



Direct Hydrogen PEMFC Manufacturing Cost Estimation for Automotive Applications

Fuel Cell Tech Team Review September 24, 2008

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The following report summarizes the results of a DOE funded assessment of the cost of a 80 kW (net) direct hydrogen Polymer Electrolyte Membrane (PEM) fuel cell system for transportation applications.

The results of the model should be considered only in conjunction with the assumptions used in selecting and sizing the system components. The PEM fuel cell stack and system cost analysis assumes Year 2008 technology status for individual components and projects their cost at production volumes of 500,000 vehicles/year.

In developing the system configuration and component manifest we have tried to capture all of the essential engineering components and important cost contributors. However, the system selected for costing does not claim to solve all of the technical challenges facing fuel cell transportation systems or satisfy DOE or FreedomCAR fuel cell vehicle performance targets.



Overview

This year's PEMFC cost analysis was based on minor updates to the bottom-up high-volume stack and BOP cost model developed in 2007.

Timeline

Start date: Feb 2006

Base period: May 2008

>

100% complete

Option Year 1: Feb 2009

| Barriers | | | | | |
|---|--------------------------------|--|--|--|--|
| ◆ Barriers addressed | | | | | |
| » B. Cost | » B. Cost Cost Targets (\$/kW) | | | | |
| 2008 2010 2015 | | | | | |
| Fuel Cell System 70 45 30 | | | | | |
| Fuel Cell Stack 25 15 | | | | | |
| * Manufactured at volume of 500,000 per year. | | | | | |

Budget

- Total project funding
 - » Base Period = \$415K
 - » No cost share, no contractors
- FY07 = \$214K
- ♦ FY08 = \$50K

Partners

- Project lead: TIAX
- Collaborate with ANL on system configuration and modeling
- Feedback from Fuel Cell Tech Team, Developers, Vendors



Objectives

Objectives

Overall

Bottom-up manufacturing cost assessment of 80 kW direct-H₂
 PEMFC system for automotive applications

2008

- High-volume (500,000 units/year) cost projection of ANL 2008
 PEMFC system configuration assuming an NSTFC-based MEA and a 30 μm 3M-like membrane
 - Bottom-up manufacturing cost analysis of stack and BOP components
 - Sensitivity analyses on stack and system parameters
- ◆ EOS impacts on 2007/2008 BOP costs (EOS analysis of 2005 stack completed in FY2006)

Background

This year, we updated the 2007 PEMFC cost assessment based on input from ANL on the 2008 stack performance parameters.

- In 2007, the PEMFC system configuration, materials, processes, performance assumptions and component specifications were evaluated
 - Based cost assessment on ANL 2007 PEMFC system configuration assuming an NSTFC-based MEA and a 30 μm 3M-like membrane
 - Performed bottom-up cost assessment of both stack and BOP components
- In 2008, we updated key stack performance specifications, with no change to the system layout, cell voltage, or stack operating conditions (no change to stack efficiency)
 - Revised power density and Pt loading based on ANL inputs
 - Gross stack power density = 716 mW/cm² (2007 = 753 mW/cm²)
 - Total Pt loading = 0.25 mg/cm² (2007 = 0.3 mg/cm²)
 - Gross stack power = 86.9 kW (2007 = 86.4 kW)



Approach Overall Cost Assessment

Manufacturing cost estimation involves technology assessment, cost modeling, and industry input to vet assumptions and results.

Technology Assessment

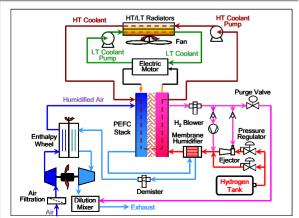
- Perform Literature Search
- Outline Assumptions
- Develop System
 Requirements and
 Component Specifications
- Obtain Developer Input

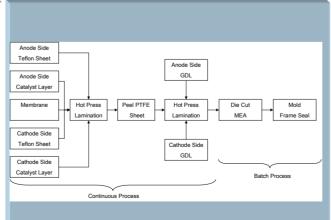
Cost Model and Estimates

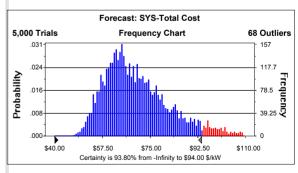
- Develop Bulk Cost Assumptions
- Develop BOM
- Specify Manufacturing Processes and Equipment
- Determine Material and Process Costs

Overall Model Refinement

- Obtain Developer and Industry Feedback
- Revise Assumptions and Model Inputs
- Perform Sensitivity Analyses



