

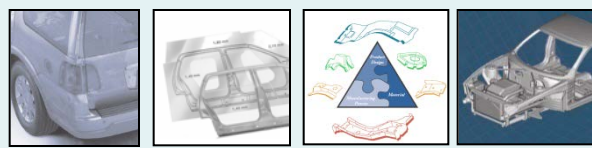
# Lightweight Sealed Steel Fuel Tanks for Advanced Hybrid Electric Vehicles ASP-400

Philip A Yaccarino  
General Motors  
May 18, 2012



Auto/Steel  
Partnership

Project ID # LM066  
[www.a-sp.org](http://www.a-sp.org)



## Timeline

- Start: Jan. 2, 2011
- Finish: Sept 30, 2011
- Project complete
  - No further funding

## Budget

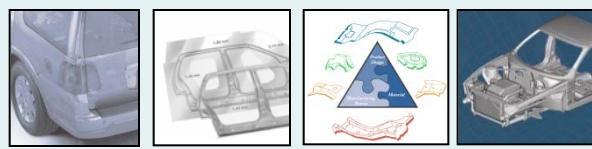
- Total project funding
  - DOE: \$158K
  - Contractor: \$158K
- DOE funding received
  - FY 2011: \$99K
  - FY 2012: \$56K

## Barriers

- High mass of current generation sealed steel tanks
- Forming, rigidity and fatigue of thin wall, low mass tanks
- Manufactured cost

## Partners

- Ford, GM
- ArcelorMittal
- Henkel Corporation
- No. American Stainless
- Nippon Steel, USA
- Soutec Ltd.
- Spectra Premium Inds. Inc.
- ThyssenKrupp Steel – USA
- US Steel Corp.
- EDAG Inc.

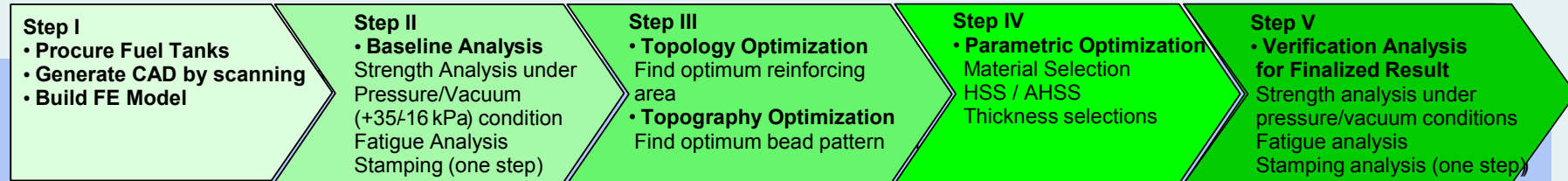


Enable and demonstrate the manufacturing feasibility of low-mass, sealed steel fuel tanks suitable for use in advanced hybrid electric vehicles (AHEV) while achieving equivalent performance and cost to the production tank.

Critical to allow a low mass metal option for fuel tanks for advanced hybrid electric vehicles which require pressurized fuel tank systems.

*Target mass reduction 30-40%*

## TWO BENCHMARK TANKS



### Input

Physical Sealed  
Fuel Tank

EDAG CAE  
Stiffness Analysis  
Guidelines

EDAG CAE  
Optimization  
Analysis Guidelines

ASP  
Steel Material Database  
  
Terokal 5089 Adhesive  
Properties

Optimize  
candidates to  
finalize solution

### Output

Systems and parts  
dimensions, weight  
  
CAD Data  
  
FE Model

Fuel tank stiffness  
baseline analysis  
results

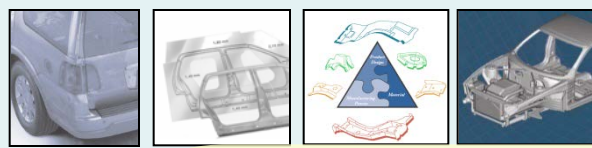
Optimum  
reinforcing concept  
and locations  
  
Optimum Bead  
pattern

Optimum material  
and thickness  
combination for  
light weight

**LWSSFT  
Fuel  
Tank**

### Tools Used

ANSA, Hyper Works, NASTRAN, Design Life, ABAQUS



## **Phase 1: Establish methodology**

**Establish project metrics**

**January 2011 – February 2011**

**Completed**

## **Phase 2: Optimize mass for flat fuel tank (Lexus)**

**CAE/Forming Analysis**

**February 2011 – March 2011**

**Completed**

**Optimize Shape**

**February 2011 – April 2011**

**Completed**

## **Phase 3: Optimize mass for large, saddle, fuel tank (Mercedes)**

**CAE/Forming Analysis**

**May 2011 – August 2011**

**Completed**

**Optimize Shape**

**August 2011 – September 2011**

**Completed**

## **Phase 4: Report preparation and technology transfer**

**September 2011**

**Completed**

# CHARACTERISTICS OF BENCHMARK TANKS

2010 Model	Vehicle Type	Tank			Steel	
		Capacity gal (liter)	Mass pound (kg)	Weld Method	Thickness inch (mm)	Type
LEXUS RX 450h	CUV	16 (60.6)	* 65.6 (29.83)	Electric Resistance Seam	0.079 (2.0)	Low Carbon
MERCEDES M 450H * Including post paint, ** with fuel tank accessories	SUV	24 (90.8)	** 67.5 (30.68)	Plasma	0.059 (1.5)	301 LN Stainless



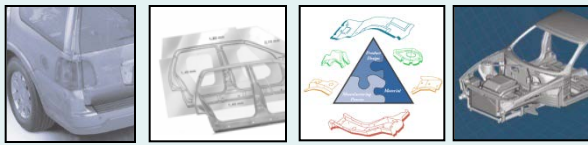
LEXUS RX 450h



MERCEDES M 450H

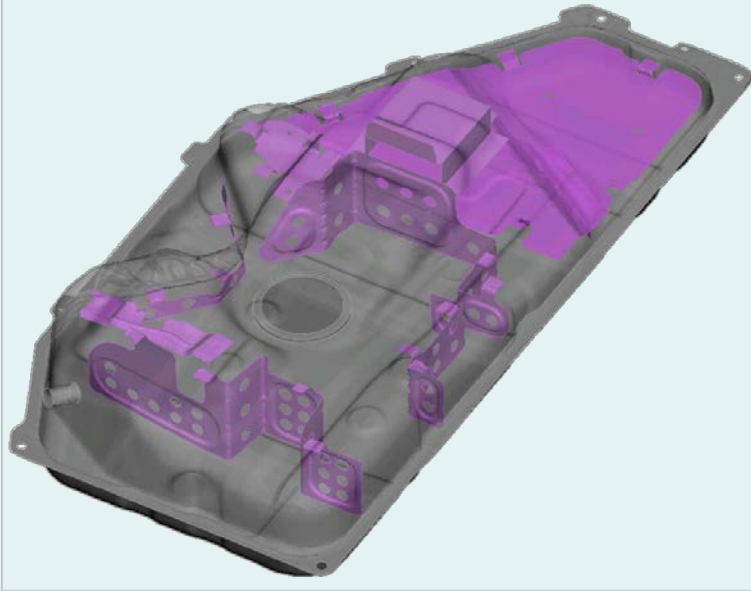






# LEXUS – BASELINE STRESS AND FATIGUE ANALYSIS

## ❑ Load Condition: Static Pressure / Vacuum



### ❑ Set up Condition

- ❑ Pressure Load : 35 kPa
- ❑ Vacuum Load : -16 kPa

### ❑ Initial Tank Condition

- ❑ Shell Thickness - Upper / Lower : 2.0 mm
- ❑ Shell / Baffle Material : Low Carbon Steel
- ❑ Baffle Shell Thickness : 0.7 mm
- ❑ Total Mass : 29.3 kg

