Hydrogen Supply: Cost Estimate for Hydrogen Pathways—Scoping Analysis

January 22, 2002—July 22, 2002

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Table of Contents

Table of Contents	i
Acronyms and Abbreviations	. ii
Introduction	. 1
Summary	. 3
Consistency and Transparency	. 5
Ease of Comparison	
Flexibility Improvements	. 6
Potential Improvements for Hydrogen Economics	. 6
Central Plant Hydrogen Production	. 6
Hydrogen Distribution	. 6
Hydrogen Fueling Stations	. 7
Hydrogen Economic Module Basis	
Hydrogen Production Technology	. 8
Reforming	. 9
Gasification	. 9
Electrolysis	10
Central Plant Hydrogen Production	11
Hydrogen Handling and Storage	13
Hydrogen Liquefaction	
Gaseous Hydrogen Compression	14
Hydrogen Storage	14
Hydrogen Distribution	15
Road Delivery (Tanker Trucks and Tube Trailers)	16
Pipeline Delivery	17
Hydrogen Fueling Station	17
Liquid Hydrogen Based Fueling	
Gaseous Hydrogen Based Fueling	19
Forecourt Hydrogen Production	19
Sensitivity	21
Special Acknowledgement	22
References	22
General	22
Gasification	
Large Steam Methane Reforming	23
Small Steam Methane Reforming	26
Electrolysis	26
Pipeline	27
High Pressure Storage	
High Pressure Compression	27
Delivery	27

Acronyms and Abbreviations

ASU	air separation unit
ATR	autothermal reforming
BDT	bone-dry ton
Btu	British thermal unit
EOR	enhanced oil recovery
FC	fuel cell
gal	gallon
GPS	global positioning system
H2	molecular hydrogen
ICE	internal combustion engine
IHIG	International Hydrogen Infrastructure Group
kg	kilogram
kg/d	kilograms per day
O&M	operating and maintenance
PO	partial oxidation
PSA	pressure swing adsorption
psig	pounds per square inch gauge
SMR	steam methane reforming

Introduction

The International Hydrogen Infrastructure Group (IHIG) requested a comparative "scoping" economic analysis of 19 pathways for producing, handling, distributing, and dispensing hydrogen for fuel cell (FC) vehicle applications. Of the 19 pathways shown in Table 1, 15 were designated for large-scale central plants and the remaining four pathways focus on smaller modular units suitable for forecourt (fueling station) on-site production. Production capacity is the major determinant for these two pathways. The central hydrogen conversion plant is sized to supply regional hydrogen markets, whereas the forecourt capacity is sized to meet local service station demand.

Original Feedstocks	Revised Feedstocks	Location of H ₂ Production
Biomass	Biomass	Central
Natural gas	Natural gas	Central and forecourt
Water	Water	Central and forecourt
Coal	Coal	Central
Petroleum coke	Petroleum coke	Central
Methanol	Methanol	Forecourt
Gasoline	Gasoline	Forecourt
H ₂ from ethylene or refinery	Residue/pitch	Central

Table 1 IHIG Hydrogen Pathways

The by-product source of hydrogen defined by IHIG in the original proposal has been replaced with residue/pitch. For all practical purposes, by-product hydrogen from ethylene plants and naphtha reforming is fully utilized by petrochemical and refining processes. In the future, the demand for hydrogen will increase at a higher rate than the growth of by-product production. Since the mid-1990s, the demand for hydrogen in refineries has been growing at an annual rate of 5%-10%. More hydroprocessing treatment of feedstocks and products are required to meet increasingly stringent clean fuel specifications for gasoline and diesel. Meanwhile, by-product hydrogen production has been declining during the same period. Specifically:

- Hydrogen yields from naphtha reforming have been declining as refineries adjust their operational severity downward to reduce the aromatic content in the reformat; a major gasoline blending stock.
- Most of the new ethylene capacities are based on less hydrogen-rich liquid feedstocks such as naphtha.

Hydrogen could be extracted from the eight feedstocks listed in Table 3 using the following five commercially proven technologies.

Steam methane reforming Methanol reforming Gasoline reforming Gasification/partial oxidation Electrolysis Table 2 shows feedstocks, associated conversion technologies, and distribution methods for the 14 central facility pathways. For central production plants, there are several intermediate steps before the hydrogen could be dispensed into FC vehicles. The purified hydrogen has to be either liquefied or compressed before it can be transported by cryogenic trucks, pipelines, or tube trailers. In the base case, the delivered hydrogen has to be pressurized to 400 atmospheres (6,000 psig) to be dispensed into FC vehicles outfitted with 340 atmospheres (5,000 psig) on-board cylinders.

Table 5 shows four forecourt hydrogen production pathways. On-site production eliminates the need for intermediate handling steps and distribution infrastructure.

Case No.	Feedstock	Conversion Process	Method of Distribution
C4	Natural gas	Steam methane reforming	Liquid H ₂ via truck
C11	Natural gas	Steam methane reforming	Gaseous H ₂ via tube trailer
C3	Natural gas	Steam methane reforming	Gaseous H ₂ via Pipeline
C9	Coal	Partial oxidation	Liquid H_2 via truck
C15	Coal	Partial oxidation	Gaseous H ₂ via tube trailer
C8	Coal	Partial oxidation	Gaseous H ₂ via Pipeline
C6	Water	Electrolysis	Liquid H ₂ via truck
C12	Water	Electrolysis	Gaseous H ₂ via tube trailer
C5	Water	Electrolysis	Gaseous H ₂ via Pipeline
C2	Biomass	Gasification	Liquid H ₂ via truck
C10	Biomass	Gasification	Gaseous H ₂ via tube trailer
C1	Biomass	Gasification	Gaseous H ₂ via Pipeline
C7	Petroleum coke	Gasification	Gaseous H ₂ via Pipeline
C13	Residue	Gasification	Gaseous H ₂ via Pipeline

Table 2Central Hydrogen Production Pathways

Table 3Forecourt Hydrogen Production Pathways

Case No.	Feedstock	Conversion Process
F1	Methanol	Methanol reforming
F2	Natural gas	Steam methane reforming
F3	Gasoline	Gasoline reforming
F4	Water	Electrolysis

Summary

SFA Pacific has developed consistent and transparent infrastructure cost modules for producing, handling, distributing, and dispensing hydrogen from a central plant and forecourt (fueling station) on-site facility for fuel cell (FC) vehicle applications. The investment and operating costs are based on SFA Pacific's extensive database and verified with three industrial gas companies (Air Products, BOC, and Praxair) and hydrogen equipment vendors.

The SFA Pacific cost module worksheets allow users to provide alternative inputs for all the cells that are highlighted in light gray boxes. Flexibilities are provided for assumptions that include production capacity, capital costs, capital build-up, fixed costs, variable costs, distribution distance, carrying capacity, fueling station sales volume, dispensing capacity, and others. Figure 1 compares the costs of hydrogen produced from a 150,000 kg/d central plant based on natural gas, coal, biomass, and water, delivered to forecourt by either liquid truck, gas tube trailer, or pipeline with a 470 kg/d forecourt production based on natural gas and water. The base case capacity was chosen at the beginning of the project to represent infrastructure requirements for the New York/New Jersey region.



Figure 1 Central Plant and Forecourt Hydrogen Costs

Generally, the higher costs of commercial rates for feedstock and utilities coupled with lower operating rates lead to higher hydrogen costs from forecourt production. Regardless of the source for hydrogen, the above comparison shows the following trends for central plant production.

- The energy intensive liquefaction operation leads to the highest production cost, but incurs the lowest transportation cost
- The high capital investment required for pipeline construction makes it the most expensive delivery method
- The cost for gas tube trailer delivery is also high, slightly less than the pipeline cost, because the low hydrogen density limits each load to about 300 kg.

Other findings from this evaluation could facilitate the formulation of hydrogen infrastructure development strategies from the initial introductory period through ramp-up to a fully developed market.

- Advantages of economy of scale and lower industrial rates for feedstock and power compensate for the additional handling and delivery costs needed for distributing hydrogen to fueling stations from central plants.
- Hydrocarbon feedstock-based pathways have economic advantages in both investment and operating costs over renewable feedstocks such as water and biomass.
- Economics of forecourt production suffer from low utilization rates and higher commercial rates for feedstock and electricity. For natural gas based feedstock, the hydrogen costs from forecourt production are comparable to those of hydrogen produced at a central plant and distributed to fueling stations by tube trailer, and are 20% higher than the liquid tanker truck delivery pathway.
- To meet the increasing demand during the ramp-up period, a "mix and match" of the three delivery systems (tube trailers, tanker trucks, and pipelines) is a likely scenario. Tube trailers, which haul smaller quantities of hydrogen, are probably best suited for the introductory period. As the demand grows, cryogenic tanker trucks could serve larger markets located further from the central plant. As the ramp-up continues, additional production trains would be added to the existing central plants, and ultimately a few strategically placed hydrogen pipelines could connect these plants to selected stations and distribution points.
- On-board liquid (methanol or naphtha) reforming or direct FC technology could leverage the existing liquids infrastructure. It would eliminate costly hydrogen delivery and dispensing infrastructures, as well as avoid regulatory issues regarding hydrogen handling.

Consistency and Transparency

The SFA Pacific cost modules are "living documents." The flexible inputs allow revisions for infrastructure adjustments and future improved capital and operating cost bases.

Ease of Comparison

Table 4 shows that, at comparable capacity, SFA Pacific's models yield cost estimates similar to those developed by Air Products for the Hydrogen Infrastructure Report [1] sponsored by Ford and the U.S. Department of Energy (DOE). Key findings from the Air Products evaluation were also published in the International Journal of Hydrogen Energy [2].

Table 4 Comparison of Hydrogen Costs Developed by SFA Pacific and Air Products

			Investmen	nt (\$million)	Hydrogen	Cost (\$/kg)
	H ₂ Capacity		SFA	Air	SFA	Air
Feedstock	(t/d)	H ₂ Source	Pacific	Products	Pacific	Products
Natural Gas	27	Liquid	102	63	4.34	3.35
Natural Gas	27	Pipeline ^a	71	82	3.08	2.91
Natural Gas	2.7	Forecourt	6.2	9.6	3.30	3.57
Methanol	2.7	Forecourt	6.0	6.8	3.46	3.76

^a To be consistent with the estimates from Air Products, SFA Pacific excluded fueling state investment and operating costs in this comparison.

Source: SFA Pacific, Inc.

The differences between SFA Pacific and Air Products costs for hydrogen delivered by cryogenic tanker trucks could be attributed to a large discrepancy shown in the capital investment for fueling station infrastructure (Table 5).

Table 5Capital Investment Allocations for Methane Based Liquefied Hydrogen
(\$Million)

	SFA Pacific	Air Products
Steam Methane Reformer	21	19
Liquefier	44	41
Tanker Trucks	7	n/a
Fueling Stations	30	3
Total	102	63

Flexibility Improvements

Currently, the central plant storage matches the form of hydrogen for a designated delivery option. A separate and independent module for handling and storing purified gaseous hydrogen would increase the model's flexibility in evaluating mix-match storage and delivery options to meet the rising demand during the ramp-up period.

Potential Improvements for Hydrogen Economics

All hydrogen pathways were developed based on conventional technology and infrastructure deployment. However, new technologies and novel operating options could potentially reduce the cost of hydrogen, thus making it a more attractive fuel option.

Central Plant Hydrogen Production

- Polygeneration (a term referring to the co-production of electric power for sale to the grid) would improve the hydrogen economics. Central gasification units have advantages of economy of scale and lower marginal operating and maintenance costs compared with the same option for forecourt production.
- Installing a liquefaction unit would lower the central storage costs and provide greater flexibility. It is more practical to store large amounts of liquid than gaseous hydrogen. More storage capacity would allow the hydrogen plant to operate at a higher utilization rate. If the hydrogen is to be transported either by pipelines or tube trailers, a slipstream from the boil-off could supply the gaseous hydrogen for distribution.
- Using a hybrid technology or heat-exchange design improves steam reforming operation and increases conversion. Autothermal reforming (ATR), which combines partial oxidation with reforming, improves heat and temperature management. Instead of a single-step process, ATR is a two-step process in hydrogen plants—the partially reformed gases from the primary reformer feed a secondary oxygen blown reformer with additional methane. The exothermic heat release from the oxidation reaction supplies the endothermic heat needs of the reforming reactions. Including reforming reactions allows co-feeding of CO₂ or steam to achieve a wider range of H₂/CO ratios in the syngas.
- Capturing CO₂ for enhanced oil recovery (EOR) or for future CO₂ trading could improve the economics of hydrogen production if CO₂ mitigation is mandated and supported by trading.

