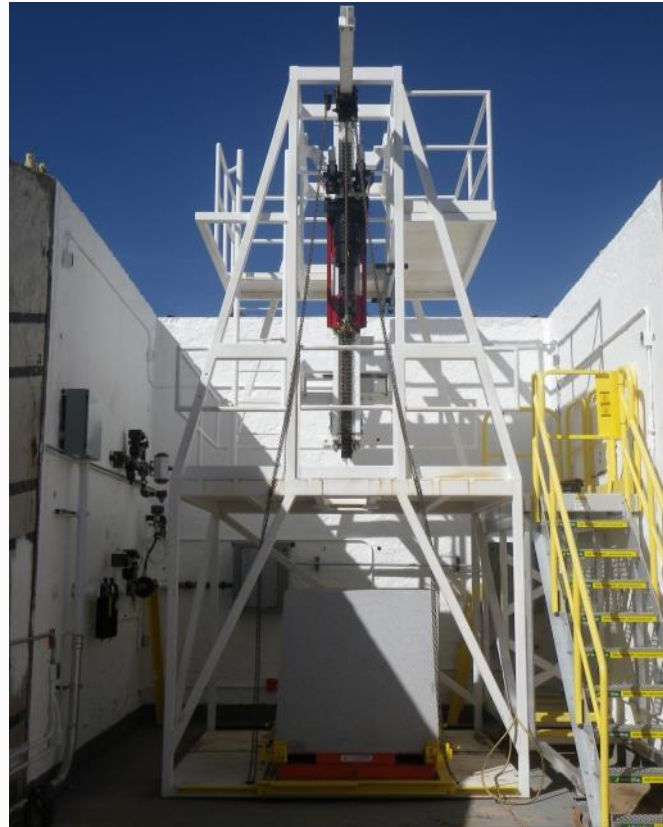




Atlas Copco



Sandia National Laboratories

Advanced Percussive Drilling Technology for Geothermal Exploration and Development

Project Officer: Michael Weathers

Total Project Funding: \$3.2M

May 13, 2015

Principal Investigator

Dale Wolfer

ATLAS COPCO SECOROC, LLC

HRC

- Purpose: To develop percussive hammer technology capable of operating in high-temperature geothermal formations
- Percussive hammers have the potential to reduce overall well construction costs by significantly improving the penetration rate.
 - Example: 3000 m well, Rig costs \$50K/day
 - Conventional method: Avg. ROP 7 m/hr ; Time 429 hr ; Cost \$900K
 - HTDTHH method: Avg ROP 21 m/hr ; Time 143 hr ; Cost \$300K
- Technical Barriers and Challenges
 - Find alternative design solutions to conventional polymer components
 - Find alternative design solutions to conventional elastomeric seals
 - Eliminate the need for hydrocarbon based lubricants
 - Find alternative solutions to metal parts with low temperature heat treatment
 - Develop laboratory testing facilities capably of validating the design at the target temperature