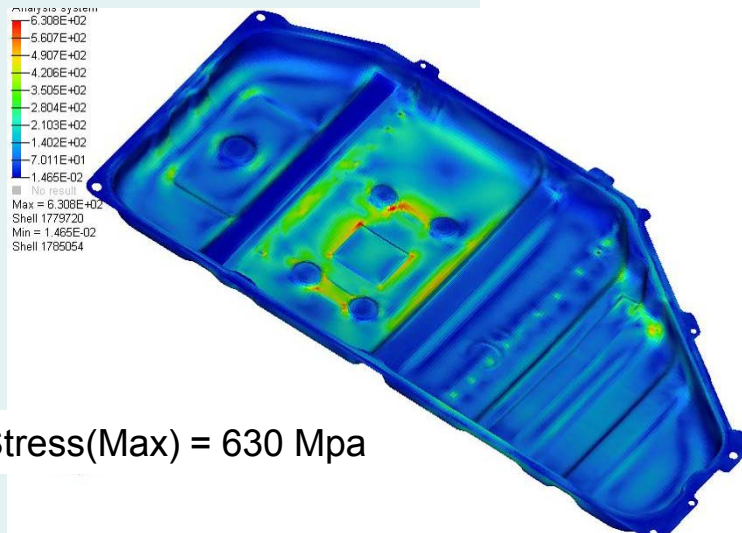
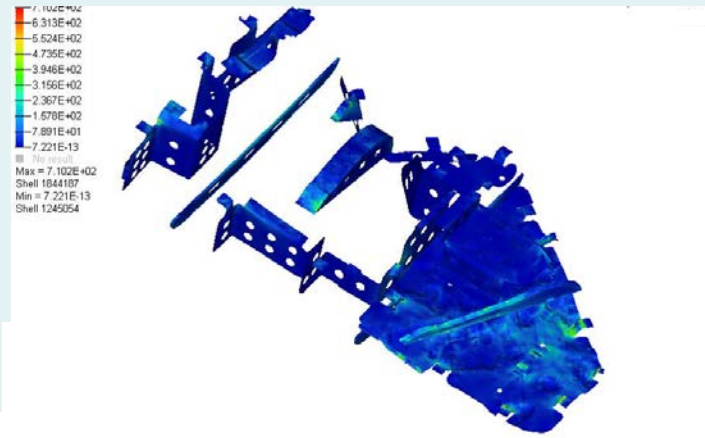
## ❑ Fatigue Loads & Requirements :

- ❑ Pressure / Vacuum : 35kPa to -16 kPa
- ❑ Minimum Life 12,000 cycle x 1.5 SF = 18,000 cycles

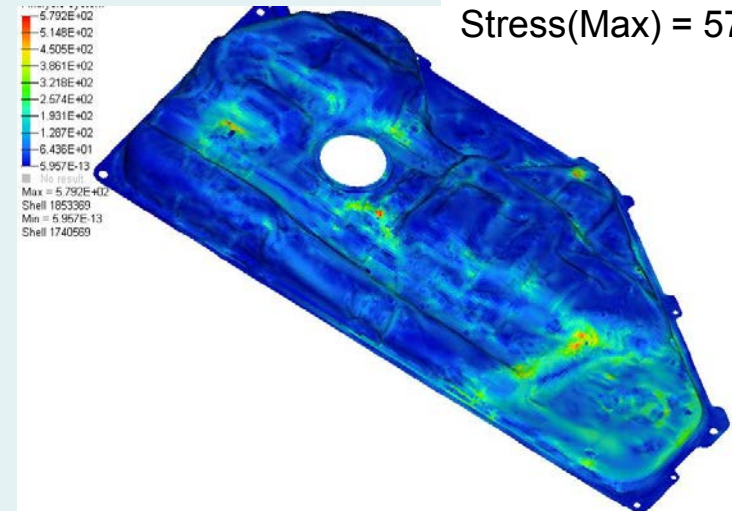
# LEXUS - STRUCTURAL IMPROVEMENTS

## □ Stress Analysis / Optimization Results

Additional Structural Baffles (1.0 mm Upper/Lower Shell thickness)



Stress(Max) = 630 Mpa

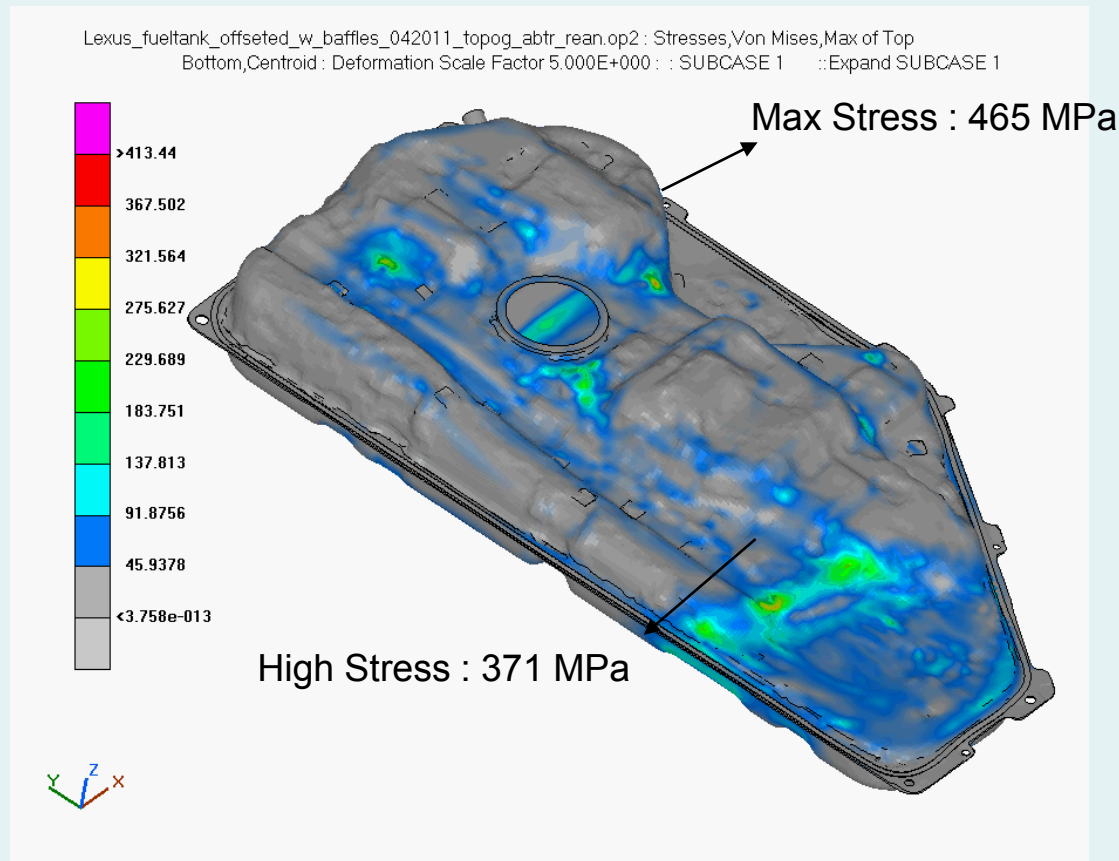


Stress(Max) = 579 Mpa



## □ Stress Analysis / Optimization Result based on Topography Optimization Result

❖ Load Condition: 35 kPa Pressure



## □ Parametric Analysis Results Summary (with additional baffles)

Case#	Shell Thickness (mm)	Baffle Thickness (mm)	Mass (kg)	Mass Saving (%)	Von-Mises Max Stress (MPa)	Von-Mises High Stress @ Fatigue (MPa)
1	2.0	0.7	29.3	0.0	506.5	506.5
2	2.0	0.7	29.3	0.0	413	413
3	2.0	0.7	29.3	0.0	541	386
4	2.0	0.7	29.3	0.0	465	371
5	2.0	0.7	30.1	+2.7	465	250
6	2.0	0.7	30.1	+2.7	303	265
7	1.5	0.7	23.4	-20.3	447	388
8	1.0	0.7	16.6	-43.3	838	716
9	0.9	0.7	15.8	-46.0	994	834
10	1.5 Upper	0.7	19.4	-34.5	433	381
10	0.9 Lower				834	
11	2.0	0.7/1.0/1.4	30.4	+3.6	279	268
12	1.8	0.7/1.0/1.4	27.7	-5.6	312	302
13	1.6	0.7/1.0/1.4	25.0	-14.7	363	344
14	1.4	0.7/1.0/1.4	22.3	-23.9	464	415
15	1.2	0.7/1.0/1.4	19.6	-33.5	592	522
16	1.0	0.7/1.0/1.4	16.9	-42.3	744	678
17						
18	1.4 Upr	0.7/1.4	22.8	-22.3	341	550
18	1.4 Lwr				336	
19	1.3 Upr	0.7/1.4	20.1	-31.4	398	529
19	1.1 Lwr				529	
20	1.0 Upr	0.7/1.4	17.4	-40.6	579	631
20	1.0 Lwr				631	
21	1.0 Upr	0.7/1.4	18.7	-36.2	571	571
21	1.2 Lwr				450	
22	1.1 Upr	0.7/1.4	19.4	-33.8	500	531
22	1.2 Lwr				450	
23	0.9 Upr	0.7/1.4	17.4	-40.7	667	676
23	1.1 Lwr				529	