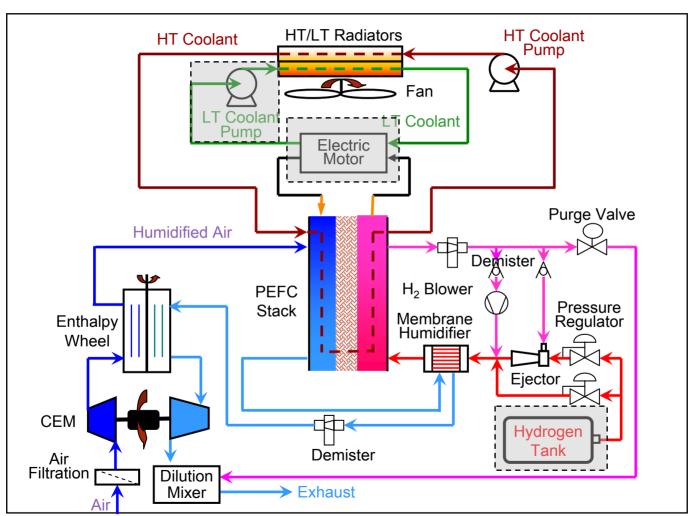






Approach System Configuration

We worked with Argonne National Laboratory (ANL) to define the 2008 system configuration, performance and component specifications¹.



Not included in the fuel cell system cost assessment

¹ R. K. Ahluwalia, X. Wang and R. Kumar, Fuel Cell Systems Analysis, 2008 USDOE Hydrogen Program Review, Arlington, VA, June 9-13, 2008.



Approach Costing Methods

We used a bottom-up approach to determine high-volume (500,000 units/year) manufacturing cost for the major stack and BOP components.

Stack Components

- Catalyst Coated Membrane
- Flectrodes
- Gas Diffusion Layer (GDL)
- Membrane Electrode Assembly (MEA)
- Bipolar Plates
- Seals
- » Develop production process flow chart for key subsystems and components
- » Obtain raw material prices from potential suppliers
- Estimate manufacturing costs using TIAX cost models (capital equipment, raw material costs, labor rates)

BOP Components

- Radiator
- Membrane Humidifier (MH)
- Enthalpy Wheel Humidifier (EWH)
- Compressor-Expander-Module (CEM)
- H₂ Blower
- » Develop Bill of Materials (BOM)
- » Obtain raw material prices from potential suppliers
- » Develop production process flow chart for key subsystems and components
- » Estimate manufacturing costs using TIAX cost models and Boothroyd Dewhurst Design for Manufacturing & Assembly (DFMA®) software
- We used experience-based estimates for stack components such as sensors, controls, control board and wire harness. We also used experience-based estimates for BOP components such as the enthalpy wheel motor, H₂ ejectors, radiator fan, coolant pump, valves and regulators.
- We used the TIAX technology-based cost model for the radiator, MH and EWH, while we used DFMA® software for the CEM and H₂ blower.



We used two different bottom-up costing tools to perform the cost analysis on the BOP components.

Costing Tools

- TIAX Technology-Based Cost Model
 - Radiator
 - Enthalpy Wheel Humidifier
 - Membrane Humidifier
- DFMA[®] Concurrent Costing Software
 - Compressor Expander Module
 - H₂ Blower

¹ We used experience-based estimates (as opposed to bottomup costing) for components such as the enthalpy wheel motor, H₂ ejectors, radiator fan, coolant pump, valves and regulators.



TIAX Technology-Based Cost Model

- Defines process scenarios according to the production volume
- Easily defines both continuous as well as batch processes
- Breaks down cost into various categories, such as material, labor, utility, capital, etc.
- Assumes dedicated process line yields higher cost at low production volumes

DFMA® Concurrent Costing

- Has a wide range of built-in manufacturing databases for traditional batch processes, such as casting, machining, injection molding, etc.
- Initially developed for the automotive industry; not well suited for processes used in manufacture of PEMFC stacks
- Does not assume dedicated process line yields lower cost at low production volumes

Approach BOP Economies of Scale

For the EOS analysis, we developed three production scenarios - pilot plant, semi-scaled, and full-scaled - to represent a phased advance from proof-of-concept to mature manufacturing process.

