

# Cost Effective 6.5% Silicon Steel Laminate for Electric Machines

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Project ID:  
elt091

IOWA STATE  
UNIVERSITY



**United Technologies  
Research Center**

# Overview

## Timeline

- October 1, 2016
- September 30, 2019
- Percent complete: 45%

## Budget

- Total project funding
  - \$3,835K (Federal)
  - \$433K (Cost share)
- Funding for FY 2017: \$1,489K
- Funding for FY 2018: \$1,428K

## Barriers and targets

- Magnet cost and rare-earth element price volatility
- Non-rare-earth electric motor performance
- 2020 DOE EDT cost target of \$4.7/kW and power density target of 5.7 kW/L.

## Partners

- Iowa State University (Lead)
- Ames Laboratory
- United Tech. Research Center
- University of Delaware

# Relevance

- MnBi based non-rare earth magnet:
  - Objective: Scale up and enable MnBi magnet for motor application
  - Impact: The price of MnBi bulk magnet is estimated at \$26/kg (NdFeB-Dy Grade N42HS, was \$69/kg in March 2016).
- Electrical steel with 6.5%Si:
  - Objective: Solve the brittleness problem and enable 6.5%Si steel for motor application
  - Impact: Reduces iron loss at higher frequency, improve motor power density and efficiency
- Non-rare earth motor
  - Objective: Demonstrate motor with MnBi as permanent magnet and 6.5%Si steel as the soft magnetics
  - Impact: Improve non-rare earth motor power density

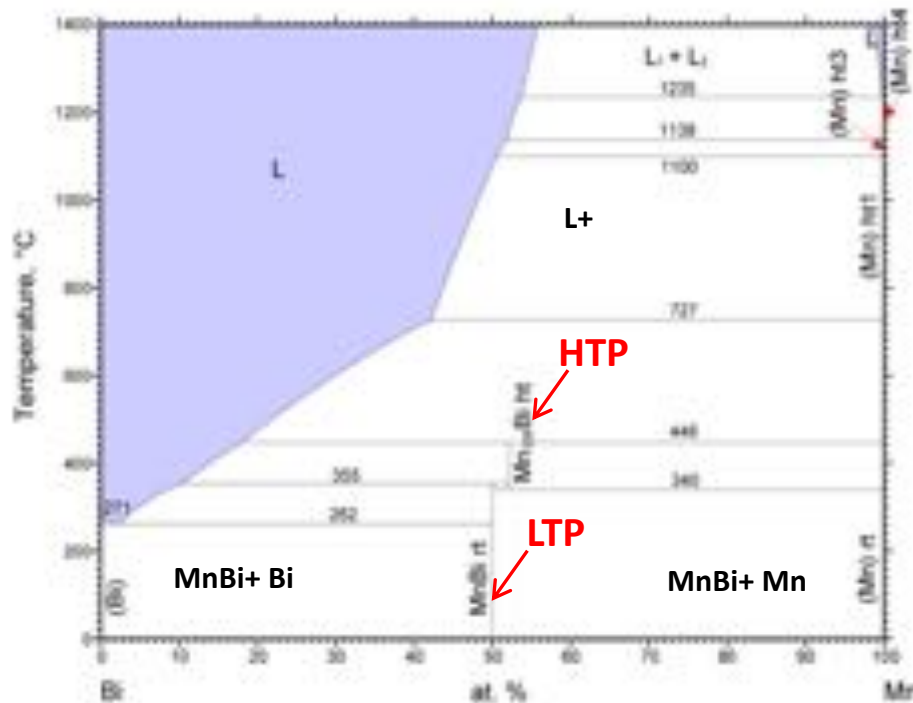
# Milestones

[illegible]

# Challenges (MnBi)

## Advantages of MnBi

- Large coercivity that is increasing with temperature.
- Theoretical energy product  $(BH)_{\max}$  20 MGOe



## Challenges of MnBi

- Peritectic reaction at 355°C, Mn precipitation is inevitable, making it difficult to maintain high purity
- LTP magnetization is limited (~90 kG), any impurity will reduce the energy product
- At 340°C LTP-MnBi decomposes to HTP-Mn<sub>1.08</sub>Bi and liquid Bi, making it difficult to fabricate bulk magnet using the conventional sintering or warm compaction method

# Approach (MnBi)

- Refine the previously developed powder preparation and bulk magnet fabrication process
- Scale up 5 gram magnet to 100 gram
- Use amorphous feedstock to reduce Mn precipitation and improve energy product from 8.5 to 10 MGOe

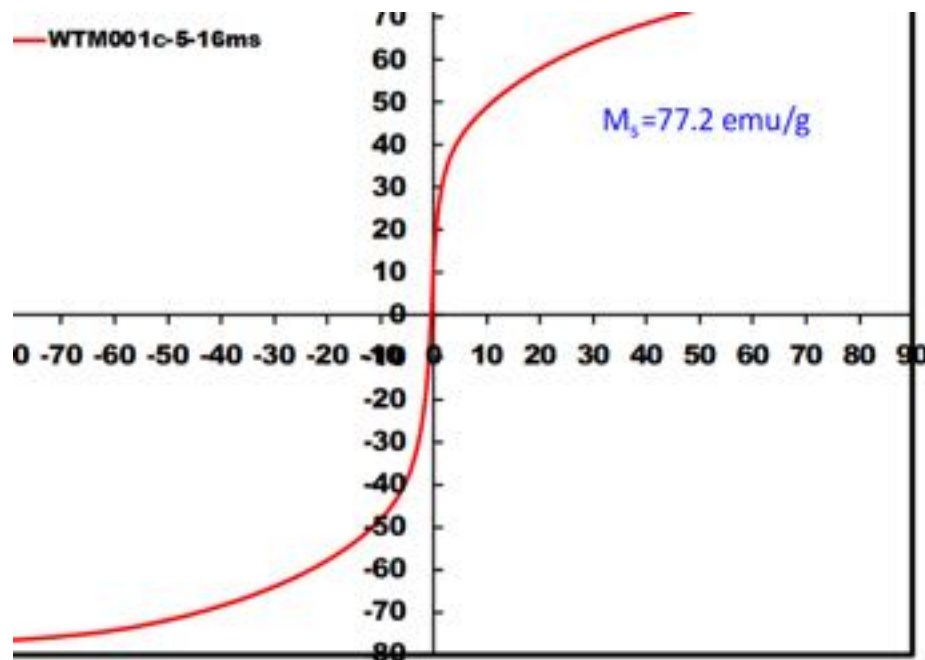
	End results and annual go/no-goes
Yr 1	<ol style="list-style-type: none"><li>1. Produced 8 MGOe MnBi magnet (5 gram)</li><li>2. Finished a large warm-compaction system capable of (200 gram/pcs)</li><li>3. Produced 5 gram MnBi with 90% amorphous</li></ol>
Yr 2	<ol style="list-style-type: none"><li>1. Fabricated one 100 gram/pcs 8.5 MGOe MnBi magnet</li><li>2. Fabricate one small 10 MGOe MnBi (&gt;2 gram)</li></ol>
Yr 3	<ol style="list-style-type: none"><li>1. Delivered 50 pieces of 8.5 MGOe MnBi magnet (100 gram each) machined to the desired dimension and coated.</li></ol>

# Technical Accomplishments (MnBi)

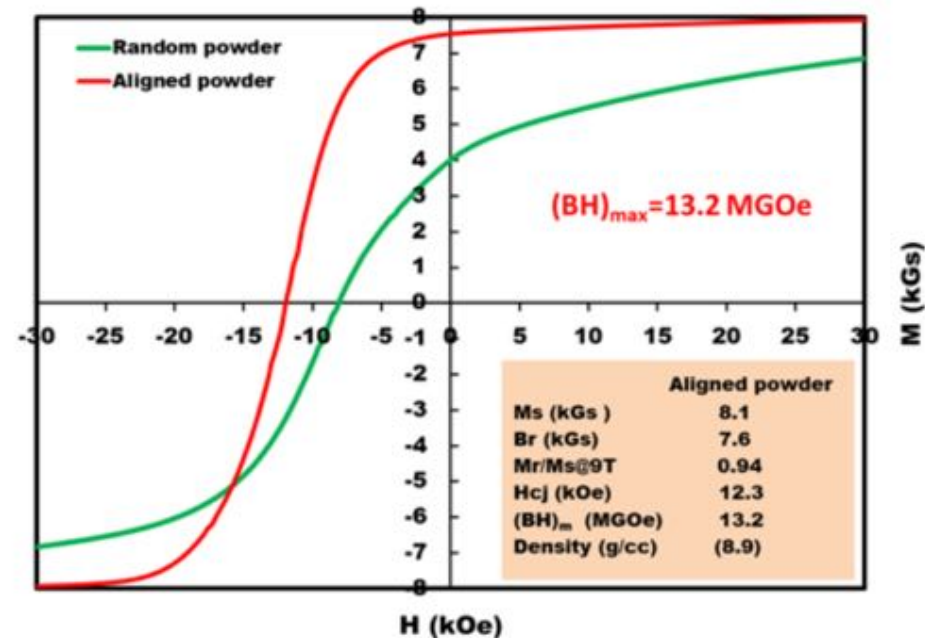
New records were established for feedstock powder preparation

