



**Argonne**  
NATIONAL  
LABORATORY

*... for a brighter future*



U.S. Department  
of Energy



THE UNIVERSITY OF  
CHICAGO

A U.S. Department of Energy laboratory  
managed by The University of Chicago

# ***SPRAY STRUCTURE MEASURED WITH X-RAY RADIOGRAPHY***

*Alan Kastengren, Christopher Powell  
Center for Transportation Research, Argonne National  
Laboratory*

*Thomas Riedel  
Corporate Research, Robert Bosch GmbH*

*Seong-Kyun Cheong, Kyoung-Su Im, Xin Liu, and Jin Wang  
Advanced Photon Source, Argonne National Laboratory*

*DOE FreedomCAR & Vehicle Technologies Program  
Program Managers: Kevin Stork and Gupreet Singh*

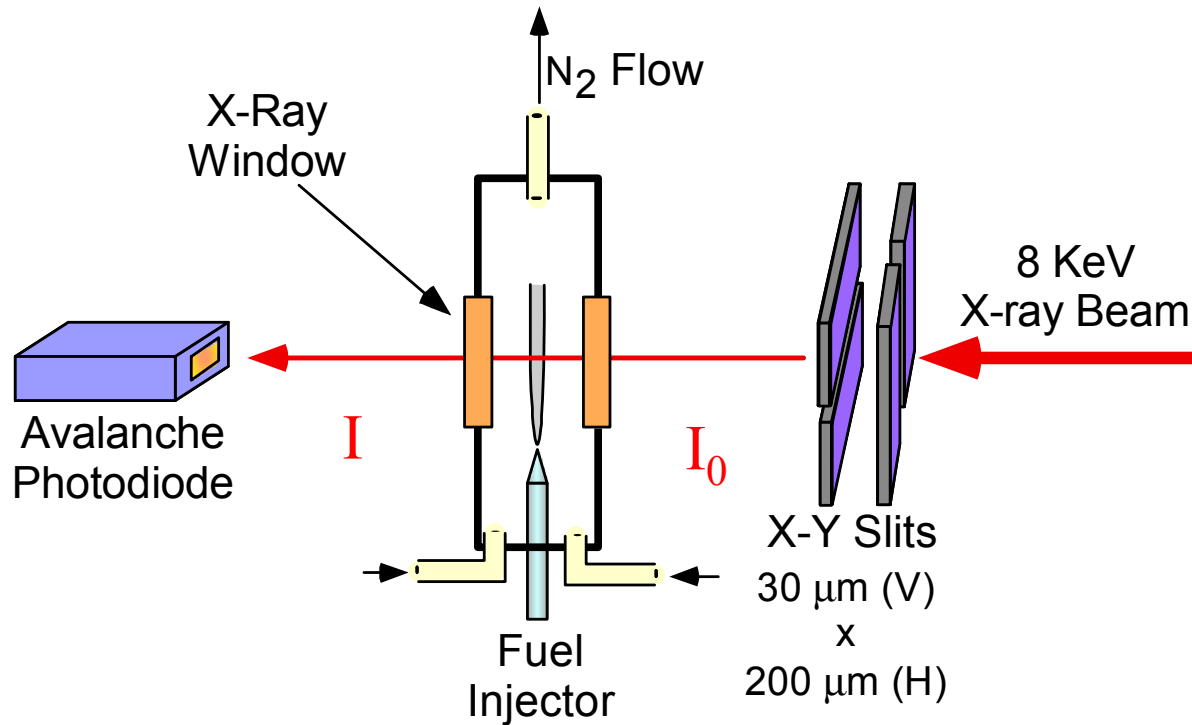
## *Good Understanding of Spray Structure is Important in Diesel Combustion*

- Performance and emissions of diesel engines are closely tied to the spray from the injector
  - Excessive penetration → wall wetting → UHC emissions
  - Excessive premixed combustion → NOx emissions
- Led to progressive development of diesel injection systems to achieve better mixture preparation
  - Pump-Line-Nozzle → Unit Injectors → Common Rail Systems
  - Smaller injector holes
  - Higher injection pressure

## *Current Spray Diagnostic Techniques Inadequate*

- Understanding of the atomization of diesel sprays is still incomplete
- Mechanical Measurements
  - Intrusive
- Optical Measurements
  - Can't probe internal spray structure in dense regions
  - Often not quantitative, due to strong scattering effects
- **Need a nonintrusive, quantitative technique to measure sprays**

## Schematic of X-Ray Setup



### Quantitative relationship between x-ray transmission and projected mass density

- $I_0$  Incident x-ray intensity
- $I$  Measured x-ray intensity
- $\mu_M$  Fuel absorption constant, area/mass
- $M$  Projected mass density, mass/area