- Pilot Plant
 - Low volume production
 - Proof-of-concept of the manufacturing process
 - Goal is to adapt the manufacturing process to high volume production
- Semi-Scaled
 - Low-to-medium volume production
 - Adapted manufacturing process
 - Goal is to validate the manufacturing process for high volume production
- Full-Scaled
 - High volume production
 - Mature manufacturing process
 - Goal is to sustain a low-cost, high-throughput, high-reliability manufacturing process

Material price, process type, process parameters, choice of equipment and level of automation (i.e. equipment capital cost) were varied across each of the three scenarios.



Results Stack Material Assumptions

To be consistent with the 3M-like stack design, we made the following material assumptions for the cost projection.

| Component | Parameter | Selection |
|--------------------------------|-----------|---|
| Membrane | Material | 3M PFSA (EW=825) |
| Wembrane | Supported | No |
| | Catalyst | Ternary PtCo _x Mn _y alloy |
| Electrodes (Cathode and Anode) | Туре | Nano-Structured Thin Film |
| | Supported | Organic whiskers |
| Coo Diffusion Lover (CDL) | Material | Woven carbon fiber |
| Gas Diffusion Layer (GDL) | Porosity | 70% |
| Bipolar Plate | Туре | Expanded graphite foil |
| Seal | Material | Viton® |

There are no differences between the material assumptions for the 2007 and 2008 PEMFC stack.



Results Stack Performance Assumptions

Stack performance assumptions were updated by ANL based on their modeling of an NSTFC-based MEA and a 30 μ m 3M-like membrane.

| Key Stack Performance | 2005 ¹ | 2007 ^{2,3} | 20084 | |
|----------------------------|----------------------------|---------------------|-------|-------|
| Net power | kW_e | 80 | 80 | 80 |
| Gross power | kW _e | 89.5 | 86.4 | 86.9 |
| Gross power density | mW/cm ² | 600 | 753 | 716 |
| Cell voltage (rated power) | Cell voltage (rated power) | | 0.68 | 0.685 |
| Pt loading (total) | mg/cm ² | 0.75 | 0.30 | 0.25 |
| Membrane thickness | μm | 50 | 30 | 30 |
| Stack temperature | °C | 80 | 90 | 90 |
| Pressure (rated power) | atm | 2.5 | 2.5 | 2.5 |
| Stack eff. (rated power) | % LHV | 52 | 54 | 54 |

¹ E.J. Carlson et al., Cost Analysis of PEM Fuel Cell Systems for Transportation, Sep 30, 2005, NREL/SR-560-39104



² R.K. Ahluwalia and X. Wang, Reference Fuel Cell System Configurations for 2007: Interim Results, ANL, Feb. 6, 2007

³ R.K. Ahluwalia, X. Wang and R. Kumar, Fuel Cell Systems Analysis, DOE Hydrogen Program Review, May 15-18, 2007

⁴ R. K. Ahluwalia, X. Wang and R. Kumar, Fuel Cell Systems Analysis, 2008 USDOE Hydrogen Program Review, Arlington, VA, June 9-13, 2008

Results Stack Specifications

We developed stack specifications consistent with the performance assumptions.

| TIAX Assumptions | Units | 2005 ¹ | 2007 | 2008 |
|-----------------------------|--------------------------|-------------------|----------------|----------------|
| Production volume | units/yr | 500,000 | 500,000 | 500,000 |
| Pt price | \$/g (\$/tr.oz.) | 29.0 (900) | 35.4 (1100) | 35.4 (1100) |
| Number of stacks | # | 2 | 2 | 2 |
| Number of cells per stack | # | 231 | 221 | 219 |
| Active cell area | % Total cell area | 85% | 85% | 85% |
| Active area per cell | cm ² | 323 | 260 | 277 |
| Cell pitch | cells/inch (cells/cm) | 9.55 (3.76) | 9.75 (3.84) | 9.75 (3.84) |
| Stack voltage (rated power) | V | 150 | 150 | 150 |

¹ E.J. Carlson et al., Cost Analysis of PEM Fuel Cell Systems for Transportation, Sep 30, 2005, NREL/SR-560-39104

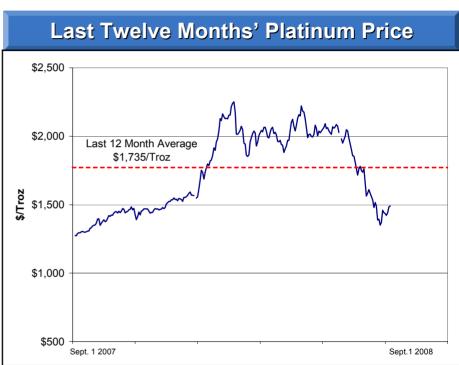
We assumed a Pt price of \$1,100/tr.oz. for the baseline analysis and captured the impact of variation in Pt price through single- and multivariable sensitivity analyses.