$M_S$  77.2 emu/g,  $(BH)_{max} \sim 13.2$  MGOe

Previous records were  $M_S$  74.5 emu/g,  $(BH)_{max} \sim 12$  MGOe



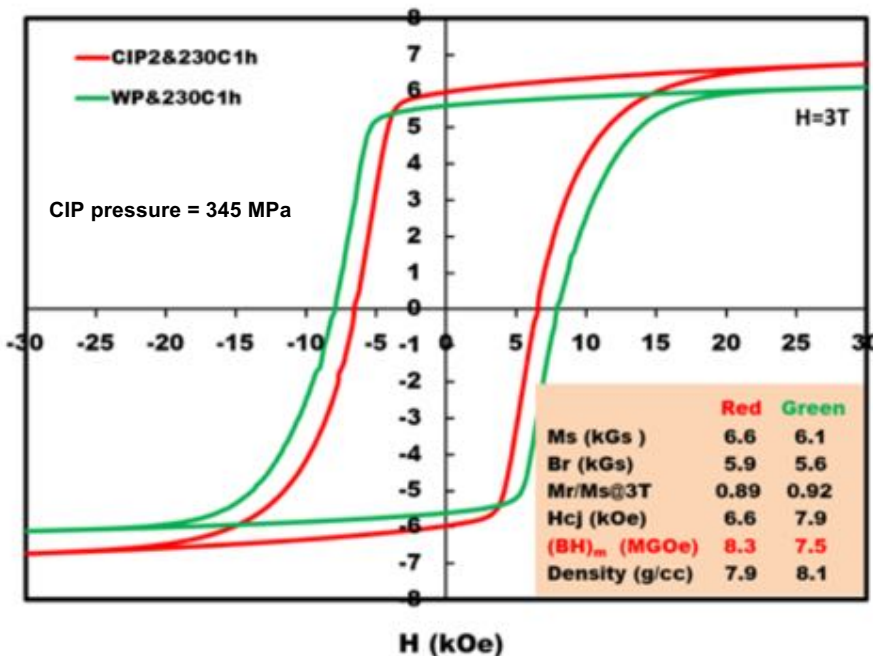
M-H of coarse powder



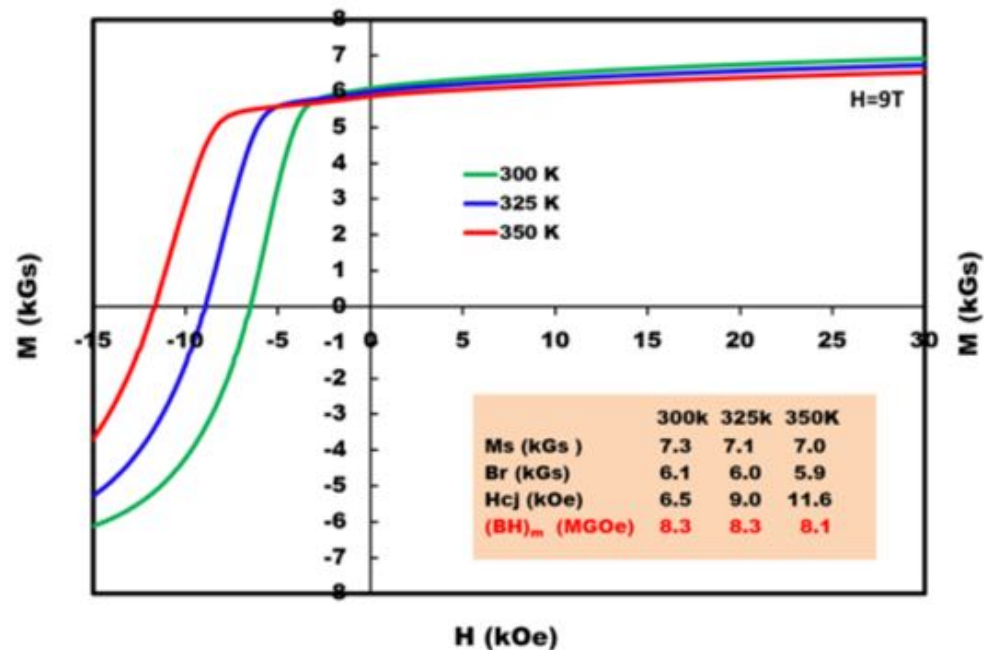
M-H of ball-milled powder

# Technical Accomplishments (MnBi)

- Milestone 8.5 MGOe is closely met (8.3 MGOe demonstrated)
- Optimized the cost-effective Cold-Iso-Press (CIP) and sintering process to replace the expensive warm-compaction (WP) method
- The CIP bulk magnet exhibited excellent temperature stability:  $(BH)_{\max}$  drops 2% at 350K (15% for NdFeB)



M-H loops of CIP & WP samples



Demag curves at 300/325/350 K



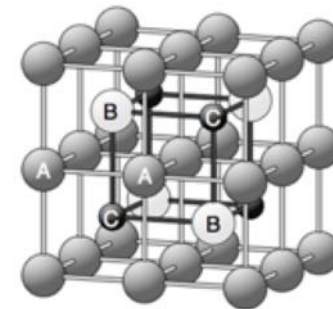
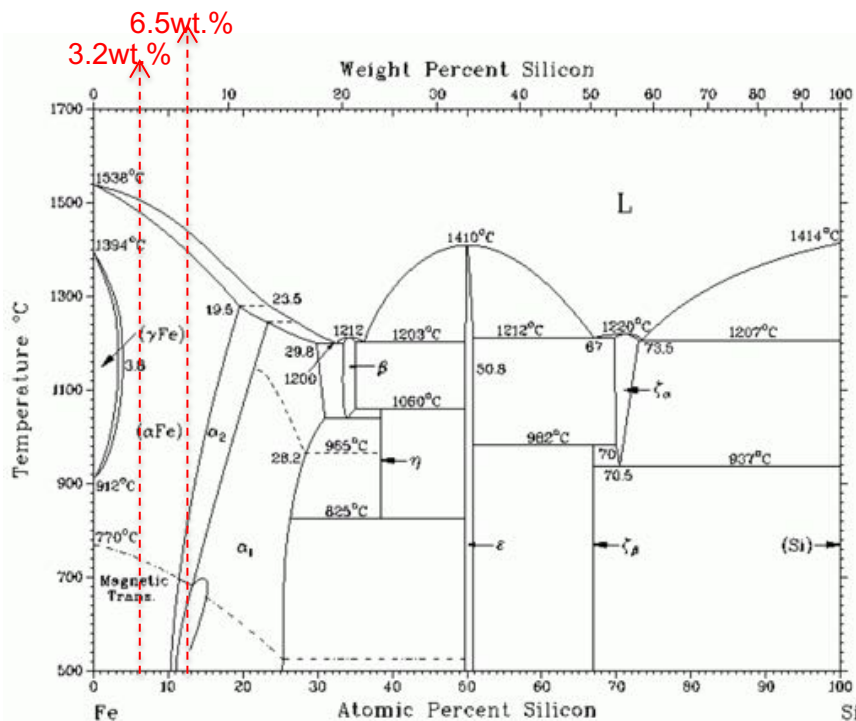
# Challenge (6.5% Si Steel)

## Advantages of 6.5% Si Steel

FeSi steels	Ms (T)	DC relative permeability	Electric resistivity ( $\mu\Omega\text{-cm}$ )	Magnetostriction (ppm)	Core loss $W_{10/400}$ (W/kg)
3.2% Si	1.96	18,000	52	7.8	14.4
6.5% Si	1.8	23,000	82	0.1	5.7

## Challenges of 6.5% Si Steel

- Too brittle to be manufactured using cost effective cast/hot-roll/cold-roll process