with  
Additional  
Baffle

Min. thickness range  
focused on stress range

Upper : 1.0 mm  
Lower : 1.1 mm

## Forming Analysis Results Summary

Case#	Model Description	Shell Thickness (mm)	Baffle Thickness (mm)	Mass (kg)	Mass Saving (%)	Von-Mises Max Stress (MPa)	Von-Mises High Stress @ Fatigue (MPa)	Steel Candidates
18	Model v8 07/17/11, Iter 1	1.4 Upr	0.7/1.4	22.8	-22.3	341	550	TRIP 350/600
18		1.4 Lwr				336		TRIP 350/600
19	Model v8 07/17/11, Iter 2	1.3 Upr	0.7/1.4	20.1	-31.4	398	529	TRIP 400/700 OR TRIP 450/800
19		1.1 Lwr				529		TRIP 450/800 OR 301LN-1/4 Hard
20	Model v8 07/17/11, Iter 3	1.0 Upr	0.7/1.4	17.4	-40.6	579	631	301LN-1/4 Hard
20		1.0 Lwr				631		301LN-1/4 Hard
21	Model v8 07/17/11, Iter 4	1.0 Upr	0.7/1.4	18.7	-36.2	571	571	301LN-1/4 Hard
21		1.2 Lwr				450		TRIP 450/800 OR 301LN-1/4 Hard
22	Model v8 07/17/11, Iter 5	1.1 Upr	0.7/1.4	19.4	-33.8	500	531	TRIP 450/800 OR 301LN-1/4 Hard
22		1.2 Lwr				450		TRIP 450/800 OR 301LN-1/4 Hard
23	Model v8 07/17/11, Iter 6	0.9 Upr	0.7/1.4	17.4	-40.7	667	676	301LN-1/4 Hard
23		1.1 Lwr				529		TRIP 450/800 OR 301LN-1/4 Hard

- AHSS (TRIP450/800) → Case # 22
- Stainless (301 LN-1/4 hard) → Case # 20, 21, 22, 23

## Fatigue Life Analysis Results – Case#21 (Iteration# 14)

- Analyzed fatigue life 72,420 Cycles (minimum) >> 18,000 Cycles (targeted)

# LEXUS - COST ANALYSIS

## □ Cost comparison

### AHSS (TRIP) (with post paint)

- High product volume (150,000/yr)  
+ 2.1 %
- Low product volume (50,000/yr)  
+ 5.6 %

Cost per kilogram saved:  
\$0.14 (high volume)

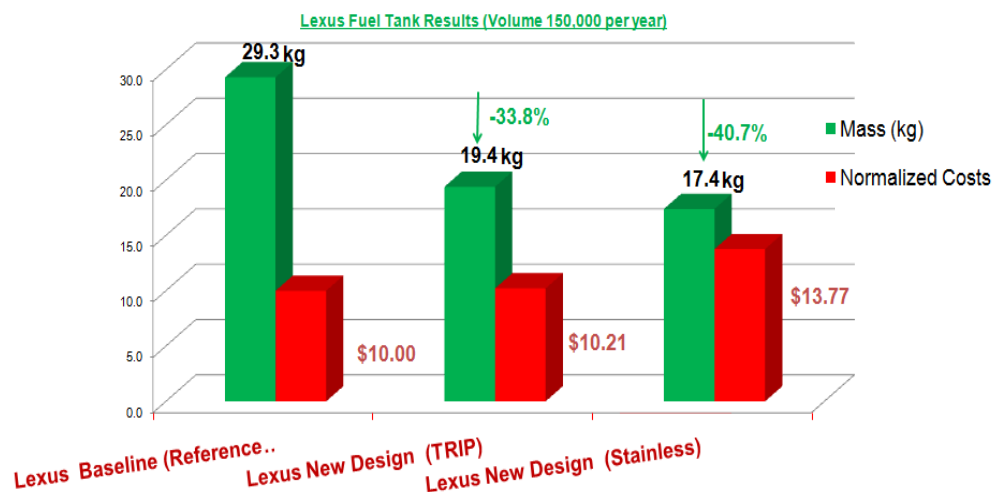
### Stainless (301 LN 1/4 hard) (without post paint)

- High product volume (150,000/yr)  
+ 37.7 %
- Low product volume (50,000/yr)  
+ 35.0 %

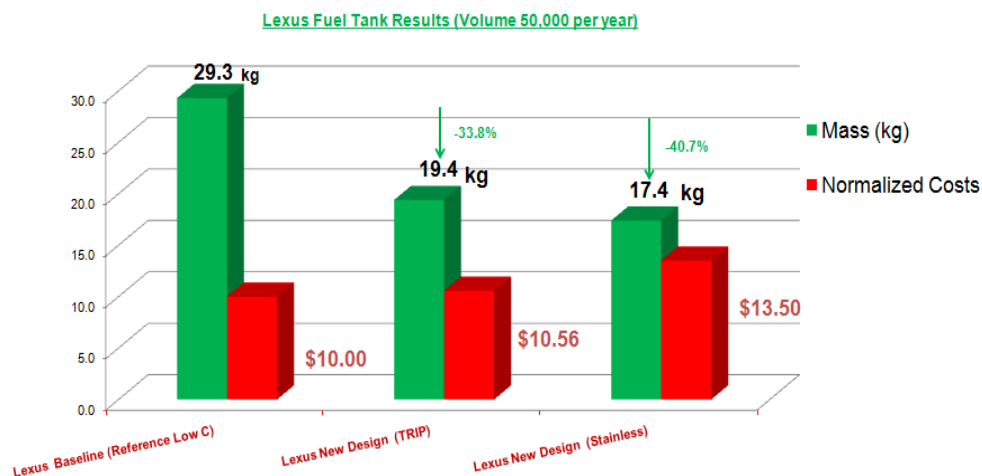
Cost per kilogram saved:  
\$2.10 (high volume)

