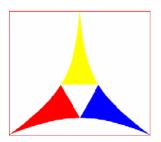
SYSTEM IMPACT STUDY

MAR 2014 (REVISION 3)

CLEAN LINE ENERGY PARTNERS

SHELBY - 3500 MW



PLANNING & SYSTEMS ENGINEERING (901) 528 - 4292

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Disclaimer

While every effort has been made to ensure that the content of this report is accurate, the engineering staff makes no representation or warranties in relation to the accuracy or completeness of the information found within. The content of this report is provided in good faith, according to the study inputs that were provided from the interconnecting party and the other affected parties.

SIGNATURES

* *	CLEAN LINE SYSTEM IMPACT STUDY REV. 3	
PREPARED:	DATE: 3-25-14 Randell Lynding Friginger Planning & Systems Engineering	
PREPARED: _	DATE: 3-25-14 Bryant Williamson, P.E. Lead Bulk Planting Engineering Planning & Systems Engineering	
APPROVED:	Mason Favora, P.B. Supervisor Planning and Systems Engineering	

EXECUTIVE SUMMARY

CLEAN LINE SYSTEM IMPACT STUDY REV. 3

The proposed 3500 MW interconnection at Shelby was studied for both MLGW peak and off-peak conditions, using the full generation capacity at Allen Steam Plant. Each case demonstrated a 2016 power flow model which included TVA's proposed system improvements as a result of the interconnection. The cases also include an Entergy system upgrade not evaluated in earlier versions of this system impact study. A fault study was also performed with ASPEN software to compare pre and post interconnection injected fault models using equivalents at all TVA/MLGW delivery points. TVA contracts a third party to run a stability study on their service area. MLGW is included in the TVA system therefore is covered by the TVA stability study.

The MLGW results are as follows:

Shelby:

Contingency #01 Result Pg #: 7,8,16,17 Uprate Allen – Holmes transmission line (35 – 47):

Contingency #02 Result

Pg #: 7,9,16,17

Uprate Allen – Pidgeon transmission line (35 – 82):

Contingency #03 Result

Pg #: 7,10,16-18

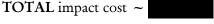
Mitigation Plan - Close Normally-Open Sectionalizing Breaker at Shelby (65)

Contingency #04 Result

Pg #: 7,11-13,16,17,19,20

Uprate Shelby - NE Gate transmission line #1 (65 - 33):

Uprate Shelby – NE Gate transmission line #2 (65 – 33):



^{*} Colors correspond to contingencies throughout the System Impact document.

Expiration:

A new System Impact Study may be required if a Facility Study is not requested by June 25, 2014 (90 calendar days from the date of this document's approval)

ACKNOWLEDGEMENTS

CLEAN LINE SYSTEM IMPACT STUDY REV. 3

MLGW's Bulk Transmission Planning team would like to acknowledge the technical assistance and expertise received from the Transmission Interconnection Planning team at TVA. The collaboration of both teams made the success of this study possible.

PROCESS

CLEAN LINE SYSTEM IMPACT STUDY REV. 3

As stated above, this System Impact Study (SIS) consists of a power flow analysis and a short circuit analysis. A stability analysis for the MLGW system is included in TVA's impact study.

The purpose of this impact study is to provide a preliminary cost estimate and project time duration that is necessary to rectify the impacts identified in this study. A detailed cost estimate and construction schedule is to be included in the Facility Study, to be performed at the request of the interconnecting party, as outlined in the latest MLGW Facility Connection Requirements document. This System Impact Study is valid for 90 days after the report submission to the interconnecting party. If the Requesting Entity decides to proceed with the proposed interconnection, the Requesting Entity should request a Facility Study before this System Impact Study expires. (See page 2)

All costs presented within the content of this study are present value.