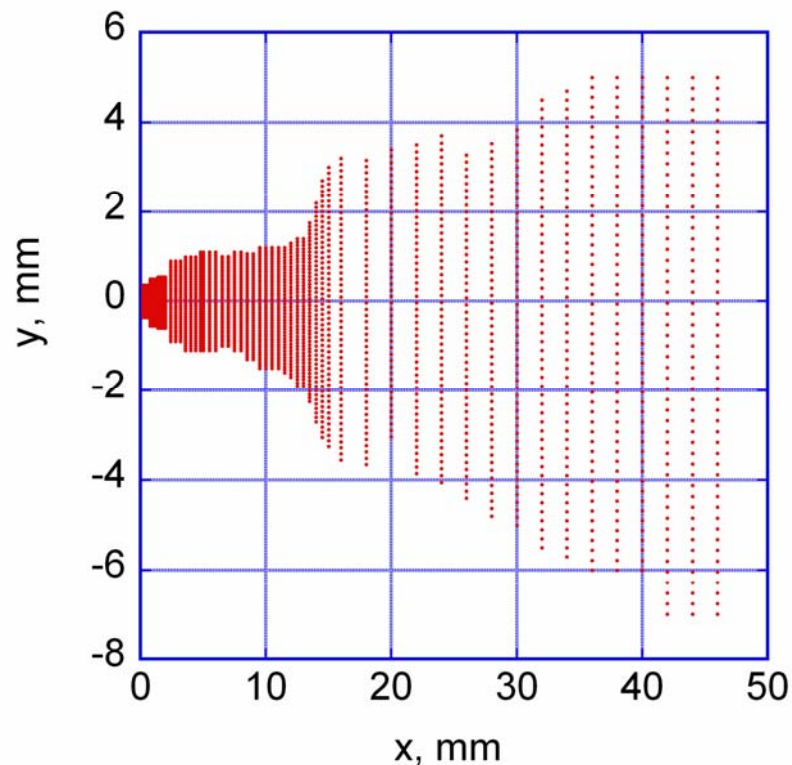
$$I = I_0 e^{-M\mu_M}$$

$$M = \frac{\ln(I_0 / I)}{\mu_M}$$



# Radiography Has Good Spatial and Time Resolution

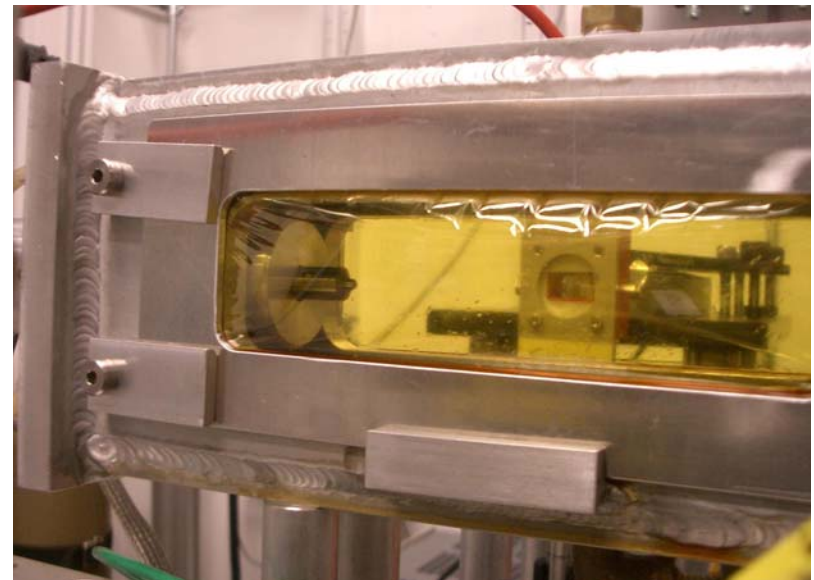
## Measurement Grid



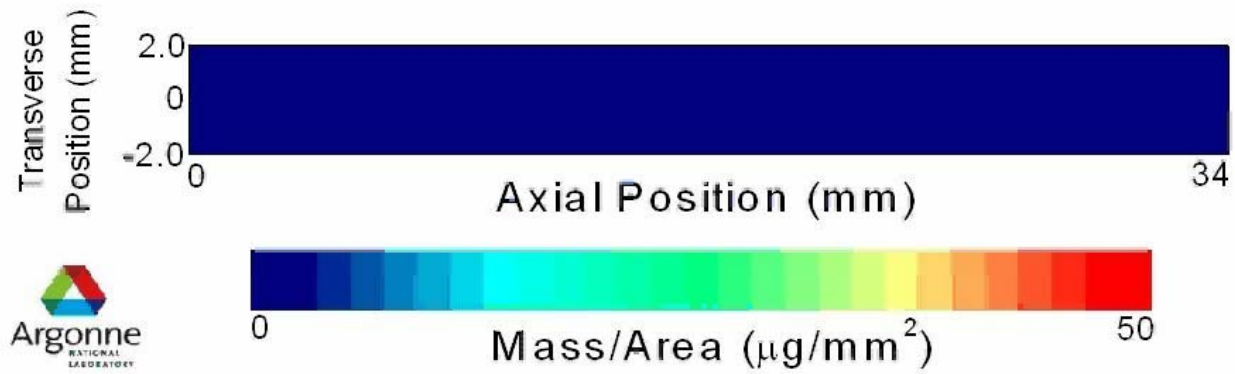
- Radiography is a pointwise measurement
  - Raster injector to build up measurement grid
  - Example grid: 2250 points
  - Data in discrete columns
- Also good temporal resolution: time step  $3.68 \mu\text{s}$ 
  - 1 CAD at 3000 rpm =  $56 \mu\text{s}$