$\alpha$ -FeSi    B2    All sites are randomly occupied by Fe or Si

$\alpha_2$ -FeSi    B2    C, B sites are randomly occupied by Fe or Si

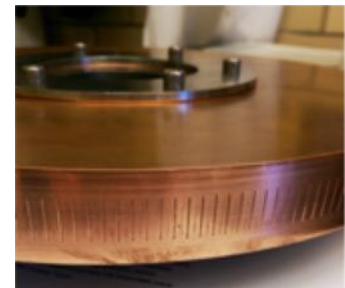
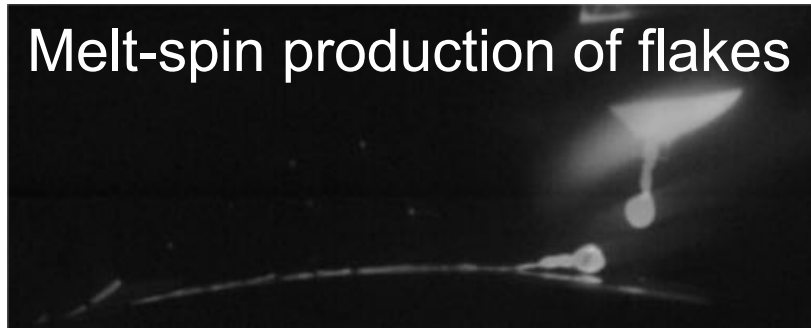
$\alpha_1$ -FeSi    D0<sub>3</sub>    C sites are randomly occupied by Fe or Si

# Approach (6.5%Si Steel)

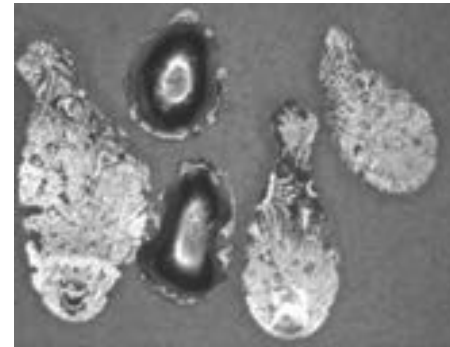
- Use rapid solidification to suppress the deleterious ordering phase and produce ductile thin flakes.
- Dip-coat flakes with thin  $\text{CaF}_2$  layer for insulation.
- Consolidate ductile flakes into near-net-shape part with laminated internal structure.

	End results and annual go/no-goes
Yr 1	1. Delivered 10 gram of ductile Fe-6.5%Si flakes (30 $\mu\text{m}$ thick, 1x1 mm <sup>2</sup> , 180° bending no crack)
Yr 2	1. Delivered Fe-6.5%Si rings with 0.1, 0.4, 1, and 4 mm thickness (OD: 1.5", ID: 1.25", 98% dense, various levels of oxidization) 2. Validated power loss $W_{10/400} < 6$ W/kg for the ring with 0.4 mm thickness.
Yr 3	1. Delivered 8" OD stator laminate with $W_{10/400} < 6$ W/kg 2. Project manufacturing cost for small scale mass production

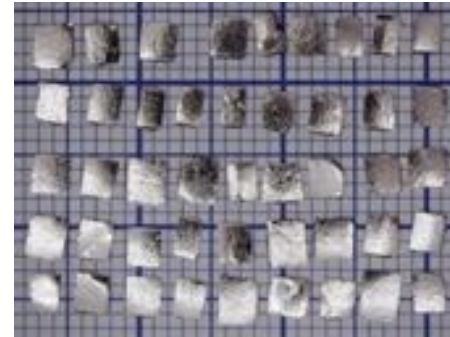
# Technical Accomplishments (6.5%Si Steel)



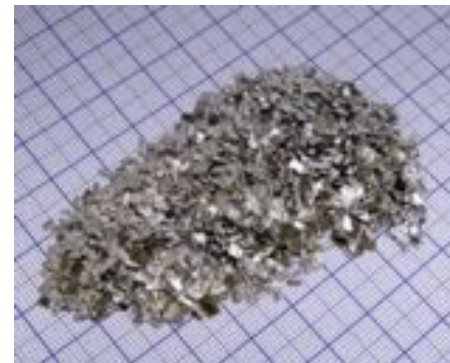
Grooved wheel breaking continuous ribbon to flakes



Early stage:  
Melt didn't stick to wheel properly



2017 (1<sup>st</sup> year)  
Flakes with desired size produced in 5 gram quantity

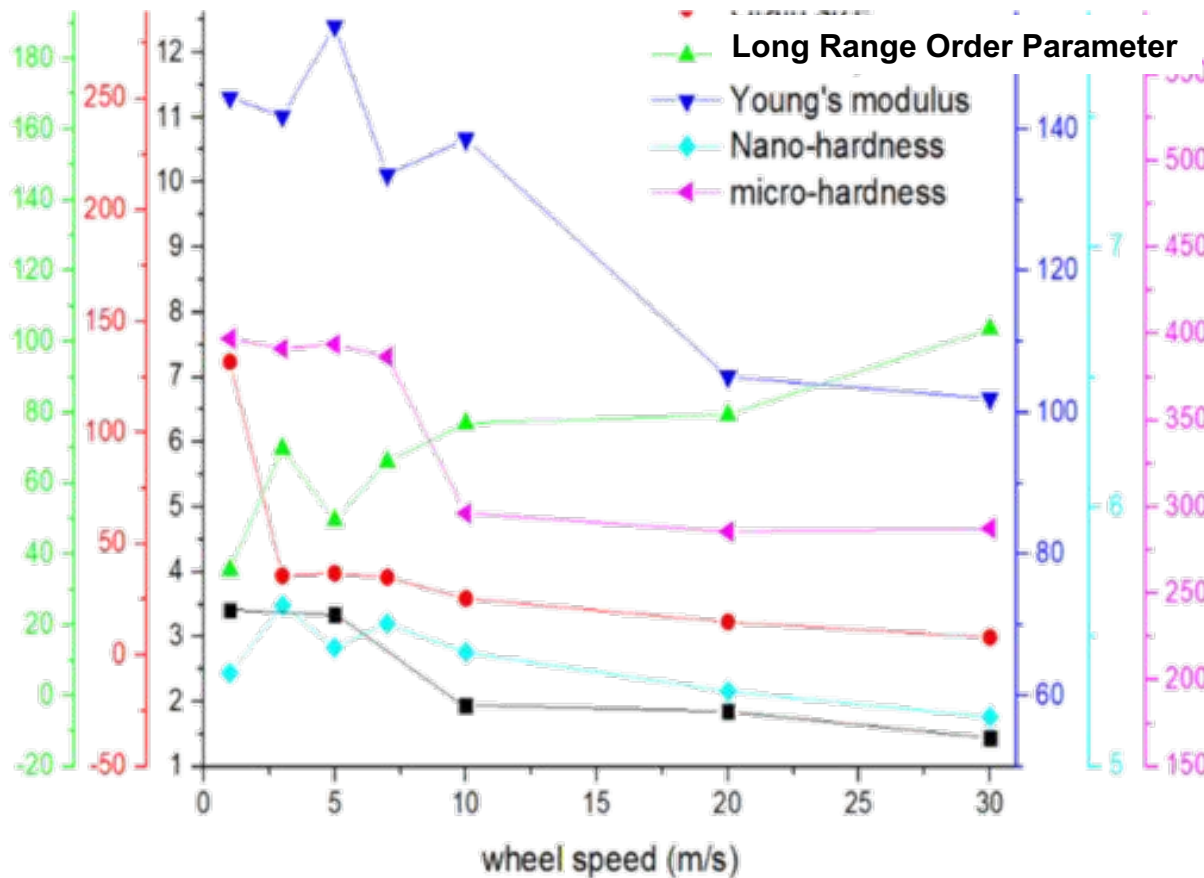


2018 (2<sup>nd</sup> year)  
Flakes with desired size produced in 150 gram quantity

- Developed the process for producing flakes ( $2 \times 2 \times 0.1 \text{ mm}^3$ )
- Approximately 75% yield of the flakes with the desired size
- System capable of 500 gram per batch was acquired/installed

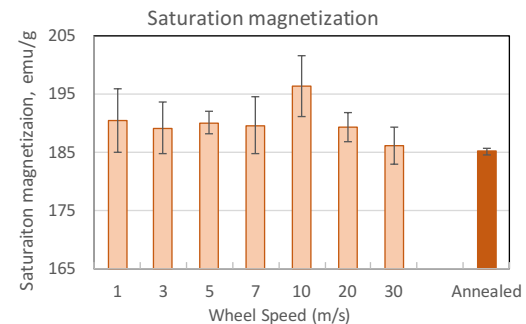
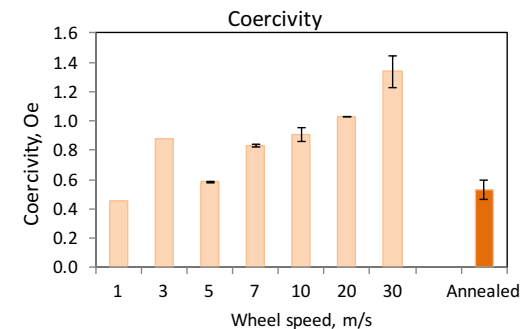
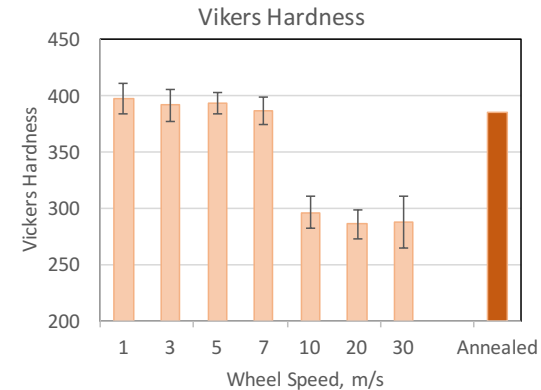
# Technical Accomplishments (6.5%Si Steel)