DEFINITION OF SYSTEM IMPACT

CLEAN LINE SYSTEM IMPACT STUDY REV. 3

MLGW defines a "system impact" as follows:

A loading increase ≥ 5% on transmission lines or transformers	AND	Loading on transmission lines and/or transformers ≥ 100%	For Category A, B and select Category C power flow studies
A total fault current increase ≥ 5%	AND	Any breaker that is susceptible to total fault currents ≥ 95% of rating	In Isc studies
Bus voltage change ≥ 5%	AND	Bus voltage ≤ 0.95 nominal	For Category A, B and select Category C power flow studies
Any new transient stability issues**			In dynamic studies performed by TVA
Any new negative impacts on existing stability issues**			In dynamic studies performed by TVA

Table 1: MLGW System Impact Criteria

These criteria definitions are listed MLGW's most recent Facility Connection Requirements document that is published by MLGW's Bulk Planning Engineering department. This document is also available for evaluation at http://www.mlgw.com/images/content/files/pdf/FacilityConnectionReqmts.pdf. MLGW's Category A, B and C power flow study definitions are defined in MLGW's annual Transmission Reliability Assessment and are available upon request to approved parties.

** -- TVA has performed the associated transient stability studies for MLGW's system for this study, and TVA's report will include any transient stability issues on MLGW's system.



METHODOLOGY

SHELBY STUDY - 3500 MW

Prior to this MLGW Revision 3 study, TVA performed an additional power flow system impact study and determined the impacts to their system. TVA has developed solutions to these impacts, which MLGW has included in the power flow cases that were shared by TVA for analysis. MLGW has verified that the TVA cases model accurate data for the MLGW system.

MLGW then studied peak and off-peak case conditions with full generation capability at Allen Steam Plant. The generation level at the TVA-owned Allen Steam Plant has a direct impact on transmission loadings in Shelby County. Under normal conditions, the coal-fired units are running without the gas-fired units; however, there are times when both the coal-fired and gas-fired units are online. Furthermore, MLGW's peak loadings occur in the summer while TVA experiences peak loading conditions in the summer as well as the winter. For this study, TVA and MLGW have chosen to examine what is considered "worst case" scenarios. These cases include the proposed Shelby interconnection in both summer and winter peak cases, with coal-fired and gas-fired units online.

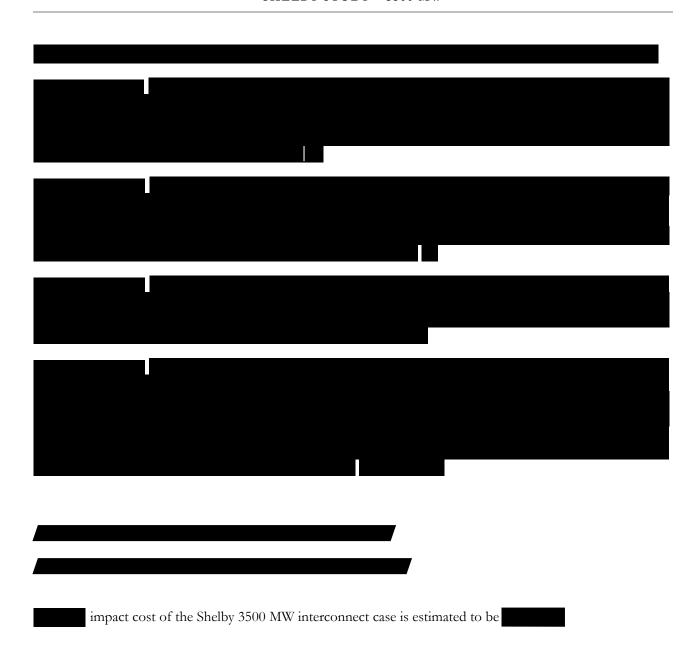
Below are the cases examined for the Shelby Study:

- 2016 Summer base case, Allen coal & gas units
- 2016 Winter base case, Allen coal & gas units
- 2016 Summer with 3500 MW inject at "Shelby", with TVA's improvements, Allen coal & gas units
- 2016 Winter with 3500 MW inject at "Shelby", with TVA's improvements, Allen coal & gas units

TVA provided fault analysis equivalents for cases with and without the proposed 3500 MW Clean Line interconnection. MLGW verified that the TVA cases modeled the MLGW system accurately. MLGW then compared the fault current for each bus within its system, considering the symmetrical and unsymmetrical portions of the fault to determine the impacts. See page 4 for the definition of an impact.