Hydrogen Distribution

- Hydrogen pipeline costs could be reduced by placing the pipelines in sewers, securing utility status, or converting existing natural gas pipelines to carry a mixture of hydrogen/natural gas (town gas).
- Using ultra high-pressure (10,000 psig) tube trailers could potentially triple the carrying load.

Hydrogen Fueling Stations

The infrastructure investment for fueling stations could reach 60% of the total capital costs. By using the global positioning system (GPS), which has gained wide consumer acceptance, we could significantly lower the traditional strategy of 25% urban and 50% rural area hydrogen service station penetration. The GPS system would enable FC vehicle drivers to locate fueling stations more efficiently. Additional strategies for reducing infrastructure investment include:

- Using ultra high-pressure (about 800 to 900 atmospheres) vessels to increase forecourt hydrogen storage capacity. It may be possible to have large vertical vessels underground or to use them as canopy supports to minimize land usage.
- Replacing on-board hydrogen cylinders with pre-filled ones instead of the traditional fillup option could eliminate fueling station infrastructure investment.
- Dispensing liquid hydrogen into FC vehicles (an idea brought up by BMW during the April 4, 2002 meeting) could eliminate the need for expensive compression and storage costs at forecourts. However, an innovative on-board liquid hydrogen storage design is needed to prevent boil-off when the FC vehicle is not in use.

Hydrogen Economic Module Basis

SFA Pacific developed simplified energy, material balance, capital investment, and operating costs to achieve transparency and consistency. Cost estimates are presented in five workbooks (Appendix A) include central plant, distribution, fueling station, forecourt, and overall summary. Each worksheet includes a simplified block flow diagram and major line items for capital and operating costs. Capital investment and operating costs are based on an extensive proprietary SFA Pacific database, which has been verified with industrial gas producers and hydrogen equipment vendors. The database contains reliable data for large and small-scale steam methane reforming and gasification units. Although SFA has confirmed the estimates for electrolyzers with industrial gas companies, they could probably be improved further. There are many advocates and manufacturers giving quotes that are significantly lower than those used in this analysis. Some of these discrepancies could be attributed to the manufacturers' exclusion of a processing step to remove contaminants, and others could result from optimistic estimates based on projected future breakthroughs.

The investment and operating costs modules are developed based upon commonly accepted cost estimating practices. Capital build-up is based on percentages of battery limit process unit costs. Variable non-fuel and fixed operating and maintenance (O&M) costs are estimated based on percentages of total capital per year. Capital charges are also estimated as percentages of total capital per year assumptions for capital investment. Operating costs (variable and fixed) and capital charges are listed in Table 6. For ease of comparison, all unit costs are shown in \$/million Btu, \$/1,000 scf, and \$/kg (\$/gal gasoline energy equivalent).

The capital cost estimates are based on U.S. Gulf Coast costs. A location factor adjustment is provided to facilitate the evaluation of costs for three targeted states: high cost urban areas such as New York/New Jersey and California and low-cost lower population density Texas. Two provisions are made at forecourt/fueling stations to allow "what-if" analysis: (1) road tax input accommodates possible government subsidies to jump-start the hydrogen economy and (2) gas station mark-ups permit incentives for lower revenue during initial stages of low hydrogen demand.

Capital Build-up	% of Process Unit	Typical Range
General Facilities	20	20-40 ^a
Engineering, Permitting, and	15	10-20
Startup		
Contingencies	10	10-20
Working Capital, Land, and	7	5-10
Others		
Operating Costs Build-up	%/yr of Capital	Typical Range
Variable Non-Fuel O&M	1.0	0.5-0.5
Fixed O&M	5.0	4-7
Capital Charges	18.0	20-25 for refiners
		14-20 for utilities

Table 6Capital and Operating Costs Assumptions

^a 20%-40% for steam methane reformer and an additional 10% for gasification.

Source: SFA Pacific, Inc.

Hydrogen Production Technology

Three distinct types of commercially proven technologies were selected to extract hydrogen from the eight feedstocks. Fundamental principles for each technology apply regardless of the unit size. A brief technical review of reforming, gasification, and electrolysis describes the major processing steps required for each hydrogen production pathway.

- Reforming is the technology of choice for converting gaseous and light liquid hydrocarbons
- Gasification or partial oxidation (PO) is more flexible than reforming—it could process a range of gaseous, liquid, and solid feedstocks.
- Electrolysis splits hydrogen from water.

Reforming

Steam methane reforming (SMR), methanol reforming, and gasoline reforming are based on the same fundamental principles with modified operating conditions depending on the hydrogen-to-carbon ratio of the feedstock.

SMR is an endothermic reaction conducted under high severity; the typical operating conditions are 30 atmospheres and temperatures exceeding 870°C (1,600°F). Conventional SMR is a fired heater filled with multiple tubes to ensure uniform heat transfer.

 $CH_4 + H_2O \iff 3H_2 + CO$ (1)

Typically the feedstock is pretreated to remove sulfur, a poison which deactives nickel reforming catalysts. Guard beds filled with zinc oxide or activated carbon are used to pretreat natural gas and hydrodesulfurization is used for liquid hydrocarbons. Commercially, the steam to carbon ratio is between 2 and 3. Higher stoichiometric amounts of steam promote higher conversion rates and minimize thermal cracking and coke formation.

Because of the high operating temperatures, a considerable amount of heat is available for recovery from both the reformer exit gas and from the furnace flue gas. A portion of this heat is used to preheat the feed to the reformer and to generate the steam for the reformer. Additional heat is available to produce steam for export or to preheat the combustion air.

Methane reforming produces a synthesis gas (syngas) with a $3:1 \text{ H}_2/\text{CO}$ ratio. The H₂/CO ratio decreases to 2:1 for less hydrogen-rich feedstocks such as light naphtha. The addition of a CO shift reactor could further increase hydrogen yield from SMR according to Equation 2.

$$CO + H_2O \implies H_2 + CO_2 \tag{2}$$

The shift conversion may be conducted in either one or two stages operating at three temperature levels. High temperature (660°F or 350°C) shift utilizes an iron-based catalyst, whereas medium and low (400°F or 205°C) temperature shifts use a copper based catalyst. Assuming 76% SMR efficiency coupled with CO shift, the hydrogen yield from methane on a volume is 2.4:1.

There are two options for purifying crude hydrogen. Most of the modern plants use multi-bed pressure swing adsorption (PSA) to remove water, methane, CO_2 , N_2 , and CO from the shift reactor to produce a high purity product (99.99%+). Alternatively, CO_2 could be removed by chemical absorption followed by methanation to convert residual CO_2 in the syngas.

Gasification

Traditionally, gasification is used to produce syngas from residual oil and coal. More recently, it has been extended to process petroleum coke. Although not as economical as SMR, there are a number of natural gas-based gasifiers. Other feedstocks include refinery wastes, biomass, and municipal solid waste. Gasification of 100% biomass feedstock is the most speculative technology used in this project. Total biomass based gasification has not been practiced

commercially. However, a 25/75 biomass/coal has been commercially demonstrated by Shell at their Buggenm refinery. The biomass is dried chicken waste.

In addition to the primary reaction shown by Equation 3, a variety of secondary reactions such as hydrocracking, steam gasification, hydrocarbon reforming, and water-gas shift reactions also take place.

$$C_{a}H_{b} + a/2O_{2} \implies b/2H_{2} + aCO$$
 (3)

For liquid and solids gasification, the feedstocks react with oxygen or air under severity operating conditions (1,150°C -1,425°C or 2,100°F -2,600°F at 400-1,200 psig). In hydrogen production plant, there is an air separation unit (ASU) upstream of the gasifier. Using oxygen rather than air avoids downstream nitrogen removal steps.

In some designs, the gasifiers are injected with steam to moderate operating temperatures and to suppress carbon formation. The hot syngas could be cooled directly with a water quench at the bottom of the gasifier or indirectly in a waste heat exchanger (often referred to as a syngas cooler) or a combination of the two. Facilitating the CO shift reaction, a direct quench design maximizes hydrogen production. The acid gas (H₂S and CO₂) produced has to be removed from the hydrogen stream before it enters the purification unit.

When gasifying liquids, it is necessary to remove and recover soot (i.e., unconverted feed carbon), ash, and any metals (typically vanadium and nickel) that are present in the feed. The recovered soot can be recycled to the gasifier, although such recycling may be limited when the levels of ash and metals in the feed are high. Additional feed preparation and handling steps beyond the basic gasification process are needed for coal, petroleum coke, and other solids such as biomass.

Electrolysis

Electrolysis is decomposition of water into hydrogen and oxygen, as shown in Equation 4.

 $H_2O + electricity \implies H_2 + \frac{1}{2} O$ (4)

Alkaline water electrolysis is the most common technology used in larger production capacity units (0.2 kg/day). In an alkaline electrolyzer, the electrolyte is a concentrated solution of KOH in water, and charge transport is through the diffusion of OH⁻ ions from cathode to anode. Hydrogen is produced at the cathode with almost 100% purity at low pressures. Oxygen and water by-products have to be removed before dispensing.

Electrolysis is an energy intensive process. The power consumption at 100% efficiency is about 40 kWh/kg hydrogen; however, in practice it is closer to 50 kWh/kg. Since electrolysis units operate at relatively low pressures (10 atmospheres), higher compression is needed to distribute the hydrogen by pipelines or tube trailers compared to other hydrogen production technologies.

Central Plant Hydrogen Production

Figure 2 shows that each central production hydrogen pathway consists of four steps: hydrogen production, handling, distribution, and dispensing.



Table 7 lists feedstocks and utility costs used in this analysis. Central plant hydrogen production benefits from lower industrial rates, whereas the fueling stations are charged with the higher commercial rates.

Table 7 Central Hydrogen Production Feedstock and Utility Costs

- Natural gas (industrial) Electricity (industrial) Electricity (commercial) Biomass Coal Petroleum coke Residue (Pitch)
- Unit Cost \$3.5/MMBtu HHV \$0.045/kW \$0.070/kW \$57/bone dry ton \$1.1/MMBtu dry HHV \$0.2/MMBtu dry HHV \$1.5/MMBtu dry HHV

Source: Annual Energy Outlook 2002 Reference Case Tables, EIA.

The design production capacity for each central plant ranges from 20,000 kg/d to 200,000 kg/d hydrogen with a 90% utilization rate. An arbitrary design capacity of 150,000 kg/d has been chosen for discussion purposes. Table 8 shows that the cost of hydrogen for hydrocarbon based feedstock is lower than renewables. For each feedstock, the cost of hydrogen via cryogenic liquid tanker truck delivery pathway is 10%-25% lower than by tube trailer and 15%-30% less than by pipeline. Since the cost of liquid delivery is relatively small (less than 5%), the costs for hydrocarbon based feedstock, production, and fueling account for close to 67% and 33% of the total hydrogen costs, respectively. For renewables (biomass and water), the production cost accounts for 70%-80% of the total hydrogen cost. With high investment costs, the tube trailer and pipeline delivery account for 50% of the total cost.

Delivery Pathway	Liquid Tanker Truck, \$/kg	Gas Tube Trailer, \$/kg	Pipeline, \$/kg
Natural Gas Production Delivery Dispensing	2.21 0.18 <u>1.27</u>	1.30 2.09 <u>1.00</u> 4.20	1.00 2.94 <u>1.07</u> 5.00
Total	3.66	4.39	5.00
Coal Production Delivery Dispensing Total	3.06 0.18 <u>1.27</u> 4.51	2.09 2.09 <u>1.00</u> 5.18	1.62 2.94 <u>1.07</u> 5.62
Biomass Production Delivery Dispensing Total	3.53 0.18 <u>1.27</u> 4.98	2.69 2.09 <u>1.00</u> 5.77	2.29 2.94 <u>1.07</u> 6.29
Water Production Delivery Dispensing Total	6.17 0.18 <u>1.27</u> 7.62	5.30 2.09 <u>1.00</u> 8.39	5.13 2.94 <u>1.07</u> 9.13
Petroleum Coke Production Delivery Dispensing Total			1.35 2.94 <u>1.07</u> 5.35
Residue Production Delivery Dispensing Total			1.27 2.94 <u>1.07</u> 5.27

Table 8Summary of Central Plant Based Hydrogen Costs(1,000 kg/d hydrogen)

Numerous studies have been conducted to evaluate the economics of using renewable feedstocks to produce energy and fuels. Waste biomass and co-product biomass are very seasonal and have high moisture content, except for field-dried crop residues. As a result, they require more expensive storage and extensive drying before gasification. Furthermore, very limited supplies are available and quantities are not large or consistent enough to make them a viable feedstock for large-scale hydrogen production. Cultivated biomass is the only guaranteed source of biomass feedstock, and as a crop, the yield is relatively low (10 ton/hectare). As a result, large land mass is required to provide a steady supply of feedstock. This dedicated renewable biomass comes at a cost of \$57/bone dry ton (BDT), which includes \$500/hectare/yr and \$7/BTD delivery cost. However, available biomass could supplement other solid feeds to maximize the utilization of the gasification unit. Finally, biomass gasification processes are not effective for pure hydrogen production due to their air-blown operations or a product gas that is high in methane and requires additional reforming to produce hydrogen.