## Lexus Tank Results

### High Product Volume



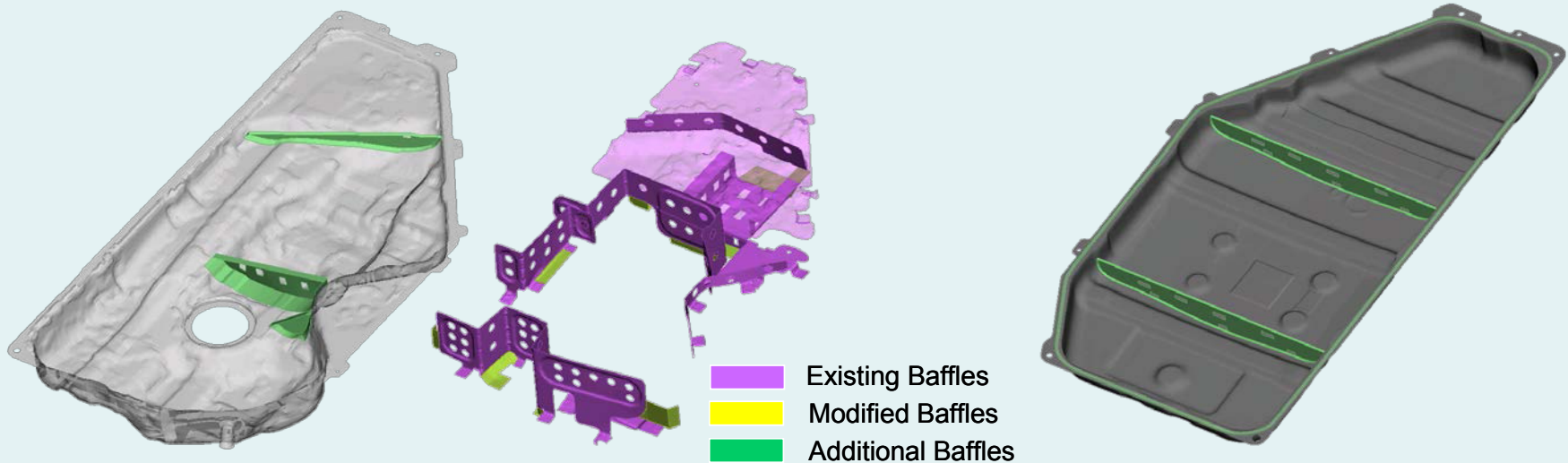
### Low Product Volume



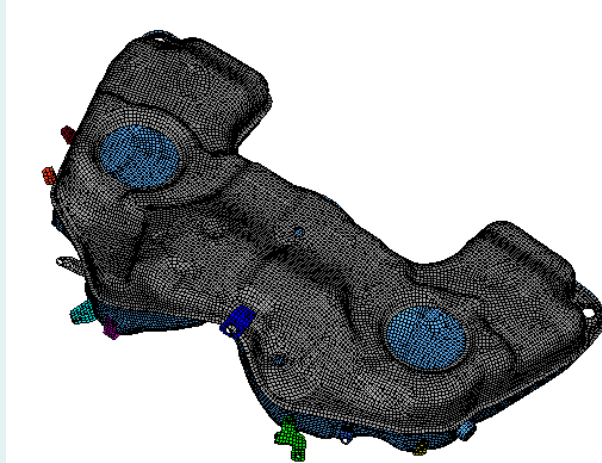
## □ Conclusions

- Optimized results are shown in following table with baffles present and achieved 34%~41% mass reductions
- No significant tank volume change
- Structural baffles are built on existing sloshing baffles by extension and welding

		Steel Grade	Initial Tank Mass (kg)	Reduced Tank Mass (kg)	Mass Saving (%)	Cost Changes High / Low Vol. (%)	Shell Thickness (mm)	
							Upper	Lower
Material Type	AHSS	TRIP 450/800	29.3	19.4 (-9.9)	33.8	+2.7 / +6.8	1.1	1.2
	Stainless Steel	301LN - 1/4 Hard		17.4 (-11.9)	40.7	+37.7 / +35.0	0.9	1.1



## ❑ Load Condition : Static Pressure / Vacuum



### ❑ Set up Condition

❑ Pressure Load : 35 kPa

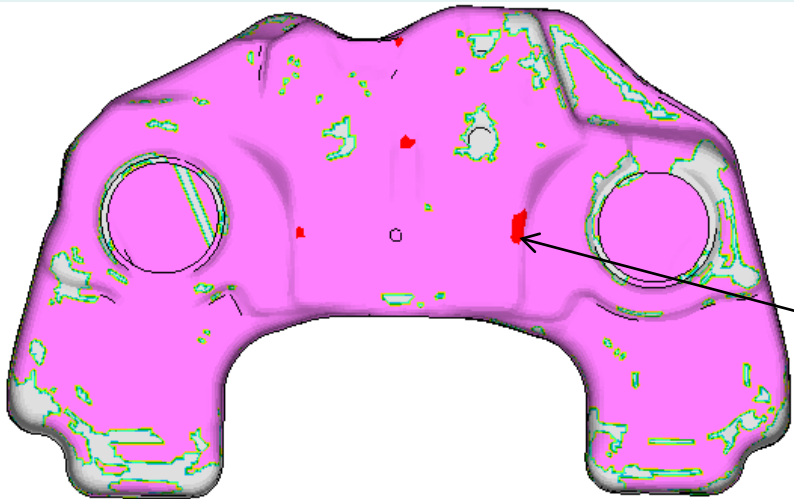
❑ Vacuum Load : -16 kPa

### ❑ Initial Tank Condition

❑ Shell Thickness - Upper / Lower : 1.5 mm

❑ Shell / Baffle Material : Stainless 301 LN

❑ Total Mass : 24.2 kg



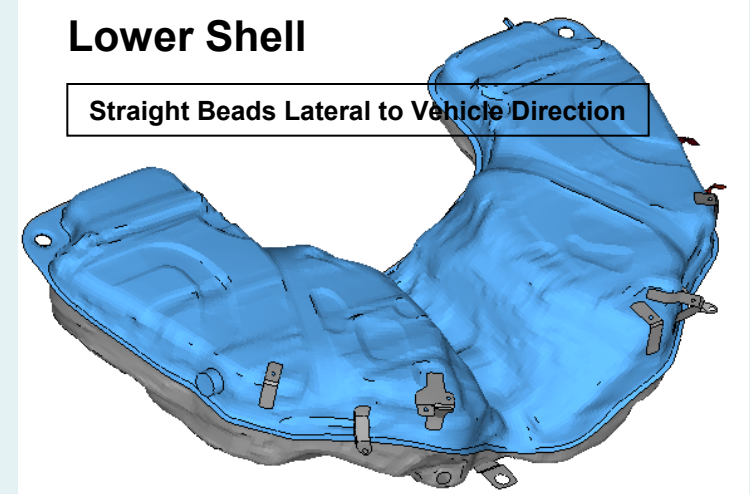
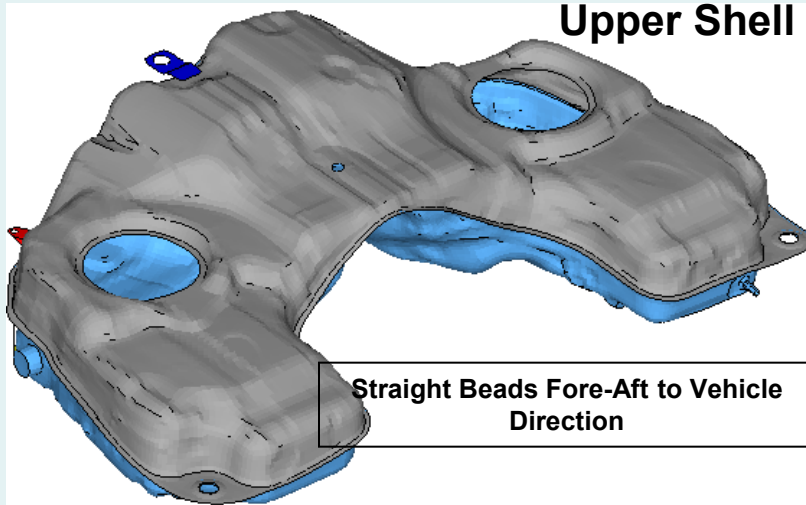
### Fatigue Life of Baseline Mercedes Tank