RESULTS

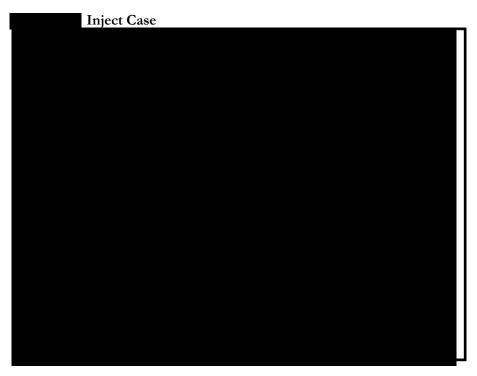
SHELBY STUDY -3500 MW



SHELBY STUDY - 3500 MW

Contingency #01: Loss of circuit Allen – Pidgeon (35-82)

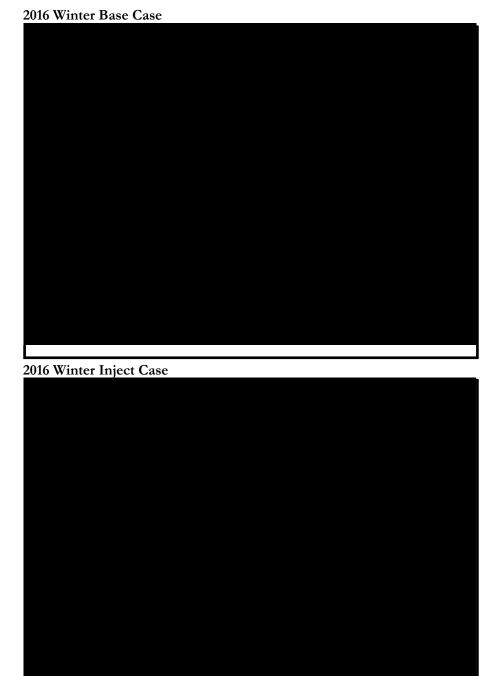




Proposed generation causes the overload of MLGW circuit #35661. Due to a previous system study, circuit #35561 will be uprated to its 100° C rating. No cost will be associated with this uprate.

SHELBY STUDY - 3500 MW

Contingency #02: Loss of double circuit tower, Allen – Holmes AND Allen – Horn Lake (35-47, 35-Horn Lake)



Proposed generation causes the overload of MLGW circuit #35671. Due to a previous system study this circuit was identified to be uprated to its 100°C rating. The uprate reduces the cost for this overload to \$0.

SHELBY STUDY - 3500 MW

Contingency #03: N-1-1 Contingency, Shelby#1 Transformer & Fite -- Shelby (65-36)

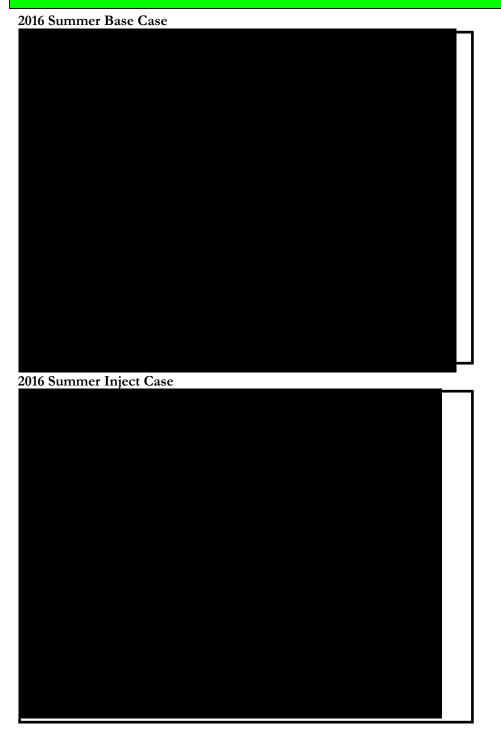
2016 Summer Base Case

2016 Summer Inject Case

Proposed generation causes the overload of circuit #33629. MLGW will relieve the overload on circuit #33629 by operating the normally-open sectionalizing breaker at Shelby substation.