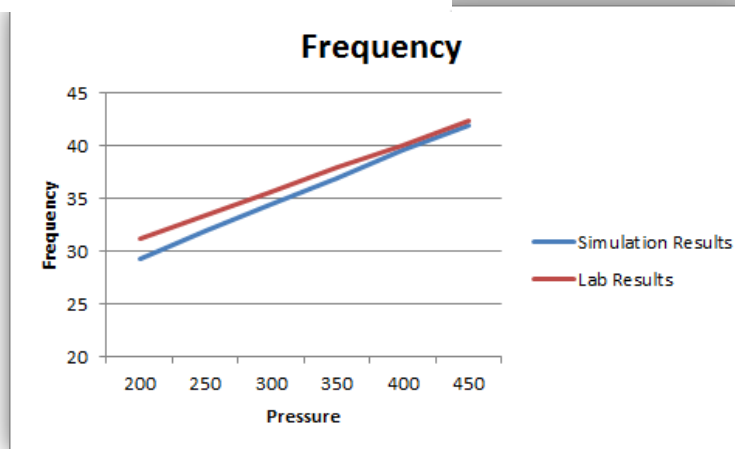
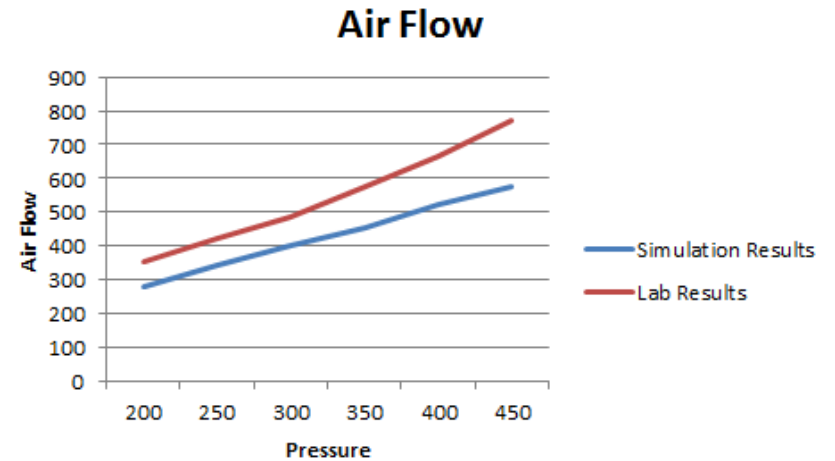
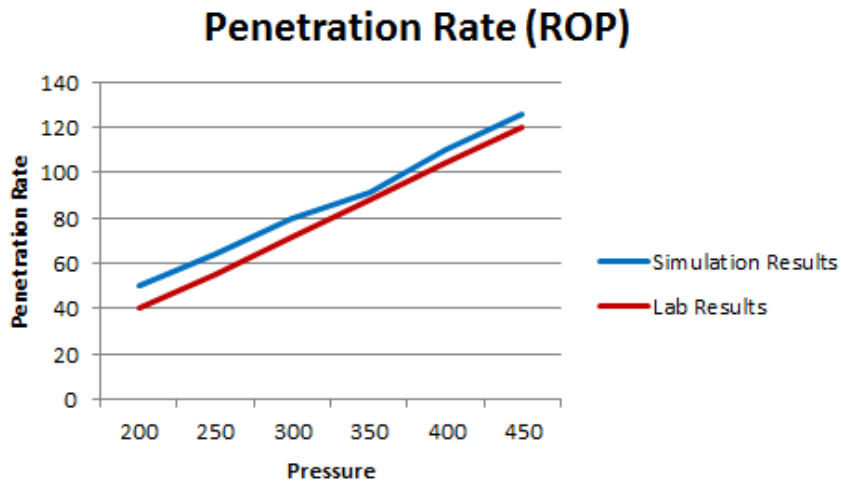
- Success within this project will impact the Geothermal Technologies Office's goals by:
 - Reducing geothermal well drilling costs, thereby reducing the overall cost of a project, thereby reducing LCOE
 - Driving industry deployment by making proposed projects more economically attractive
- Technical Targets
 - Achieve 3X drilling rate vs. conventional rotary drilling methods
 - Capability to drill to 3000 meters depth and formation temperature of 300 C
 - Develop percussive hammer design to operate reliably within the expected temperature range
 - Develop viable internal sealing systems at HT
 - Identify and develop lubricating strategies at HT
 - Insure material properties are sufficient for reliable operation in high temperature, corrosive drilling environment

- Phase 1: Proof of Concept
 - Requirements definition for operating conditions
 - Thermodynamic cycle computational modeling of proposed DTH cycles
 - Finite Element Analysis (FEA) of structural components and systems
 - Systems solution and configuration definition
 - HT percussive hammer design, analysis and evaluation
 - Materials selection, qualification and testing along with review of technical literature for identification of potential materials and/or processes
 - Coupon level environmental coatings and bulk property testing