## Experiment Details

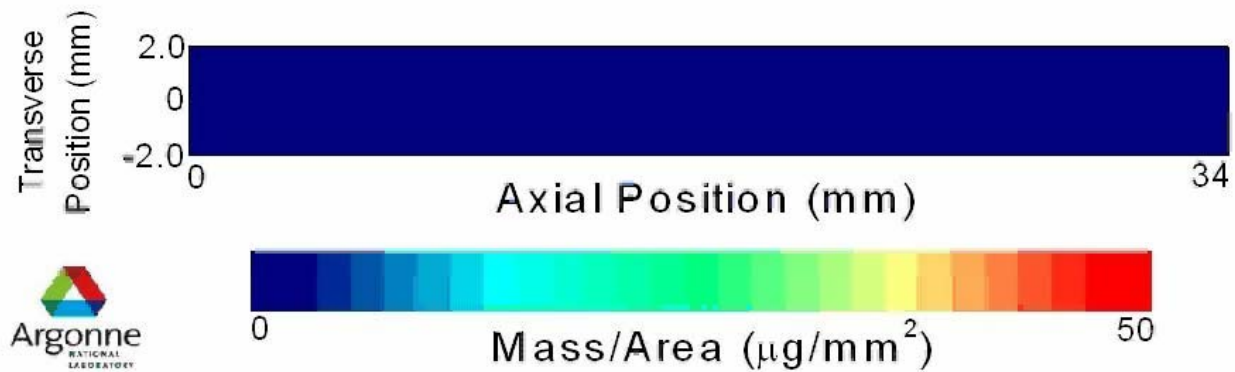
- Light-duty diesel common-rail injector
- Two nozzles: axial single hole
  - Hydroground
    - *Subjected to 24% hydrogrinding*
    - *Orifice diameter: 183  $\mu\text{m}$*
  - Non-hydroground
    - *Orifice diameter 207  $\mu\text{m}$*
  - Designed to have the same steady-state flowrate
- Injection parameters
  - Injection pressure: 250 bar
  - Injection duration: 400 and 1000  $\mu\text{s}$
  - Ambient gas:  $\text{N}_2$
  - Ambient pressure: 1 bar
  - Averaged over 64 injections
  - Liquid: Calibration fluid with cerium additive