Results Historic Pt Price

Platinum at \$1,100/tr.oz. is close to the average price (\$1,059/tr.oz.) over the last five years.



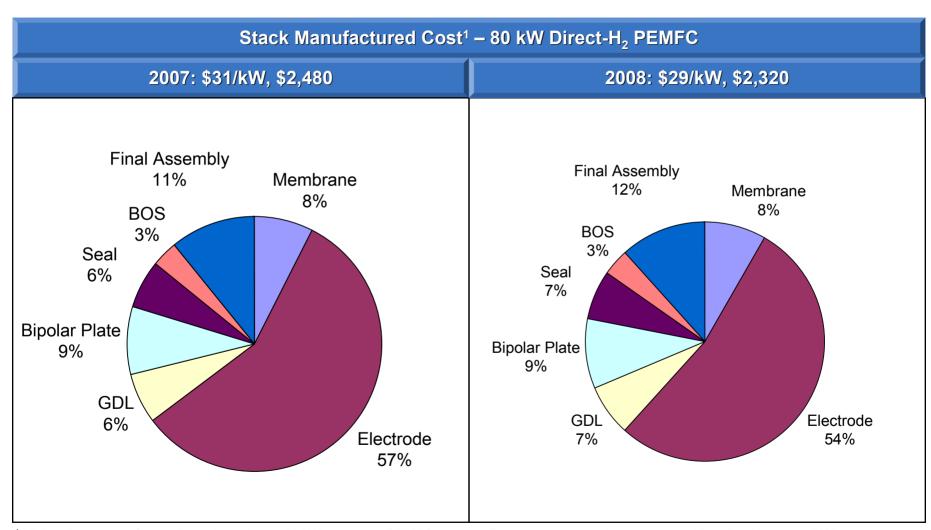


The Pt price averaged over the last 12 months is ~ \$1,735/tr.oz.



Results Stack Cost Breakout

The electrodes represent approximately 54% of the \$29/kW fuel cell stack cost in 2008.



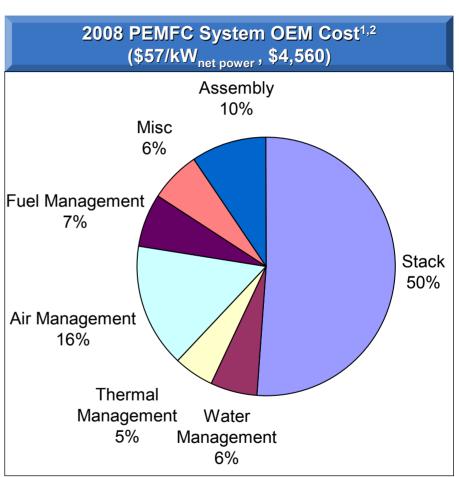
¹ High-volume manufactured cost based on a 80 kW net power PEMFC system. Does not represent how costs would scale with power (kW).



Both stack and BOP component costs are significantly reduced from the 2005 cost assessment.

| PEMFC System Cost ¹ (\$/kW) | 2005 OEM Cost | 2007 OEM Cost ^{1,2} | 2008 OEM Cost ^{1,2} |
|--|---------------------|------------------------------------|------------------------------------|
| Stack | 67 | 31 | 29 |
| Water Management | 8 | 3.3 | 3.3 |
| Thermal Management | 4 | 2.8 | 2.8 |
| Air Management | 14 | 8.9 | 8.9 |
| Fuel Management | 4 | 3.8 | 3.8 |
| Miscellaneous | 7 | 3.1 | 3.1 |
| Assembly | 4 | 5.5 | 5.5 |
| Total | 108 | 59 | 57 |

¹ High-volume manufactured cost based on a 80 kW net power PEMFC system. Does not represent how costs would scale with power (kW).



BOP and assembly costs together represent ~ 50% of the PEMFC system cost in 2008, as compared to ~ 38% in 2005.