- Phase 2: Component and System Level Testing
 - Establish baseline prototype hammer performance at the Atlas Copco Roanoke test facility
 - Provide Proof-of-Concept (POC) validation via laboratory testing of representative design features.
 - Build full-scale prototype hammers based on design and material selection from Phase 1
 - Test and characterize prototype hammers under ambient conditions at the Atlas Copco Roanoke test facility
 - Identify options and test requirements for high-temperature test facility
 - Design, build and test high-temperature test facility
 - Validate performance of prototype HT hammer at temperatures up to 300° C on the high-temperature facility

- Flow / Counterflow modeling of deep hot borehole
- Requirements defined for drilling environment and operational specifications
- Establish baseline DTHH performance
- Design and build full scale Proof of Concept DTHH
- Computational modeling of performance for full scale POC DTHH
- Identify current materials and identify candidate materials and coatings for qualification testing
- Analyze and test bit button retention for hot drilling environment
- Construct prototype DTHH for low temperature component and system level lab testing
- Complete material and coating qualification testing
- Select materials and coatings for HT prototype
- Validate selected materials and coatings by bench-scale testing
- Complete low temperature component and prototype testing and cycle optimization
- Identify options for internal sealing at high temperature
- Design and build prototype for high temperature testing.
- Design and construct test facility for high temperature testing of HTDTHH prototype, including process gas heater, hammer heater, rock sample positioning, feed and rotation system, controls and instrumentation.
- Begin low temperature validation of HT prototype vs LT prototype results.

Simulation vs Prototype Results



Internal Sealing

- Initial testing showed internal leakage between the Air Distributor and Cylinder dramatically limited hammer performance
- Low temperature testing using a conventional Buna –N o-ring showed that effective sealing would correct the problem
- Alternatives for High Temperature sealing
 - Interference fit
 - Permanent joining of Air Distributor and Cylinder
 - High temperature, graphite filled valve packing seal
 - High temperature elastomer
- Evaluated valve packing and Kalrez o-ring
 - Valve packing provided fair sealing performance, more development is necessary
 - Kalrez o-ring is a drop in replacement for standard elastomers and is fully capable of performing satisfactory in the target environment (Max. temperature rating 327 C)

Button Retention Testing

- Impact testing up to 12,000 g
- Varying interference fits to simulate button hole expansion due to temperature
- Two buttons with the least interference began shifting at 10,000 g
- All other buttons remained in place up to 12,000 g
- Conclusion: current interference fit is suitable to retain buttons in a bit, up to 600 F