Water is another feedstock commonly referred to as a renewable energy source. Although hydrogen occurs naturally in water, the extraction costs are still considerably higher than conventional hydrocarbon based energy sources.

Hydrogen Handling and Storage

Purified hydrogen has to be either liquefied for cryogenic tanker trucks or compressed for pipeline or tube trailer delivery to fueling stations.

Hydrogen Liquefaction

Liquefaction of hydrogen is a capital and energy intensive option. The battery limit investment is \$700/kg/d for a 100,000 kg/d hydrogen plant, and compressors and brazed aluminum heat exchanger cold boxes account for most of the cost. The total installed capital cost for the liquefier, excluding land and working capital is \$1,015 kg/d, which agrees well with the \$1,125 estimate from Air Products. Multi-stage compression consumes about 10-13 kWh/kg hydrogen.

Gaseous crude hydrogen from the PSA unit undergoes multiple stages of compression and cooling. Nitrogen is used as the refrigerant to about 195°C (-320°F). Ambient hydrogen is a mixture 75% ortho- and 25% para-hydrogen, whereas liquid hydrogen is almost 100% para-hydrogen. Unless ortho-hydrogen is catalytically converted to para-hydrogen before the hydrogen is liquefied, the heat of reaction from the exothermic conversion of ortho-hydrogen to para-hydrogen, which doubles the latent heat of vaporization, would cause excessive boil-off during storage. The liquefier feed from the PSA unit mixes with the compressed hydrogen and enters a series of ortho/para-hydrogen converters before entering the cold end of the liquefier. Further cooling to about -250°C (-420°F) is accomplished in a vacuum cold box with brazed aluminum flat plate cores. The remaining 20% ortho-hydrogen is converted to achieve 99%+ para-hydrogen in this section.

Gaseous Hydrogen Compression

Gaseous hydrogen compressors are major contributors to capital and operating costs. To deliver high-pressure hydrogen, 3-5 stages of compression are required because water-cooled positive-displacement compressors could only achieve 3 compression ratios per stage. Compression requirements depend on the hydrogen production technology and the delivery requirements. For pipeline delivery, the gas is compressed to 75 atmospheres for 30 atmospheres delivery. Higher pressures are used to compensate for frictional loss in pipelines without booster compressors along the pipeline system. The gaseous hydrogen has to be compressed to 215 atmospheres to fill tube trailers. In this study, the unit capital cost is between \$2,000/kW and \$3,000/kW and the power requirement ranged from 0.5 kW/kg/hr to 2.0 kW/kg/hr.

Hydrogen Storage

On-site storage allows continuous hydrogen plant operation in order to achieve higher utilization rates. It is more practical to store large amounts of hydrogen as liquid. At less than \$5/gallon (physical volume) capital cost, liquid hydrogen storage is relatively inexpensive compared to compressed gaseous hydrogen. Table 9 shows that hydrogen is the lowest energy density fuel on earth. It would take 3.73 gallons of liquid hydrogen to provide equivalent energy of one gallon of gasoline. Gaseous hydrogen has to be pressurized for storage. At the base case pressure of 400 atmospheres (6,000 psig), it would require about 8 gallons of gaseous hydrogen to have the same energy content as one gallon of gasoline. The higher the gas pressure, the lower the storage volume needed. However, the tube becomes weight limited as the thickness of the steel wall increases to prevent embrittlement (cracking caused by hydrogen migrating into the metal).

Table 9 Density of Vehicle Fuel

Fuel Type	Density (kg/l)
Compressed Hydrogen	0.016
Gasoline	0.8
Methanol	0.72

Figure 3 shows how the cost of gaseous storage tubes increases with pressure. The cost could increase from less than \$400/kg hydrogen at 140 atmospheres to \$2100/kg hydrogen at 540 atmospheres. Companies such as Lincoln Composites and Quantum Technologies are developing new synthetic materials to withstand high pressures at a larger range of temperatures.



Source: SFA Pacific, Inc.

Hydrogen Distribution

This study includes three hydrogen distribution pathways: cryogenic liquid trucks, compressed tube trailers, and gaseous pipelines. Figure 4 shows that each option has a distinct range of practical application.



Figure 4 Hydrogen Distribution Options

Source: Air Products.

A combination of these three options could be used during various stages of hydrogen fuel market development.

- Tube trailers could be used during the initial introductory period because the demand probably will be relatively small and it would avoid the boil-off incurred with liquid hydrogen storage.
- Cryogenic tanker trucks could haul larger quantities than tube trailers to meet the demands of growing markets.
- Pipelines could be strategically placed to transport hydrogen to high demand areas as more production capacities are placed on-line.

Road Delivery (Tanker Trucks and Tube Trailers)

Based on the assumptions shown in Table 10, the cost of liquid tanker truck delivery is about 10% of tube trailer delivery (\$0.18/kg vs. \$2.09/kg).

	Cryogenic Truck	Tube Trailer
Load, kg	4,000	300
Net delivery, kg	4,000	250
Load/unload, hr/trip	4	2
Boil-off rate, %/day	0.3	na
Truck utilization rate, %	80	80
Truck/tube, \$/module	450,000	100,000
Undercarriage, \$	60,000	60,000
Cab, \$	90,000	90,000

Table 10Road Hydrogen Delivery Assumptions

Source: SFA Pacific, Inc.

Delivery by cryogenic liquid hydrogen tankers is the most economical pathway for medium market penetration. They could transport relatively large amounts of hydrogen and reach markets located throughout large geographic areas. Tube trailers are better suited for relatively small market demand and the higher costs of delivery could compensate for losses due to liquid boil-off during storage. However, high-pressure tube trailers are limited to meeting small hydrogen demands. Typically, the tube-to-hydrogen weight ratio is about 100-150:1. A combination of low gaseous hydrogen density and the weight of thick wall, high quality steel tubes (80,000 pounds or 36,000 kilograms) limit each load to 300 kilograms of hydrogen. In reality, only 75%-85% of each load is dispensable, depending on the dispensing compressor configuration. Unlike tanker trucks that discharge their load, the tube and undercarriage are disconnected from the cab and left at the fueling station. Tube trailers are used not only as transport container, but also as on-site

storage. As a result, the total number of tubes provided equals the number of tubes left at the fueling stations and those at the central plants to be picked up by the returning cabs.

Liquid hydrogen flows into and out of the tanker truck by gravity and it takes about two hours to load and unload the contents. SFA Pacific estimates the physical delivery distance for truck/trailers is 40% longer than the assumed average distance of 150 kilometers between the central facility and fueling stations.

Pipeline Delivery

Pipelines are most effective for handling large flows. They are best suited for short distance delivery because pipelines are capital intensive (\$0.5 to \$1.5 million/mile). Much of the cost is associated with acquiring right-of-way. Currently, there are 10,000 miles of hydrogen pipelines in the world. At 250 miles, the longest hydrogen pipeline connects Antwerp and Normandy.

Operating costs for pipelines are relatively low. To deliver hydrogen to the fueling stations at 30 atmospheres, the pressure drop could be compensated with either booster compressors or by compressing the hydrogen at the central plant. In this study, the pipeline investment is based on four pipelines radiating from the central plant.

Hydrogen Fueling Station

The conceptual hydrogen fueling station for this study is designed based on equivalent conventional internal combustion engine (ICE) requirements as shown in Table 11.

Table 11 Assumed FC Vehicle Requirements

	ICE-gasoline	FC requirement
Vehicle mileage	23 km/liter	23 km/liter
Vehicle annual mileage	12,000 miles	218 kg H ₂ or 12,000 miles
Fuel sales per station	150,000 gal/month	10,000 kg H_2 /monthor 10,000 gal gasoline equivalent

Source: SFA Pacific, Inc.

Table 12 shows that the key fueling station design parameters. At a 70% operating rate, each service station dispenses about 329 kg/d, assuming a daily average of 4.0 kg per fill-up and five fill-ups an hour. Each fueling hose is sized to meet daily peak demand.

Table 12 Fueling Dispenser Design Basis

Design capacity	470 kg/d
Operating rate	70%
Operating capacity	329 kg/d
Number of dispenser	2
Average fill-up rate	4 kg
Average number of fill-up	5 /hr
Peak fill-up rate (3 times daily average)	48 kg/hr
Dispensing pressure, psig	6,000

Source: SFA Pacific, Inc.

Sizing hydrogen dispensers is no different than sizing gasoline dispensers; they must be designed to meet peak demands. As shown in Figure 5, the peak demand could be triple that of the daily average.



Figure 5 Fueling Station Dispensing Utilization Profile

Source: Praxair.

This study developed analyses for two types of high-pressure gaseous fueling stations: one to handle liquid based hydrogen and the other for gaseous hydrogen. Components handling compressed hydrogen (6,000 psig) are the same regardless of the form of hydrogen delivered to the fueling station. Since positive displacement pumps and compressors cannot provide instantaneous load or meet the high-rate demand for dispensing hydrogen directly to FC vehicles, each filling station is provided with three hours of peak demand high-pressure hydrogen buffer storage. The dispenser meters the hydrogen into a FC vehicle fitted with 5,000 psig cylinders.

Liquid Hydrogen Based Fueling

Liquid hydrogen from storage (15,000 gallons) is pressurized to 6,000 psig with variable speed reciprocating positive displacement pumps. An ambient or natural convection vaporizer, which uses ambient air and condensed water to supply the heat requirement for vaporizing and warming the high-pressure gas, does not incur additional utility costs.

Gaseous Hydrogen Based Fueling

Gaseous hydrogen could be delivered either by pipeline at 30 atmospheres or by tube trailer at 215 atmospheres to the fueling station. To minimize the high cost of hydrogen storage, both pipeline and tube trailer gases are compressed to 6,000 psig and held in a buffer storage. Two other possible options (multi-stage cascade system and booster system) require considerably more expensive hydrogen storage.

Forecourt Hydrogen Production

Forecourt production pathways were developed to evaluate the potential economic advantages of placing small modular units at fueling stations to avoid the initial investment of under utilized large central facilities and delivery infrastructures. The forecourt hydrogen facility is sized to supply and dispense the same amount of hydrogen as each fueling station in the central plant pathways. Each unit is designed to produce 470 kg/d of hydrogen with a 70% utilization rate. Figure 6 shows that forecourt hydrogen production is a self-contained operation. Ideally, hydrogen is compressed to 400 atmospheres (6,000 psig) after purification and dispensed directly into the FC vehicle with 340 atmosphere (5,000 psig) cylinders.



Figure 6

Table 13 lists commercial rates for feedstocks and power. The commercial rates charged to small local service stations are consistently 50%-70% higher than industrial rates for large production plants. Natural gas delivered to forecourt costs 70% more than that delivered to a central facility (\$6/million Btu vs. \$3.5/million Btu) and the power cost is 55% higher (7¢/kWh vs. 4.5¢/kWh). Often, proponents of a hydrogen economy provide cost estimates based on off-peak power rates (~\$0.04/kWh). Off-peak is only available for 12 hours, after which the forecourt would be charged with peak rates (\$0.09/kWh). To circumvent peak power rates, forecourt plants have to

Source: SFA Pacific, Inc.

be built with oversized units operated at low utilization rates with large amounts of storage. This option would require considerable additional capital investment.