## Spray Evolution: 400 $\mu$ s Injection

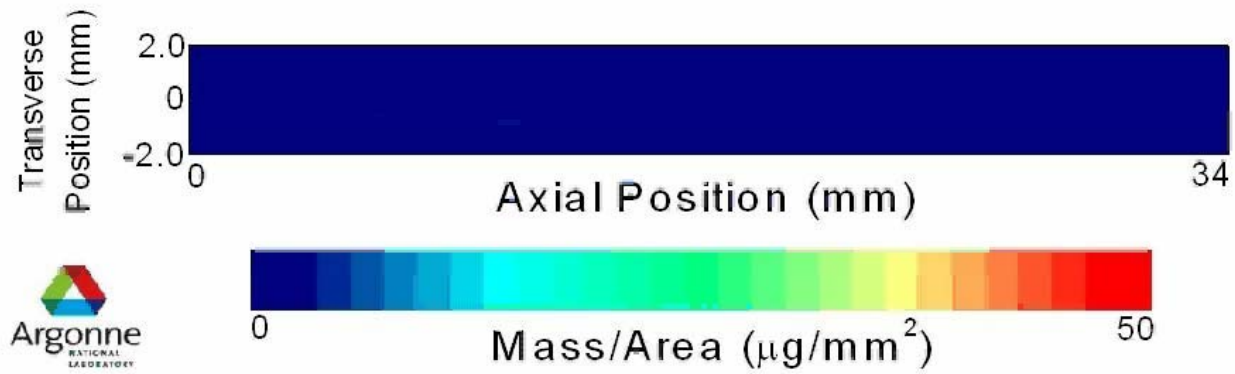


### Hydroground

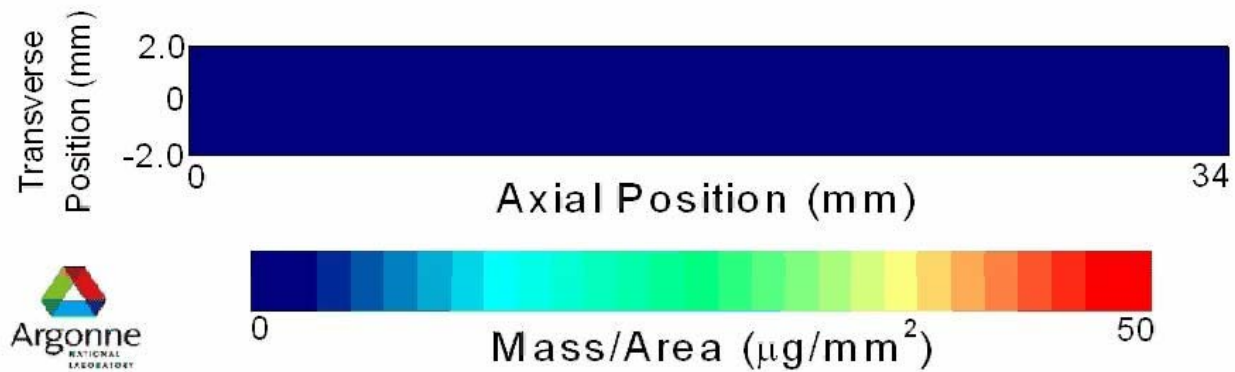


### Non-hydroground

## Spray Evolution: 1000 $\mu$ s Injection

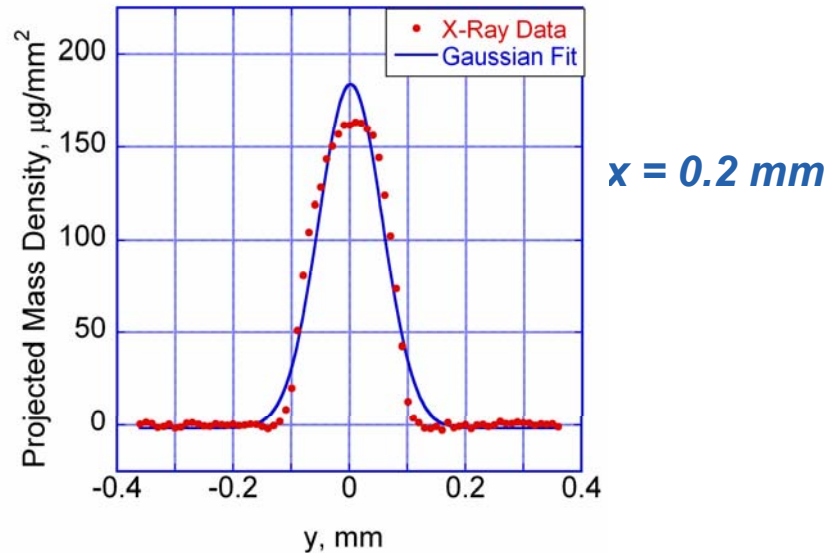


### Hydroground

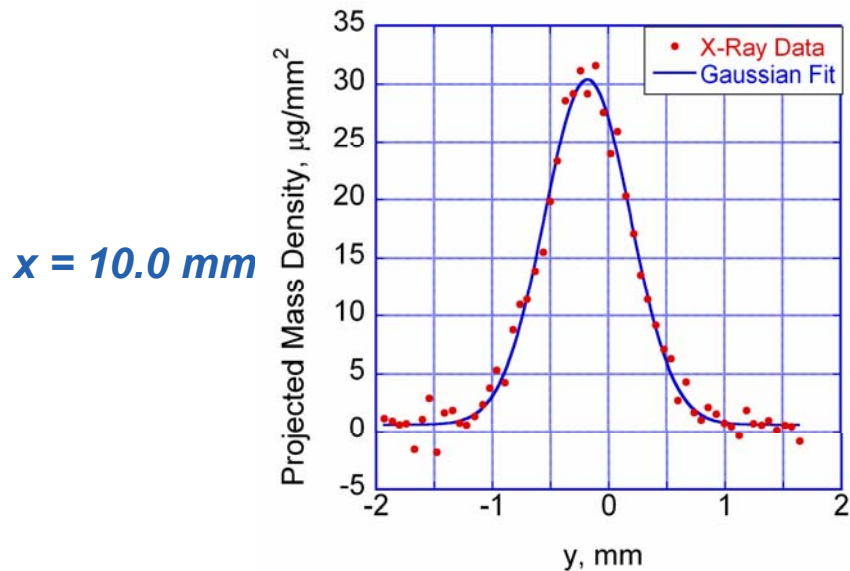


### Non-hydroground

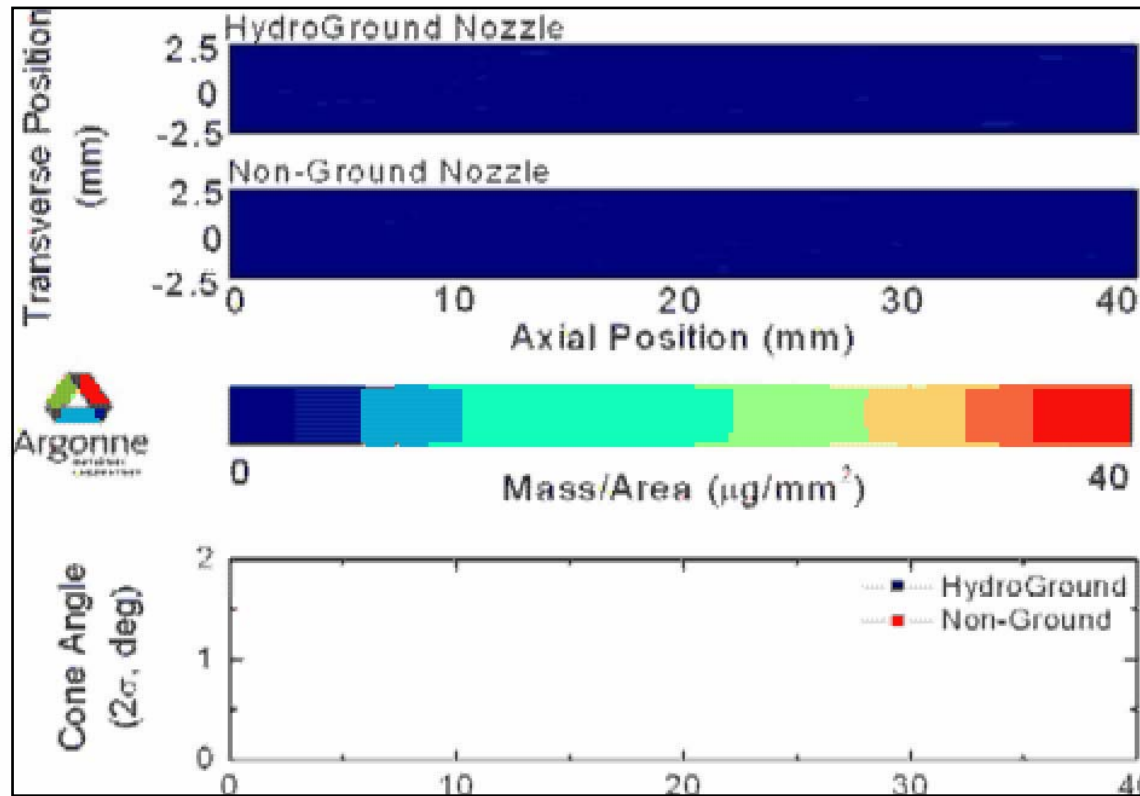
## Transverse Mass Distributions Gaussian Except Near Nozzle



- Examine the mass density of the spray along a slice perpendicular to the spray axis
- Generally Gaussian shape
  - Matches expected behavior of a fully developed jet
- Distribution has flatter top than a Gaussian within 1 mm of the nozzle
  - Suggests that there is a relatively high-density core of fuel