❑ 29,000 cycles

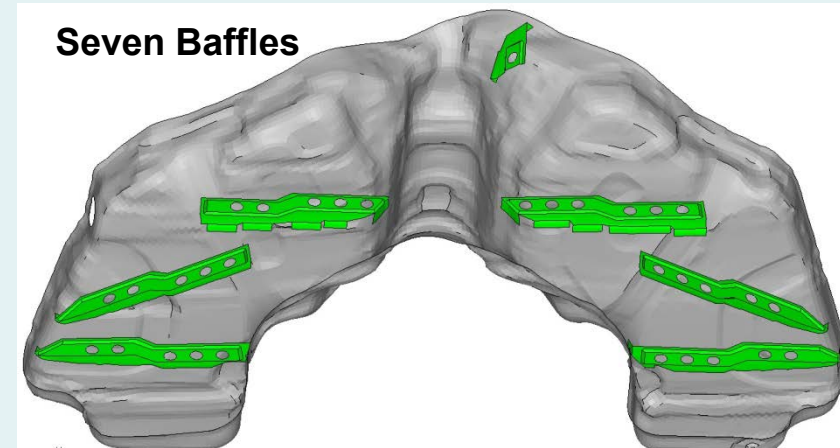
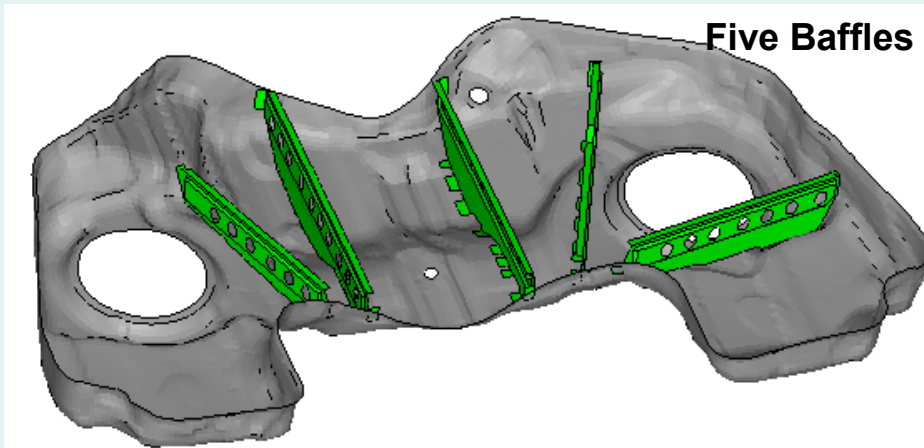


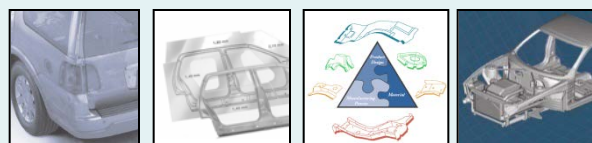
# MERCEDES - OPTIMIZATION RESULTS

## □ Topography Optimization



## □ Structural Improvements



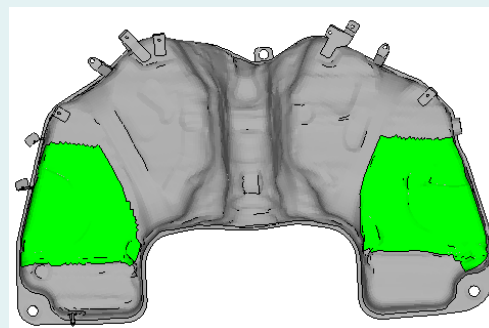
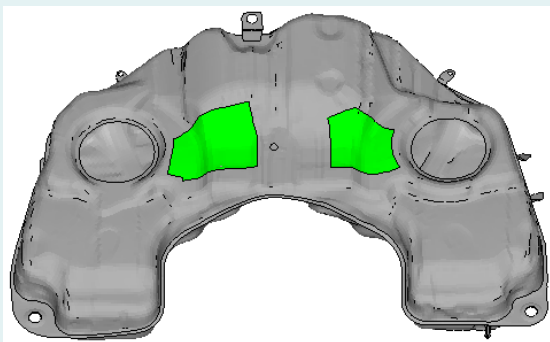


# MERCEDES - STRUCTURAL IMPROVEMENTS AND RESULTS

## ❑ Model - Iteration WB2

1.1mm Upper and Lower Shell

0.3mm Steel Reinforcements with 1.0 mm Terokal 5089 structural adhesive



## ❑ MERCEDES - Mass Reductions

Iteration #	Description	Shell Thickness (mm)	Baffle/Reinf Thickness (mm)	Total Mass (kg)	Mass Change (kg)	Mass Change (%)	Von-Mises Max Stress (Mpa)
B	Baseline	1.5	---	24.2	---	---	282
O	Topography Optimized	1.5	---	24.2	---	---	252
B1	Baffles Added	0.8	0.7	14.9	-9.3	-38.4	262
WB1	Weld Bonded Reinf Added	0.8	0.3	15.1	-9.1	-38.6	272
WB2	Weld Bonded Reinf Added	1.1	0.3	18.2	-6.0	-24.8	275

WB1 and WB2 iterations do not include baffles

# MERCEDES - VERIFICATION ANALYSIS

## Forming Analysis Results Summary – Upper Shell (Lower Shell Similar)

Material Type		Shell Thickness (mm)								
		1.6	1.5	1.4	1.3	1.2	1.1	1.0	0.9	0.8
Stainless HSS	201 LN								thinning	thinning
	301 1/4-hard	crack	crack	crack	crack	crack	crack	crack	crack	crack
	304 annealed								thinning	thinning
HSS	HSLA 350/450	crack	crack	crack	crack	crack	crack	crack	crack	crack
	TRIP 350/600	crack	crack	crack	crack	crack	crack	crack	crack	crack
	TRIP 400/700	crack	crack	crack	crack	crack	crack	crack	crack	crack

➤ Acceptable materials due to the forming geometry

## Fatigue Analysis Results Summary

Iteration #	Description	Shell Thickness (mm)	Baffle/Reinf Thickness (mm)	Total Mass (kg)	Mass Change (kg)	Mass Change (%)	Von-Mises Max Stress (Mpa)	Fatigue Life (cycles)	Steel Type
B	Baseline	1.5	---	24.2	---	---	282	29,000	Stainless 301LN
O	Topography Optimized	1.5	---	24.2	---	---	252	---	---
B1	Baffles Added	0.8	0.7	14.9	9.3	-38%	262	40,000	Stainless 201LN
WB1	Weld Bonded Reinf Added	0.8	0.3	15.1	9.1	-38%	272	39,000	Stainless 201LN
WB2	Weld Bonded Reinf Added	1.1	0.3	18.2	4.4	-25%	275	39,000	Stainless 201LN

# MERCEDES - COST ANALYSIS

## Mercedes Result – Stainless Steels

High Product Volume

### ❑ Cost Comparison Facts

#### Baffle only

- High product volume (150,000/yr)  
-32.4 %
- Low product volume (50,000/yr)  
-22.0 %

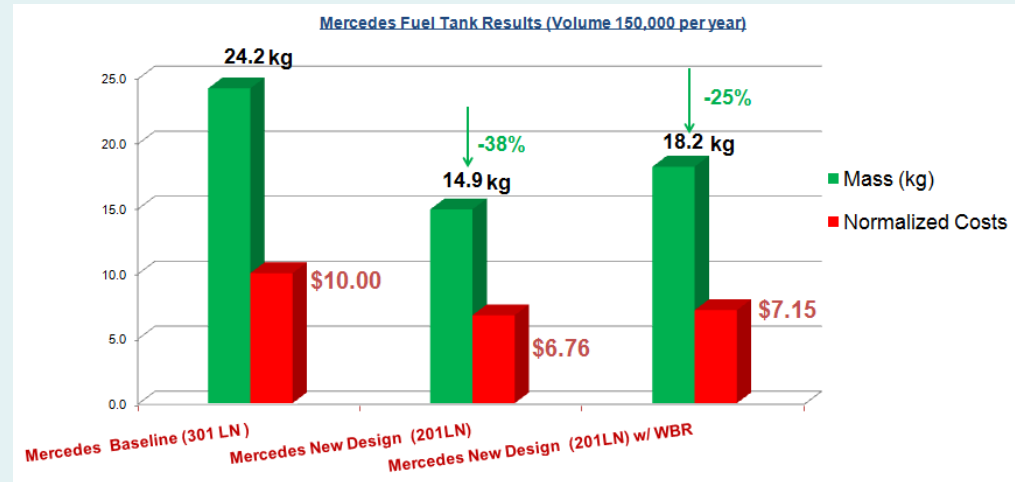
Savings per kg \$4.69 (High Volume)

