

Vehicle Thermal System Modeling in Simulink



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Overview

Timeline

Project Start Date: FY14 Project End Date: FY17 Percent Complete: 65%

Budget

Total Project Funding:

- DOE Share: \$775K
- Partner contributions*: \$200K

Funding Received in FY15: \$275K

Funding for FY16: \$175K

*Direct funds and in-kind contributions (not included in total)

Barriers

- Cost Timely evaluation of vehicle thermal systems to assist with R&D
- Computational models, design, and simulation methodologies – Develop tool to assist with optimization of future vehicle thermal system designs and prediction of impacts on fuel economy and range
- Constant advances in technology Help industry to advance technology with improved tools

Partners

- Hanon Systems
- MAHLE
- Daimler Trucks
- Kenworth Trucks
- Cummins
- Oak Ridge National Laboratory (ORNL)
- VTO Advanced Power Electronics and Electric Motors (APEEM) Team
- Argonne National Laboratory (ANL)

Project Lead: NREL

Relevance

THE CHALLENGE

- Heating and air conditioning (A/C) have a large impact on electric vehicle (EV) range
- With increasing electrification, vehicle thermal systems are increasingly important for effective and efficient light- and heavy-duty vehicle design
- Electrified heavy-duty A/C systems may provide necessary infrastructure to add heating at limited additional cost
- Autonomie lacks thermal system models based on first principles.

THE OPPORTUNITY

- Tools will assist with evaluation of advanced thermal management and heating solutions using a flexible, freely available framework developed for MATLAB/Simulink that can cosimulate with Autonomie
- Leverage NREL's vehicle thermal management expertise
 - Energy storage thermal management
 - APEEM thermal management
 - Integrated vehicle thermal management
 - Heating, ventilating, and air conditioning (HVAC) expertise, building on the A/C system model developed previously.

Relevance

- HVAC loads account for more than 5% of the fuel used annually for light-duty vehicles (LDVs) in the United States^[1]
- Climate control can reduce EV efficiency and range by more than 50%
- Limited waste heat
- More efficient HVAC methods allow for modes of operation based on driving and ambient conditions.



Climate Control Impact on Focus EV Driving Range - UDDS Cycle

Advanced EV thermal management systems, however, can be more complex.

UDDS = Urban Dynamometer Driving Schedule

- 1. Rugh et al., 2004, Earth Technologies Forum/Mobile Air Conditioning Summit
- 2. Argonne National Laboratory's Advanced Powertrain Research Facility

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Relevance/Objectives

Goals

- By 2017, develop a flexible, publically available framework in the MATLAB/Simulink environment for modeling of vehicle thermal management systems capable of co-simulations with vehicle level models.
- Use the framework to help the industry partners with R&D of advanced thermal management systems

Objectives

- Develop analysis tools to assess the impact of technologies that reduce thermal load, improve climate control efficiency, and reduce vehicle fuel consumption
- Connect climate control, thermal systems, and vehicle-level models to assess the impacts of advanced thermal management technologies on fuel use and range
- Develop an open, accurate, and transient thermal system modeling framework using the MATLAB/Simulink environment for co-simulations with vehicle-level models such as Autonomie.

Approach: Milestones and Go/No-Go



Milestones:

- M1 Complete initial modeling framework. Run system simulation with basic cooling system components and demonstrate feasibility. **Go/No-Go**: Models of concept demonstration systems predict reasonable trends.
- M2 Validated single-phase model built from building blocks, allowing for easy modification. **Go/No-Go:** Confirm that model can **On Track** be successfully validated and is predicting performance with acceptable accuracy (20%).
- M3. Improve solution method, allowing for dynamic valves. Validate model to within 10% of available data.
- M4. Improve model capabilities expanding on the single-phase, energy storage, and power electronics thermal models and validate. Apply developed Simulink tools with industry partners to look at system tradeoffs in co-simulation with vehicle model. Do initial thermal control investigations. Release updated code with expanded capabilities.

Approach/Strategy: Advanced Thermal System Modeling Framework

Develop MATLAB/Simulink-based models of the entire thermal system of a vehicle

- 1-D simulation tool based on first principles; conservation of mass, momentum, and energy
- Develop a flexible software platform capable of modeling the full range of vehicle thermal systems
- Include major components: heat exchangers, pumps, transport lines, fans, power electronics, battery chiller, thermostat, etc.
- Build on prior successful two-phase A/C model, adding single-phase coolant loop models for advanced vehicle thermal system simulations
- Develop models that run faster than real time
- Compatible with vehicle-level models for cosimulations in Simulink



Approach/Strategy: NREL's Advanced Combined Fluid Loop (CFL)