Relationship between wheel speed and physical properties established



**With increasing wheel speed:**

Grain size (↓); Young's Modulus (↓); Hardness (↓); Magnetization (↓); Coercivity (↑); Electrical resistivity (~flat)



# Technical Accomplishments (6.5%Si Steel)

- Rings with OD~1" and 0.4, 2, 5mm thickness were fabricated.
- Process for OD~2" is being developed
- The rings comes with various levels of inter flake coatings
- Power loss  $W_{10/400}$  15.1 W/kg was demonstrated with 0.4mm ring with coating-free flake before heat treatment.

0.4 mm thick



2 mm thick



5 mm thick



8mm thick



Fe-6.5wt.%Si

CaF<sub>2</sub> insulating layer

50  $\mu$ m

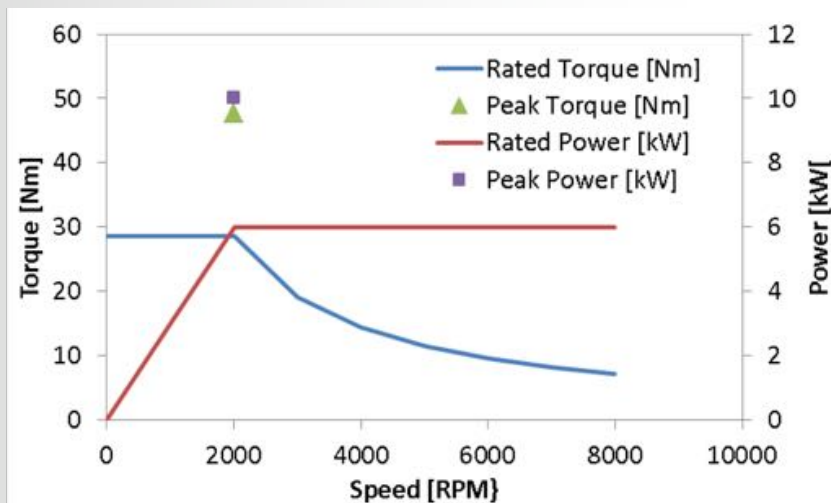
10.00 kV 0.40 nA 10.5 mm 500 x 254  $\mu$ m ABS All 32  $\mu$ m

Material	composition	thickness	B Max	Br	Hc	$\mu$ Max	B8	B25	W10/400
		(mm)	(T)	(T)	(A/m)		(T)	(T)	(W/kg)
Ameslab Hp142	Fe-6.5Si	2	1.74	0.88	39.02	8470	1.19	1.32	66.1
JNEX-core	Fe-6.5Si	0.1	1.8			23000	1.29	1.4	5.7
JNHF-core	Gradient Fe-6.5Si	0.2	1.94			3900	1.09	1.47	14.5

# Challenges (Non-RE Motor)

Machine Performance Specifications for 10 kW Peak, 6 kW Rated Power

Technical Targets		
Cost	Specific Power	Power Density
$\leq \$4.7/\text{kW}$	$\geq 1.3 \text{ kW/kg}$	$\geq 5.7 \text{ kW/Liter}$



## Target Specifications Table

Specifications	Units	Values
Peak Power	kW	10
Continuous Power	kW	6
Max Speed	RPM	8000
Min Frequency	Hz	300
Voltage	V	325
Max per Phase Current	A rms	35
Characteristics Current	A rms	< 35
Weight	kg	7.69
Volume	l	2.2
Unit Material Cost	\$	47
Max Efficiency @ 1/2 Speed & 1/2 Torque	%	95%
Based Speed	RPM	2000
Peak Torque @ Rated Speed	Nm	47.75
Rated Torque @ Rated Speed	Nm	28.65
Max Speed	RPM	8000
Torque @ Max Speed	Nm	7.16



# Approach (Non-RE Motor)

Model development to automate and minimize iterative enhancements

## Model Development Process

### Tool

Excel spread sheet equipped with VBA script enabling new design and FE model development



### Model Input

Initial dimensions, poles and slot combination, winding type, current density, slot fill factor, soft and hard magnetic materials

### Finite Element Model

Built FE model with geometric features (magnets dimensions, stator tooth basic dimensions, back iron thickness, etc.), simulation conditions, excitations



### Computation of Initial State

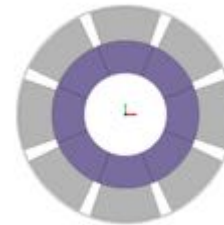
Computation of torque for given electric and magnetic loading

### Optimization

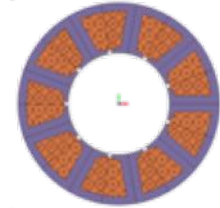
Defined objectives (total weight);  
constraints (required torque);  
Parameter bounds (geometric variables with bounds)



## Configurations Under Consideration

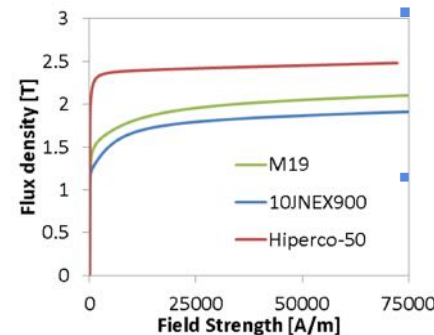


Surface PM



Fractional Slot  
Concentrated Winding

## Material Properties



### Lamination materials

- HIPERCO (6 mils)
- M19 - 3.5 Si (14 mils)
- 10JNEX900 - 6.5% Si (4 mils)

### Magnet Material

- NdFeB48
- MnBi
- Ferrite

Material	Remnant Flux Density [T]	Coercive Force [kA/m]	Energy Product [MGOe]
NdFeB48	1.39	1060	46.2
MnBi	0.6	405.8	8.4
Ferrite	0.45	33.5	4.9

# Technical Accomplishments (Non-RE Motor)

Topology optimization: Genetic algorithm based 2d optimization for reduced weight and cost

The image shows three overlapping screenshots of the OptiNet software interface. The top screenshot displays the 'Model' tab with a table of objectives. The middle screenshot shows the 'Constraints' tab with a table of constraints. The bottom screenshot shows the 'Variables' tab with a table of variables.

Objective	Argument(s)	Goal	Reference	Weight	Test
1	Mass of all components	Minimize	1	1	Test
2		Minimize	1	1	Test

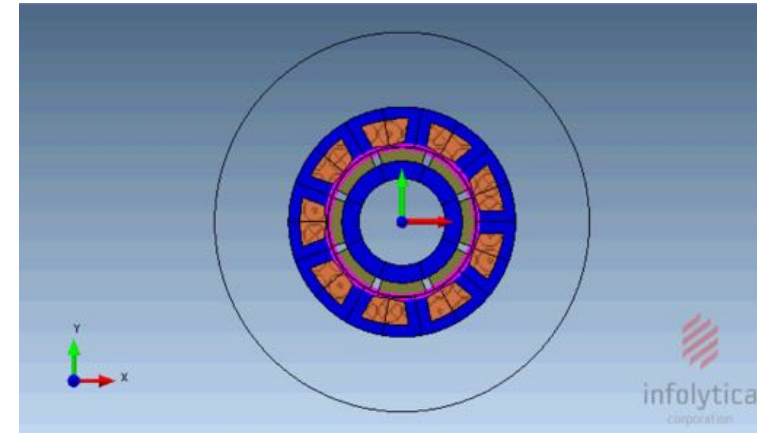
  

Constraint	Argument(s)	Type	Value	Weight	Test
1	Torque on comp.	Should be >=	52.5	10000	Test
2		Must be >=	False	10000	Test