#### Weld Bonded Reinforcement (WBR)

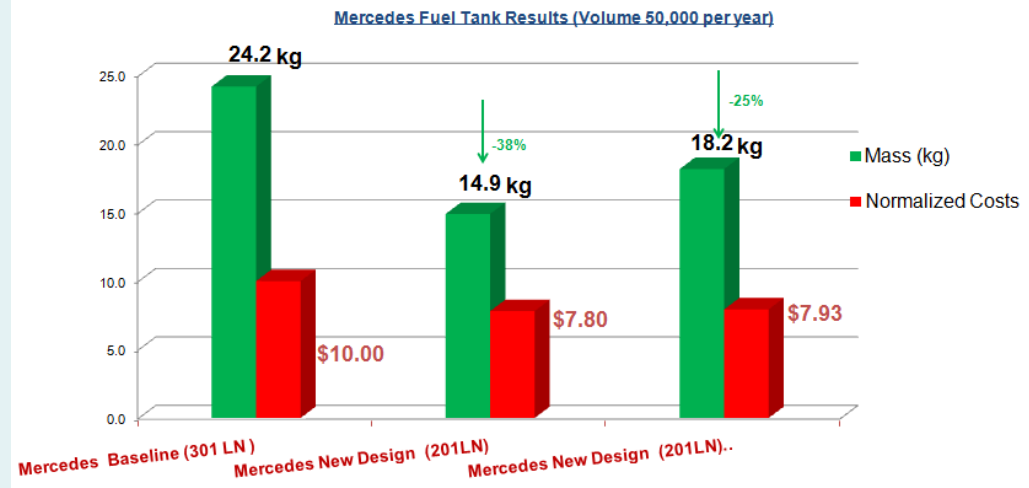
- High product volume (150,000/yr)  
-28.5 %
- Low product volume (50,000/yr)  
-20.7 %

Savings per kg \$6.37 (High Volume)

\*Seam welding assumed as joining method for all cost calculations and without post paint



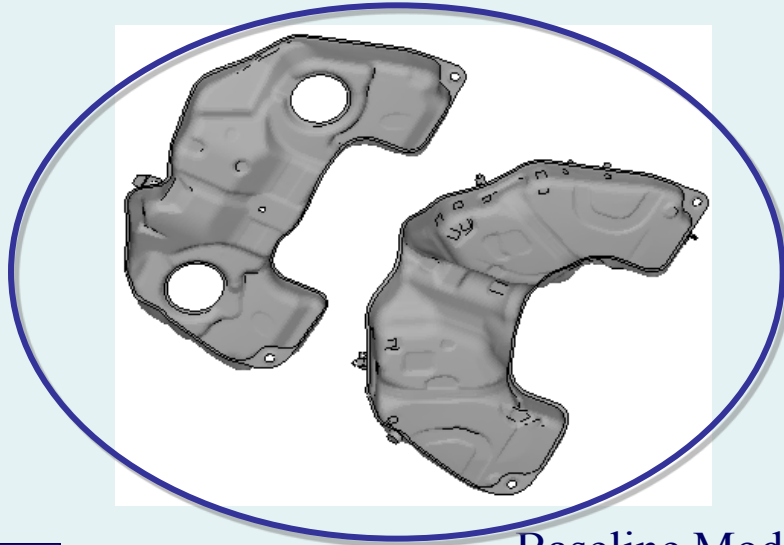
Low Product Volume



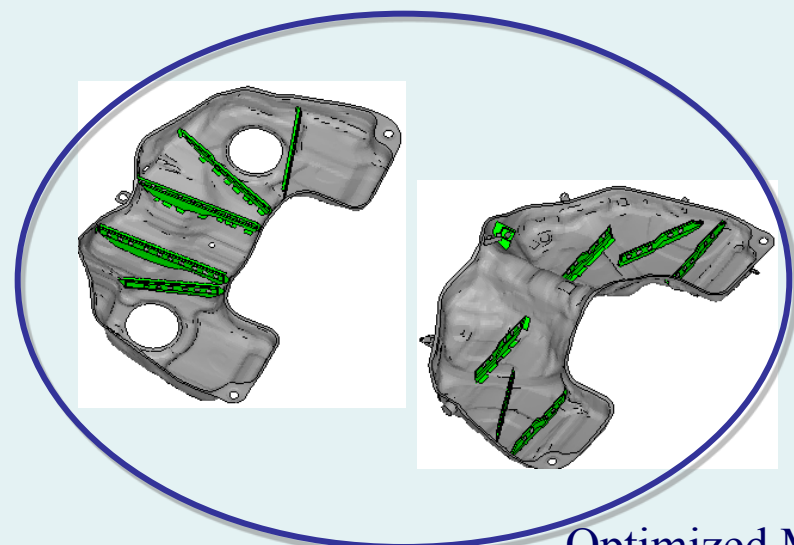
## Conclusions

- Significant mass reduction achieved by using stainless steel
- Achieved mass reduction : 38.5% (24.2 kg → 14.9 kg)
- Optimized stainless steel tanks exceed fatigue & rigidity requirements and are lower cost

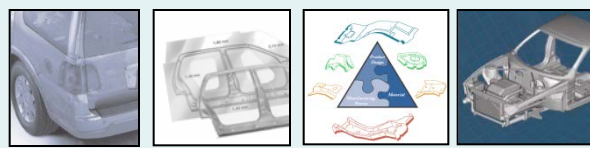
		Steel Grade	Initial Tank Mass (kg)	Reduced Tank Mass (kg)	Mass Saving (%)	Cost Changes High / Low Vol. (%)	Shell Thickness (mm)	
							Upper	Lower
Material Type	Stainless Steel	201LN - Annealed	24.2	14.9 (-9.3)	38.5	-32.4 / -20.7	0.8	0.8



Baseline Model



Optimized Model



- ☐ **Target mass reductions of 30-40% achieved**

- ☐ **Enablers:**

  - Structural supports:**

    - Stiffening ribs

    - Structural baffles

    - Weld-bonded adhesive patches

  - Thinner steels for tank walls:**

    - Carbon AHSS (TRIP) steel

    - Stainless steel

- ☐ **Fatigue and structural rigidity requirements met**

- ☐ **Low cost/kg of mass savings**

- ☐ **Vehicle level crashworthiness of designs not evaluated**

- Follow up Work Recommended:**

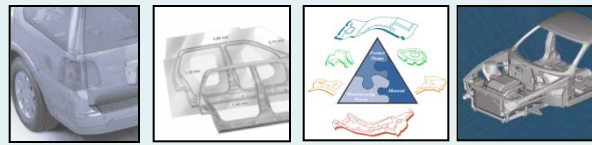
- ☐ **Evaluation of crashworthiness of proposed designs**