² Assumes 15% markup to the automotive OEM for BOP components

Results BOP Cost

The high-volume factory cost for the 2007/2008 BOP components is projected to be \$1,350.

| BOP Sub- system | Component | Technology Basis | Factory Cost ¹ , \$ (without supplier markup) | OEM Cost ¹ , \$ (with 15% supplier markup) |
|-----------------------|-------------------------------------|------------------|--|--|
| | Enthalpy wheel air-humidifier | Emprise | 160 | 184 |
| Water Management | Membrane H ₂ -humidifier | PermaPure | 58 | 66 |
| Wanagement | Other | - | 10 | 10 |
| | Automotive tube-fin radiator | Modine | 57 | 65 |
| Thermal | Radiator fan² | - | 35 | 35 |
| Management Coolant pu | Coolant pump ³ | - | 120 | 120 |
| | Other | - | 5 | 5 |
| Air | Compressor-Expander-Motor (CEM) | Honeywell | 535 | 615 |
| Management | Other | - | 97 | 97 |
| | H ₂ blower | Parker Hannifin | 193 | 222 |
| Fuel Management | H₂ ejectors⁴ | - | 40 | 40 |
| | Other | | 41 | 41 |
| TOTAL | | | 1351 | 1500 |

¹ High-volume manufactured cost based on a 80 kW net power PEMFC system.

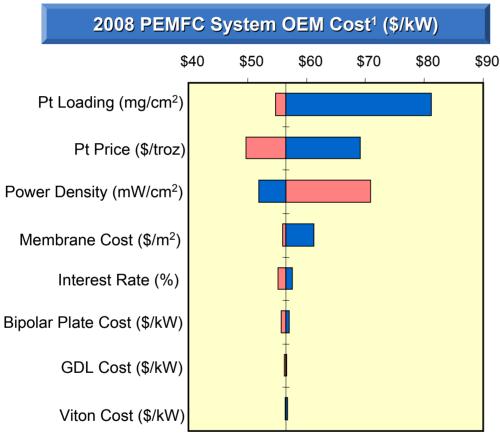
² Assumes \$35/unit based on automotive radiator vendor catalog price, scaled for high volume production

³ Assumes \$120/unit, based on 2005 PEMFC Costing Report: E.J. Carlson et al., Cost Analysis of PEM Fuel Cell Systems for Transportation, Sep 30, 2005, NREL/SR-560-39104

⁴ Assumes \$20/unit, and 2 ejectors, based on 2005 PEMFC Costing Report: E.J. Carlson et al., Cost Analysis of PEM Fuel Cell Systems for Transportation, Sep 30, 2005, NRFL/SR-560-39104

Results 2008 Stack Single Variable Sensitivity

Pt loading, power density, and Pt cost are the top three drivers of the PEMFC system cost¹.



| # | Variables | Min. | Max. | Base | Comments |
|---|----------------------------------|------|------|------|--|
| 1 | Pt Loading (mg/cm²) | 0.2 | 0.75 | 0.25 | Minimum: DOE 2015 target ² ; Maximum: TIAX 2005 report ³ |
| 2 | Pt Cost (\$/tr.oz.) | 450 | 2250 | 1100 | Minimum: ~ 108-year min. in 2007 \$ ⁴ ; Maximum: 12-month maximum LME price ⁵ |
| 3 | Power Density (mW/cm²) | 350 | 1000 | 716 | Minimum: industry feedback; Maximum: DOE 2015 target ² . |
| 4 | Membrane Cost (\$/m²) | 10 | 50 | 16 | Minimum:GM ⁶ study; Maximum: DuPont ⁷ projection from 2002 |
| 5 | Interest Rate | 8% | 20% | 15% | Based on industry feedback |
| 6 | Bipolar Plate Cost (\$/kW) | 1.8 | 3.4 | 2.7 | Based on component single variable sensitivity analysis |
| 7 | GDL Cost (\$/kW) | 1.7 | 2.2 | 2.0 | Based on component single variable sensitivity analysis |
| 8 | Viton Cost (\$/kg) | 39 | 58 | 48 | Based on industry feedback |

^{1.} High-volume manufactured cost based on a 80 kW net power PEMFC system. Does not represent how costs would scale with power (kW). Assumes a % markup to automotive OEM for BOP components.

^{7.} Curtin, D.E., "High volume, low cost manufacturing process for Nafion membranes", 2002 Fuel Cell Seminar, Palm Springs, Nov 2002



^{2.} http://www1.eere.energy.gov/hydrogenandfuelcells/mypp/pdfs/fuel_cells.pdf

^{3.} Carlson, E.J. et al., "Cost Analysis of PEM Fuel Cell Systems for Transportation", Sep 30, 2005, NREL/SR-560-39104