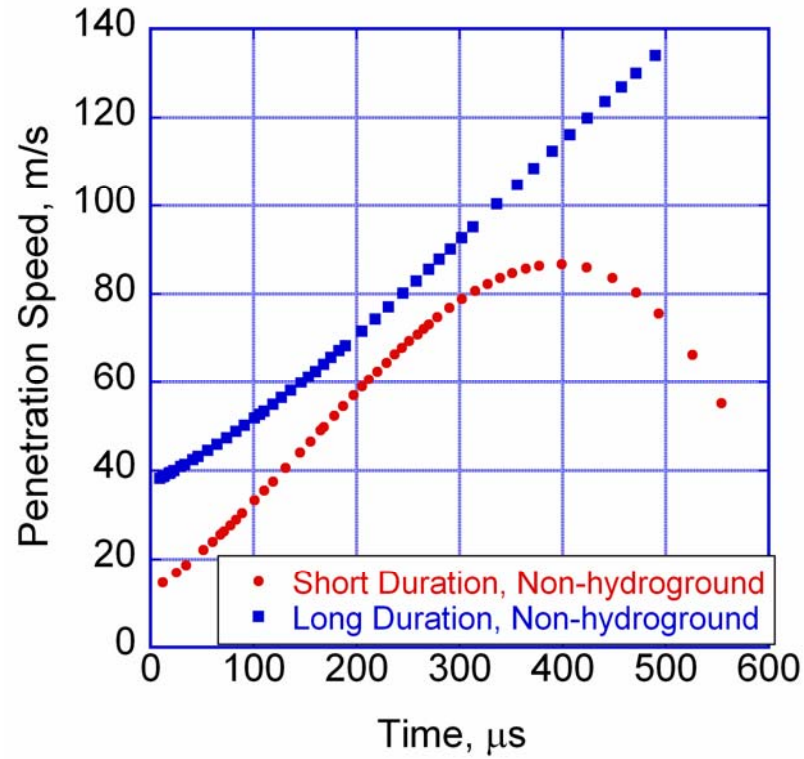
# Radiography Can Measure Cone Angle Dynamics



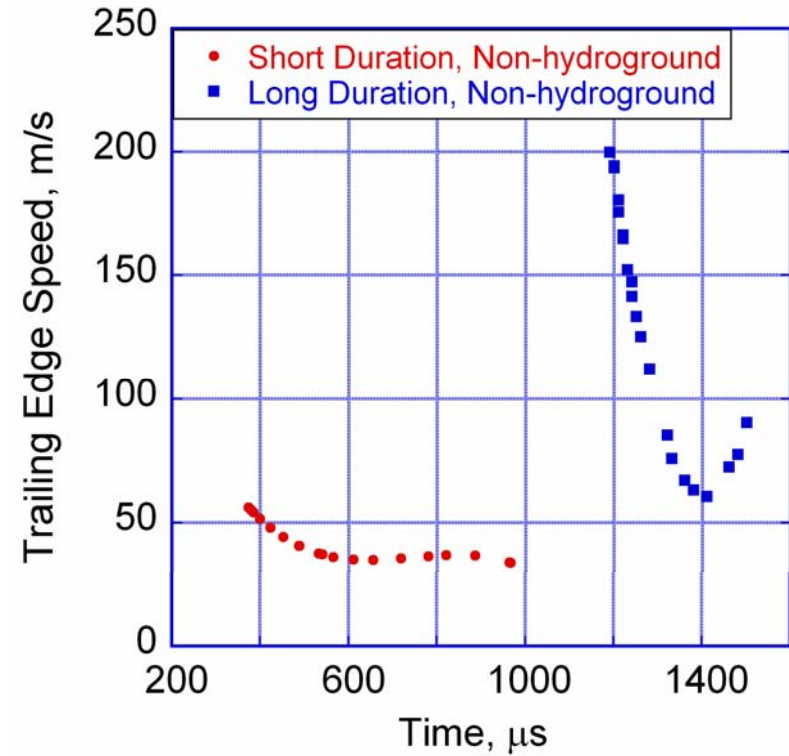
- Benefits of radiography over optical cone angle measurements
  - Dynamics
  - Based on spray core, not outside of droplet cloud



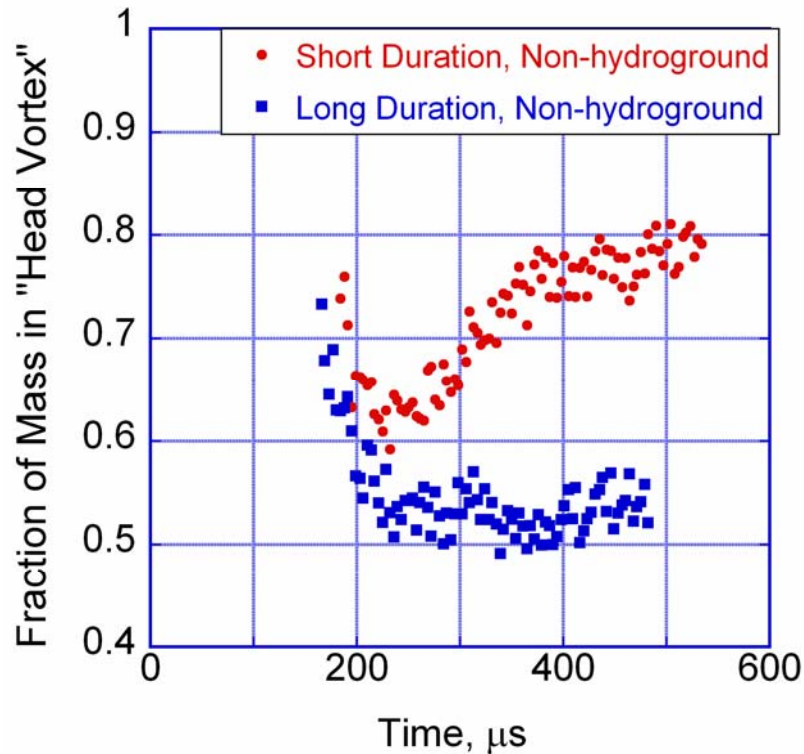
# Radiography Can Measure Both Leading and Trailing Edge Speed