Instead of developing a complete production and delivery infrastructure for methanol, this evaluation uses market prices for methanol. Methanol prices are based on current supplies to chemical markets, and distribution costs per gallon of methanol are twice that of gasoline per gallon or four times that of gasoline on an energy basis.

Table 13Forecourt Hydrogen Production Feedstock and Utility Costs

Natural gas (commercial) Electricity (commercial) Methanol Gasoline Unit Cost \$5.5/MMBtu HHV \$0.07/kW \$7.0/MMBtu HHV \$6.0/MMBtu HHV

Source: Annual Energy Outlook 2002 Reference Case Tables, EIA. Current Methanol Price, Methanex, February, 2002.

Table 14 shows that the costs for forecourt production of hydrogen from hydrocarbon based feedstocks are within 10%-15% of each other, ranging from \$4.40/kg to \$5.00/kg hydrogen. The cost for electrolysis based hydrogen is two to three times that of the other three feedstocks. The high cost of electrolytic hydrogen is attributable to high power usage and high capital costs— electricity and capital charges account for 30% and 50% of the total cost, respectively.

Table 14 Summary of Forecourt Hydrogen Costs (470 kg/d Hydrogen)

Feedstock	\$/kg
Methanol	4.53
Natural Gas	4.40
Gasoline	5.00
Water	12.12

Source: SFA Pacific, Inc.

For the two feedstocks common to both the central and forecourt plant, Table 15 shows that the lower infrastructure requirements of forecourt production do not compensate for the higher operating costs.

Table 15 Hydrogen Costs: Central Plant vs. Forecourt (\$/kg Hydrogen)

	Central Plant ^a	Forecourt
Natural Gas	3.66	4.40
Water	7.62	12.12

^a Liquid hydrogen delivery pathway.

Source: SFA Pacific, Inc.

The proposed option of utilizing the hydrogen produced at the forecourt to fuel on-site power generation during initial low hydrogen demand does not make economic sense. Excluding the high capital cost of fuel cell power generation and commercial scale grid connections for exporting electricity, the marginal load dispatch cost of power alone would make this strategy non-competitive. As a result, this pathway was eliminated from our analysis during the kick-off meeting on January 23, 2002.

Sensitivity

SFA Pacific developed a 700 atmospheres (10,000 psig) FC vehicle sensitivity case. This ultra high pressure would allow the vehicle to meet ICE vehicle standards (equal or greater distance between fill ups). Similarly detailed worksheets for the ultra high-pressure case are presented in Appendix B.

Between 1920 and 1950, the process industry had extensive commercial operating experience with 10,000 psig operation in ammonia synthesis and the German coal hydrogenations plants. Improvements in catalytic activity had lowered the operating pressures for these processes, which in turn significantly reduced capital and operating costs. Even though there is less demand for equipment to handle very high-pressure hydrogen, several companies still manufacture ultra high-pressure compressors and vessels. The cost of hydrogen compressors capable of handling 875 atmospheres (13,000 psig) is significantly more than the base case (\$4,000/kW vs. \$3,000/kW). The higher cost could be attributed mostly to expensive premium-steels to avoid hydrogen stress cracking at ultra high pressures. However, data on these costs are not readily available and are also inconsistent due to the lack of common use, small sizes, and the special fabrication requirements. Until a time when composite material becomes economically viable for high-pressure storage, it is may be best to develop the fueling infrastructure for 5,000 psig FC vehicle cylinders.

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References

- 1. C.E. Thomas et al, "Hydrogen Infrastructure Report Prepared for The Ford Motor Company," July 1997.
- 2. R.B. Moore and V. Raman, "Hydrogen Infrastructure for Fuel Cell Transportation," *International Journal of Hydrogen Energy*, Vol. 23, No. 7, pp. 617-620, 1998.

General

1. Hydrogen Infrastructure Report, prepared by the Ford Motor Company, DOE Contract No. DE-A-CO2-94CE50389, July 1997.

Gasification

- 1. D. Simbeck, "A Portfolio Selection Approach for Power Plant CO₂, Capture, Separation and R&D Options," Fourth International Conference on Greenhouse Gas Control Technologies (GHGT-4), Interlaken, Switzerland, September 1, 1998.
- 2. "Coal Gasification Guidebook: Status, Applications, and Technologies," EPRI TR-102034, Final Report December 1993.
- 3. "Biopower: Biomass and Waste-Fired Power Plant Performance and Cost Model, Version 1.0," EPRI TR-102774, Final Report March 1995.
- 4. F. Fong (Texaco), "Texaco's HyTEX Process for High Pressure Hydrogen Production," presented at the KTI Symposium, Caracas, Venezuela, April 27, 1993.
- 5. W.F. Fong and L.F. O'Keefe (Texaco), "Syngas Generation From Natural Gas Utilizing the Texaco Gasification Process," presented at the 1996 NPRA Annual Meeting, San Antonio, Texas, March 17-19, 1996.
- 6. J.S. Falsetti (Texaco), "Gasification Process for Maximizing Refinery Profitability," *Hydrocarbon Technology International 1993*, published by Sterling Publications Limited.
- 7. "Texaco Gasification Process for Gaseous or Liquid Feedstocks," Texaco Development Corporation brochure, 1993.
- 8. N. Hauser (Shell) and C. Higman (Lurgi), "The Use of the Shell Gasification Process (SGP) in Refining Heavy Crude and Tar Sands," presented at the Sixth UNITAR

International Conference on Heavy Crude and Tar Sands, Edmonton, Alberta, Canada, February 16, 1995.

- 9. "Texaco Gasification Process for Solid Feedstocks," Texaco Development Corporation brochure, 1993.
- 10. P.F. Curran and K.A. Simonsen (Texaco), "Gasification of Mixed Plastic Waste," presented at 8th Annual Recycling Plastic Conference, Washington, D.C., June 1993.
- 11. D.R. Simbeck and A.D. Karp (SFA Pacific), "Air-Blown Versus Oxygen-Blown Gasification," presented at the Institution of Chemical Engineers' Conference, "Gasification: An Alternative to Natural Gas," London, England, November 22-23, 1995.

Large Steam Methane Reforming

- 1. J.N. Gøl and I. Dybkjaer (Haldor Topsøe), "Options for Hydrogen Production," *HTI Quarterly*, Summer 1995.
- R. Vannby and C. Stub Nielsen (Haldor Topsøe) and J.S. Kim (Samsung-BP Chemicals), "Operating Experience in Advanced Steam Reforming," presented at the Symposium on Large Chemical Plants, Antwerp, Belgium, October 12-14, 1992.
- 3. "Catalyst components Team Up for the Shift-gas Reaction," *Chemical Engineering*, September 1995, p. 23.
- 4. "Carbides Catalyze Methane Reforming," *Chemical & Engineering News*, January 13, 1997, p. 5.
- 5. A.P.E. York, J.B. Claridge, C. Marquez-Alvarez, A.J. Brungs, and M.L.H. Green (Oxford University Catalysis Centre), "Group (V) and (VI) Transition Metal Carbides as New Catalysts for the Reforming of Methane to Synthesis Gas," presented at ACS National Meeting, San Francisco, California, April 13-17, 1997.
- 6. N.R. Udengaard and J-H Bak Hansen (Haldor Topsøe) and D.C. Hanson and J.A. Stal (Sterling Chemicals), "Sulfur Passivated Reforming Process Lowers Syngas H₂/CO Ratio," *Oil & Gas Journal*, March 9, 1992, pp. 62-67.
- B.J. Cromarty (ICI Katalco), "How to Get the Most Out of Your Existing Refinery Hydrogen Plant," presented at the AIChE Spring National Meeting, Houston, Texas, March 9-13, 1997.
- 8. J.B. Abbishaw and B.J. Cromarty (ICI Katalco), "New Reforming Technology for the Hydrogen Industry," Company Brochure (undated).
- 9. R.V. Schneider and G. Joshi (M.W. Kellogg), "Reforming Exchanger System for Largescale Methanol Plants," *Petroleum Technology Quarterly*, Summer 1997, pp. 85-91.

- I. Dybkjaer and J.N. Gøl (Haldor Topsøe) and D. Cieutat and R. Eyguessier (Air Liquide), "Medium Size Hydrogen Supply Using the Topsøe Convection Reformer," presented at the 1997 NPRA Annual Meeting, San Antonio, Texas, March 16-18, 1997.
- 11. U.S. Department of Energy, personal communication, May 1997.
- 12. B.T. Carvill, J.R. Hufton, M. Anand, and S. Sircar (APCI), "Sorption-Enhanced Reaction Process," *AIChE Journal*, Vol. 42, No. 10, October 1996, pp. 2765-2772.
- 13. E. Kikuchi, "Hydrogen-permselective Membrane Reactors," *Cattech*, March 1997, pp. 67-74.
- R.W. Morse, P.W. Vance and W.J. Novak (Acreon Catalysts) and J.P. Franck and J.C. Plumail (Procatalyse), "Improved Reformer Yield and Hydrogen Selectivity with Trimetallic Catalyst," presented at the 1995 NPRA Annual Meeting, San Francisco, California, May 19-21, 1995.
- 15. A.K. Rhodes, "Catalyst Suppliers Consolidate Further, Offer More Catalysts," *Oil and Gas Journal*, October 2, 1995, p. 37.
- 16. "Refining Processes '96," Hydrocarbon Processing, November 1996, pp. 96-98.
- 17. S. Ratan (KTI), "Flexibility of 'On-Purpose' Hydrogen Generation in Refineries," presented at AIChE Spring meeting, Houston, Texas, March 9-13, 1997.
- B.J. Cromarty, K. Chlapik, and D.J. Ciancio (ICI Katalco), "The Application of Prereforming Technology in the Production of Hydrogen," presented at the 1993 NPRA Annual Meeting, San Antonio, Texas, March 21-23, 1997.
- I. Dybkjaer, "Tubular Reforming and Autothermal Reforming of Natural Gas An Overview of Available Processes," *Fuel Processing Technology*, Vol. 42, pp. 85-107, 1995.
- 20. "Autothermal Catalytic Reforming," company brochure, Lurgi Öl Gas Chemie GmbH, 1994.
- 21. Krupp Uhde GmbH, "CAR A Modern Gas Generation Unit," report on Combined Autothermal Reforming provided to SFA Pacific by (undated).
- 22. H. Göhna (Lurgi), "Low-cost Routes to Higher Methanol Capacity," *Nitrogen*, No. 224, November/December 1996.
- 23. T.S. Christensen and I.I. Primdahl (Haldor Topsøe), "Improve syngas production using autothermal reforming," *Hydrocarbon Processing*, March 1994, pp. 39-46.

- M. Schwartz, J.H. White, M.G. Myers, S. Deych, and A.F. Sammells (Eltron Research), "The Use of Ceramic Membrane Reactors for the Partial Oxidation of Methane to Synthesis Gas," presented to the ACS National Meeting, San Francisco, California, April 13-17, 1997.
- 25. C.A. Udovich et al. (Amoco) and U. Balachandran et al. (Argonne National Laboratory), "Ceramic Membrane Reactor for the Partial Oxygenation of Methane to Synthesis Gas," presented to the AIChE Spring National Meeting, Houston, Texas, March 9-13, 1997.
- 26. *Hydrogen: Manufacture and Management*, a private multiclient-sponsored report, SFA Pacific, Inc., December 1991.
- 27. "Small-Scale Partial Oxidation Reformer Offered for Hydrogen Production," *The Clean Fuels Report*, June 1996, p. 149.
- 28. B.M. Tindal and M.A. Crews (Howe-Baker), "Alternative Technologies to Steam-Methane Reforming," *Hydrocarbon Processing*, November 1995, pp. 75-82.
- 29. B.J. Cromarty (ICI Katalco), "How to Get the Most Out of Your Existing Refinery Hydrogen Plant," presented to the AIChE Spring National Meeting, Houston, Texas, March 9-13, 1997.
- G.Q. Miller (UOP) and J. Stoecker (Union Carbide), "Selection of a Hydrogen Separation Process," paper AM-89-55 presented at the 1989 NPRA Annual Meeting, San Francisco, California, March 19-21, 1989.
- 31. T.R. Tomlinson and A.J. Finn (Costain Engineering), "H₂ Recovery Processes Compared," *Oil & Gas Journal*, January 15, 1990, pp. 35-39.
- 32. E.J. Hoffman et al., "Membrane Separations of Subquality Natural Gas," *Energy Progress*, March 1988, pp. 5-13.`
- 33. W.S.W. Ho and K.K. Sirkar (Eds.), Membrane Handbook, Van Nostrand Reinhold, 1992.
- 34. R.W. Spillman (W.R. Grace), "Economics of Gas Separation Membranes," *Chemical Engineering Progress*, January 1989, pp. 41-62.
- 35. G. Markiewicz (APCI), "Membrane System Lowers Treating Plant Cost," *Oil & Gas Journal*, October 31, 1988, pp. 71-73.
- 36. U.S. Department of Energy, *Membrane Separation Systems, A Research Needs Assessment*, DE 90-011770, April 1990.
- 37. "Membrane Uses 'Reverse Logic' for Hydrogen Recovery," *Chemical Engineering*, January 1997, p. 15.