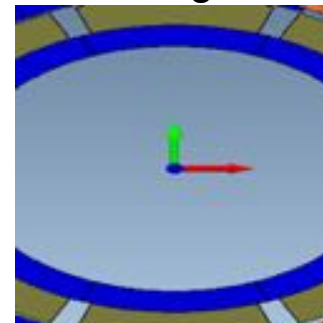
  

Variable	Type	Initialization	Unit	
10	rotorLaminationMaxMeshSize	Constant	Value: 4	
11	rotorNot_Ratio_backIron_perNth	Continuous	Initial: 0.35 Minimum: 0.15 Maximum: 0.6	
12	rotorNot_perDipFactor	Constant	Value: 0	
13	rotorNot_perHeight	Discrete Step	Initial: 15 Minimum: 3 Maximum: 25 Step: 0.1	
14	rotorNot_perPoleFactor	Continuous	Initial: 0.85 Minimum: 0.6 Maximum: 0.95	
15	rotorNotMaxMeshSize	Constant	Value: 4	
16	rotorRotationAngleString	Constant	Value: 0	
17	slotWFactor	Constant	Value: 0.5	
18	slotRatio	Continuous	Initial: 0.85 Minimum: 0.3 Maximum: 0.8	
19	stackLength	Discrete Step	Initial: 50 Minimum: 5 Maximum: 150 Step: 0.1	
20	statorCoilMaxMeshSize	Constant	Value: 6	
21	statorLaminationMaxMeshSize	Constant	Value: 4	
22	statorNot_Ratio_backIron_toothNth	Continuous	Initial: 0.5245 Minimum: 0.2 Maximum: 0.9	
23	statorNot_Ratio_slotOpening_openSlot	Constant	Value: 0.2	
24	statorNot_Ratio_toothNth_slotPitch	Continuous	Initial: 0.413 Minimum: 0.2 Maximum: 0.8	
25	statorNot_toothBaseAngledSectionHeight	Constant	Value: 2	

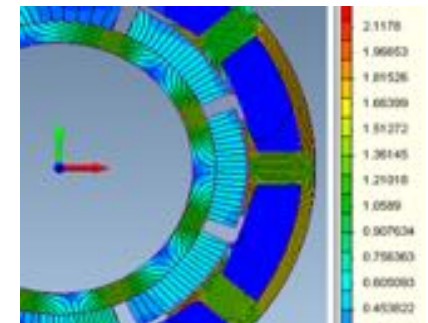
## Topology Optimization (Video)



Optimized design



Magnetic Field Distribution



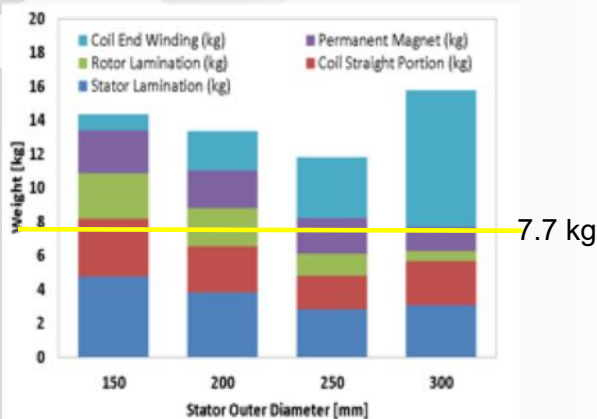
- 2d model design/topology optimization
- Objective: Minimize weight
- Constraints: Torque > 52.5 Nm (10% higher than peak torque)



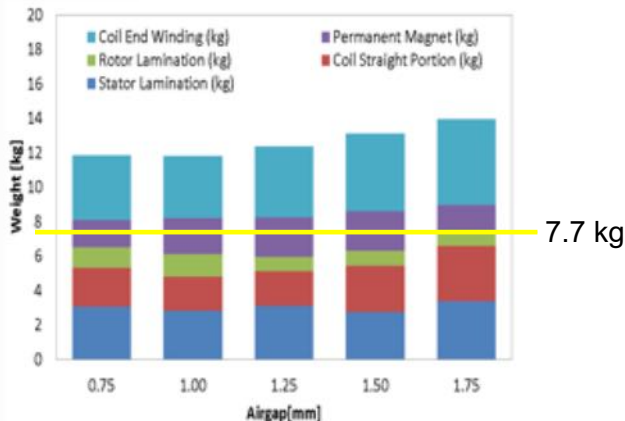
# Technical Accomplishments (Non-RE Motor)

End winding contribution to total weight is significant for smaller power

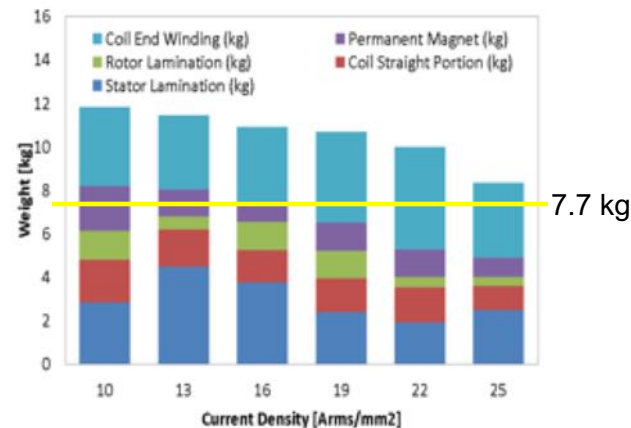
Trade Studies: Outer Diameter



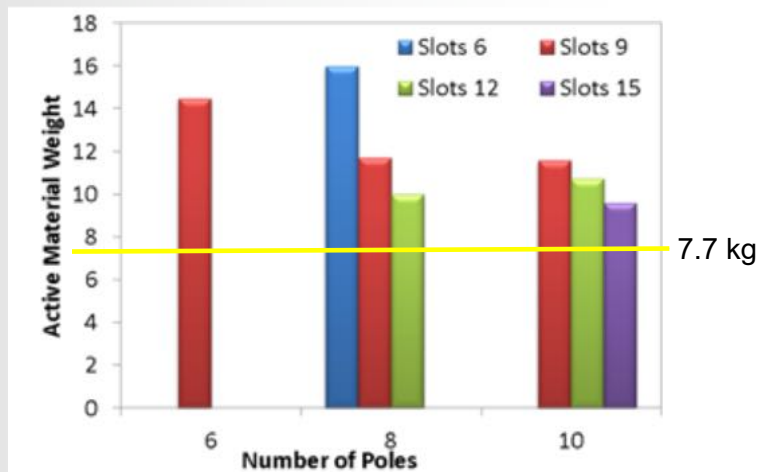
Trade Studies: Airgap



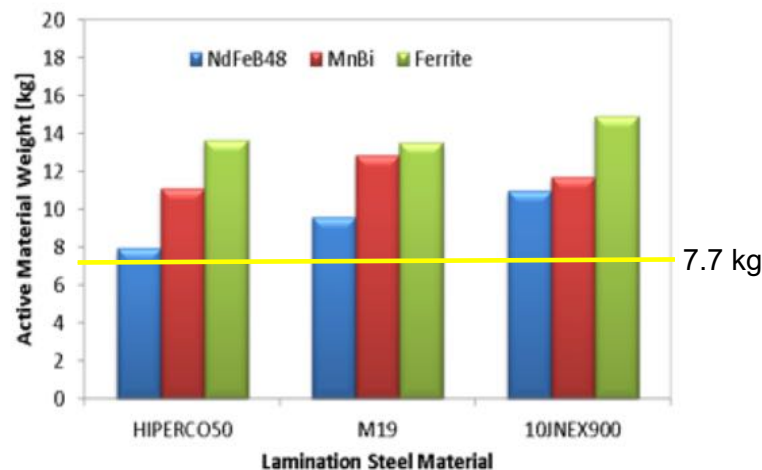
Trade Studies: Current Density



Trade Studies: Slot Pole Combination



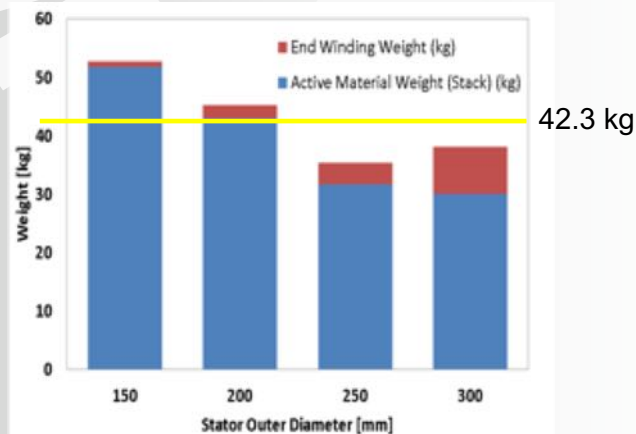
Trade Studies: Materials



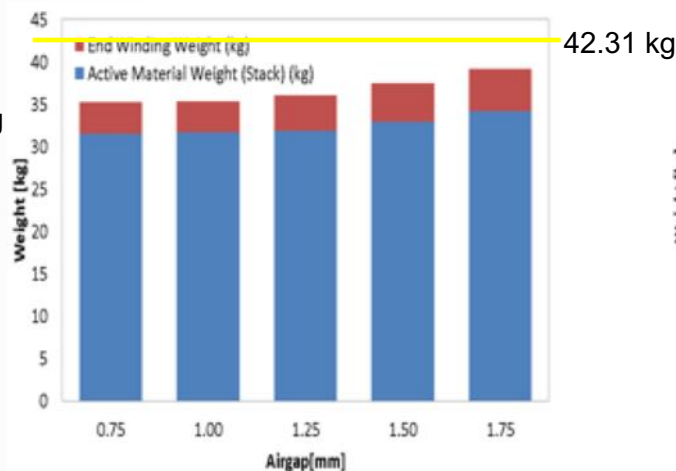
# Technical Accomplishments (Non-RE Motor)