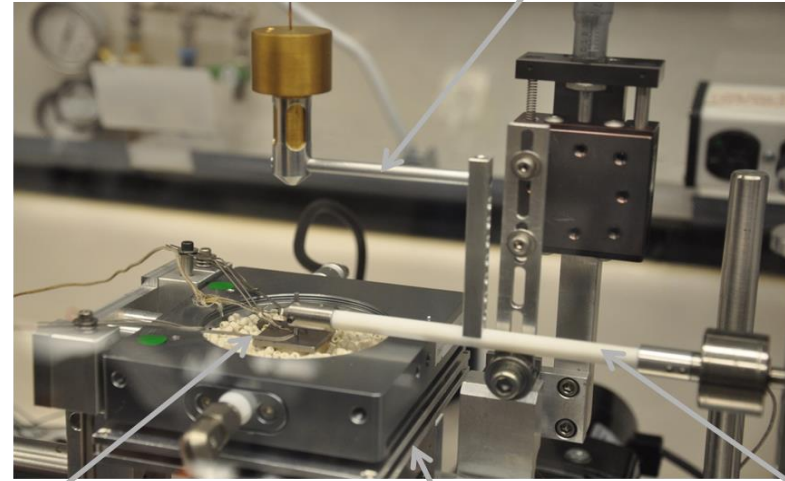
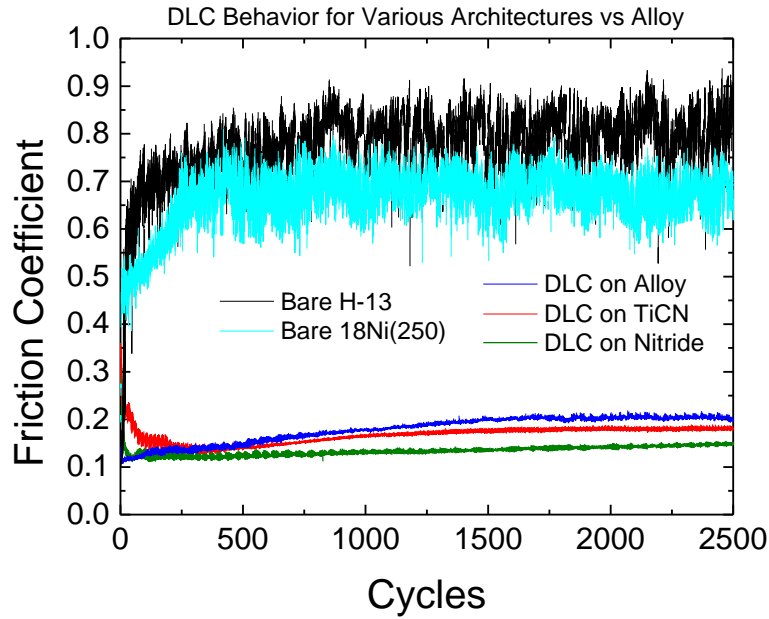
Material Selection

- Focus on Casing, Air Distributor, Piston, Bearing
 - Conventional parts are tempered below the target geothermal operating temperature
 - Fatigue resistance is a key property
 - Corrosion resistance is important
- Selection Process
 - Literature search to determine properties of current materials and identify candidate materials with good physical properties at 300 C
 - Qualification testing of candidate material, including
 - Tensile strength
 - Charpy impact toughness
 - Fatigue
 - Abrasion resistance
 - Friction and wear characteristics
- Results
 - No candidate material showed better properties than the existing casing material. Surface hardening will be omitted from part specifications
 - A precipitation hardening stainless steel was selected for the piston
 - A hot working tool steel was selected for the Air Distributor and Bit Bearing

Lubricious and Wear Resistant Coatings

- Thermal Spray Coatings
 - Four (4) commercially available coatings tested
 - Addition of hBN or MoS₂ was also evaluated
 - Testing Conducted:
 - Hardness
 - Abrasive wear
 - Friction
 - Tensile adhesion of coating
 - Impact fatigue resistance
- Vapor Deposition Coatings
 - Two (2) candidate coatings evaluated
 - Diamond Like Coating (DLC) with ceramic barrier level
 - DLC with multiple barrier layers (TiCN nanolaminate and ceramic barrier layer)
 - Tested for friction and wear properties at 300 C
 - Multiple layer sample developed cracks and delaminated
 - DLC with single SiO barrier layer showed good friction resistance and no delamination



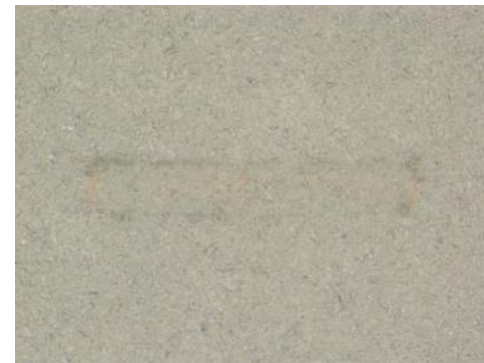


Dead weight load arm cantilevered to reduce conduction heat loss to weights.