SHELBY STUDY - 3500 MW

Contingency #04: Loss of double circuit towers, Shelby – Fite AND Shelby – Millington (65-36, 65-15)



Proposed generation causes the overload of circuits #33629 and #33687. During a previous system study, these lines were identified to be uprated to their 100°C rating. Despite this, the terminal equipment still limits the circuits to ratings that are unacceptable for these conditions. The upgrades and costs are discussed on the following pages.

ONE – LINE: TERMINAL EQUIPMENT

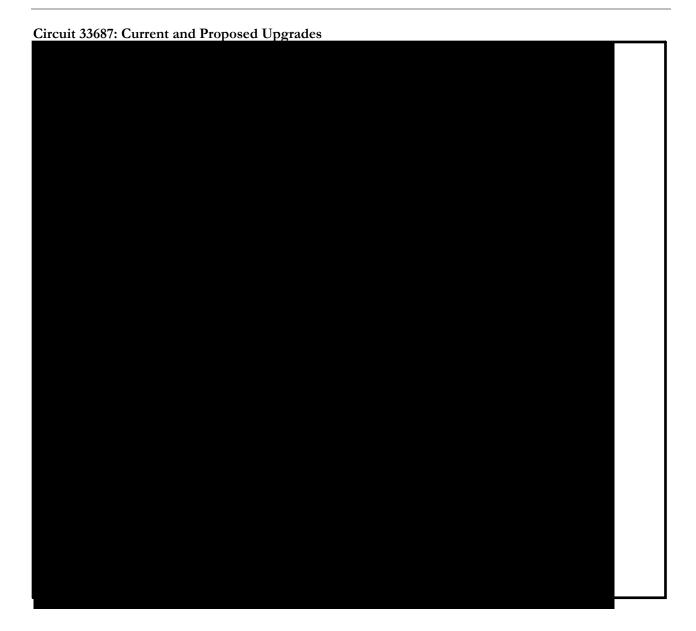
SHELBY STUDY - 3500 MW

For Contingency #04, proposed generation causes the bus cable, wave trap, relay and meters at Substations 33 and 65 to need replacing at a total approximate cost of the following figures show the one-line diagrams of current and proposed upgrades.