**Trailing Edge**



## Large Amount of Fuel in “Head Vortex”



- Partition spray into “head vortex” and trailing jet
  - While entire spray remains in measurement domain
- “Head vortex” more prominent for short duration injections
  - Nearly 80% of mass after end of short duration injection
- Trailing jet remains relatively dense for long duration injections
  - “Head vortex” contains the majority of the mass
- Implications for spray modeling

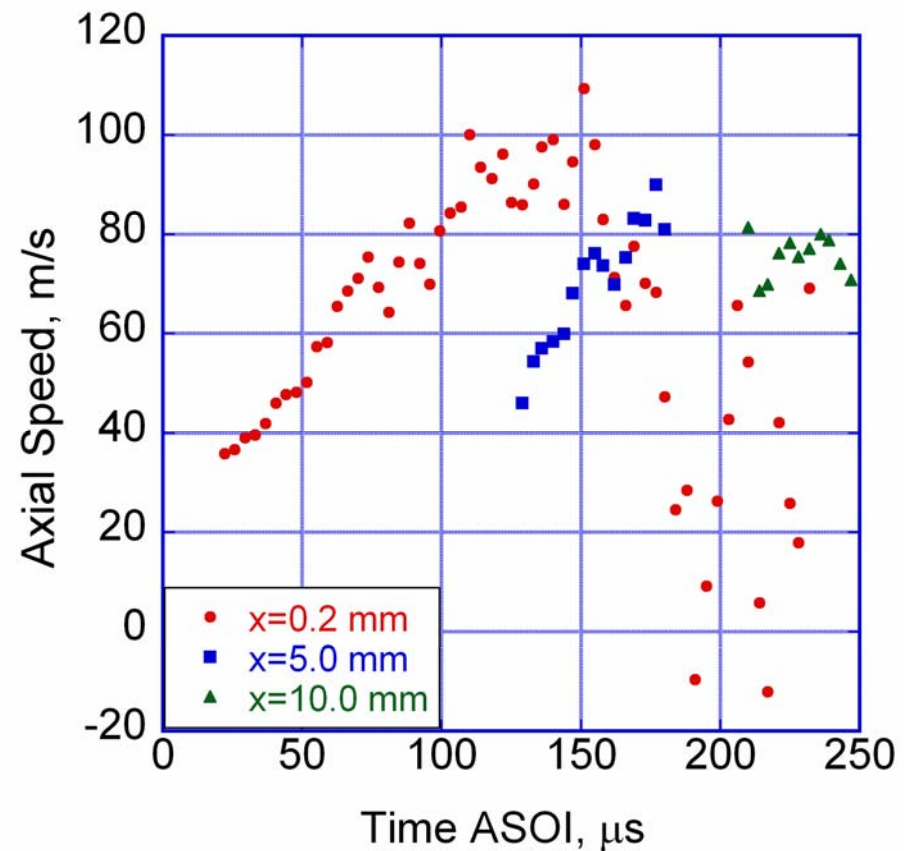


## *Future Work*

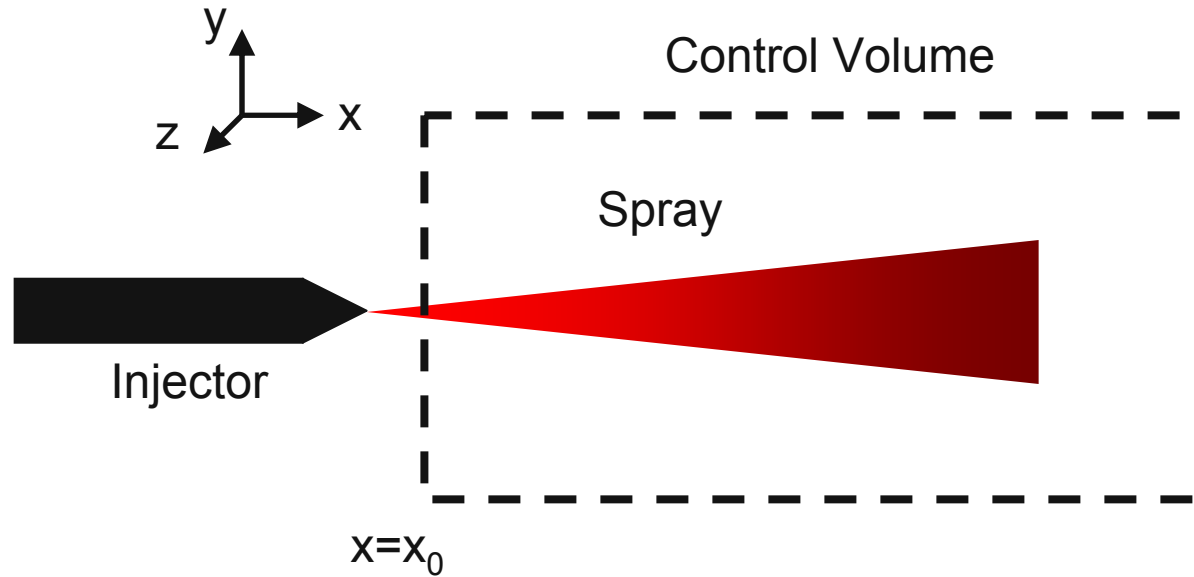
- Extend current experimental conditions
  - Shrink the size of the x-ray beam: better spatial resolution
  - Increase ambient pressure: density closer to engine conditions
    - *Recently achieved 30 bar ambient pressure*
  - Experiments in multi-hole nozzles: closer to applied equipment
  - Single-shot & image-based measurements
- Improved Data Analysis
  - Projection inversion: estimate true fluid density from projected mass density
  - Refine determination of the “head vortex”
  - Axial velocity determination