- ☐ **Evaluation of manufacturing feasibility**



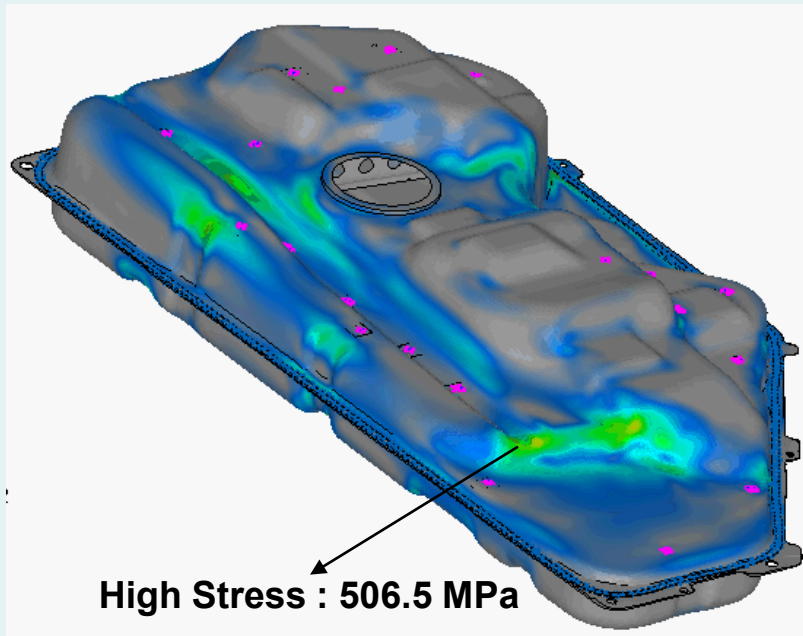
# TECHNICAL BACK-UP SLIDES

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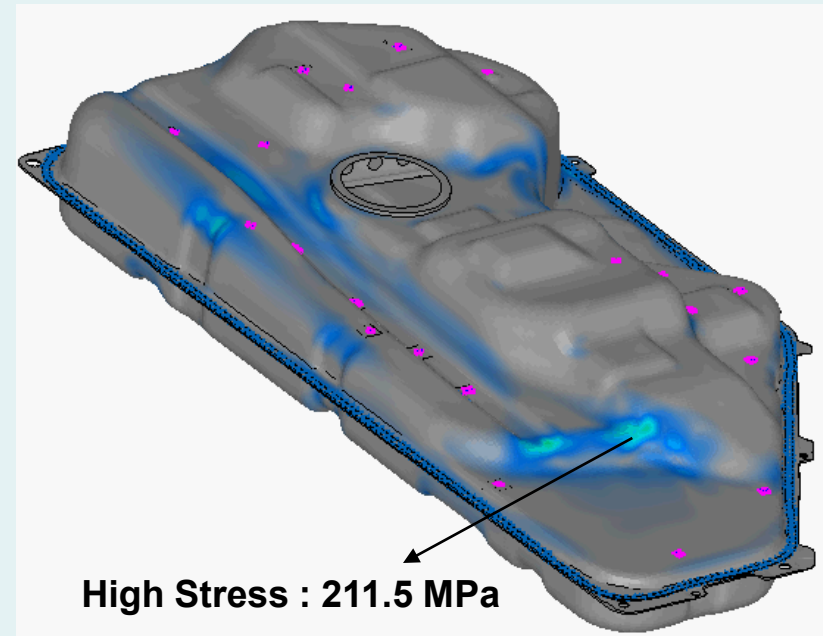


