Research and Development of HCNG Internal Combustion Engines

Fanhua Ma, Mingyue Wang, Xihao Li, He Zhang, Nashay Naeve and Shiuli Zhao

State Key Laboratory of Automotive Safety & Energy

Tsinghua University









发展HCNG、CNG汽车的背景和意义

Background and Significance of Developing HCNG and CNG Vehicles

• 环保节能及实现我国汽车工业跨越式发展的挑战

Environment protection, energy saving and the challenges of development of China auto industry

- ◆ 石油依赖性和国家能源安全
 Oil dependence and China's energy security
- 汽车保有量增加,污染加剧
 Vehicle population growing and environment pollution aggravating
- ✤ 未来氢能发展提供的机遇

Opportunity from hydrogen energy development in the future



发展HCNG、CNG汽车的背景和意义 Background and Significance of Developing HCNG and CNG Vehicles

● 在天然气发动机燃料中加入适量的氢气(即氢气/天然气混合气,简称 "HCNG"),可以提高混合气燃烧速度、扩大稀燃极限,从而提高发动机的热效 率、可降低排放,这是目前国内外正在研究的热点问题。 Taking hydrogen enriched compressed natural gas (HCNG) as a fuel in CNG engine can increase the burning speed, widen the lean burn limit. For its high efficiency and better emission, HCNG engine is being studied worldwide.

● 近年来,国外开展了HCNG发动机的基础研究及应用研究,其中美国、加拿大、 欧盟日本等国的研究最为活跃。在美国能源部(DOE)等支持下,美国Colorado 州立大学、HCI公司(Hydrogen Components Inc.)、加拿大Westport等单位 较早就开始了氢气/天然气发动机的研究,取得了许多研究开发及示范应用成果。 In recent years, some countries carried out the basic research on HCNG engine actively, especially in the USA, Canada, EU and Japan. With the supports of Department of Energy (DOE) etc., Colorado University HCI company (Hydrogen Components Inc.), Westport Inc. etc. started the research on HCNG engine early, and got lots of achievements of research and demonstration.



发展HCNG、CNG汽车背景和意义

Background and Significance of Developing HCNG and CNG Vehicles



Cummins – Westport's

HCNG Engine



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|------|-------------------|--------|
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| | -1911- | J.J. |
| | $\mathbf{\nabla}$ | |

HCNG buses demonstration in Sunline Transit, California, USA

| Engine | Cummins-Westport B Gas plus 6 cylinders, inline, Turbocharged and intercooled | | |
|----------------------|---|--|--|
| Bore, Stroke | 102mm, 120mm | | |
| Compression Ratio | 10.5: 1 | | |
| Displacement | 5.9 L | | |
| H2/HCNG by volume | 20% | | |
| Power | 230 BHP (172 Kw) @ 2800 RPM | | |
| Torque | 677 Nm @ 1600 RPM | | |

从天然气汽车到氢能汽车的发展路径

The Development Path from CNG Vehicles to Hydrogen Vehicles





HCNG、CNG发动机试验台 HCNG and CNG engine's Test Bench



发动机与电涡流测功相连,可测量和控制转速 与负荷。

The engine was coupled to an eddy-current dynamometer for engine speed & load measurement and control.







CNG and HCNG Engine's Experimental Systems







Three performance 、 emission experiment benches
 Reliability test base in Nanchong Dongfeng
 CVS total flow test equipment and transient test-bed
 Catalyst test bench





发动机缸内压力的测量系统 Engine's In-cylinder Pressure Measurement System



Engine

The test engine was an in-line 6-cylinder, throttle body injection one designed for city bus application. It was modified from a diesel engine by replacing fuel injector with spark plug and reshaping the piston head to reduce compression ratio.