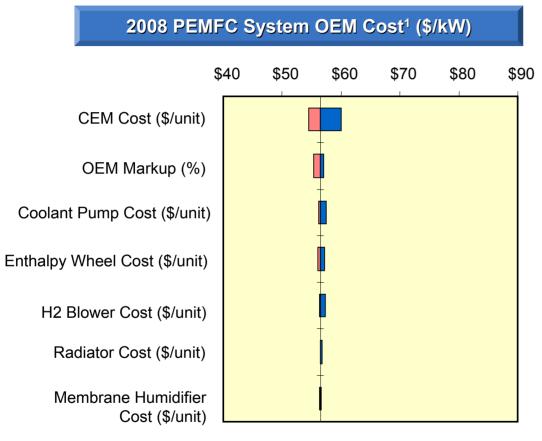
^{4.} www.platinum.matthey.com

^{5.} www.metalprices.com

^{6.} Mathias, M., "Can available membranes and catalysts meet automotive polymer electrolyte fuel cell requirements?", Am. Chem. Soc. Preprints, Div. Fuel Chem., 49(2), 471, 2004

Results 2007/2008 BOP Single Variable Sensitivity

Among the BOP components, the CEM has the greatest impact on the PEMFC system cost¹.



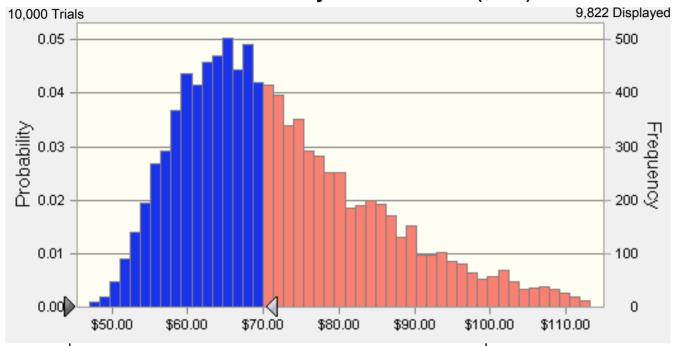
| # | Variables | Min. | Max. | Base | Comments |
|---|---|------|------|------|---|
| 1 | CEM Cost (\$/unit) | 368 | 808 | 535 | Based on component single variable sensitivity analysis |
| 2 | OEM Markup | 5% | 20% | 15% | Based on industry feedback |
| 3 | Coolant Pump Cost (\$/unit) | 80 | 200 | 120 | Based on industry feedback |
| 4 | Enthalpy Wheel Cost (\$/unit) | 123 | 217 | 160 | Based on component single variable sensitivity analysis |
| 5 | H2 Blower Cost (\$/unit) | 178 | 259 | 193 | Based on component single variable sensitivity analysis |
| 6 | Radiator Cost (\$/unit) | 46 | 71 | 56 | Based on component single variable sensitivity analysis |
| 7 | Membrane Humidifier Cost (\$/unit) | 46 | 62 | 58 | Based on component single variable sensitivity analysis |



¹ High-volume manufactured cost based on a 80 kW net power PEMFC system. Does not represent how costs would scale with power (kW). Assumes a % markup to automotive OEM for BOP components.

Monte Carlo analysis shows that the high-volume PEMFC system OEM cost ranges between \$45/kW and \$101/kW ($\pm 2\sigma$).





| Cost ¹ | \$/kW |
|-------------------|-------|
| Mean | 73 |
| Median | 70 |
| Std. Dev. | 14 |
| TIAX Baseline | 57 |



TIAX Baseline Median Mean \$57/kW \$73/kW \$70/kW 2σ

¹ High-volume manufactured cost based on a 80 kW net power PEMFC system. Does not represent how costs would scale with power (kW). Assumes a % markup to automotive OEM for BOP components.

The 2008 PEMFC stack and system costs are \sim 15-30% higher than the DOE 2010 cost targets.

| PEMFC Sub-System | Factory Cost ¹ , \$/kW (without supplier markup) | OEM Cost ^{1,2} , \$/kW (with 15% supplier markup) | DOE 2010 Cost Target³, \$/kW |
|--|---|---|---------------------------------|
| Stack | 2 | 9 | 25 |
| Balance of Plant | 26 | 28 | 20 |
| Water management (enthalpy wheel, membrane humidifier) | 2.8 | 3.3 | |
| Thermal management (radiator, fan, pump) | 2.7 | 2.8 | |
| Air management (CEM, motor controller) | 7.9 | 8.9 | 5 |
| Fuel management (H ₂ blower, H ₂ ejectors) | 3.4 | 3.8 | |
| Miscellaneous and assembly | 8 | .6 | |
| Total System | 55 | 57 | 45 |

³ FreedomCAR targets are \$20/kW for the stack and \$35/kW for the total system.



