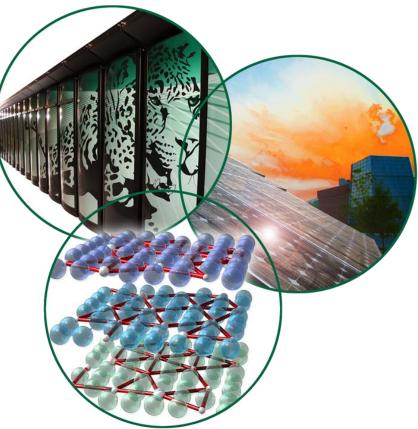
# Load Expansion of Stoichiometric HCCI Using Spark Assist and Hydraulic Valve Actuation

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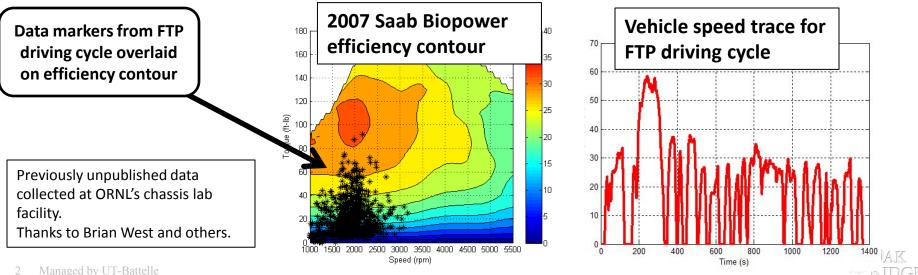




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# Purpose of advanced combustion strategies in gasoline engines: improve efficiency without increasing tailpipe-out emissions

- Tailpipe-out emissions are extremely low for gasoline engines due to mature 3-way catalyst exhaust aftertreatment at stoichiometric conditions
- Advanced combustion techniques must provide improved efficiency while not increasing tailpipe-out emissions
  - Either extremely low NOx or stoichiometric operation to maintain compatibility with a 3-way catalyst
- To have largest impact, advanced combustion strategies must be applicable over portion of engine map where engine operates most



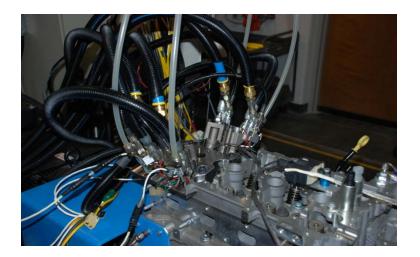
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Szybist\_SA-HCCI

# Single cylinder research engine with Sturman hydraulic valve actuation (HVA)

- Modified 2.0L GM Ecotec engine with direct injection
- Cylinders 1-3 are disabled, cylinder 4 modified for Sturman HVA system
- Engine management performed with Drivven engine controller
- Custom pistons to increase compression ratio
- UTG-96 certification gasoline

	SI Combustion	SA-HCCI
Fuel Rail Pressure (bar)	95	95
Fuel Injection Timing (CA)*	-280	-340
Equival ence Ratio	1.0	1.0
Intake Valve Opening (CA)*	-344	-313 to -234
Intake Valve Closing (CA)*	-180	-180 to -124
Intake Valve Lift (mm)	9	3 to 6
Exhaust Valve Opening (CA)*	180	170
Exhaust Valve Closing (CA)*	349	234 to 313
Exhaust Valve Lift (mm)	9	2 to 3.5
*0 CA refers to combustion TD	C	

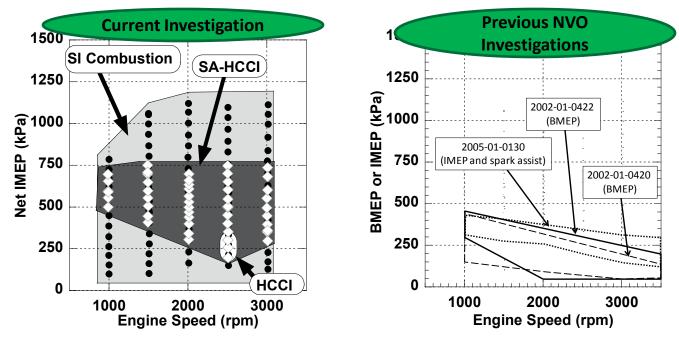


Bore	86 mm	
Stroke	86 mm	
Connecting Rod	145.5 mm	
Fueling	<b>Direct Injection</b>	
<b>Compression Ratio</b>	11.85	
Valves per Cylinder	4	