Multiple modes of operation without reversing VCC^{*} for greater efficiency





- Air conditioning
- Heat pump
- Free PEEM and battery cooling
- Free heating
- Battery heating
- Battery cooling

- PTC heating
- FEHX defrosting
- Cabin air dehumidifying

*VCC = Vapor Compression Circuit FEHX = Front End Heat Exchanger PTC = Positive Temperature Coefficient

Previous Technical Accomplishments

Two-phase refrigerant circuit simulation





Accomplishments: Quasi-Transient Approach for Coolant Loops

Finite volume solution method

Liquid/vapor networks modeled by 0-D volumes and 1-D pipes

In finite volumes, "stiffness" is proportional to *dp/dm* and is large for liquids



With the goal of reducing "stiffness":

• Use low artificial bulk modulus to make stiffness uniform across the network, allowing for larger time-steps

 $dp = \frac{B}{V} \frac{dm}{\rho_{ref}}$; $\frac{B}{V}$ = constant (and small)

Consequence:

- Mass and energy imbalances with fast transients, accurate in steady state
- Solution at every time step tends to approach a steady state solution corresponding to the instantaneous values of boundary conditions
- Provides much faster simulations
- Does not require specification of flow direction

Accomplishments: Added HFO-1234yf capability

1234yf shows slightly lower performance as expected, providing qualitative agreement



Accomplishments: Added Internal Heat Exchanger

Effectiveness based model



Technical Accomplishments: Application

Advanced Combined Fluid Loop



Top Level: A/C Model

Quasi-Transient model example



*Cycle Data = Vehicle and ambient data

2nd Level: Vapor Compression Cycle Circuit



- Pink blocks are the bottom level
- Yellow blocks have blocks below them

Accomplishments: Chiller Model

Using 1-D and 0-D blocks, various serial/parallel heat exchangers can be modeled



Photo by: Gene Titov (NREL)

Accomplishments: System Control Model Implemented

Added flexible controls of the system and modes



Technical Accomplishments: Application

Advanced Combined Fluid Loop



Combined Loops A/C mode All Modes

The approach allows for a simple and natural manipulation with valves to define system modes





Combined Loops A/C mode Active Cooling Mode

By changing valve positions the model can be switched to active cooling mode





Combined Loops Heat Pump Mode Active Heating Mode

A single model can be used to dynamically simulate various modes of operation





Accomplishment: Simulated and Measured Coolant Temperatures

Note mode switch of the front end heat exchanger (FEHX)



Accomplishments: Simulated and Measured Capacities (R134a)

9 out of 10 points fall within 95% of uncertainty intervals



RMS=4.18%. Error bars show 95% confidence intervals for measurement uncertainties.

Accomplishments: CFL Mode Control Test Case

At 150 sec, valves change to switch from active cooling to heating mode





350

Accomplishments: CFL Mode Control Test Case

Coolant loops stabilize following a mode switch



Accomplishments: CFL Mode Control Test Case

Heat sources and sinks change as the system switches modes



Accomplishments: Control Algorithm Development Potential

Select best mode for operating condition with declining waste heat



- Ambient temperature at -2°C
- PEEM heat assumed to linearly diminish from 5 kW to 0 kW
- After 350 seconds, model switches from free heating to heat pump mode to maintain the cabin temperature set point

Collaboration: Applications

Cummins and Oak Ridge National Lab

- Provide high-fidelity simulations of proposed A/C architectures
- Understand the impacts on the vehicle load
- Provide support for future hardware-in-the-loop testing.



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Collaboration:

Leveraging CoolSim on other projects

• MAHLE Behr – UTEMPRA FOA

- More operating modes than NREL CFL
- Modeling and testing

NREL FOA with Huyndai & Hanon

- A/C system impact on vehicle
- Coupling with CoolCalc analysis

Hannon-led FOA

- Thermal storage concepts
- Advanced heat pump modeling

Daimler Trucks

- Supported SuperTruck
- Assessing advanced HVAC concepts

Other collaborations

- o ANL
- In discussions with others







*Chowdhury, S., Zima, M. "Unitary Thermal Energy Management for Propulsion Range Augmentation (UTEMPRA)". DOE AMR 2015. Project ID VSS157

Responses to FY15 AMR Reviewer Comments

- Comment: The reviewer would like to see this program leverage the Cool Cab HD sleeper program and understand if there are other cooling philosophies that can be applied such as zoning, etc.
- Response: NREL's detailed HVAC and thermal system model, CoolSim, is a critical part of the CoolCab HD sleeper national-level analysis. CoolSim provides the link between cab thermal loads and mechanical/electrical loads on the vehicle. These system details drive the coefficient of performance of the system, which is important to determining the vehicle load and resulting fuel use. As the reviewer suggests, these tools can be used together to understand other advanced cooling philosophies such as zoning, etc.
- Comment: The reviewer asked if there is a commitment by DOE to maintain compatibility of these models and enough support to ensure that this capability will function long enough to provide significant return on investment (e.g., three to five years).
- Response: We agree with the reviewer that providing support for the tool maintenance, improvement, and application over a period of time will strengthen this capability and add more value and increase return on investment. We believe this tool is adding significant value to DOE's program and our industry partners.