## □ Stress Analysis Results - LEXUS

### ❖ Static Pressure



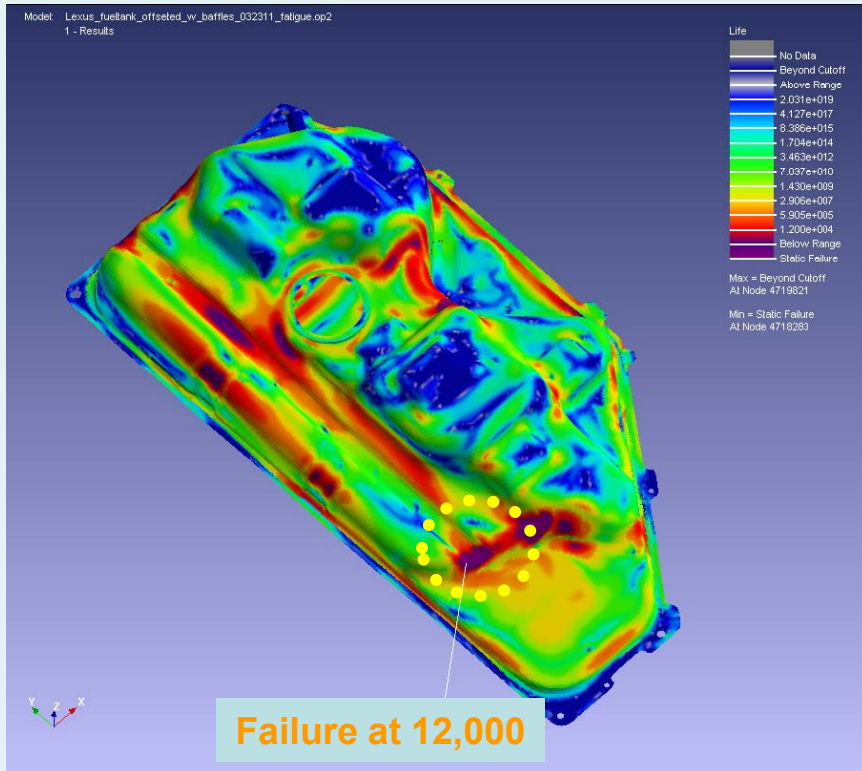
### ❖ Static Vacuum



# FATIGUE ANALYSIS - BASELINE RESULTS

## LEXUS TANK

### ❑ Fatigue Analysis Results

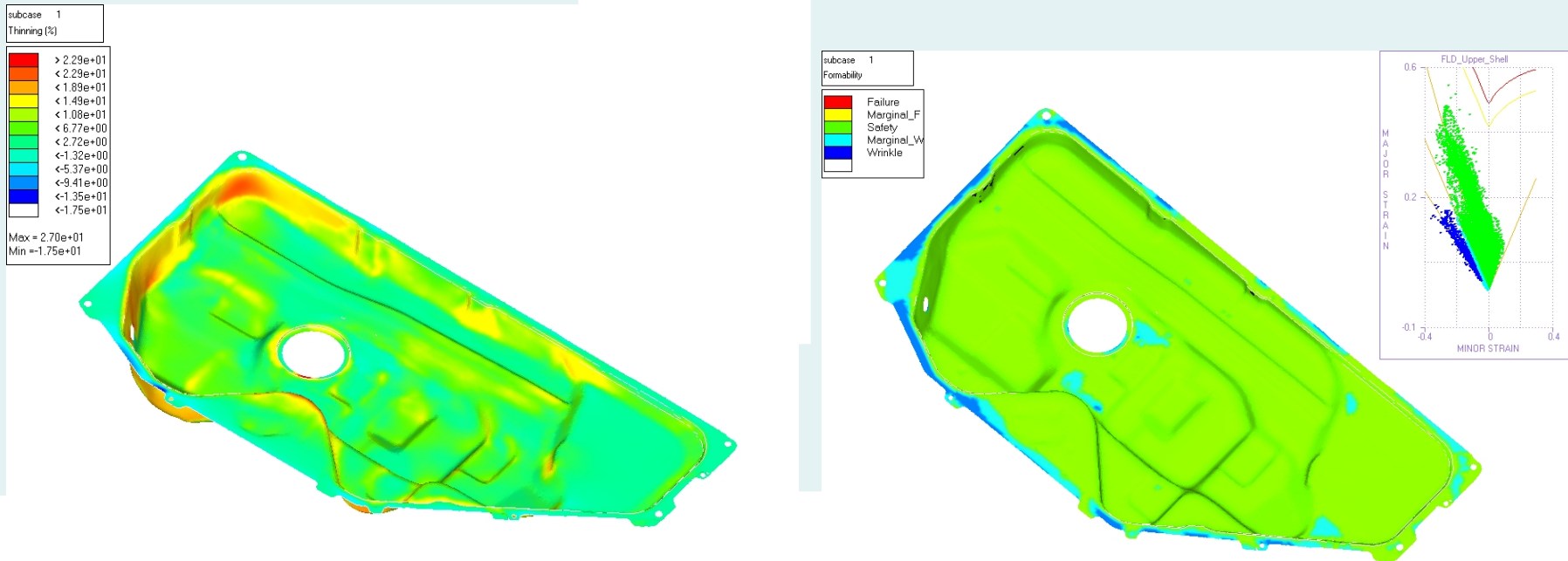


Fatigue Life of Lexus Tank

Test Result by GM



## ❑ Formability Results (one step forming) - Upper Shell - LEXUS

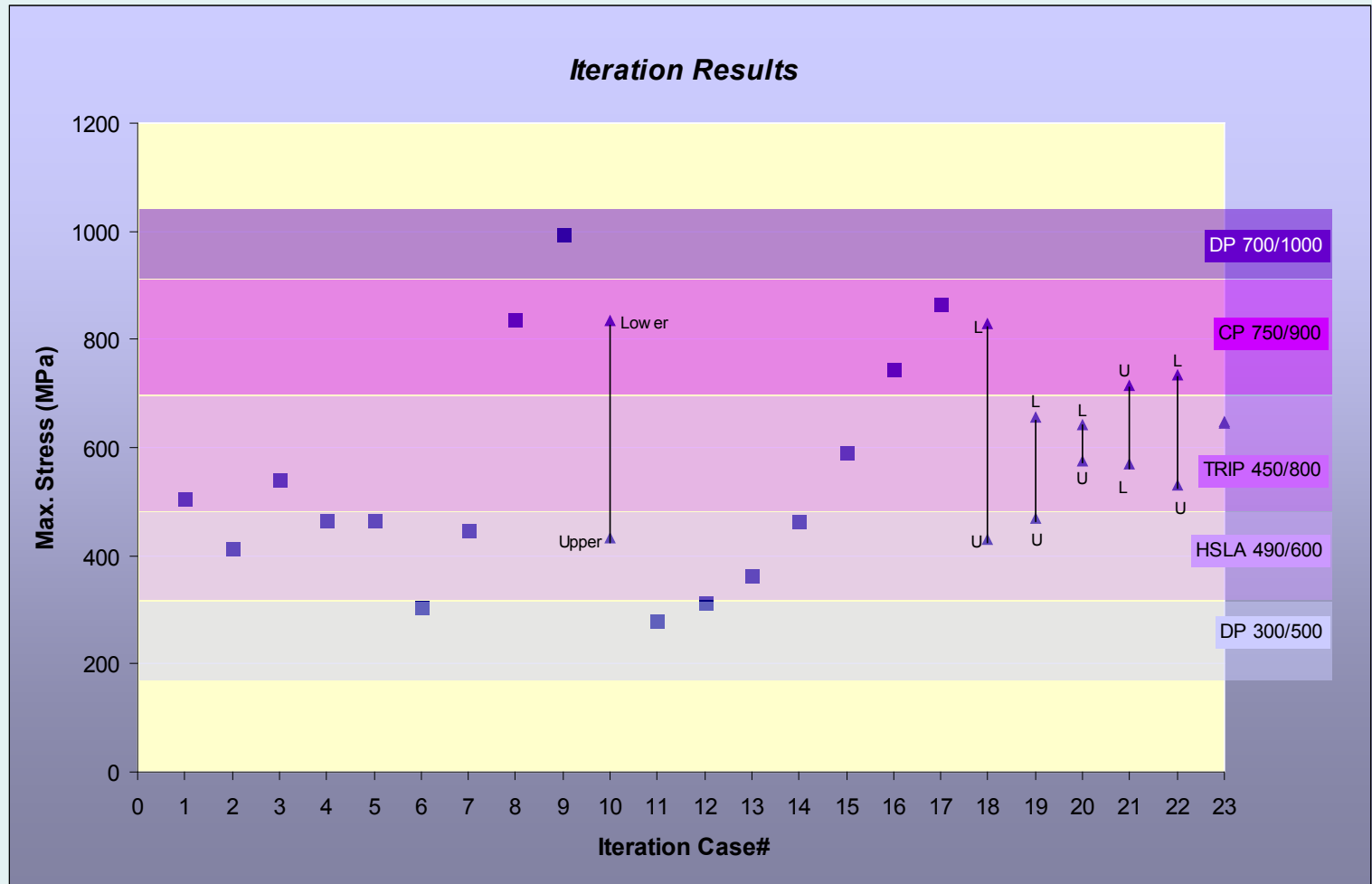


Max. Thinning 27%

The physical tank thicknesses have been measured and correlate with the forming simulation

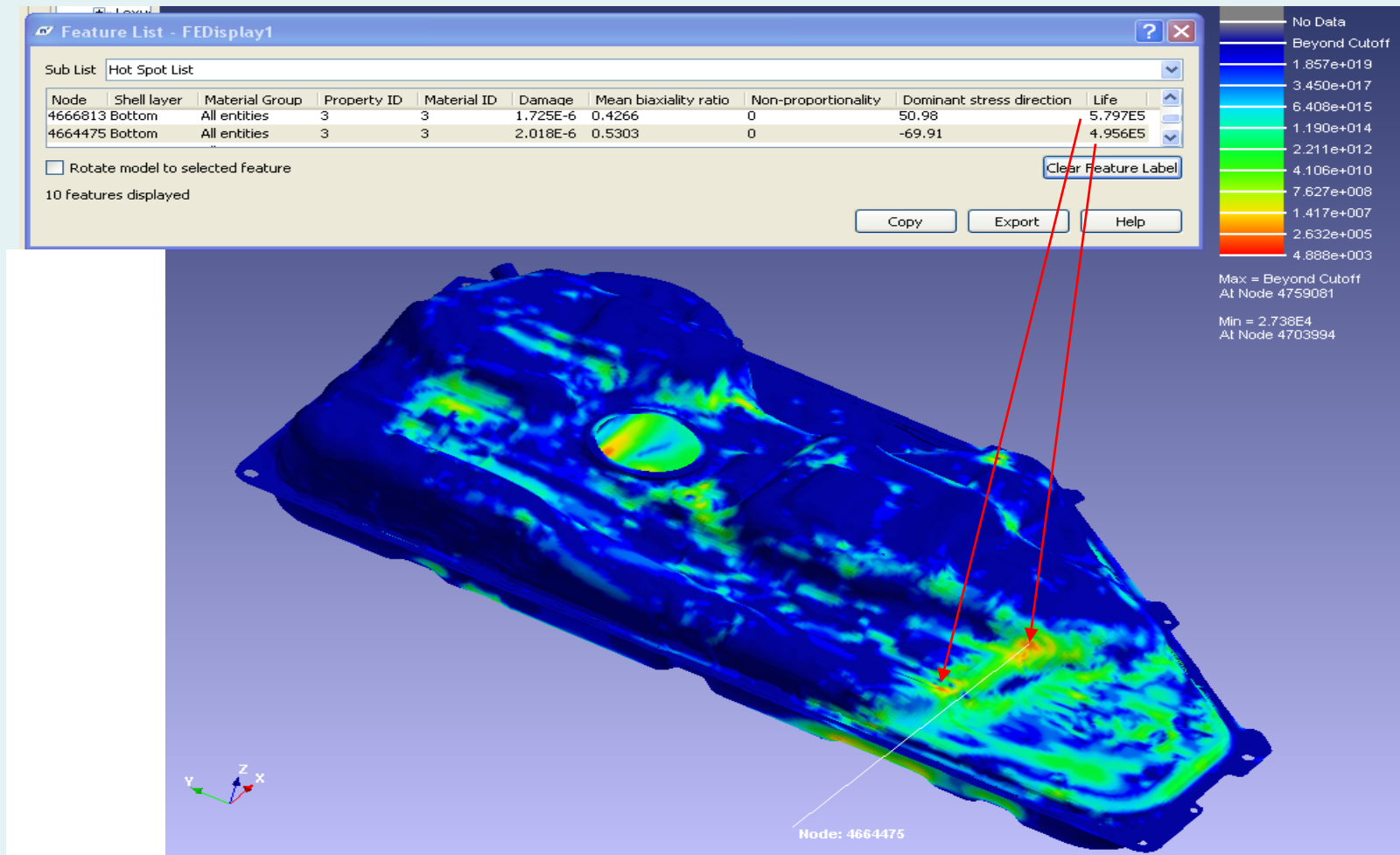
Formability Results  
No Failures

## □ Parametric Analysis Results Summary





## □ Fatigue Life Analysis Results – Case#22 (Iteration# 15)



- Analyzed fatigue life 27,380 Cycles (minimum) >> 18,000 Cycles (targeted)