 M.V. Narasimhan (KTI), M. Whysall (UOP), and B. Pacalowska (Petrochemia Plock), "Design Considerations for a Hydrogen Recovery Scheme from Refinery Offgases," presented at AIChE Spring National Meeting, Houston, Texas, March 9-13, 1997.

Small Steam Methane Reforming

- D.L. King & C.E. Bochow, Jr. (Howe-Baker Engineers, Inc.), "What should an owner/operator know when choosing an SMR/PSA plant?" *Hydrocarbon Processing*, May 2000, pp. 39-48.
- 2. Phillip Morris and William Baade (Air Products & Chemicals, Inc.), "Outsourcing Hydrogen," *Hydrocarbon Engineering*, February 2001, pp. 75-82.
- 3. Howe-Baker brochure, "Hydrogen Steam Reforming Technology for Hydrogen Plants."
- 4. Ib Dybhjaer, et al (Haldor Topsøe), "Medium Size Hydrogen Supply Using the Topsøe Convection Reformer," Paper AM-97-18, NPRA Annual Meeting, San Antonio, TX, March 16-18, 1997.
- 5. Olimpia Loiacono (Technip KTI), "Consuming Hydrogen," *Hydrocarbon Engineering*, November 2001, pp. 45-50.
- 6. Air Products and Chemicals, Inc., 1998, from Internet 1/16/01.
- 7. Hydro-Chem, a Division of Pro-Quip Corporation (Linde Group), "Hydro-Chem Modular Hydrogen Plants," from Internet 12/14/01.
- 8. David Cepla, Fuel Processor Group, UOP LLC, Des Plaines, IL, (847) 391-3534, January 22, 2002.
- 9. Hydrogen Burner Technology, Long Beach, CA, (562) 597-2442, January 18, 2002 and <u>www.hbti.net/</u>.
- 10. Sandy Thomas, H₂Gen Innovations Inc., Alexandria, VA, (703) 212-7444, December 7, 2001 and <u>www.h2gen.com</u>.
- 11. "ZTEK Prepackaged Steam Reformer," http://www.ztekcorp.com/ztekreformer.
- 12. R.E. Stoll and F. von Linde, "Hydrogen—What are the Costs?" Hydrocarbon Processing, December 2000, pp. 42-46.
- 13. "Fuel Cells—Progressing, But Far From Proven or Economical," The SFA Quarterly *Report*, Fourth Quarter 2000.

Electrolysis

- 1. M.N. Tazima, et. al. "Development on Solid Polymer Electrolyte Water Electrolysis Technonogy for High Density and Energy Efficiency," Mitsubishi Heavy Industries
- 2. Packaged Hydrogen Generators, Electrolyser Corp.
- 3. The IMET Package, <u>www.hydrogensystems.com</u>
- 4. Personal Contact, Air Products

Pipeline

- 1. "Transportation and Handling of Medium Btu Gas in Pipelines," EPRI AP-3426, Final Report, March 1984.
- 2. "Pipeline Transmission of CO2 and Energy Transmission Study-Report," IEA Greenhouse Gas R&D Programme, Woodhill Engineering Consultants.

High Pressure Storage

- 1. Andrew Haaland, "High Pressure Conformable Hydrogen Storage for Fuel Cell Vehicles," Preceeding of the 2000 Hydrogen Program Review.
- 2. "Fill'er Up-With Hydrogen," Mechanical Engineering, Features, February 2002, <u>www.memagazine.org</u>.
- "Lincoln Composites Delivers High Pressure Hydrogen Tanks," <u>www.lincolncomposites.com/</u>
- 4. S.M. Aceves et. al, "Low Temperature and High Pressure Evaluation of Insulated Pressure Vessels for Cryogenic Hydrogen Storage," Proceeding of the 2000 Hydrogen Program Review, NREL/CP-570-28890.

High Pressure Compression

- 1. Robert Chellini, "12,000 Hp Hydrogen Compressors Enhance Reformulated Gasoline Production in California," Compressor Tech. May-June 2001.
- 2. Hydro-Pack Brochure.

Delivery

- 1. Wade A. Amos, "Cost of Storing and Transporting Hydrogen," November 1998, NREL/TP-570-25106.
- 2. Susan M. Schoenung, "IEA Hydrogen Annex 13 Transportation Applications Analysis," Proceedings of 2001 DOE Hydrogen Program Review.

Appendix A Complete Set of Spreadsheets For Base Case Input

Summary of Natural Gas Based Hydrogen Production Final Version June 2002 IHIG Confidential

Design hydrogen product Supporting	ion		kg/d H2 and FC Vehicles at		Annual ave. load faco Filling station
Hydrogen per filling statio	on	10,000	kg/mo H2 or		kg/d H2
Capital Investment	Liquid H2	Pipeline	Tube Trailer		
·	Million \$/yr	Million \$/yr			
H2 production	230	79	133		
H2 delivery	13	603	141		
H2 fueling	279	212	212		
Total	522	894	486		
Annual Operating Costs	Liquid H2	Pipeline	Tube Trailer		
	\$ million/yr	\$ million/yr	\$ million/yr		
H2 production	109	49	64		
H2 delivery	9	145	103		
H2 fueling	63	53	49		
Total	180	246	216		
Unit H2 Cost in \$/kg which is the same as \$/gallon gasoline energy equivalent					
	Liquid H2	Pipeline	Tube Trailer	Forecourt	
	\$/kg	\$/kg	\$/kg	\$/kg	
H2 production	2.21	1.00	1.30		
H2 delivery	0.18	2.94	2.09		
H2 fueling	1.27	1.07			
Total	3.66	5.00	4.39	4.40	

Summary of Resid Hydrogen Production Final Version June 2002 IHIG Confidential

Design hydrogen production Supporting Hydrogen per filling station	225,844	kg/d H2 and FC Vehicles at kg/mo H2 or	90%Annual ave. load facor411Filling station329kg/d H2	
Capital Investment	Pipeline Million \$/yr			
H2 production	185			
H2 delivery	603			
H2 fueling	212			
	1,000	-		
	1,000			
Annual Operating Costs	Pipeline			
	\$ million/yr			
H2 production	62			
H2 delivery	145			
H2 fueling	53			
Total	260	-		
Unit H2 Cost in \$/kg which is the same as \$/gallon gasoline energy equivalent				
	Pipeline			
	\$/kg			
H2 production	1.27			
H2 delivery	2.94			
H2 fueling	1.07			
Total	5.27			

Summary of Petroleum Coke Based Hydrogen Production Final Version June 2002 IHIG Confidential

Design hydrogen production Supporting Hydrogen per filling station	225,844	kg/d H2 and FC Vehicles at kg/mo H2 or	411	Annual ave. load facor Filling station kg/d H2	
Capital Investment	Pipeline Million \$/yr				
H2 production	238				
H2 delivery	603				
H2 fueling	212				
	1,053	-			
Annual Operating Costs	Pipeline \$ million/yr				
H2 production	66				
H2 delivery	145				
H2 fueling	53				
Total	264	-			
Unit H2 Cost in \$/kg which is the same as \$/gallon gasoline energy equivalent Pipeline \$/kg					
H2 production	1.35				
H2 delivery	2.94				
H2 fueling	1.07				
Total	5.35				
Summary of Coal Based Hydrogen Production Final Version June 2002 IHIG Confidential

Design hydrogen productio Supporting			kg/d H2 and FC Vehicles at	90% 411	Annual ave. load facor Filling station	
Hydrogen per filling station	1	10,000	kg/mo H2 or	329	kg/d H2	
Capital Investment	Capital Investment Liquid H2		Tube Trailer			
Capital Investment	Million \$/yr	Pipeline Million \$/yr				
H2 production	•	•	-			
H2 production	448	259	339			
H2 delivery	13	603	141			
H2 fueling	279	212	212			
	740	1,074	692			
Annual Operating Costs	Liquid H2	Pipeline	Tube Trailer			
	\$ million/yr	\$ million/yr	\$ million/yr			
H2 production	151	80	103			
H2 delivery	9	145	103			
H2 fueling	63	53	49			
Total	222	277	255			
Unit H2 Cost in \$/kg which	is the same a	as \$/gallon g	asoline energy	equivalent		
	Liquid H2	Pipeline	Tube Trailer			
	\$/kg	\$/kg	\$/kg			
H2 production	3.06	1.62	-			
H2 delivery	0.18	2.94	2.09			
H2 fueling	1.27	1.07				
Total	4.51	5.62	5.18			

Summary of Biomass Based Hydrogen Production Final Version June 2002 IHIG Confidential

Supporting	Design hydrogen production Supporting Hydrogen per filling station		kg/d H2 and FC Vehicles at kg/mo H2 or	90% Annual ave. loa 411 Filling station 329 kg/d H2	ad facor
Capital Investment	Liquid H2 Million \$/yr	Pipeline Million \$/yr			
H2 production	452	295	362		
H2 production	-		141		
H2 delivery	13	603			
H2 fueling	279	212	212		
	744	1,110	715		
Annual Operating Costs	Liquid H2	Pipeline	Tube Trailer		
	\$ million/yr	\$ million/yr	\$ million/yr		
H2 production	174	113	132		
H2 delivery	9	145	103		
H2 fueling	63	53	49		
Total	246	310	284		
Unit H2 Cost in \$/kg which	is the same a	as \$/ɑallon ɑ	asoline energy	equivalent	
••••••••••••••••••••••••••••••••••••••	Liquid H2	Pipeline		-	
		\$/kg			
H2 production	3.53	2.29			
H2 delivery	0.18	2.23			
H2 fueling	1.27	1.07			
Total	4.98	6.29	5.77		

Summary of Electrolysis Based Hydrogen Production Final Version June 2002 IHIG Confidential

Design hydrogen productio Supporting Hydrogen per filling station			kg/d H2 and FC Vehicles at kg/mo H2 or	90% Annual ave. load facor 411 Filling station 329 kg/d H2
Capital Investment	Liquid H2	Pipeline		
	Million \$/yr	Million \$/yr	Million \$/yr	
H2 production	688	566	602	
H2 delivery	13	603	141	
H2 fueling	279	212	212	
	980	1,382	955	
Annual Operating Costs	Liquid H2	Pipeline	Tube Trailer	
	\$ million/yr	\$ million/yr	\$ million/yr	
H2 production	304	253	261	
H2 delivery	9	145	103	
H2 fueling	63	53	49	
Total	376	450	413	
Unit H2 Cost in \$/kg which	is the same a	as \$/gallon g	asoline energy	equivalent
	Liquid H2	Pipeline	Tube Trailer	Forecourt
	\$/kg	\$/kg	\$/kg	\$/kg
H2 production	6.17	5.13	-	-
H2 delivery	0.18	2.94	2.09	
H2 fueling	1.27	1.07		
Total	7.62	9.13	8.39	12.12