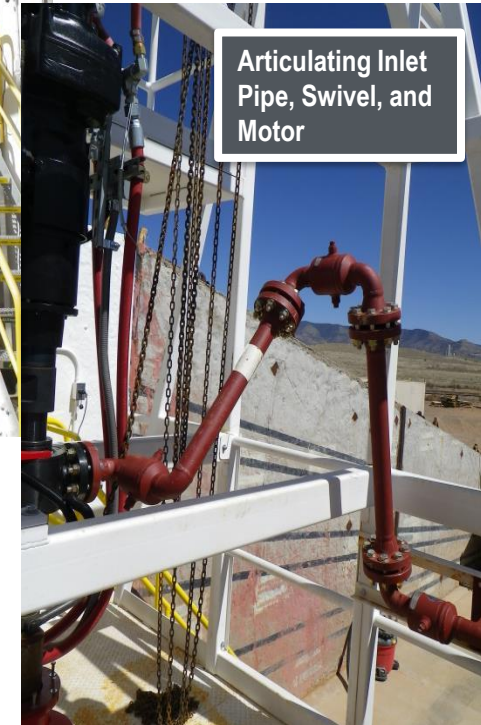
Bed of ceramic beads used to isolate heat application and test coupon.

Thermal barrier and heat exchanger fins to prevent conduction to the rest of the assembly.

Ceramic rod used to prevent heat conduction to load cell.

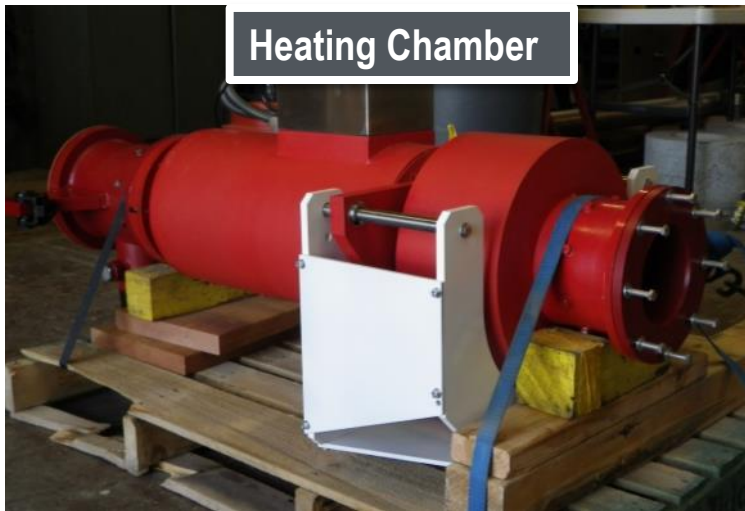


- Capability to simulate high-temperature drilling conditions (up to 300°C)
- Evaluate effects of thermal shock on hammer components
- Evaluate effectiveness of coatings and materials in simulated geothermal conditions
- Enabling features for safely testing at high-temperatures
 - Pneumatic operation
 - Dual-stage air filtration system for process gas
 - High-temperature swivel
 - Atlas Copco pneumatic motor
 - Articulating feed pipe joint
 - Rock positioning system



High Temperature Test Cell

- Capacities
 - Weight on Bit (WOB) – to 6000 lbf
 - Rotation speed – up to 60 rpm
 - Rotation torque – up to 2500 ft -lbf
 - Feed Rate - up to 100 ft/hr
 - Hammer heater – up to 300 C (9kW heater)
 - Process gas heater – up to 300C (190 kW heater)



Heating Chamber



Process Gas Heater

- Future Work and Directions
 - Conduct ambient temperature testing to validate HT Prototype - Complete March 31, 2015
 - Qualification testing of HT test apparatus – Complete by April 30, 2015
 - Conduct HT testing of HT DTHH and validate results – Complete by December 31, 2015
 - Prepare and submit Final Report for Project

- **Conclusions to Date**
 - Low temperature prototype testing shows ROP target can be met.
 - Low temperature test results compare favorably with computational model predictions.
 - Current interference fit of cutting elements in the bit body can successfully retain them at target operating temperature.
 - Laboratory based material and coating testing show selected materials and coatings can be effective in a high temperature drilling environment