Technical Approach of the Engine

- 电子控制CNG进气管喷射
 Electronic control CNG injection in the engine's manifold
- > 空燃比开环控制→闭环控制

 $Open \rightarrow Close - loop$ control of Air-Fuel ratio

> 电控高能点火

High-energy ignition with electronic control

- ▶ 稀薄燃烧
 - Lean burn
- > 水冷式增压器

water-cooled supercharger

氧化型催化器

Oxidation catalyst

Engine's Structural Parameter and Performance

| Туре | EQD180N-30 |
|------------------------------|---|
| Pattern | Four strokes、water-cooled、turbocharged and intercooled、single-point electronic control injection、ignition engine、 Oxidation catalyst |
| Cylinder diameter ×stroke | 105mm×120mm |
| | |
| Compression ration | 10: 1 |
| Displacement | 6.234L |
| Fuel | CNG |
| Ignition | high-energy free distributor electric control |
| Combustion Form | Lean burn |
| Rated power | 132kW/2800r/min |
| Maximum torque | 540N.m/1400r/min |
| Lowest full-load fuel | 225g/kW.h |
| 新生 Emission | Europe III |

Injected HCNG/CNG Supply System



Schematic of the fuel supply system



Schematic of the on-line hydrogen- natural gas mixing system used

Principles of HCNG on-line mixing system



At first the measured NG mass flow rate is converted to an analog voltage signal which is then transferred to a computer for further processing after A/D converting. By using the stocked control software and the input value of blending ratio as well as the received signal of NG mass flow rate, the computer then calculates out the desired hydrogen mass flow rate.

This calculated value is used as an immediate input into the hydrogen flow controller, which controls the flow rate according to the desired value through varying the openness of the integrated valve. This resulted hydrogen flow rate need to be re-checked by a high accuracy mass flow meter located downstream the flow controller. If significant difference between the measured hydrogen flow rate and previously calculated one is found, a feedback control would become active to ensure control accuracy.

掺氢对稀燃极限的影响

Effect of Hydrogen Addition on Lean Operation Limit



稀燃极限定义为平均 指示压力的循环变动 达到10%时的过量空 气系数

COVIMEP

The lean operation limit was defined as the excess air ratio at which COVIMEP reaches 10%.

掺氢比的提高可以拓宽稀燃极限,改善发动机的稀燃性能。



Hydrogen enrichment could significantly extend the lean operation limit, improve the engine's lean burn ability.

Combustion Duration



在空燃比确定的情况下,随着掺氢比的提高,燃烧持续期会缩短。 这表明,掺氢确实可以提高火焰传播速度。



At a given lambda, combustion duration shortened as hydrogen fraction increased. This illustrated that hydrogen addition could indeed speed up flame propagation.

发动机热效率和排放特性

Engine Thermal Efficiency and Emission Characteristics



At fixed ignition timing

NOx

图中λm_0和 λm_10% 分别表示 CNG和掺氢比为 10%的HCNG的稀燃 极限。

 λm_0 and $\lambda m_10\%$ in these figures represent lean limit for NG and 10% hydrogen fraction mixture respectively.

同一空燃比下,掺氢比越高,NOx排放量越大。这是因为氢气的 加入提高了燃烧温度,而高温是NOx形成的主要因素。

More hydrogen added would result in more NOx emission at a given lambda, this is thought to be caused by the elevated combustion temperature due to hydrogen addition since high temperature was a catalyst for the formation of NOx







HC

由上图可看出,掺氢可降低HC的排放,这是因为氢气可以提高火焰传播速度,减 小淬熄距离,从而降低了不完全燃烧的可能性。C浓度由于氢气的加入而有所降低 也是HC排放下降的一个原因。

Reduced HC emission by hydrogen enrichment was observed in our study which could be explained by the fact that hydrogen could speed up flame propagation and reduce quenching distance, thus decreasing the possibilities of incomplete combustion. Carbon concentration of the fuel decreased due to hydrogen addition was another reason for HC emission reduction.



n=1200rpm MAP=105kPa spark timing=30BTDC

CO

在过量空气系数小于1.7的区域,掺氢与否对于CO排放的影响不明显, 但一旦过量空气系数超过1.7,掺氢越多,CO排放越低。 这归功于氢气 良好的燃烧特性,特别是在稀燃料的情况下。

In the region where lambda was less than 1.7, adding hydrogen or not showed no significant difference on CO emission, but once lambda exceeded 1.7, more hydrogen addition resulted in much less exhaust CO. This was also attributed to hydrogen's ability to strengthen combustion, especially for lean fuel-air mixtures.



Indicated Thermal Efficiency



当过量空气系数小于1.5时,掺氢并没改善发动机的热效率,反而50% 掺氢时的热效率与纯天然气发动机相比有明显的下降。

when lambda was under 1.5, hydrogen addition was not beneficial to engine's efficiency improvement. Rather, the engine's thermal efficiency exhibited an obvious drop when fuelled by HCNG containing 50% hydrogen compared to pure NG operation.