Scalability studies show that proposed design meets target power density

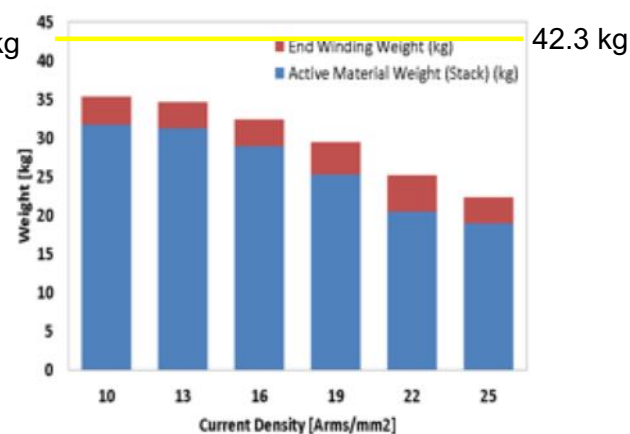
Trade Studies: Outer Diameter



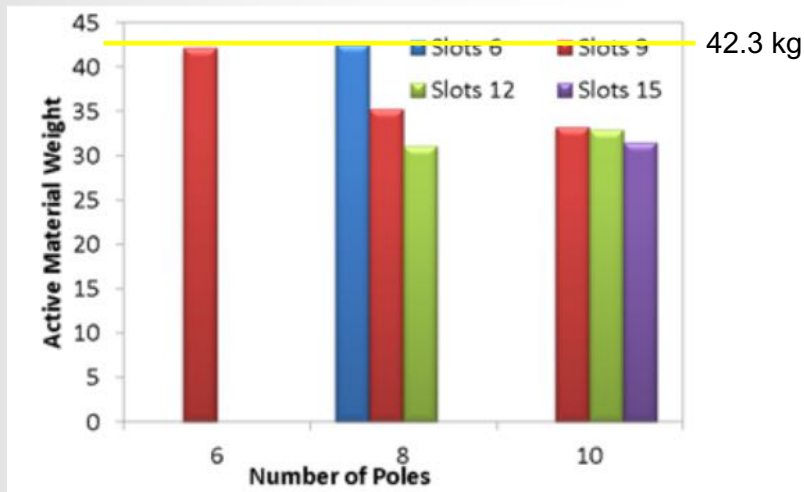
Trade Studies: Airgap



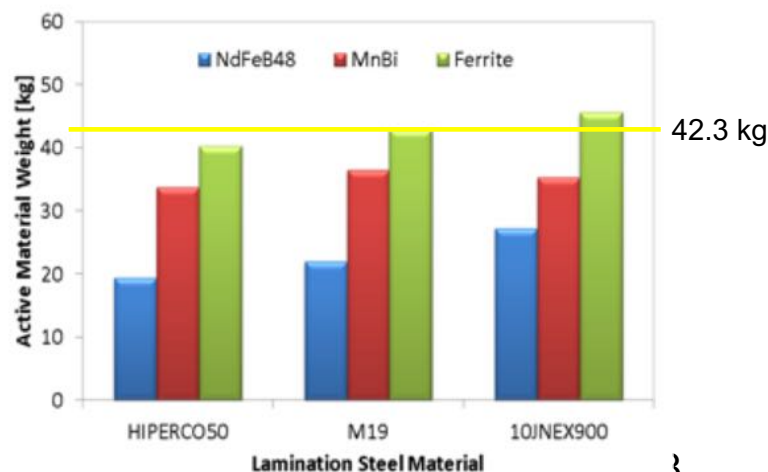
Trade Studies: Current Density



Trade Studies: Slot Pole Combination



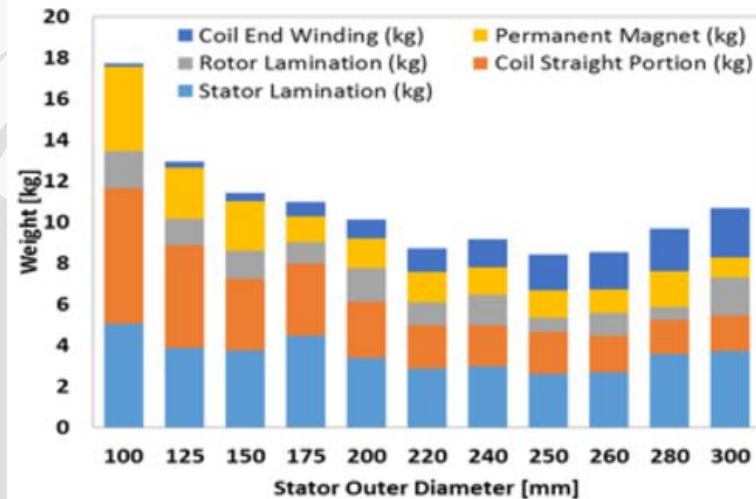
Trade Studies: Materials



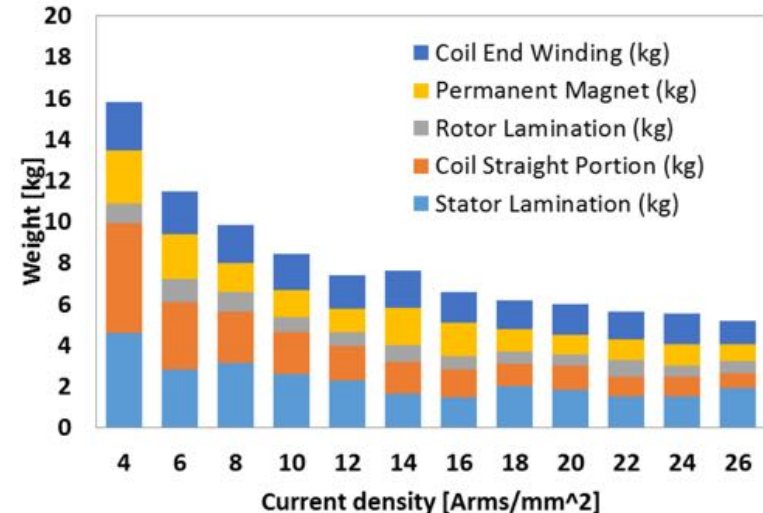
# Technical Accomplishments (Non-RE Motor)

Detailed design with key design parameters (Power density & efficiency)

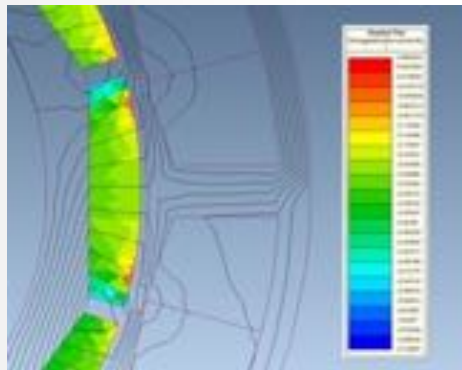
**Finer Outer Diameter Sensitivity**



**Finer Current Density Sensitivity**



**Demagnetization**

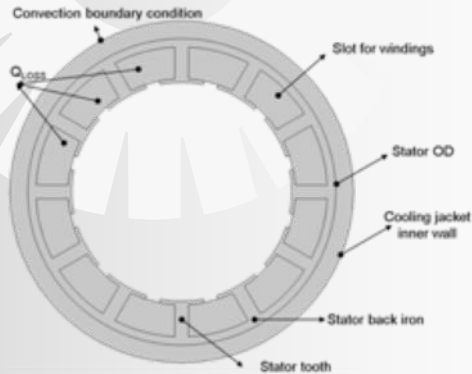


- Design space exploration to identify optimal design parameters
- Preliminary design performed using magnetic (B airgap) and electric loading (Ampere Turns)