# High load limit increased to 7.5 bar from 1000 to 3000 rpm with operating strategy



#### Attributes of the advanced combustion strategy

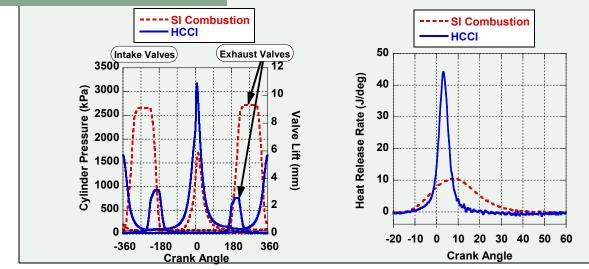
- Stoichiometric A/F ratio
- Spark assist
- Negative valve overlap for internal
  - No external EGR

- Unthrottled operation
- Variable intake valve closing angle to control effective compression ratio

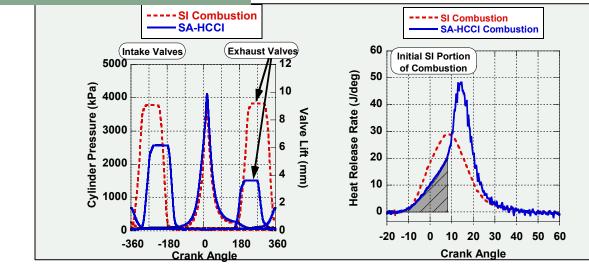


# **Combustion analysis reveals role of spark assist**

#### 2500 rpm, 2 bar IMEP



#### 2500 rpm, 6.5 bar IMEP



- By retarding spark timing and intake valve closing angle as load increases, pressure rise rate can be controlled to < 7bar/deg at all points</li>
- Under light-load conditions, combustion event is dominated by volumetric combustion
- As engine load increases, a larger portion of the heat release occurs during the spark-ignited portion of combustion

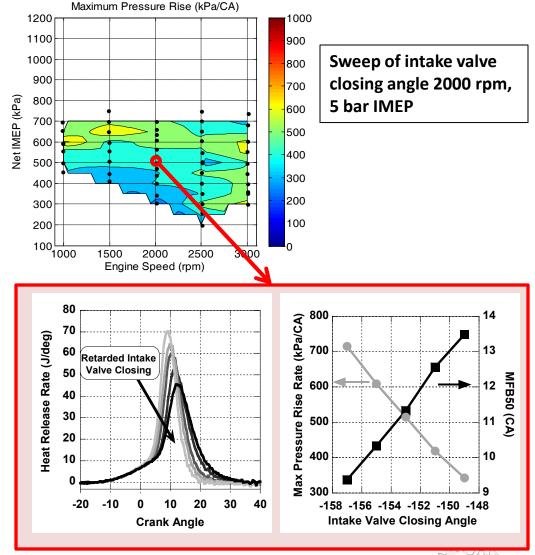


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# Late intake valve closing allows control of maximum pressure rise rate

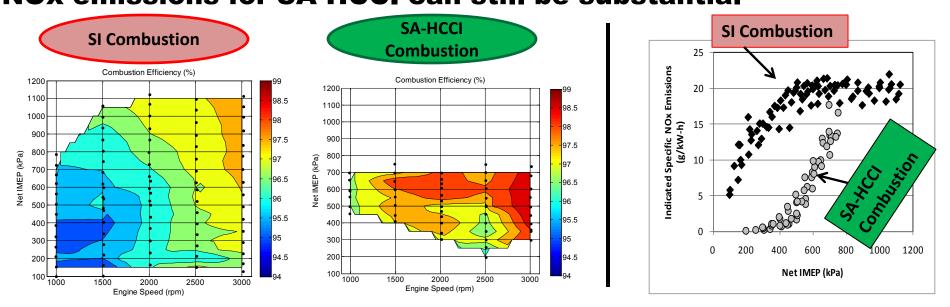
- Retarding intake valve closing reduces the effective compression ratio
  - Similar to technique using late intake valve closing angle to mitigate knock demonstrated during ethanol optimization work\*
  - Effective CR varied from 11.85:1, which is the geometrical compression ratio, to 10:1
- Some tradeoff exists between spark timing and intake valve closing angle