## Future Work: Spray Axial Velocity Determination

- Axial velocity of spray in dense regions of the spray is not well known
- Measure mass-averaged axial velocity for each measurement column
  - Internal speed of liquid
- Axial velocity affects:
  - Penetration speed
  - Shear with ambient gas
  - Initialize spray breakup models
- Calculated axial velocity for a 400  $\mu\text{s}$  spray from a hydroground nozzle
  - Speed from Bernoulli's equation: 236 m/s

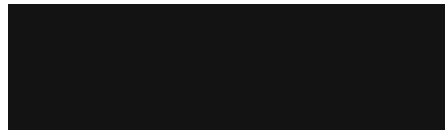


## Future Work: Spray Axial Velocity Determination

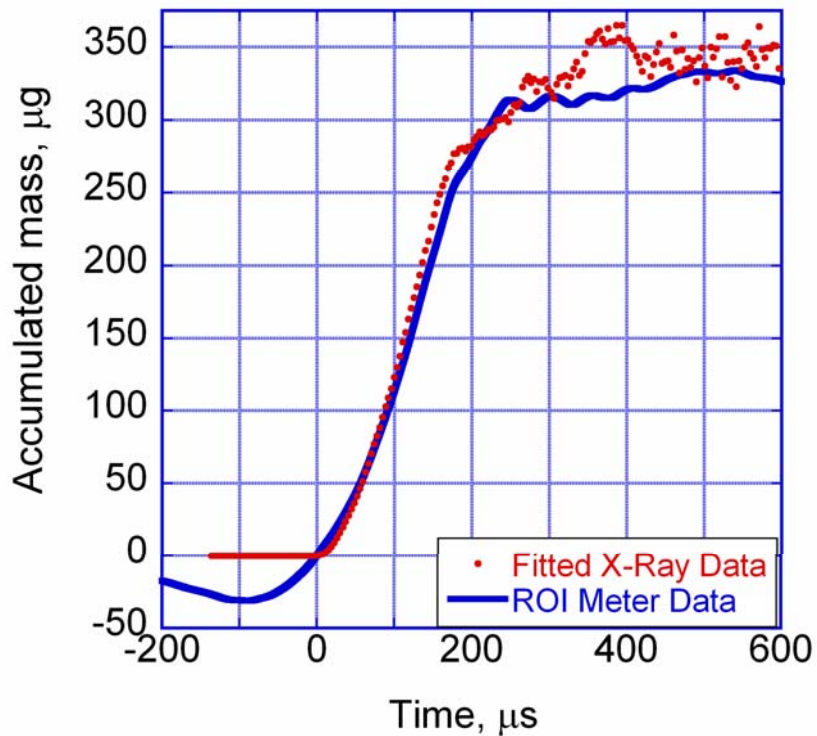


$$\begin{aligned} \dot{m}_{cv}(x > x_0, t) &= - \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} \rho(x_0, y, z, t) \cdot \vec{V}(x_0, y, z, t) \cdot \hat{n} \cdot dz \cdot dy \\ &= \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} \rho(x_0, y, z, t) \cdot V_x(x_0, y, z, t) \cdot dz \cdot dy \end{aligned}$$

$$V_{ma}(x_0, t) = \frac{\int_{-\infty}^{\infty} \int_{-\infty}^{\infty} \rho(x_0, y, z, t) \cdot V_x(x_0, y, z, t) \cdot dz \cdot dy}{\int_{-\infty}^{\infty} \left[ \int_{-\infty}^{\infty} \rho(x_0, y, z, t) \cdot dz \right] \cdot dy}$$



## Radiography Mass Measurements Match Mechanical Measurements

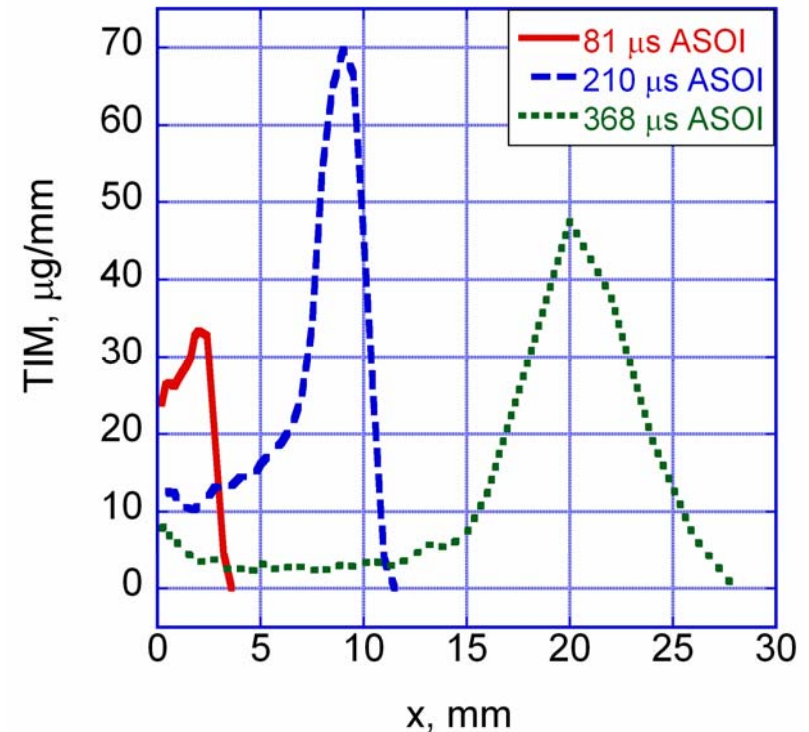


*Hydroground nozzle, 400  $\mu\text{s}$  spray*

- Accumulated mass as a function of time
- Generally good agreement with Bosch Rate-of-Injection meter
- Total injected mass by mechanical measurement is 334  $\mu\text{g}$ , which agrees well with the x-ray data