¹ High-volume manufactured cost based on a 80 kW net power PEMFC system. Does not represent how costs would scale with power (kW).

² Assumes 15% markup to the automotive OEM for BOP components

While our focus is on cost, we also independently evaluated power density and specific power for the stack and system.

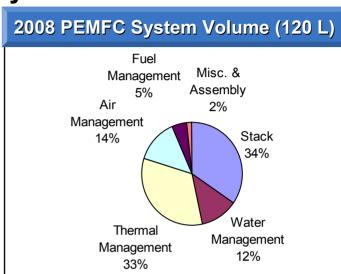
| | | | |
|--|----------------------------|-------------|--------------------|
| PEMFC Sub-System | Volume ¹ (L) | Weight (kg) | DOE 2010 Target |
| Stack | 41 | 44 | |
| Power density ^{1,2} (W _e /L) | 1,9 | 40 | 2,000 |
| Specific power ² (W _e /kg) | 1,8 | 03 | 2,000 |
| Balance of Plant | 79 | 71 | |
| Water management (enthalpy wheel, membrane humidifier) | 15 | 11 | |
| Thermal management (radiator, fan, pump) ³ | 40 | 16 | |
| Air management (CEM, motor controller) | 17 | 21 | |
| Fuel management (H ₂ blower, H ₂ ejectors) | 5 | 7 | |
| Miscellaneous and assembly | 2 | 15 | |
| Total System | 120 | 115 | |
| Power density ^{1,2} (W _e /L) | 668 | | 650 |
| Specific power ² (W _e /kg) | 69 | 4 | 650 |



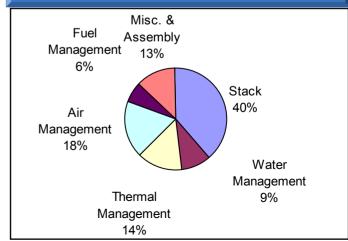
² Based on stack net power output of 80 kW, and **not** on the gross power output of 86.9 kW

³ The radiator fan and coolant pump were in the Misc. category in 2005 and 2007





2008 PEMFC System Weight (115 kg)



Future Work

We will obtain industry feedback on our 2008 input assumptions and cost results and write a comprehensive, peer-reviewable report covering our 2007 PEMFC cost analysis.

- Prepare a comprehensive report on the 2007 PEMFC cost analysis (high-volume, bottom-up stack and BOP cost)
- Interview developers and stakeholders for feedback on 2008 PEMFC performance and cost assumptions and overall results
- Incorporate feedback into stack and BOP bottom-up cost models



Thenk You

Questionsp



2008 stack costs on a per kW basis are slightly lower than the 2007 stack costs primarily due to the decreased Pt loading.

| Manufactured Cost¹, \$/kW | 2005 | 2007 | 2008 | 2010 DOE Target | Cost drivers / Comments |
|------------------------------|------|------|------|-----------------------|--|
| Membrane | 4 | 2 | 2 | | Power density changed from 600 mW/cm ² (2005), to |
| Electrodes | 52 | 18 | 16 | | 753 mW/cm ² (2007), to 716 mW/cm ² (2008) |
| GDL | 3 | 2 | 2 | 40 | Pt loading decreased from 0.75 mg/cm ² (2005), to 0.3 mg/cm ² (2007), to 0.25 mg/cm ² (2008) |
| Seal | 1 | 2 | 2 | 10 | Woven carbon fiber cost decreased from \$30/kg (2005) to \$20/kg (2007 & 2008) Changed window frame from nitrile rubber (\$5/lb, 2005) to Viton® (\$20/lb, 2007 & 2008) |
| Bipolar plates | 3 | 3 | 3 | 5 | |
| BOS | 1 | 1 | 1 | | Includes stack manifold, bolts, end plates, current collector |
| Final Assembly | 2 | 3 | 3 | | 2007 & 2008 cost includes QC but not stack conditioning, while 2005 cost includes neither |
| Total ² | 67 | 31 | 29 | 25 | |

¹ High-volume manufactured cost based on a 80 kW net power PEMFC system. Does not represent how costs would scale with power (kW). Estimates are not accurate to the number of significant figures shown.

² Results may not appear to calculate due to rounding of the 2005, 2007, and 2008 cost results.



2008 stack costs on an active area basis are slightly lower than the 2007 stack costs primarily due to the decreased Pt loading.