\*For Example see SAE 2010-01-0619





#### Improved combustion efficiency and NOx emissions for SA-HCCI NOx emissions for SA-HCCI can still be substantial

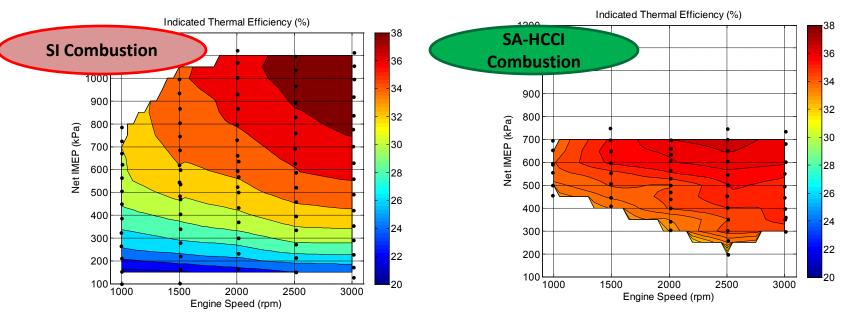


- CO and HC emissions reduced by more than a factor of 2 at most operating points, resulting in very good combustion efficiency
  - Low combustion efficiency for SI combustion can be attributed to un-optimized combustion and engine breathing differences caused by HVA valvetrain
- Near-zero NOx emissions at lowest loads, but sharp increase with increasing load
  - Due to a combination of larger fraction of SI combustion, less internal EGR, and more fuel consumed per cycle
  - Stoichiometric A/F ratio and sufficiently high exhaust temperature maintains compatibility with 3-way catalyst technology





# **SA-HCCI** provides a substantial efficiency improvement at most operating conditions



- Efficiency benefits for SA-HCCI are greatest at low-load conditions
  - Thermal efficiency for SA-HCCI is nearly constant across entire operating range
  - Wide variations in efficiency in SI
- Increased efficiency for SA-HCCI is attributed to 3 factors
  - 1. Higher combustion efficiency
  - 2. Reduced pumping work
  - 3. Shorter combustion duration



### **Summary and conclusions**

- A mode of advanced combustion has been developed and base-lined
  - Stoichiometric SA-HCCI with negative valve overlap
  - Unthrottled operation
  - Late intake valve closing angle and spark timing control pressure rise rate
- Capable of higher engine load than most advanced combustion strategies because of increased control over pressure rise rate
  - Combustion event dominated by volumetric heat release at low loads
  - Larger fraction of fuel energy burned during SI combustion at higher loads
- Improvement in CO and HC emissions compared to SI combustion
- Improvement in NOx emissions, but sufficiently high that there is a need for NOx aftertreatment
  - Stoichiometric A/F ratio maintains compatibility with conventional 3-way catalysts
- Efficiency benefit at most operating conditions
  - Efficiency benefit greatest at low load
- This study will be presented at the 2010 SAE Powertrains, Fuels and Lubricants Conference as SAE Technical Paper 2010-01-2172



# **Paths to SA-HCCI implementation**

- SA-HCCI combustion on cam valvetrain is the most likely route to commercial viability
  - HVA valvetrains face numerous implementation barriers
- 2-step valvetrains have the potential to switch between conventional SI combustion and advanced combustion modes
  - Conventional valve lifts and duration for SI combustion
  - Low lift, short duration valve events for advanced combustion
- Valve lift and duration of the advanced combustion cams will be fixed
  - Phase cams for desired NVO duration and intake valve closing angle
  - Fixed cam duration and lift will ultimately limit the operating range compared to HVA



### **Future work**

- This study is being done as part of the DOE fuels program
- A single, high octane gasoline was used in this initial study to baseline the operating strategy
- Continuing work is primarily investigating fuel effects
  - Fuels include low octane gasoline, ethanol blends (E10 and E85) and butanol blends
  - Additional investigation and refinement of the operating strategy will continue as part of fuel effects investigations

### Acknowledgement

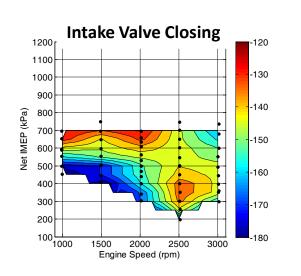
This research was supported by the US Department of Energy (DOE) Office of Vehicle Technology under the fuels technologies program with a DOE management team of Kevin Stork and Dennis Smith.