Circuit 33629: Current and Proposed Upgrades

ONE – LINE: TERMINAL EQUIPMENT

SHELBY STUDY - 3500 MW



ALTERNATIVES CONSIDERED

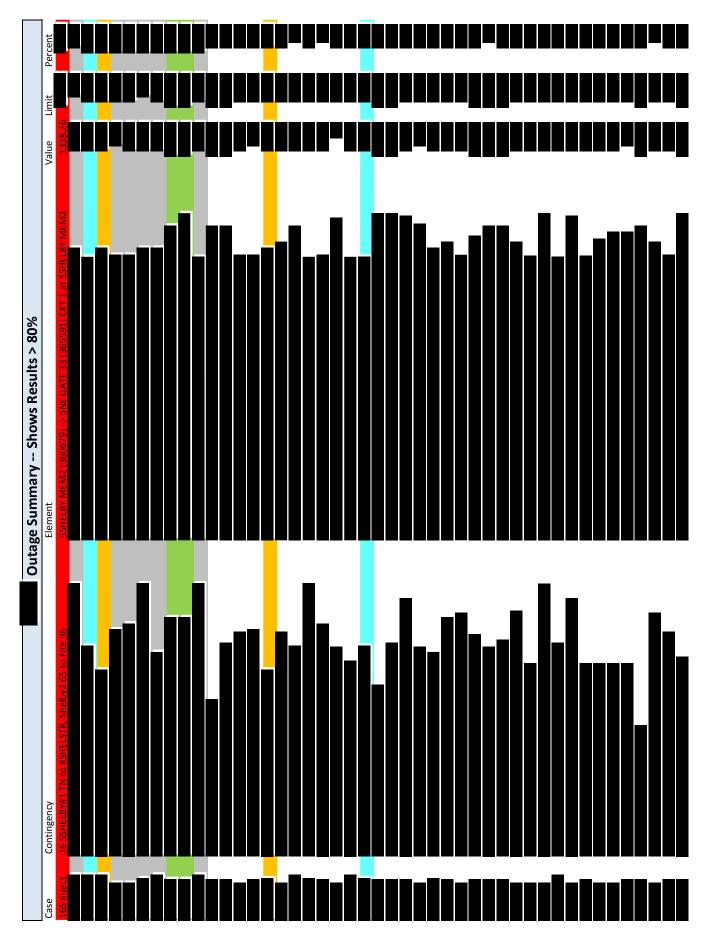
SHELBY STUDY - 3500 MW

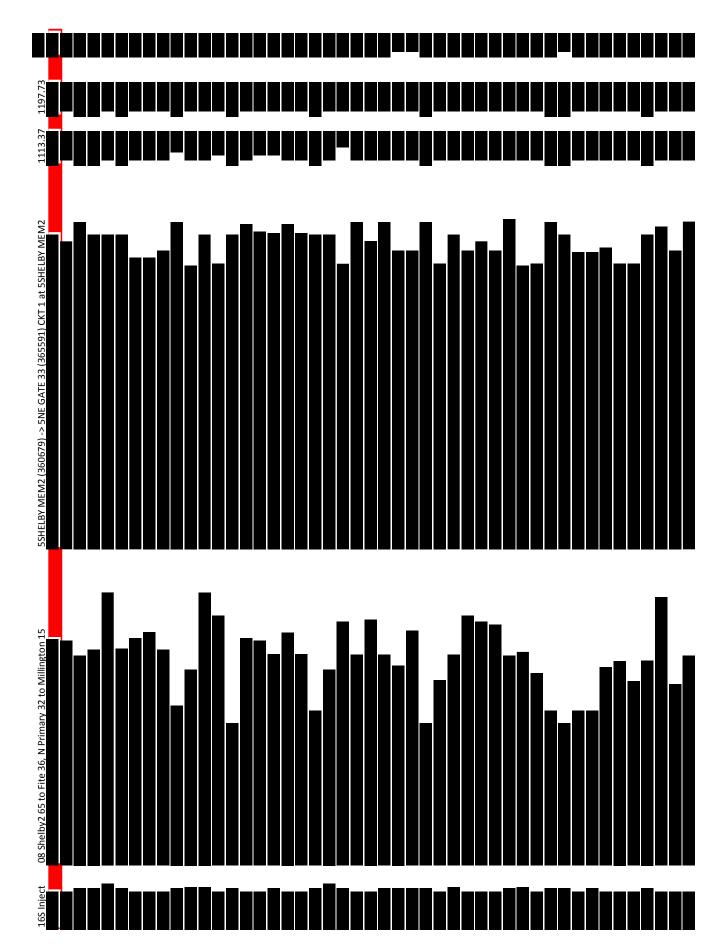
Alternatives considered in this SIS include the possible addition of a transmission switching station on the MLGW BES. However, as in iteration 1 of this study, that proposal was proved to be cost ineffective.