Forecourt Summary of Inputs and Outputs

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Inputs Boxed in	n yellow are the key input variabl	es you must choose, current inputs are just an example
design basis		
Key Variables In	puts	Notes
Hydrogen Production Inputs		1 kg H2 is the same energy content as 1 gallon of gasoline
Design hydrogen production	470 kg/d H2	194,815 scf/d H2 100 to 10,000 kg/d range for forecourt
Annual average load factor	70% /yr of design	10,007 kg/month actual or 120,085 kg/yr actual
High pressure H2 storage	3 hr at peak surge rate	"plug & play" 24 hr process unit replacements for availability
FC Vehicle gasoline equiv mileage	55 mpg (U.S. gallons) or	23 km/liter 329 kg/d average
FC Vehicle miles per year	12,000 mile/yr thereby requires	218 kg/yr H2 for each FC vehicle
Capital Cost Buildup Inputs from pro	ocess unit costs	All major utilities included as process units
General Facilities	20% of process units	20-40% typical, should be low for small forecourt
Engineering, Permitting & Startup	10% of process units	10-20% typical, assume low eng. of multiple standard designs
Contingencies	10% of process units	10-20% typical, should be low after the first few
Working Capital, Land & Misc.	9% of process units	5-10% typical, high land costs for forecourt
Site specific factor	110% above US Gulf Coast	90-130% typical; sales tax, labor rates & weather issues
Product Cost Buildup Inputs		
Road tax or (subsidy)	\$ - /gal gasoline equivalent	may need subsidy like EtOH to get it going
Gas Station mark-up	\$ - /gal gasoline equivalent	may be needed if H2 sales drops total station revenues
Non-fuel Variable O&M	1.0% /yr of capital	0.5-1.5% is typical
Fuels Methanol	\$ 7.15 /MM Btu HHV	\$7-9/MM Btu typical chemical grade delivered rate
Natural Gas	\$ 5.50 /MM Btu HHV	\$4-7/MM Btu typical commercial rate, see www.eia.doe.gov
Gasoline	\$ 6.60 /MM Btu HHV	\$5-7/MM Btu typical tax free rate go to www.eia.doe.gov
Electricity	\$ 0.070 /kWh	\$0.060.09/kWh typical commercial rate, see www.eia.doe.gov
Fixed Operating Cost	5.0% /yr of capital	4-7% typical for refiners: labor, overhead, insurance, taxes, G&A
Capital Charges	18.0% /yr of capital	20-25%/yr CC typical for refiners & 14-20%/yr CC for utilities
		20%/yr CC is about 12% IRR DCF on 100% equity where as
		15%/yr CC is about 12% IRR DCF on 50% equity & debt at 7%
		20-25%/yr CC typical for refiners & 14-20%/yr CC for utilities 20%/yr CC is about 12% IRR DCF on 100% equity where as

Outputs	329	kg/d H2 that	supports	550	FC vehicles	or	10,007	kg/month for this stat	ion
actual anr	nual average	79	fill-ups/d if 1	fill-up/week @	2 4.2 kg/fill-up				
				Capital Cost	s	Operating	g Cost	Product Costs	
			Absolute	Unit cost	Unit cost	Fixed	Variable	Including capital cl	narges
Case No.	Desci	ription	\$ millions	design rate	design rate	Unit cost	Unit cost	Unit cost	Note
				\$/scf/d H2	<u>\$ kg/d H2</u>	<u>\$/kg H2</u>	<u>\$/kg H2</u>	<u>\$/kg H2</u> same	as \$/gal gaso equiv
F1	Methanol Re	eforming	1.57	8.08	3,350	0.66	1.51	4.53 into ve	ehicles at 340 atm
F2	Natural Gas	Reforming	1.63	8.35	3,460	0.68	1.28	4.40 into ve	ehicles at 340 atm
F3	Gasoline Re	forming	1.78	9.14	3,789	0.74	1.59	5.00 into ve	ehicles at 340 atm
F4	Water Electr	rolysis	4.15	21.28	8,821	1.73	4.18	12.12 into ve	ehicles at 340 atm
		Click on spe	cific Excel	worksheet ta	bs below for de	tails of cost	buildups fo	or each case	

Path F1

Forecourt Hydrogen via Steam Reformer of Methanol plus High Pressure Gas Storage



Path F2

Forecourt Hydrogen via Steam Reformer of Natural Gas plus High Pressure Gas Storage



0.051 /kWh electricity for <u>only</u> NG fuel (<u>no</u> capital charges or other O&M) to Solar 9 MWe STAC70 CC @ H2-fuel cell power sales during H2 vehicle ramp-up is questionable relative to lower capital & non-fuel O&M of small NG fired GT/CC or the much lower NG costs and higher efficiency, 60% of large industrial NGCC

note: Assume gas station has existing natural gas pipeline infrastructure, if not more capital or higher NG price

Path F3

Forecourt Hydrogen via Steam Reformer of Gasoline plus High Pressure Gas Storage



Path F4 Forecourt Hydrogen via Electrolysis of Water plus High Pressure Gas Storage



Central Hydrogen Plant Summary of Inputs and Outputs

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Innute	Deved i	n vellevu	are the key input variable	es you must choose, current inputs are just an example
Inputs		n yellow	are the key input variable	so you must choose, current inputs are just an example
design ba				Natas
Hudrogo	Key Variables In n Production Inputs	puts		Notes 1 kg H2 is the same energy content as 1 gallon of gasoline
, ,		450.000	kq/d H2	62,175,000 scf/d H2 size range of 20,000 to 900,000 kg/d
	/drogen production /erage load factor			62,175,000 scr/d H2 size range of 20,000 to 900,000 kg/d) kg/month actual or 49,275,000 kg/yr actual
	on distance to forecourt	9070	yr ol desigir 4,100,250	· · · · · · · · · · · · · · · · · · ·
			<i>(</i> , , , , , , , , , , , , , , , , , , ,	5
	e gasoline equiv mileage	55		23 km/liter
	e miles per year	12,000	mile/yr thereby requires	218 kg/yr H2 for each FC vehicle
<i>, , , , , , , , , ,</i>	asoline sales/month/station	150,000	gallons/month per station	100,000 - 250,000 gallons/month is typical or 4,932 gal/d
, ,	as % of gasoline/station	6.7%	of gasoline/station or	10,000 kg H2/month per stations or 329 kg/d/station
•	ost Buildup Inputs from proce			All major utilities included as process units
General F			of process units	20-40% typical for SMR + 10% more for gasification
•	ng, Permitting & Startup		of process units	10-20% typical
Continger			of process units	10-20% typical, should be low after the first few
•	Capital, Land & Misc.		of process units	5-10% typical
Site speci		110%	above US Gulf Coast	90-130% typical; sales tax, labor rates & weather issues
	Cost Buildup Inputs		_	
Non-fuel	√ariable O&M		/yr of capital	0.5-1.5% is typical
Fuels	Natural Gas		/MM Btu HHV	\$2.50-4.50/MM Btu typical industrial rate, see www.eia.doe.gov
	Electricity	\$ 0.045	/kWh	\$0.04-0.05/kWh typical industrial rate, see www.eia.doe.gov
	Biomass production costs	\$ 500	/ha/yr gross revenues	\$400-600/hr/yr typical in U.Slower in developing nations or wastes
	Biomass yield	10	tonne/ha/yr bone dry	8-12 ton/hr/yr typical if farmed, 3-5 ton/hr/yr if forestation or wastes
	Coal	\$ 1.10	/million Btu dry HHV	\$0.75-1.25/million Btu coal utility delivered go to www.eia.doe.gov
	Petroleum Coke	\$ 0.20	/million Btu dry HHV	\$0.00-0.50/million Btu refinery gate
	Residue (Pitch)		/million Btu dry HHV	\$1.00-2.00/million Btu refinery gate (solid at room temperature)
Fixed O&	M Costs		/yr of capital	4-7% typical for refiners: labor, overhead, insurance, taxes, G&A
Capital Cl	harges	18.0%	/yr of capital	20-25%/yr CC typical for refiners & 14-20%/yr CC typical for utilities
			_	20%/yr CC is about 12% IRR DCF on 100% equity where as

15%/yr CC is about 12% IRR DCF on 50% equity where as

Outputs	135,000 kg/d H2 that su inual average 32,263	upports fill-ups/d if 1 fill	225,844 F			g H2/month/ I-ups/d per :	station supports	411 stations 329 kg/d/station
			Capital Costs		Operating		Product Costs	U
	-	Absolute	Unit cost	Unit cost	Fixed	Variable		
Case No.	Description	\$ millions	design rate	design rate	Unit cost	Unit cost	Unit cost	Note
			\$/scf/d H2	\$/kg/d H2	\$/kg H2	\$/kg H2	\$/kg H2	same as \$/gal gaso equiv
C1	Biomass-H2 Pipeline	295	4.74	1,966	0.30	0.92	2.29	216 sq mi land
C2	Biomass-Liquid H2	452	7.28	3,017	0.46	1.42	3.53	216 sq mi land
C3	Natural gas-H2 Pipeline	79	1.27	527	0.08	0.63	1.00	into pipeline @ 75 atm
C4	Natural gas-Liquid H2	230	3.70	1,534	0.23	1.13	2.21	into liquid H2 tanker truck
C5	Electrolysis-H2 Pipeline	566	9.11	3,776	0.57	2.49	5.13	into pipeline @ 75 atm
C6	Electrolysis-Liquid H2	688	11.07	4,586	0.70	2.96	6.17	into liquid H2 tanker truck
C7	Pet Coke-H2 Pipeline	238	3.82	1,585	0.24	0.24	1.35	into pipeline @ 75 atm
C8	Coal-H2 pipeline	259	4.16	1,723	0.26	0.42	1.62	into pipeline @ 75 atm
C9	Coal-Liquid H2	448	7.21	2,989	0.46	0.97	3.06	into liquid H2 tanker truck
C10	Biomass-HP Tube H2	362	5.82	2,411	0.37	1.00	2.69	216 sq mi land
C11	Natural Gas-HP Tube H2	133	2.13	884	0.13	0.69		into tube trailer @ 400 atm
C12	Electrolysis-HP Tube H2	602	9.67	4,010	0.61	2.49	5.30	into tube trailer @ 400 atm
C13	Residue-H2 Pipeline	185	2.97	1,231	0.19	0.41	1.27	into pipeline @ 75 atm
C15	Coal-HP Tube H2	339	5.46	2,263	0.34	0.51	2.09	into tube trailer @ 400 atm
	Click on spec	ific Excel worl	csheet tabs be	low for details	s of cost buildu	os for each	case	

Click on specific Excel worksheet tabs below for details of cost buildups for each case

Path C1 Central Hydrogen via Biomass Gasification, Shipped by Pipeline



Central Hydrogen via Biomass Gasification, Shipped by Cryogenic Tanker Truck



Central Hydrogen via Steam Reformer of Natural Gas, Shipped by Gas Pipeline

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note: Assume no central plant storage or compression of hydrogen due to pipeline volume & SMR at 30 atm pressure

Central Hydrogen via Steam Reformer of Natural Gas, Shipped by Cryogenic Liquid Trucks Final Version June 2002 IHIG Confidential



plant gate still requires distribution

note: Assuming all storage liquid boil-off is recycled back to hydrogen liquefaction units, thereby no hydrogen losses

Central Hydrogen via Electrolysis of Water, Shipped by Gas Pipeline



Path C6 Central Hydrogen via Electrolysis of Water, Shipped by Cryogenic Liquid Tankers Final Version June 2002 IHIG Confidential



Assume Hydrogn Systems Electrolysis at 150 psig pressure, Norsk Hydro & Stuard systems are low pressure

Central Hydrogen via Petroleum Coke Gasification, Shipped by Pipeline



Central Hydrogen via Coal Gasification, Shipped by Pipeline



note **\$ 29.11** /tonne coal price from above **\$/MM** Btu input at

12,000 Btu/lb HHV

Central Hydrogen via Coal Gasification, Shipped by Cryogenic Tanker Truck



note **\$ 29.11** /tonne coal price from above \$/MM Btu input at

12,000 Btu/lb HHV

Central Hydrogen via Biomass Gasification, Shipped by High Pressure Gas Tube Trailers



Central Hydrogen via Steam Reformer of Natural Gas, Shipped by High Pressure Gas Tube Trailers



Total HP Hydrogen Costs from Natural Gas plant gate still requires distribution

note:

Path C12 Central Hydrogen via Electrolysis of Water, Shipped by High Pressure Gas Tube Trailers Final Version June 2002 IHIG Confidential



Assume Hydrogn Systems Electrolysis at 150 psig pressure, Norsk Hydro & Stuard systems are low pressure

Path C13 Central Hydrogen via Petroleum Residue Gasification, Shipped by Pipeline Final Version June 2002 IHIG Confidential



9.65 /barrel at 6.0 bbl/tonne \$

17,500 Btu/lb HHV

Path C15 Central Hydrogen via Coal Gasification, Shipped by High Pressure Gas Tube Trailers