发动机的热效率和排放特性 Engine Thermal Efficiency and Emission Characteristics



在最佳点火提前角处,掺氢可以提高发动机的热效率,高掺氢比有 着更高的热效率。

Hydrogen addition could improve thermal efficiency after spark timing optimization and that the more hydrogen added the more efficiency rise will be gained



相同指示热效率下,掺氢比增加可降低NOx排放。相同NOx排放 下比较,掺氢越多,热效率越高。



At given ITE, NOx emission decreased as the increase of hydrogen fraction and at given NOx emission, ITE increased as more hydrogen is added.



Brake specific NOx emission/ g/kwh

掺氢比增加,NOx排放与HC排放相对曲线向左下角偏移,这说明 了掺氢可降低NOx排放与HC排放相互矛盾的程度。



The trade-off curve moves further to the left-bottom as more hydrogen is added which meant that tradeoff between NOx and HC emission was indeed alleviated by hydrogen addition.

HCNG发动机在不同点火提前角下的 燃烧和排放特性

Combustion and Emission Characteristics of a Port-Injection HCNG Engine under Various Ignition Timings



不同掺氢比下指示热效率与点火提前角的关系

The Relationship between ITE and Ignition Timing at Various Hydrogen Fractions



最佳点火提前角随掺氢比增大而推迟,此外最佳点火提前角下的指示热效率随 掺氢比增加有所提高。这是因为推迟点火可减小压缩负功,提高燃烧等容度, 但传热损失量会因掺氢导致的缸内温度提高而增大。

The MBT is retarded as the hydrogen blend ratio is raised; furthermore the ITE at the MBT rises slightly. This is because retarding ignition timing can reduce the compression minus work, increase the constant volume degree, but the heat transfer can be raised by adding hydrogen to CHG due to the higher cylinder temperature

不同掺氢下的燃烧放热率曲线 MFB of the Fuel Blends



掺氢比增加燃烧放热会提前



The MFB is advanced as hydrogen addition increases.

不同掺氢比下的燃烧持续期和着火落后期

Combustion Duration and Ignition Delay versus Hydrogen Fractions



氢气百分数的增加会缩短快燃期,减少后燃期,同时提高燃料利用率。



The rapid combustion duration is shortened by increasing the hydrogen fraction which results in reducing in post-combustion and an increase in the rate of fuel utilization.

不同点火提前角下的缸内最高压力Pmax

The Maximum Cylinder Pressure P_{max} versus Ignition Timings





不同点火提前角下的缸内最高温度T_{max}

The Maximum in-cylinder Gas Temperature T_{max} versus Ignition Timings



Pmax 和 Tmax 随点火提前角的增大而有所提高,同时随着氢气含量的增加, 因燃烧速率提高和压力的快速增高, Pmax 和 Tmax 也会随之增大。



*P*max and *T*max rise with the increase of spark advance angle, and also rise with raising the hydrogen fractions due to enhanced burning velocity, and quickly elevated pressure

不同掺氢比下最大压力升高率与点火提前角的关系 Maximum rate of pressure rise of the fuel blends versus ignition timings





NOx 排放与点火提前角的关系

NOx Concentration versus Ignition Timings



点火提前角和掺氢比的增加都会使得NOx排放量有所增加。



The NOx emission rises with the increase of spark advance angle, as well as with the increase of hydrogen fractions.

不同掺氢比下HC排放与点火提前角的关系

HC Emission versus Ignition Timing at Various Hydrogen Fractions



点火提前角减小会降低HC的排放,这是因为这时后燃期显得比较突出,尾气温度提高,这会加速HC在膨胀冲程和排气管内的燃烧。

HC emission falls by decreasing the spark advance angle, because post-combustion becomes serious and the emission temperature rises, which accelerates the combustion of the HC emission in the expand stroke and the exhaust pipe.



通过HCNG燃料空燃比调整特性试验的结果对比原机燃用天然气的MAP数据,优先选择 在扭矩相近的前提下NOx比排放降低的最大空燃比点作为目标空燃比,由此得出HCNG发 动机的目标空燃比MAP图;在点火提前角的标定过程中,实际空燃比保持在HCNG发动 机的目标空燃比,在保持动力性不变的前提下尽量推迟点火,以降低NOX排放,最终得 到的点火提前角MAP图。

The calibrated air-fuel ratio and spark timing map were achieved based on the goals of the emission (especialy NOx), specific fuel consumption and power output of the HCNG engine.