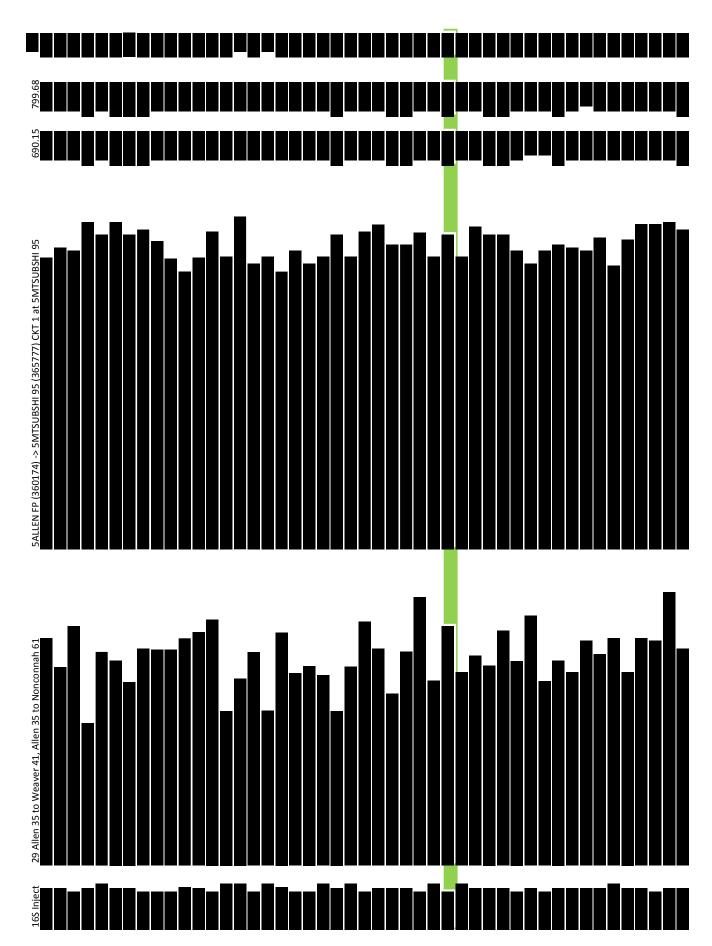
SUPPORTING DOCUMENTATION

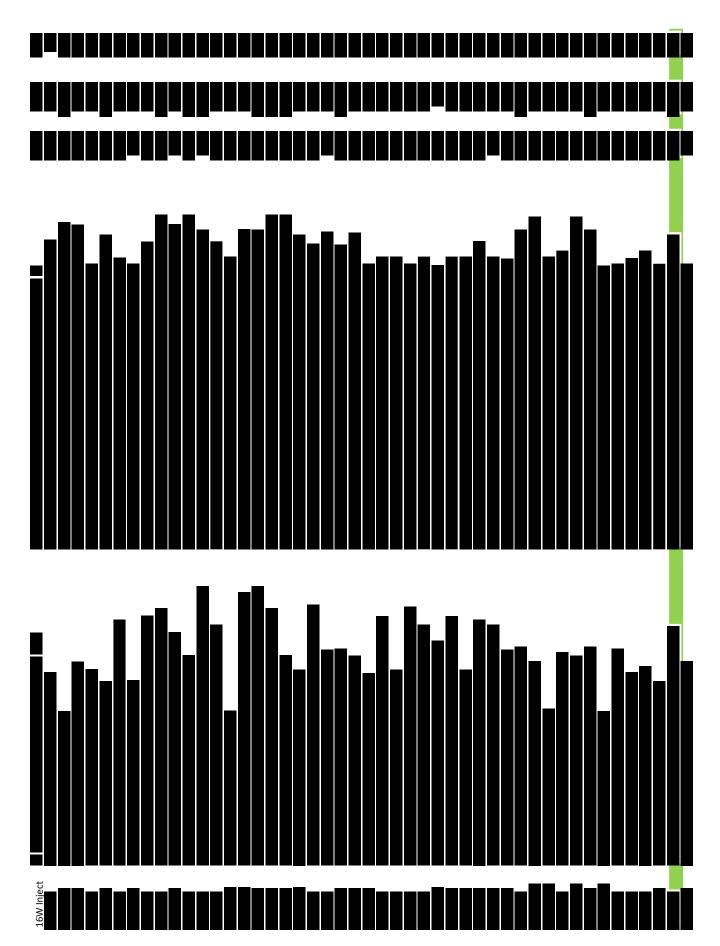
			Contingency		
	Outage of Allen 35 to Pidgeon 82	Outage of Allen 35 to Outage of SHELBY#1 Horn Lake & Allen 35 to Xfrmr & Shelby2 65 to Holmes 47 Fite 36	Outage of SHELBY#1 Xfrmr & Shelby2 65 to Fite 36	Outage of Shelby 65 to Millington 15 & Shelby 65 to Fite 36	llington 15 & Shelby 65 36
10 per 0 2000 12	Allen 35 to	Allen 35 to	Shelby2 65 to	Shelby1 65 to	Shelby2 65 to
בופווופווו סאפווסממפט	Holmes 47	Pidgeon 82	NE Gate 33	NE Gate 33	NE Gate 33
16 Summer Base Case					_
16 Summer Inject Case	1				
16 Winter Base Case					
16 Winter Inject Case					