## Transverse Integrated Mass

- Examine area of Gaussian fits to transverse mass distributions
  - Indicates how densely spray is packed axially
  - In units of mass/length
  - Aids in further analysis
  - Referred to as Transverse Integrated Mass (TIM)
- Peak value corresponds to leading edge structure
- TIM increases between nozzle and leading edge, suggesting spray slows down as it moves downstream
  - Expected behavior from fully developed jet theory
  - Transverse spread coupled with axial compression

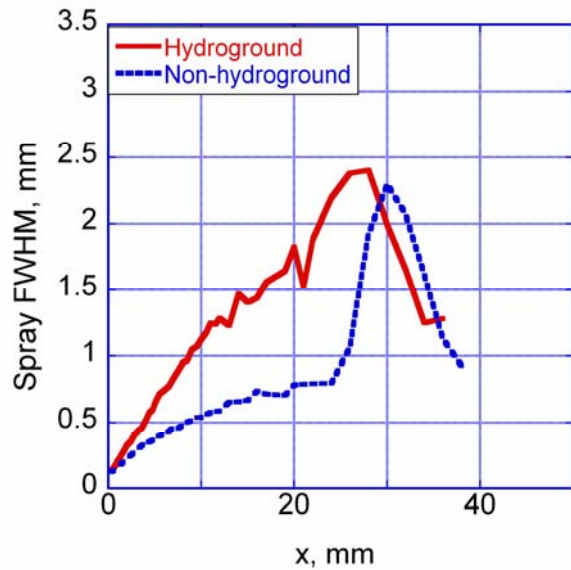


## Cone Angle for 1000 $\mu$ s Duration Sprays

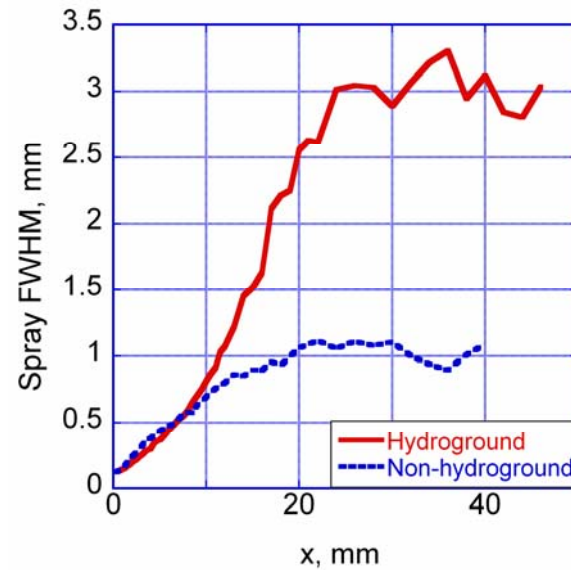
- Cone angle based on linear fit to FWHM of Gaussian fits of transverse mass distributions for  $0 < x < 10$  mm
- Far smaller angles than typically seen from optical measurements
  - Indicates that optical measurements focus on spray periphery
- Increase in cone angle at end of spray for both nozzles
  - Seen in optical measurements as well
- Cone angle changes significantly during the spray event

Spray Event	Cone Angle
Hydroground, 475 $\mu$ s ASOI	5.9°
Non-hydroground, 475 $\mu$ s ASOI	2.5°
Hydroground, 644 $\mu$ s ASOI	3.9°
Non-hydroground, 644 $\mu$ s ASOI	3.3°
Hydroground, 1072 $\mu$ s ASOI	1.2°
Non-hydroground, 1072 $\mu$ s ASOI	2.8°
Hydroground, 1219 $\mu$ s ASOI	7.1°
Non-hydroground, 1219 $\mu$ s ASOI	3.8°

# Spray Width: Hydroground vs. Non-hydroground

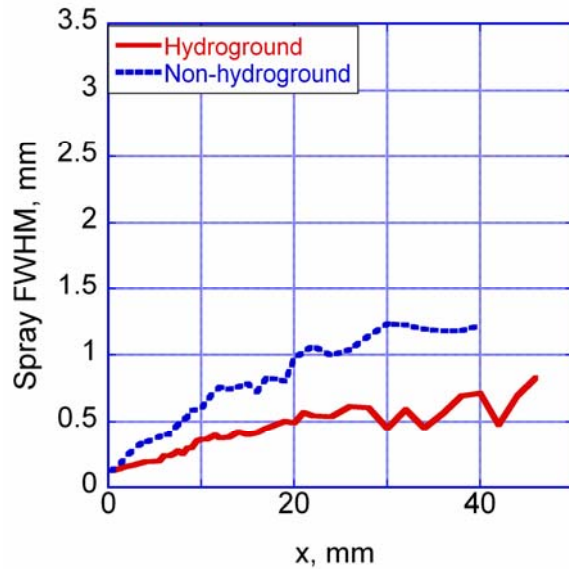


475  $\mu$ s  
ASOI



664  $\mu$ s  
ASOI

1072  $\mu$ s  
ASOI



1219  $\mu$ s  
ASOI