Summary for Hydrogen Delivery Pathways Final Version June 2002 IHIG Confidential

Inputs Boxed in yellow	are the key input variables you	ı must choose, curr	ent inputs are <u>just ar</u>	n example
Hydrogen Production Inputs				
Design hydrogen production	150,000 kg/d H2			
Annual average load factor	90% /yr of design			
Average distance to forecourt	150 km, key assumption	for tube trailer & espe	cially pipeline	
Truck utilization	80%			
Tube load		t for tube trailer		
Tube pressure full	160 Atmosphere			
Tube pressure (min)	30 Atmosphere			
Pipeline	621,504 \$/km			
Gasoline sales/month/station	10,000 kg/month thereby s	upplying 41	1 stations	
Fuel cost	<mark>1</mark> \$/gal			
Capital Cost Buildup Inputs from	·			
General Facilities	20%	20-40% typical	assume low for pipeli	
Engineering, Permits & Startup	10%	10-20% typical	assume low for pipeli	
Contingencies	10%	21 7	uld be low after the first	few
Working Capital, Land & Misc.	7%	5-10% typical		
Site specific factor	110% of US Gulf Coast	90-130% typical; sa	les tax, labor rates & we	ather issues
Product Cost Buildup Inputs				
Electricity cost	0.045 \$/kwh		al industrial rate, see www	v
Non-fuel Variable O&M	1.0% /yr of capital		could be lower for pipeli	
Fixed O&M Costs	5.0% /yr of capital		rs: labor, overhead, insurar	
Capital Charges	18.0% /yr of capital	20-25%/yr CC typical	for refiners & 14-20%/yr CC	typical for utilities
Outputs 135,000 kg/d H2 tha	A REAL PROPERTY AND	· · · · ·	h per station supports with	411 stations
actual annual average 32,290	fill-ups/d if 1 fill-up/week @ 4.2 kg	Operating Cost		329 kg/d H2
	Capital Costs		ble including return on	capital
	Absolute Unit cost Unit cost		ost Unit cost	capital

	Absolute	Unit cost	Unit cost	Unit cost	Unit cost	Unit cost
Delivery Method	\$ millions	\$/scf/d H2/	kg/d H2 or	\$/kg H2	\$/kg H2	\$/kg H2
Liquid H2 via Tank Trucks	13.2	0.6	88.0	0.02	0.10	0.18
Gaseous H2 via Pipeline	603.0	29.5	4,019.9	0.61	0.61	2.94
Gaseous H2 via Tube Trailers	140.7	6.9	938.0	0.14	0.14	2.09
011	100 00 00			A		

Click on specific Excel worksheet tabs below for details of cost buildups for each case Source: SFA Pacific, Inc.

Liquid Hydrogen Distributed via Trucks Final Version June 2002 IHIG Confidential

Central Pla					ergy equivalent		Assuming		mpg and	12,000 mile/yr
·	н	lydrogen	gasoline	million			requires			vehicle or gal/yr gaso equiv
Size range	Massian	kg/d H2	gal/d	Btu/hr	scf/d H2	MW t	Assuming			erage load factor
	Maximum	1,000,000	1,000,000	4,742.186	414,500,000	,	actual H2			H2 or gal/mo. gaso equiv
	This run	150,000	150,000	711.328	62,175,000	208.417	or			es can be supported at
	Minimum	20,000	20,000	94.844	8,290,000	27.789	thereby			4.2 kg or gal equiv/fill-up
								411	station sup	ported by this central faci
verage deliv	very distance		150 ki	m						
Delivery dista			210 ki		40%	increase to re	present physic	al distance		
ruck utilizati			80%							
					Million C		Natas			
Capital costs					Million \$	¢ 75	Notes			
Tank & und	dercarrage				11.2		/kg/d H2			
Cabe					2.0	\$ 13	/kg/d H2			
l otal tube	e trailer cost				13.2					
						\$/million		\$/kg H2 or		
ariable Ope	erating Cost				Million \$/yr	Btu LHV	\$/k scf H2	\$/gal gase	equiv	
Labor	-				4.43	0.79	0.22	0.09		
Fuel					0.54	0.10	0.03	0.01		
Variable no	on-fuel O&M		1% /y	r of capital	0.13	0.03	0.01	0.00	6,000	\$/yr/truck
Total vari	iable operatin	g costs			5.10	0.91	0.25	0.10		
ixed Opera			5% /y	r of capital	0.66	0.12	0.03	0.02		
Capital Char	rges		18% /y	r of capital	2.38	0.42	0.12	0.06		
Total ope	erating costs				8.14	1.45	0.40	0.18		
Assumption	-				0.14	1.43		0.10		
ruck costs	-		_							
ruck costs Tank unit	IS		Г		\$/module		\$/kg H2 stroag			
ruck costs Tank unit Undercarrag	IS		Γ	60,000	\$/module \$/trailer					
ruck costs Tank unit Undercarrae Cabe	is ge		[60,000 90,000	\$/module \$/trailer \$/cab					
ruck costs Tank unit Undercarrag Cabe ruck boil-off	is ge f rate		ſ	60,000 90,000 0.30	\$/module \$/trailer \$/cab %/day					
ruck costs Tank unit Undercarrag Cabe ruck boil-off ruck capaci	is ge f rate ity		[60,000 90,000 0.30	\$/module \$/trailer \$/cab %/day kg/truck					
ruck costs Tank unit Undercarrag Cabe ruck boil-off ruck capaci uel econom	ge f rate ity			60,000 90,000 0.30 4000 6	\$/module \$/trailer \$/cab %/day kg/truck mpg					
ruck costs Tank unit Undercarrag Cabe ruck boil-off ruck capaci uel econom werage spec	ge f rate ity iy ied			60,000 90,000 0.30 4000 6 50	\$/module \$/trailer \$/cab %/day kg/truck mpg km/hr	113	\$/kg H2 stroag	ge		
ruck costs Tank unit Undercarrag Cabe ruck boil-off ruck capaci uel econom verage spectod toad/unload	ge f rate ity vy time			60,000 90,000 0.30 4000 6 50 4	\$/module \$/trailer \$/cab %/day kg/truck mpg km/hr hr/trip could be I	113	\$/kg H2 stroag	ge		
ruck costs Tank unit Undercarrag Cabe ruck boil-off ruck capaci uel econom werage spec	ge f rate ity vy time			60,000 90,000 0.30 4000 6 50 4 24	\$/module \$/trailer \$/cab %/day kg/truck mpg km/hr hr/trip could be I hr/tray	113	\$/kg H2 stroag	ge		
ruck costs Tank unit Undercarraq Cabe ruck boil-off ruck capaci uel econom verage spe oad/unload ruck availab	ge f rate ity vy eed time bility			60,000 90,000 0.30 4000 6 50 4 24 24 12	\$/module \$/trailer \$/cab %/day kg/truck mpg km/hr hr/trip could be I hr/day hr/day	113	\$/kg H2 stroag	ge		
ruck costs Tank unit Undercarrag Cabe ruck boil-off ruck capaci uel econom verage sper oad/unload ruck availab lour/driver river wage	ge f rate ity vy eed time bility			60,000 90,000 0.30 4000 6 50 4 24 24 12	\$/module \$/trailer \$/cab %/day kg/truck mpg km/hr hr/trip could be I hr/day hr/day	113	\$/kg H2 stroag	ge		
ruck costs Tank unit Undercarrag Cabe ruck boil-off ruck capaci uel econom verage spe- oad/unload ruck availat our/driver rriver wage uel price	ge f rate ity vy eed time bility			60,000 90,000 0.30 4000 6 50 4 24 24 12	\$/module \$/trailer \$/cab %/day kg/truck mpg km/hr hr/trip could be I hr/day hr/triver \$/hr	113	\$/kg H2 stroag	ge		
ruck costs Tank unit Undercarrag Cabe ruck boil-off ruck capaci uel econom werage spe- oad/unload ruck availat our/driver priver wage uel price	ge frate ity iy ed time bility & benefits rement calcu			60,000 90,000 0.30 4000 6 50 4 24 24 12	\$/module \$/trailer \$/cab %/day kg/truck mpg km/hr hr/trip could be I hr/day hr/triver \$/hr	113 owered with a	\$/kg H2 stroag	ge		
ruck costs Tank unit Undercarrac Cabe ruck boil-off ruck capaci uel econom verage sper oad/unload ruck availab lour/driver rriver wage uel price ruck requir rips per yea	ge f rate ity vy eed time bility & benefits rement calcu ar			60,000 90,000 0.30 4000 6 50 4 24 12 28.75 1	\$/module \$/trailer \$/cab %/day kg/truck mpg km/hr hr/trip could be I hr/day hr/driver \$/hr \$/gal	113 owered with a 34	\$/kg H2 stroag	ge D	little high	
ruck costs Tank unit Undercarrag Cabe ruck boil-off ruck capaci uel econom verage spee oad/unload our/driver ruck availat lour/driver ruck requir ruck requir ruck requir ruck requir	ge f rate ity ved time bility & benefits rement calcu ar ce			60,000 90,000 0.30 6 50 4 24 12 28.75 1 28.75 1 1 2,319 5,173,875	\$/module \$/trailer \$/cab %/day kg/truck mpg km/hr hr/trip could be I hr/day hr/driver \$/hr \$/gal	113 owered with a 34	\$/kg H2 stroag liquid H2 pump trips per day	ge D		
ruck costs Tank unit Undercarrag Cabe ruck boil-off ruck capaci uel econom verage sper oad/unload ruck availat lour/driver priver wage uel price ruck requir rips per yea otal Distance ime for eacl rip length	ge f rate ity yed time bility & benefits rement calcu ar ce h trip			60,000 90,000 0.30 4000 6 50 4 24 22 28.75 1 12,319 5,173,875 8.4 12,4	\$/module \$/trailer \$/cab %/day kg/truck mpg km/hr hr/trip could be I hr/day hr/driver \$/hr \$/gal km/yr hr/trip hr/trip	113 owered with a 34	\$/kg H2 stroag liquid H2 pump trips per day	ge D		
ruck costs Tank unit Undercarrag Cabe ruck boil-off ruck capaci uel econom verage spec- oad/unload ruck availab lour/driver river wage uel price ruck requir rips per yea otal Distanc ime for each rip length elivered proc	ge f rate ity iy ed time bility & benefits rement calcu ar ce h trip boduct			60,000 90,000 0.30 4000 6 50 4 24 122 28.75 1 1 2,319 5,173,875 8.4 12.4 48,658,030	\$/module \$/trailer \$/cab %/day kg/truck mpg km/hr hr/trip could be I hr/day hr/driver \$/hr \$/gal km/yr hr/trip hr/trip kg/yr	113 owered with a 34	\$/kg H2 stroag liquid H2 pump trips per day	ge D		
ruck costs Tank unit Undercarrac Cabe ruck boil-off ruck capaci uel econom verage sper oad/unload ruck availat lour/driver river wage uel price ruck requir rips per yea otal Distance ime for eacl rip length elivered pro otal delivery	ge f rate ity vy eed time bility & benefits rement calcu ar ce h trip ce h trip couct y time			60,000 90,000 0.30 6 50 4 4 24 12 28.75 1 12,319 5,173,875 8.4 12.4 48,658,030 152,753	\$/module \$/trailer \$/cab %/day kg/truck mpg km/hr hr/trip could be I hr/day hr/day hr/day hr/driver \$/hr \$/gal km/yr hr/trip kg/yr hr/trip kg/yr	113 owered with a 34	\$/kg H2 stroag liquid H2 pump trips per day	ge D		
ruck costs Tank unit Undercarrac Cabe ruck boil-off ruck capaci uel econom verage sper oad/unload ruck availat lour/driver river wage uel price ruck requir rips per yea otal Distance ime for eacl rip length elivered pro otal delivery	ge f rate ity vy eed time bility & benefits rement calcu ar ce h trip ce h trip couct y time			60,000 90,000 0.30 4000 6 50 4 24 122 28.75 1 1 2,319 5,173,875 8.4 12.4 48,658,030	\$/module \$/trailer \$/cab %/day kg/truck mpg km/hr hr/trip could be I hr/day hr/day hr/day hr/driver \$/hr \$/gal km/yr hr/trip kg/yr hr/trip kg/yr	113 owered with a 34	\$/kg H2 stroag liquid H2 pump trips per day	ge D		
ruck costs Tank unit Undercarrag Cabe ruck boil-off ruck capaci uel econom verage spee oad/unload our/driver river wage uel price ruck availat our/driver river wage ouel price ruck requir rips per yea otal Distanci ime for each rip length elivered pro otal delivery Total drivin	ge f rate ity vy eed time bility & benefits rement calcu ar ce h trip ce h trip couct y time			60,000 90,000 0.30 6 50 4 4 24 12 28.75 1 12,319 5,173,875 8.4 12.4 48,658,030 152,753	\$/module \$/trailer \$/cab %/day kg/truck mpg km/hr hr/trip could be I hr/day hr/driver \$/hr \$/gal km/yr hr/trip hr/trip kg/yr hr/trip kg/yr hr/yr	113 owered with a 34	\$/kg H2 stroag liquid H2 pump trips per day	ge D		
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Gaseous Hydrogen Distributed via Pipeline Final Version June 2002 IHIG Confidential