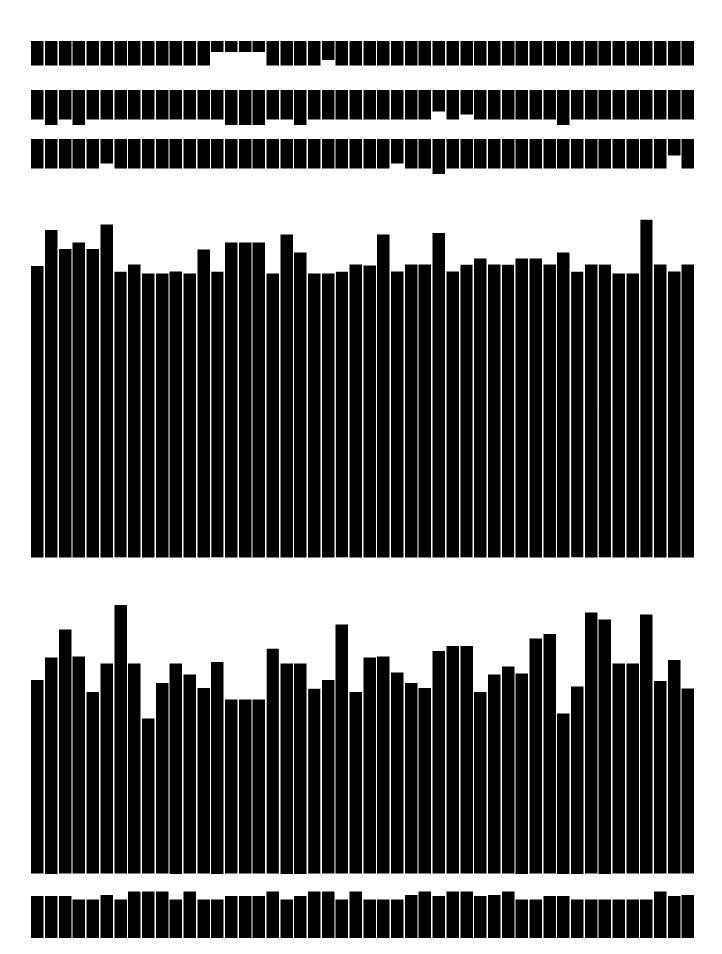
Colors correspond to outage records on next page