HCNG (20% H2) Engine Emission Data

| | 欧IV限值 Euro data | 欧V限值 EuroV data | EEV限值 EEV data | 实测值 Measured data |
|------------------|-----------------------|-----------------------|----------------------|-------------------------|
| NOx (g/kW.h) | 3.5 | 2.0 | 2.0 | 1.18-1.60 |
| CO (g/kW.h) | 4.0 | 4.0 | 3.0 | 0.26-0.80 |
| NMHC (g/kW.h) | 0.55 | 0.55 | 0.40 | 0.09-0.20 |
| CH4 (g/kW.h) | 1.1 | 1.1 | 0.65 | 0.40-0.50 |



55%HCNG发动机燃烧和排放特性

Combustion and Emission Characteristics of a Port-Injection HCNG Engine fueled by 55% hydrogen volumetric ratio



Combustion and Emission Characteristics versus excess air ratio engine speed of 1200 rpm, Wide Open Throttle, MBT spark timing





Engine's power performance versus excess air ratio


A HILLERSTY

Max heat release rate versus excess air ratio





10% to 90% MFB burn duration versus excess air ratio



A LINERSTIT

Indicated thermal efficiency versus excess air ratio



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Brake specific CO emission versus excess air ratio



Brake specific NO_x emission versus excess air ratio



HCNG发动机怠速特性研究

Idle Characteristics of HCNG Engine



Idle Combustion and Emission Characteristics idle speed=800rpm, spark timing=20BTDC



Idle Combustion and Emission Characteristics idle speed=800rpm, spark timing=20BTDC



Idle Combustion and Emission Characteristics idle speed=800rpm, spark timing=20BTDC



Idle Combustion and Emission Characteristics, idle speed=800rpm, spark timing=20BTDC



Equivalent methane consumption versus excess air ratio



Idle Combustion and Emission Characteristics, idling speed=800rpm, λ =1.2



Idle Combustion and Emission Characteristics, idling speed=800rpm, λ =1.2



A CHARTER STATE

Indicated thermal efficiency versus ignition timings

Idle Combustion and Emission Characteristics, idling speed=800rpm, λ =1.2



NO_x emission versus ignition timings



HCNG Bus Performance







HCNG客车最高车速及加速试验









HCNG客车经济性试验









HCNG bus performance compared with CNG Bus

| | Power Performance | | Fuel Economy |
|-------------|--------------------------------|------------------------|---|
| | 0~50km/ h spped time (s) | Max Speed (km/h) | Equivalent CNG consumption (kg/100km) |
| CNG Bus | 17.9 | 84.1 | 38.97 |
| HCNG Bus | 17.9 | 84.1 | 36.11 |



Some Projects

• MOST 863 Project "HCNG engine R & D"

- MOST 863 Project "HCNG Bus R/D and Hydrogen Generation by Renewable Energy", Cooperated with DOE.
- MOST 863 Project "Key Technologies Cooperation Research on Hydrogen Utilization based on Hydrogen Infrastructure"





- "Calibration method of HCNG Engine" .
 China patent: 200710062635.
- "HCNG fuel for optimized hydrogen fraction in HCNG engine" . China patent: 200710062636.
- "Control and operation methods for different hydrogen fraction in HCNG engine" China patents: 200710175797.9





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Conclusions

- Lean burn is one of the effective approach for HCNG Engine, and Spark timing optimization is necessary.
- 15~25% Hydrogen fraction in volume of HCNG is a good range for the HCNG Engine. Primary Research results indicate that 55% Hydrogen fraction in volume of HCNG is also another choice for the HCNG Engine.
- Fueled by 20% HCNG the engine's emission can meet Euro EEV (Enhanced Environmental Vehicle) power output, fuel consumption can be kept almost unchanged compared with CNG engine.





- HCNG ENGINE IS ONE OF THE BEST TECH. APPPROACH IN AUTO TO MEET MORE STRICT EMMISSION AND ENERGY REQUIREMNENTS.
- Suggest china national and domestic government fund CNG/HCNG auto projects (especially buses) scale and level.
- Suggest as soon as possible start china national and domestic HCNG (including producer gases) demo projects in order to save energy and protect environment.