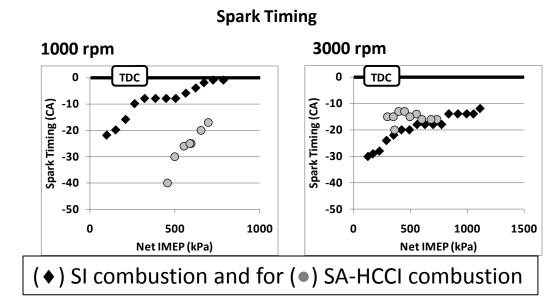


### **Backup Slides**



### Pressure rise is effectively controlled with a combination of spark timing and intake valve closing

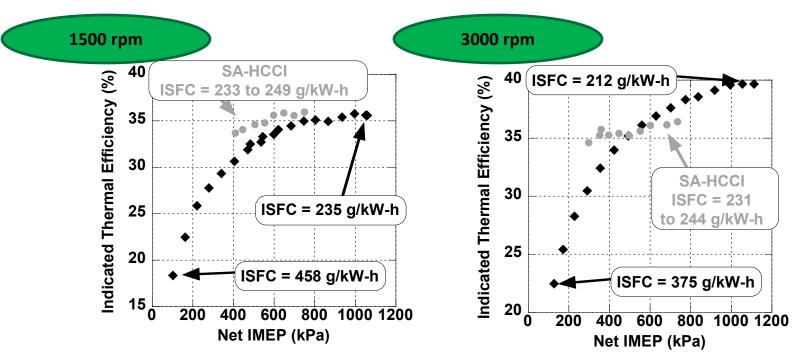




- Retarding intake valve closing reduces effective compression ratio, retards combustion, and reduces pressure rise
- Retarding spark timing delays the start of combustion, retards combustion phasing, and reduces pressure rise
- The two control strategies are, to some extent, interchangeable
  - Tradeoffs between the two are a subject of an ongoing investigation



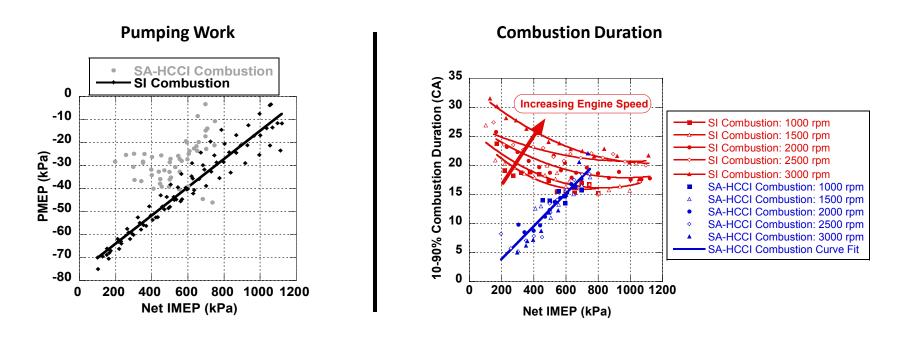
# **Efficiency comparison at constant engine speed**



- At low engine speed, SA-HCCI provides an efficiency benefit for the entire operating range
- At high engine speed, SI combustion becomes more efficient at loads > 5 bar IMEP
- Discrepancy is due to higher efficiency for SI combustion rather than efficiency degradation for SA-HCCI



# **Pumping work and combustion duration differences**



- Pumping work is reduced for SA-HCCI combustion strategy
  - Further reductions are likely possible with optimization of fuel injection timing and valve events
- Shorter combustion duration allows for better utilization of expansion stroke
  - Very different trends in combustion duration for SI and SA-HCCI combustion
  - SA-HCCI combustion achieves much shorter duration