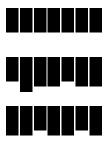


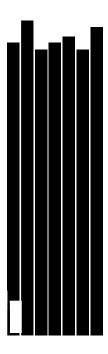


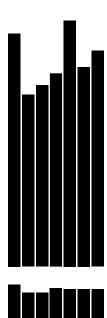












		Dana Cara	Cholby	Maximum Isc
		Base Case	Shelby	increase
BUS NAME	NOM. KV	Total Isc	Total Isc	
01 S Gate	115	28334	28341	0.0%
02E N Gate	115	24991	24999	0.0%
02W N Gate	115	25365	25374	0.0%
03 Third St	115	12407	12409	0.0%
04 Front	115	12339	12340	0.0%
05 Poplar	161	17817	17827	0.1%
06 Willett	115	19358	19363	0.0%
07 Chelsea	161	21797	21811	0.1%
11 Mallory	161	25221	25229	0.0%
13 Woodstock	115	12508	12510	0.0%
14 Frayser	115	15203	15207	0.0%
15 Millington	161	15099	15114	0.1%
21 Crump	115	20148	20153	0.0%
23 Brookfield	161	33370	33396	0.1%
24 DuPont	115	13051	13053	0.0%
25 Getwell	115	18014	18019	0.0%
26 Macon	115	16902	16907	0.0%
27 Millbranch	115	14930	14933	0.0%
28 Winchester	161	26761	26777	0.1%
31 S Primary	161	42935	42962	0.1%
32 N Primary	161	33116	33149	0.1%
33 NE Gate	115	21657	21665	0.0%
33 NE Gate	161	47373	47440	0.1%
34 SE Gate	115	25461	25468	0.0%
34 SE Gate	161	51754	51811	0.1%
35 Allen Steam Plant	161	58293	58322	0.1%
36 Fite Rd	115	11571	11573	0.0%
36 Fite Rd	161	21820	21838	0.1%
38 Raleigh	161	22103	22118	0.1%
39N Cordova	161	48330	48398	0.1%
39 S Cordova	161	42724	42767	0.1%
41 Weaver	161	23876	23883	0.1%
42 Southern	161	19362	19370	0.0%
43 Elmore	161	27842	27864	
44 Oakville	161			0.1%
45 McLemore		27193	27207	0.1%
	161	26244	26252	0.0%
46 N Frayser	161	18759	18771	0.1%
47 Holmes	161	42536	42565	0.1%
48 Yale Rd	161	28986	29012	0.1%

61 Nonconnah 161 29 62 Valero Refinery 161 25 65 Shelby 161 43 66 Collierville 161 30 67 Buoy St 161 27 68 Arlington 161 18	587 22602 453 29465 181 25189 346 43109 562 30585 048 27056	0.1% 0.0% 0.0% -0.5% 0.1%
49 University 161 225 61 Nonconnah 161 295 62 Valero Refinery 161 25 65 Shelby 161 435 66 Collierville 161 305 67 Buoy St 161 270 68 Arlington 161 185	587 22602 453 29465 181 25189 346 43109 562 30585 048 27056	0.0% 0.0% -0.5% 0.1%
61 Nonconnah 161 29 62 Valero Refinery 161 25 65 Shelby 161 43 66 Collierville 161 30 67 Buoy St 161 27 68 Arlington 161 18	181 25189 346 43109 562 30585 048 27056	0.0% -0.5% 0.1%
65 Shelby 161 433 66 Collierville 161 304 67 Buoy St 161 270 68 Arlington 161 183	346 43109 562 30585 048 27056	-0.5% 0.1%
66 Collierville 161 309 67 Buoy St 161 270 68 Arlington 161 183	562 30585 048 27056	0.1%
67 Buoy St 161 270 68 Arlington 161 18'	27056	
68 Arlington 161 18'		0.0%
	750 10700	0.07
69 Freeport 161 528	758 18768	0.1%
	861 52903	0.1%
71 Clarke Rd 161 199	551 19559	0.0%
72 TrinityRd 161 303	30339	0.1%
73 Houston Levee 161 <mark>26</mark>	137 26155	0.1%
74 Shelby Drive 161 24	136 24147	0.0%
76 Dunlap 115 193	340 19345	0.0%
77 Poplar Estates 161 <mark>33</mark>	132 33156	0.1%
79 Shelton 161 16 2	254 16261	0.0%
81 Fletcher Creek 161 28	90 <mark>7</mark> 28931	0.1%
82 Pidgeon 161 410	692 41709	0.0%
84 N Bartlett 161 15:	296 15302	0.0%
85 Lakeland 161 <mark>27</mark> 3	210 27232	0.1%
86 Collierville Gate 161 31:	360 31384	0.1%
87 Shady Grove 161 30	102 30123	0.1%
93 Praxair 115 120	695 12697	0.0%