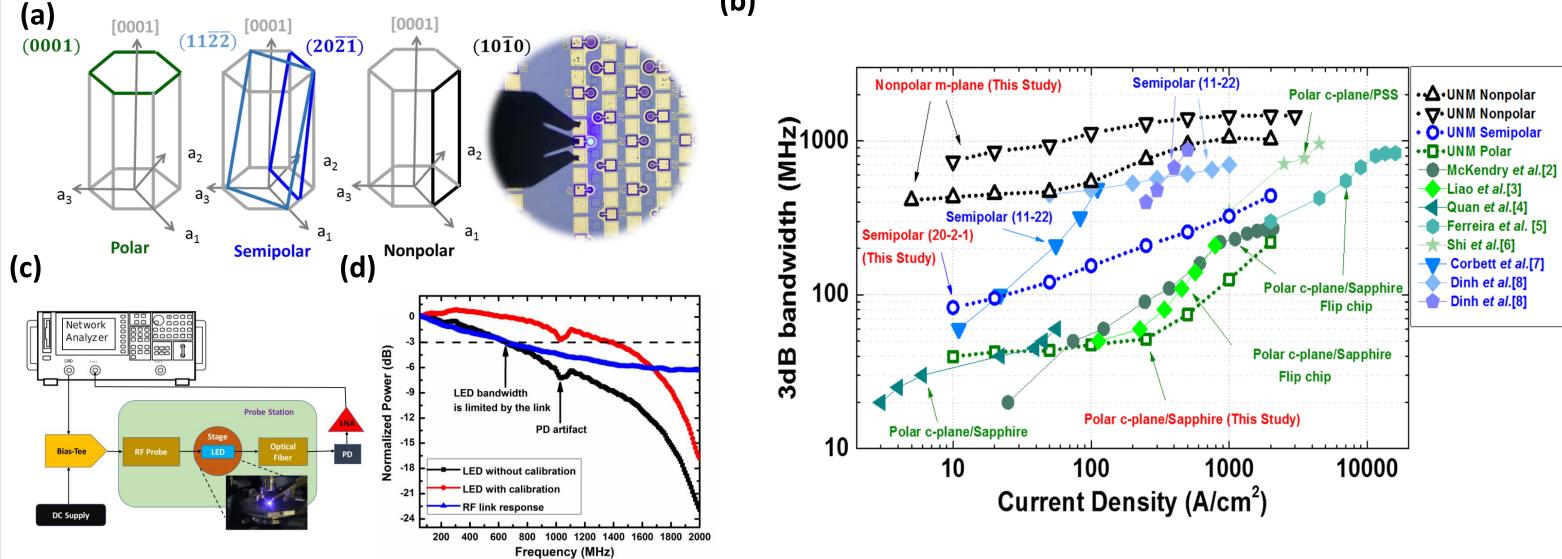


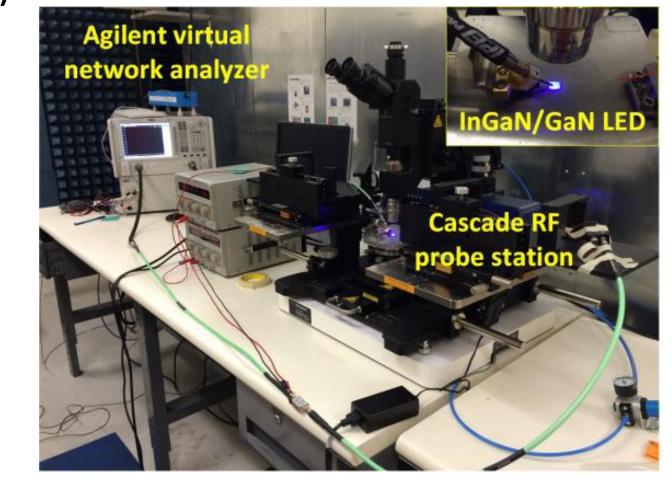
(d) Normalized EL spectra of LED, SLD, and laser on the same chip. (e) Frequency response of the TSLD. The -3 dB RF modulation bandwidth is obtained and plotted versus current density in (f). The log( $f_{3dB}$ ) goes linearly as a function of J in the superluminescene regime due to the exponential increase of the o/p power with J, evident from the above equation.

# **Record Modulation Bandwidth of Blue Micro-LEDs**









(a) Illustration of a nanowire-based micro-LED on sapphire. (b) Arrays of GaN nanowires indicative of smooth morphology on the *m*-plane

sidewalls. (c) -3dB bandwidth of the nanowire LED as a function of (a) Schematic illustration of the various crystallographic planes analyzed; The inset shows an LED device probed using a GSG RF probe. (b) Bandwidth vs. current density for the nonpolar, semipolar, and conventional c-plane microLEDs, compared to other reported c-plane LEDs on sapphire and semipolar substrates. c-plane data from Refs. [2-6] and current density. Inset image shows the EL spectra progression for semipolar data from Refs. [7-8]. (c) RF setup for measuring the frequency response of the LED. (d) Effect of calibration of the RF link on the frequency response of the LED. (e) Test different current densities. (d) Comparison of the -3dB bandwidth for station for SLD bandwidth characterization. Inset shows an InGaN/GaN LED under test. micro-LEDs on different orientations.