							55	mpg and	12,000 mile/yr
1 Central Plant D	1 Central Plant Design Design LHV energy equivalent A				Assuming	218	kg/yr H2/ve	ehicle or gal/yr gaso equiv	
Hy	ydrogen	gasoline	million			requires	90%	annual loa	d factor at
Size range	kg/d H2	gal/d	Btu/hr	scf/d H2	MW t	Assuming	120,000	kg/y H2 /sta	ation or gal/y gaso equiv
Maximum '	1,000,000	1,000,000	4,742	414,500,000	1,389	actual H2	10,000	kg/month H	l2 or gal/mo. gaso equiv
This run	150,000	150,000	711	62,175,000	208	or	550	vehicles ca	an be serviced at
Minimum	20,000	20,000	95	8,290,000	28	thereby	78	fill-ups/d @	4.2 kg or gal equiv/fill-up
							411	station sup	ported by this central facility

Delivery distance	150 km	key input
Number of arms	4 key input	Radiate four directions or 600 km of total pipeline key issue
Delivery pressure	440 psia	
Pipeline cost	621,504 \$/km	includes right of way costs which is the key cost issue in urban areas
Electricity cost	0.045 \$/kwh	if a booster compressor is required for long pipeline

Capital costs Pipeline Capital cost		372.9 372.9	
General Facilities & permitting	of unit cost	74.6	could be lower for pipelines
Eng. startup & contingencies	of unit cost	37.3	
Contingencies	of unit cost	37.3	
Working Capital, Land & Misc.	of unit cost	26.1	could be lower for pipelines
		548.2	
Location factor	110% of US Gulf Coast	603.0	

			\$/million		\$/kg H2 or	
Variable Operating Cost		Million \$/yr	Btu LHV	\$/k scf H2	\$/gal gaso	equiv
Variable non-fuel O&M	1% /yr of capital	6.03	1.08	0.30	0.12	could be lower for pipelines
Total variable operating costs		6.03	1.08	0.30	0.12	
Fixed Operating Cost	5% /yr of capital	30.15	5.38	1.48	0.61	could be lower for pipelines
Capital Charges	18% /yr of capital	108.54	19.35	5.31	2.20	
Total operating costs		144.72	25.80	7.09	2.94	

Gaseous Hydrogen Distributed via Tube Trailers Final Version June 2002 IHIG Confidential

Design per station					energy equivale	nt	Assuming		mpg and
		rogen	gasoline	million			requires		kg/yr H2
Size range		J/d H2	gal/d	Btu/hr	scf/d H2	MW t	Assuming		Annual a
Maximu	,	000,000	1,000,000	4,742.186	414,500,000	,	actual H2		kg/month
This ru Minimu		150,000 20,000	150,000 20,000	711.328 94.844	62,175,000 8,290,000	208.417 27.789	or thereby		FC vehi fill-ups/d
Willing		20,000	20,000	34.044	0,290,000	21.109	litereby		station s
verage delivery distance		150 k			. .				
Delivery distance		210 k	im l	40%	increase to repre	esent physical	distance		
ruck utilization		80%							
apital costs			Million \$		Notes				
Tubes & undercarrage			113.7	\$ 758	/kg/d H2, high du	ue to the	411	units left at	t stations
Cabe			27.0	\$ 180	/kg/d H2				
Total tube trailer cost			140.7						
				\$/million					
ariable Operating Cost			Million \$/yr	Btu LHV	\$/k scf H2	\$/gal gaso e	quiv		
perating costs			00.11	40 70	c	4.00			
Labor Fuel			60.44	10.78 1.57	2.96 0.43	1.23 0.18			
Variable non-fuel O&M	1% /yr of	capital	8.79 1.41	0.25	0.43	0.18		\$/yr/truck	
Total variable operating		capital	70.64	12.59	3.46	1.43	,	¢/yi/tiuck	
ixed Operating Cost	5% /yr of	capital	7.04	1.25	0.34	0.14			
Capital Charges	18% /yr of	capital	25.33	4.52	1.24	0.51	_		
Total operating costs			103.00	18.36	5.04	2.09			
Assumptions Fruck costs									
ruck costs Tube unit Undercarrage Cabe ruck capacity rressure (max) ressure (min) let delivery			90,000 300 160 30 244	\$/trailer \$/cab kg/truck key is atmosphere atmosphere kg/truck key is	ssue	\$/kg H2 desig	gn stoage @	160	atm
ruck costs Tube unit Undercarrage Cabe ruck capacity rressure (max) Pressure (min) let delivery uel economy			60,000 90,000 300 160 30 244 6	\$/trailer \$/cab kg/truck key is atmosphere atmosphere kg/truck key is mpg	ssue	\$/kg H2 desiç	gn stoage @	160	atm
ruck costs Tube unit Undercarrage Cabe Truck capacity Pressure (max) Pressure (min) let delivery uel economy werage speed			60,000 90,000 300 160 30 244 6 50	\$/trailer \$/cab kg/truck key is atmosphere atmosphere kg/truck key is mpg km/hr	ssue	\$/kg H2 desig	gn stoage @	160	atm
ruck costs Tube unit Undercarrage Cabe Pressure (max) Pressure (min) let delivery uel economy verage speed lour/driver			60,000 90,000 300 160 30 244 6 50 12	\$/trailer \$/cab kg/truck key is atmosphere atmosphere kg/truck key is mpg km/hr hr/driver	ssue				
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ruck costs Tube unit Undercarrage Cabe Truck capacity tressure (max) tressure (min) let delivery uel economy verage speed lour/driver oad/unload time ruck availability triver wage & benefits uel price ube trailer requirement ca trips per year otal distance	alculations		60,000 90,000 300 160 30 244 6 50 12 2 24 28.75 1 202,100 84,882,000	\$/trailer \$/cab kg/truck key is atmosphere atmosphere atmosphere kg/truck key is mpg km/triver hr/driver hr/driver hr/day \$/hr \$/gal trips/yr or km/yr	ssue this could be low 554	rer as just cha	inge tube trai		
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ruck costs Tube unit Undercarrage Cabe ruck capacity ressure (max) ressure (min) let delivery uel economy verage speed lour/driver oad/unload time ruck availability river wage & benefits uel price ube trailer requirement ca rips per year otal distance ime for each trip otal delivery time Total doi/unload time Total load/unload time ruck availability	alculations		60,000 90,000 300 244 6 50 12 2 24 28.75 1 202,100 84,882,000 84,882,000 84,882,000 84,697,640 1,697,640 1,697,640 300	\$/trailer \$/cab kg/truck key is atmosphere atmosphere kg/truck key is mpg km/hr hr/driver hr/trip hr/day \$/hr \$/gal trips/yr or km/yr hr/yr hr/yr hr/yr hr/yr hr/yr hr/yr hr/yr trucks but	this could be low 554 282,940	rer as just cha	nge tube trai	lers at static	ons
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Summary for Hydrogen Fueling Pathways Final Version June 2002 IHIG Confidential

Inputs Boxed in yellow	are the key input variables you must o	choose, current inputs are <u>just an examp</u>	<u>le</u>
Hydrogen Production Inputs Design hydrogen production Annual average load factor Gasoline sales/month/station Forecourt loading factor High pressure gas storage buffer		thereyb supplying "plug & play" 24 hr replacements for reasonable	e availability
Capital Cost Buildup Inputs from pr General Facilities Engineering, Permitting & Startup Contingencies Working Capital, Land & Misc. Product Cost Buildup Inputs	rocess unit costs 25% 10% 10% 7%	Engineering costs spread over mu	tiple stations
Road tax or (subsidy) Gas Station mark-up Electricity cost Non-fuel Variable O&M Fixed O&M Costs Capital Charges	 /gal gasoline ec /gal gasoline ec 0.07 \$/kwh 0.5% /yr of capital 3.0% /yr of capital 18.0% 	uivalent may be needed if H2 sales drops to \$0.060.09/kWh typical commerc 0.5-1.5% is typical, assumed low h 4-7% typicalfor insurance, taxes, G 20-25%/yr CC typical for refiners & ; about 12% IRR DCF	otal station revenues ial rate, see www.eia.doe.g ere for "plug & play" &A (may be low here)
Outputs 135,000 kg/d H2 that actual annual average 32,290	supports 226,032 FC vehicles fill-ups/d if 1 fill-up/week @ 4.2 kg/fill-up Capital Costs Absolute Unit cost Unit cost	10,000 kg/month per station supports each with Operating Cost Product Costs Fixed Variable including return on or Unit cost Unit cost Unit cost	411 stations 329 kg/d H2 capital

	Absolute	Unit cost	Unit cost	Unit cost	Unit cost	Unit cost
Delivery Method	\$ millions	\$/scf/d H2	/kg/d H2 or	\$/kg H2	\$/kg H2	\$/kg H2
Liquid H2 Gaseous Fueling System	279	13.64	1,857	0.17	0.08	1.27
Gaseous H2 via Pipeline	212	10.39	1,415	0.13	0.16	1.07
Gaseous H2 via Tube Trailer	212	10.39	1,415	0.13	0.09	1.00

Click on specific Excel worksheet tabs below for details of cost buildups for each case

Liquid Hydrogen Based Fueling Stations

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Hydrogen Fueling Station Cost	S
Delivery to	411 Stations
	Million \$/yr
Variable Operating Cost	4.16
Fixed Operating Cost	8.36
Capital Charges	50.14
Total Fueling Station Cost	62.65

Gaseous Hydrogen Based Fueling Stations - Pipeline Delivery

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Hydrogen Fueling Station Cost	S
Delivery to	411 Stations
	Million \$/yr
Variable Operating Cost	7.97
Fixed Operating Cost	6.37
Capital Charges	38.21
Total Fueling Station Cost	52.55

Gaseous Hydrogen Based Fueling Stations - Tube Trailer Delivery

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Hydrogen Fueling Station Cos	ts
Delivery to	411 Stations
	Million \$/yr
Variable Operating Cost	4.51
Fixed Operating Cost	6.37
Capital Charges	38.21
Total Fueling Station Cost	49.10

Hydrogen Conversions

		b	<mark>oxed yellow</mark> a	ire key input varia	bles	Change below	
	Basis	-				for any size	
kg H2	1.000	10	100	1,000	10,000	2,413	
Btu HHV	134,690	1,346,900	13,469,004	134,690,037	1,346,900,370	324,972,145	
Btu LHV	113,812	1,138,125	11,381,248	113,812,475	1,138,124,750	274,600,000	
H2 gas LHV/HHV	84.5%	84.5%	84.5%	84.5%	84.5%	84.5%	
standard cubic feet (scf) @ 60°F & 1 atm	414.5	4,145	41,447	414,466	4,144,664	1,000,000	
normal cubic meters (Nm3) @ 0°C & 1 atm	11.1	111	1,110	11,104	111,040	26,791	
gallons @ standard conditions of 60°F & 1 atm	3,100	31,004	310,042	3,100,424	31,004,242	7,480,520	
gallons gaseous H2 @ 400 atm & 60° F	8.53	85	853	8,526	85,262	20,571	
gallons liquid H2 phy vol @ 2 atm & -430°F	3.73	37	373	3,733	37,330	9,007	
kWh thermal equivalent LHV	33.3	333	3,335	33,347	333,468	80,457	
Assumed gasoline Btu/gal HHV	121,335	121,335	121,335	121,335	121,335	121,335	
Assumed gasoline LHV/HHV	93.8%	93.8%	93.8%	93.8%	93.8%	93.8%	
Assumed gasoline Btu/gal LHV	113,812	113,812	113,812	113,812	113,812	113,812	
gallons gasoline energy equiv LHV	1.000	10	100	1,000	10,000	2,413	

Note: Essential to use LHV gasoline equivalent due to the 2.5 times larger water vapor energy losses of H2 vs gasoline

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