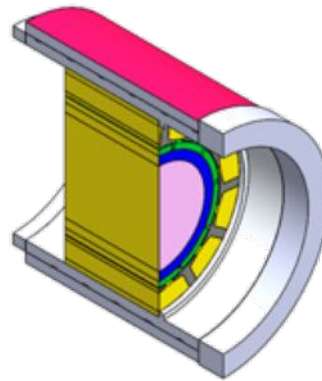
# Technical Accomplishments (Non-RE Motor)

2D/3D Thermal models to capture temperature distribution in the motor

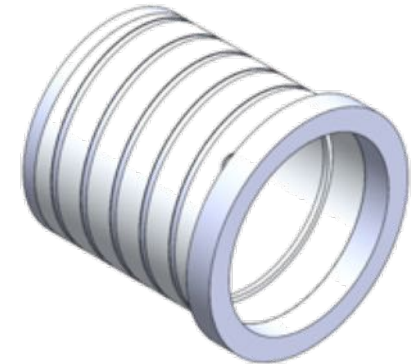
**2D Thermal Model**



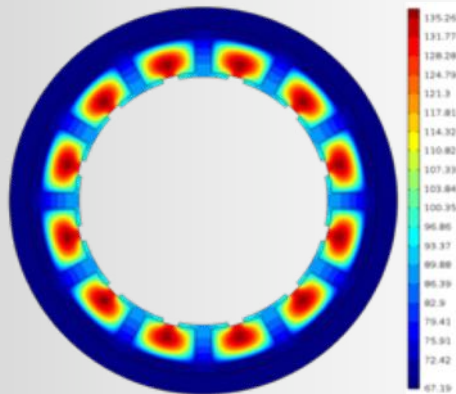
**3D CAD Model – Cut View**



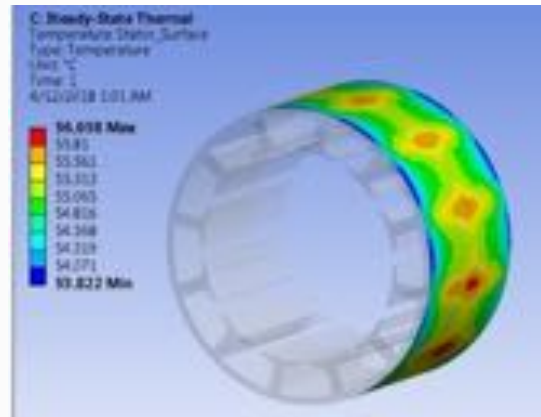
**Spiral Cooling Jacket**



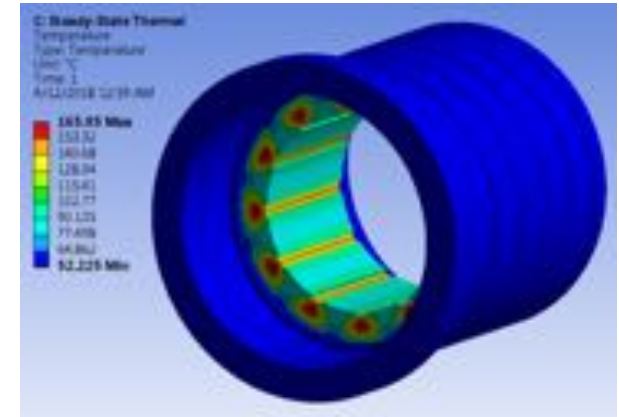
**2D Temperature Distribution**



**3D Temperature Distribution**



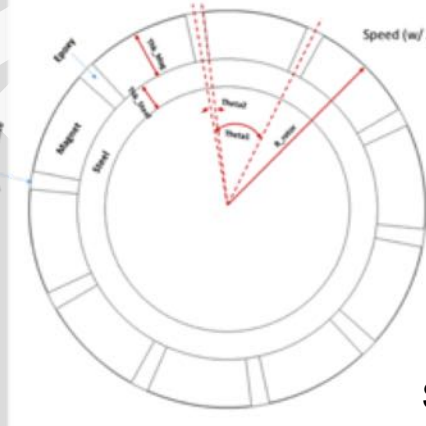
**Distribution for Complete Model**



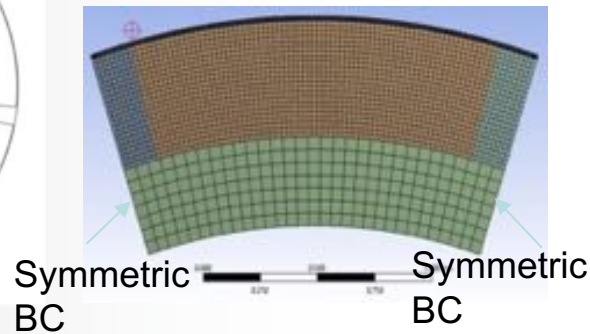
# Technical Accomplishments (Non-RE Motor)

Structural modeling to design the carbon fiber composite thickness

## Parametric Geometry



## 2D Model



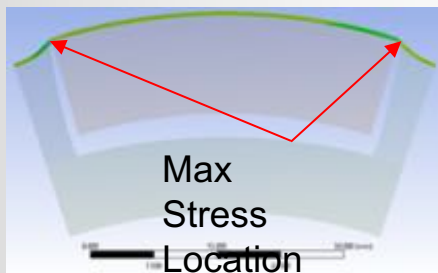
## FE Models

2D (plane strain) sector models used for analysis

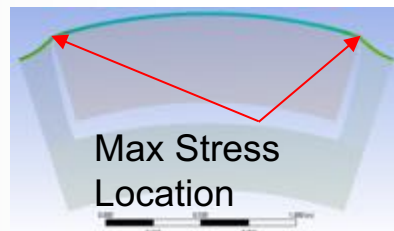
Contacts:

- Magnet is only bonded to composite wrap
- Adhesive bonded to the steel rotor and composite wrap

## Interlaminar Shear Stress (SXY)



## Hoop Stress (SY)



Angular Velocity: 8000 RPM  
20% Over speed: 9600 RPM

Composite wrap thickness: 0.5mm

# Responses to Previous Year Reviewers' Comments

- N/A (this is the first first review).

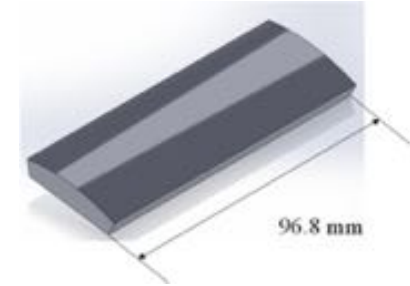
# Collaboration and Coordination

Ames Laboratory	500 gram flakes production; 100 gram magnet fabrication
United Technology Research Center	Motor design and testing
University of Delaware	Amorphous MnBi flakes production
Electron Energy Corp.	Dummy magnet simulating the performance of MnBi magnet
JFE Steel Corp.	Commercial 6.5 Si% steel sheet (0.1 mm)
Leppert-Nutmeg Inc.	Motor construction
Oak Ridge National Laboratory	Additive manufacturing of motors



# Remaining Challenges and Barriers

- MnBi:
  - Magnet shape
  - Scale up
  - Increase energy product to 10 MGOe
- 6.5% Si steel:
  - Retain the lambda texture to further reduce the core loss
  - Increase OD to 7 inch
- Motor
  - Improve power density to 5.7 kW/L





# Proposed Future Research

- MnBi

Milestone: one 100 gram 8.5 MGOe MnBi magnet; and one 2 gram 10 MGOe MnBi

- Improve fabrication process (better alignment and minimum oxidization)
- Mass produce high purity MnBi powder (5 kg, 72 emu/g)

- 6.5% Si steel

Milestone:  $W_{10/400} < 6$  W/kg for the ring with 0.4 mm thickness

- Optimize flake coating thickness and laminate architecture

- Non-Re motor

Milestone: Construct 400 Hz PM motor with dummy magnet and stator.

- Execute the motor design and coordinate with vendors

Any proposed future work is subject to change based on funding levels.