Comment: The reviewer indicated that the accomplishments appear in line with the program, although the reviewer would like to see the details behind the vehicle cabin model and whether this can be further optimized.

Response: CoolSim currently uses a fairly simple 1 or 2 air node model. Basic thermal mass, conduction, and convection are accounted for. Solar loads incident on the vehicle are an input. This model works well for basic simulation needs. However, NREL plans to develop a more detailed model for CoolSim, but these efforts have been delayed due to funding limitations.

Proposed Future Work and Remaining Challenges

Continue model development

- Add oil loop modeling capability to expand into new areas of application
- Integrate with CoolCalc for advanced cabin modeling
- Add new thermal components (such as a detailed battery model)
- Co-simulation with vehicle level models for advanced system design
- Model applications with industry partners and use to research advanced thermal systems
 - Model advanced light-duty vehicle thermal systems
 - Heat pump system
 - Advanced heat recovery concepts
 - Build validated idle-off long-haul truck A/C system model
 - Evaluate control strategies that optimize efficiency for advanced loop concepts
- Improve Autonomie co-simulation
- Leverage model results for the VTCab project impact estimation

Summary

- Improved single-phase model to allow dynamic valve switching and flow direction reversal
 - Useful for simulations of complex coupled refrigerant and liquid coolant-based thermal sub-systems where modes of operation will change
 - Validated for steady-state CFL system operating conditions;
 9 out of 10 simulated points are within the 95%
 measurement uncertainty band for capacity
- Demonstrated dynamic control, which will be used for advanced system design and impact quantification
- Added 1234yf refrigerant and internal heat exchanger model
- Collaborated with Cummins and ORNL on A/C system model
- Increased industry partnerships and leveraged developed tools for multiple advanced system projects

Contacts and Acknowledgements

Contacts

- Jason Lustbader <u>Jason.lustbader@nrel.gov</u>
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A generic A/C system model is available at:

http://www.nrel.gov/transportation/coolsim_disclaimer.html?accept

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 - Cummins
 - o ORNL
 - o Hanon



Technical Back-Up Slides

Technical Accomplishments:

Distributed parameter model

Two coolant passes in this example



- A pass is a number of plates over which the coolant and airflow can be assumed identical.
- A pass in this sense can be a traditional pass (serial pass) or some number of plates in a serial pass bundled together to create parallel passes (e.g., when airflow is very non-uniform).
- Only one plate in each pass is simulated; heat transfer and flow rates are multiplied by number of plates
- The steady-state flow conditions are calculated using conservation of mass, momentum, and energy.

Methods used for distributed parameter component models

One tube segment

$$Q_{ta} = (\dot{m}_{a} \cdot C_{p,adry} + \dot{m}_{w} \cdot C_{p,aw}) \cdot (T_{a,o} - T_{a,i})$$

$$T_{t}$$

$$T_{a,o} = T_{a,i} + (T_{t} - T_{a,i}) \cdot \left[1 - \exp\left(\frac{-\bar{h}_{ta} A}{\dot{m}_{a} \cdot (C_{p,adry} + \omega C_{p,w})}\right)\right]$$
(Effectiveness-NTU (number of transfer units) method applied for each pipe segment for the air flow)

$$Q_{ct} = \bar{h}_{ct} A (T_{c} - T_{t})$$

$$(\overline{Nu}_{D} \equiv) \frac{\bar{h}_{ct}D}{k} = 0.023Re_{D}^{0.8}Pr^{n}$$
Calculation assumptions:

$$Q_{ta} = (\dot{m}_{a} \cdot C_{p,adry} + \dot{m}_{w} \cdot C_{p,aw}) \cdot (T_{a,o} - T_{a,i})$$

$$(T_{a,o} - T_{a,i}) \cdot \left[1 - \exp\left(\frac{-\bar{h}_{ta} A}{\dot{m}_{a} \cdot (C_{p,adry} + \omega C_{p,w})}\right)\right]$$
(Effectiveness-NTU (number of transfer units) method applied for each pipe segment for the air flow)

$$(T_{a,o} - T_{c}) \cdot T_{a,o} - T_{a$$

1. Chang, Y.J.; Wang, C.C. (1997). "A Generalized Heat Transfer Correlation for Louver Fin Geometry." *Int. J. Heat Mass Transfer*, Vol. 40, No. 3, pp. 533-544.