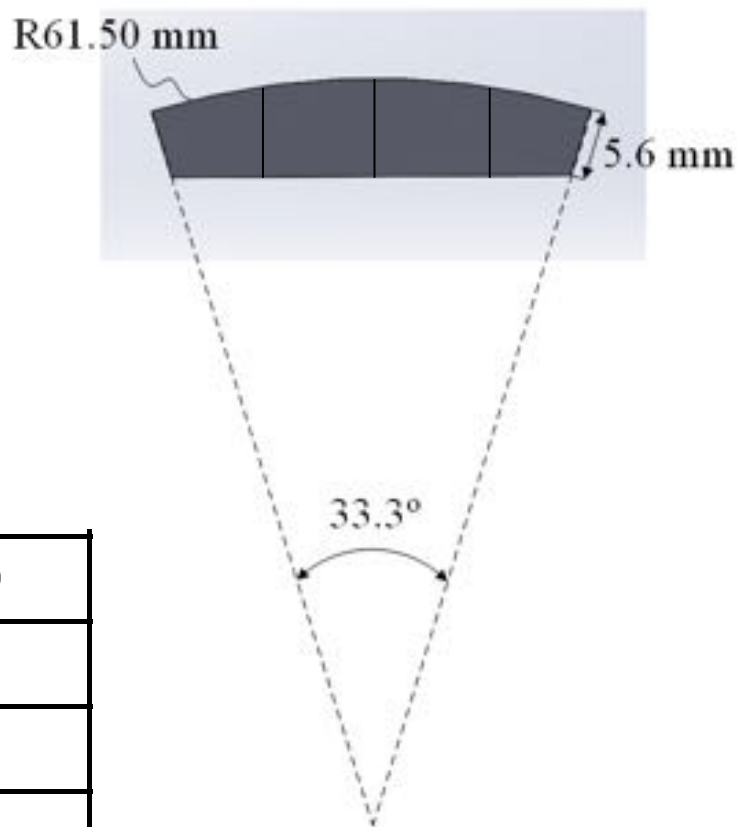
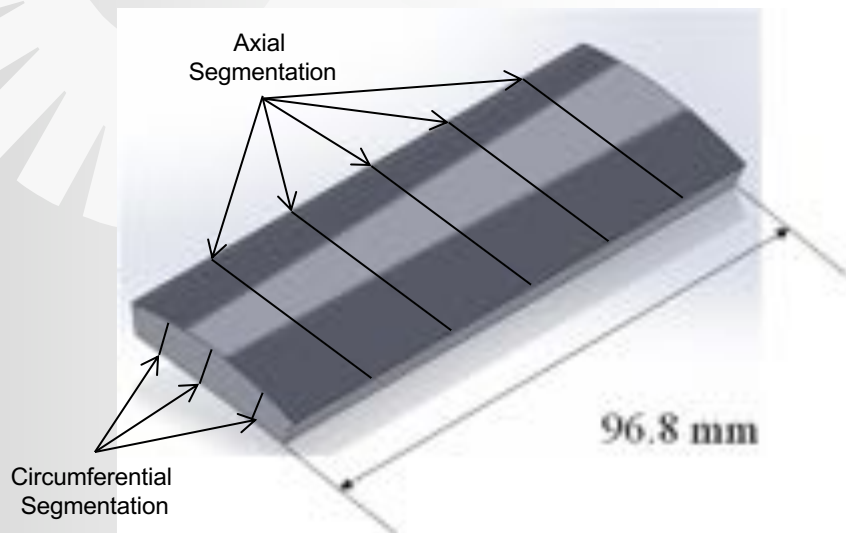
# Summary

- MnBi
  - Powder quality was improved from 65 emu/g to 70 emu/g
  - Cost effective bulk magnet fabrication method was developed
  - A 100 gram bulk magnet with 6.5 MGOe was fabricated
- 6.5% Si steel
  - Relationship between physical properties and cooling rate was established
  - Flake production method and capacity were established
  - Laminate inner structure was optimized and fabrication method was established
- Motor
  - 10 kW 400 Hz motor was designed
  - Vendors for constructing the motor were contracted.

# Technical Backup Slides

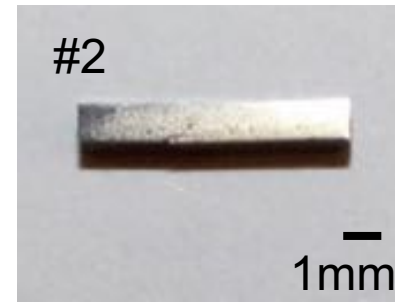
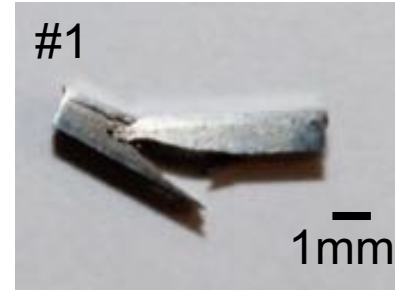
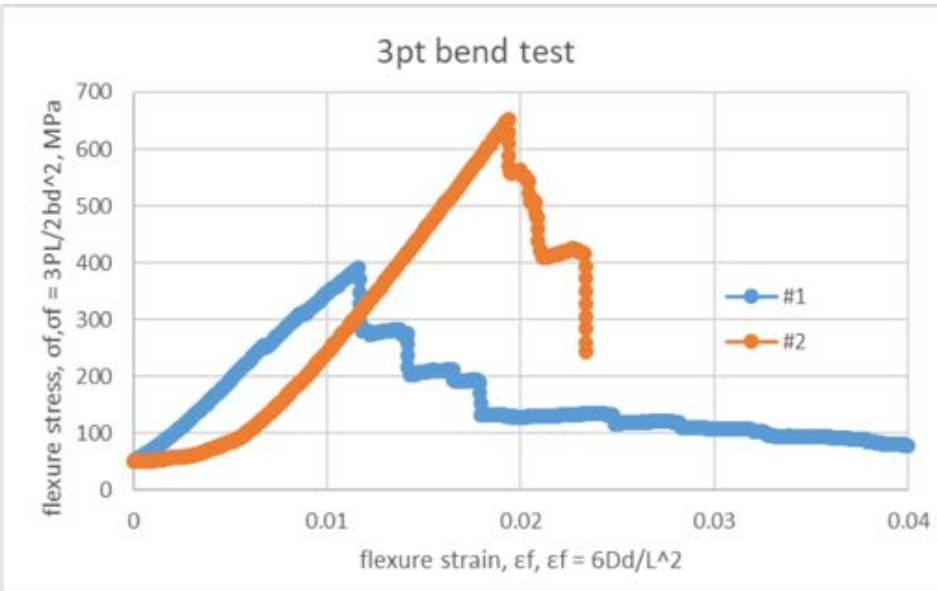
# Magnets used in this project

	Axial	Circumferential
Number of segments	4	5-10



Br [kG]	6.0
Hc [kOe]	5.1
Hci [kOe]	6.2
Bhmax [MGoe]	8.4

# Mechanical Properties



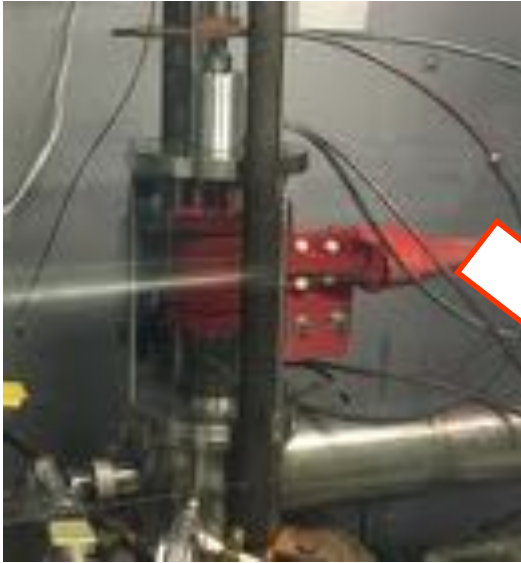
Sample #1 has pre-existing crack

The mechanical properties of the  $\text{CaF}_2$  coated is remarkable

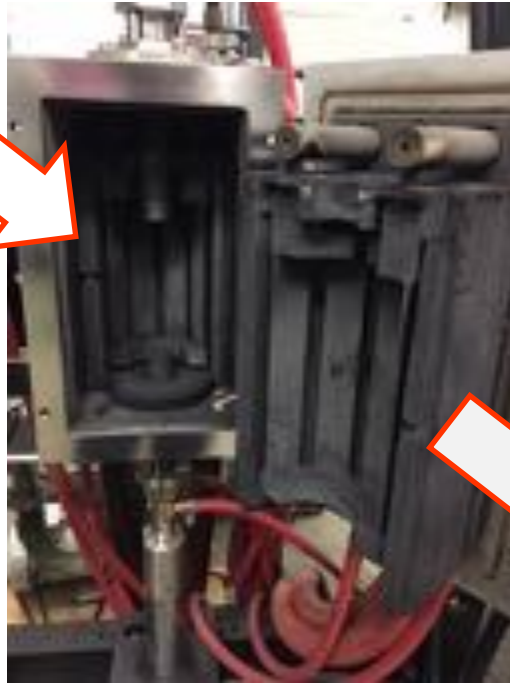
- High bending strength (650MPa)
- $\text{CaF}_2$  interlayer bonding prevented the sample from catastrophic failure on breakage.

# Current Effort To Scale Up

2" diameter



3" diameter



7" diameter