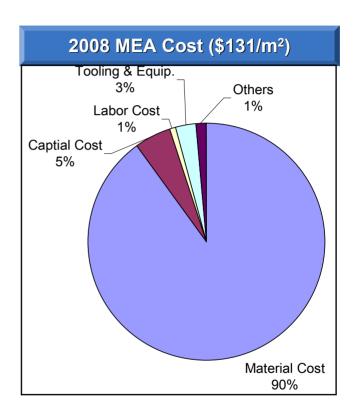
| Component | 2005 Cost ¹ (\$/m²) | 2007 Cost¹ (\$/m²) | 2008 Cost¹ (\$/m²) | Cost drivers / Comments | | | |
|----------------------------|--------------------------------------|--------------------------|--------------------------|---|--|--|--|
| Membrane | 23 | 16 | 16 | 30 μm unsupported membrane; DOE 2010 target = \$20/m² | | | |
| Electrode | 279 | 120 | 102 | Pt cost increased from \$900/tr.oz. (2005) to \$1100/tr.oz. (2007, 2008); Pt loading decreased from 0.75 mg/cm² (2005) to 0.3 mg/cm² (2007) to 0.25 mg/cm² (2008); power density changed from 600 mW/cm² (2005), to 753 mW/cm² (2007), to 716 mW/cm² (2008) | | | |
| GDL | 18 | 13 | 13 | Woven carbon fiber cost decreased from \$30/kg (2005) to \$20/kg (2007 & 2008) | | | |
| Bi-polar plate | N/A | N/A | N/A | All plates have cooling channels | | | |
| Bipolar plate with cooling | 17 | 18 | 18 | | | | |
| Seal | 6 | 13 | 13 | Changed window frame from nitrile rubber (\$5/lb, 2007) to Viton® (\$20/lb, 2007 & 2008) | | | |
| BOS | 6 | 6 | 6 | | | | |
| Final Assembly | 10 | 23 | 23 | 2007 & 2008 cost includes QC but not conditioning, while 2005 cost includes neither | | | |
| Total | 361 | 210 | 191 | | | | |

In 2005, material costs were higher for the membrane (2 mil), electrodes (Pt loading = 0.75 mg/cm²) and GDL (woven carbon fiber = \$30/kg).



Material costs dominate the manufactured cost of the stack components. For example, materials make up 90% of the total MEA cost.

| Manufactured Cost | 2007 MEA ¹ (\$/m ²) | 2008 MEA ¹ (\$/m ²) |
|---------------------------------------|---|---|
| Material - Membrane - Electrode - GDL | 135.48 - 13.89 - 109.61 - 11.98 | 117.71 - 13.83 - 91.90 - 11.98 |
| Capital Cost | 7.08 | 6.57 |
| Labor | 0.99 | 1.02 |
| Tooling & Equipment | 3.80 | 3.73 |
| Other ² | 1.73 | 1.71 |
| Total | 149 | 131 |



In 2007, the MEA cost was higher due to higher Pt loading (0.3 mg/cm²) in 2007 vs. 0.25 mg/cm² in 2008).

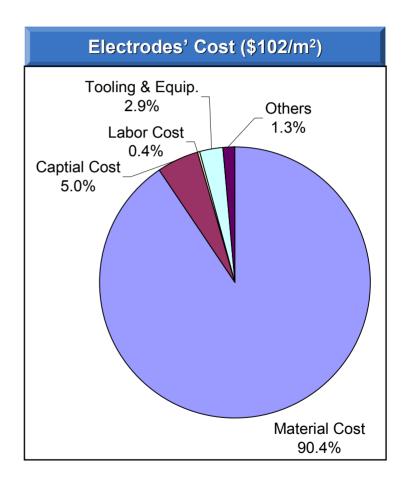


¹ m² of active area and kW of net power² Other costs include utilities, maintenance, and building

Platinum price dominates the electrode costs. We have assumed Pt price to be \$1,100/tr.oz. or \$35.4/g.

| Manufactured Cost | Anode ¹ (\$/m ²) | Cathode ¹ (\$/m ²) | Total¹ (\$/m²) | |
|----------------------|--|--|-------------------|--|
| Material | 31.19 | 60.71 | 91.90 | |
| Capital Cost | 1.86 | 3.26 | 5.12 | |
| Labor | 0.17 | 0.20 | 0.37 | |
| Tooling | 1.13 | 1.82 | 2.95 | |
| Other ² | 0.510 | 0.79 | 1.329 | |
| Total | 35 | 67 | 102 | |

¹ m² of active area



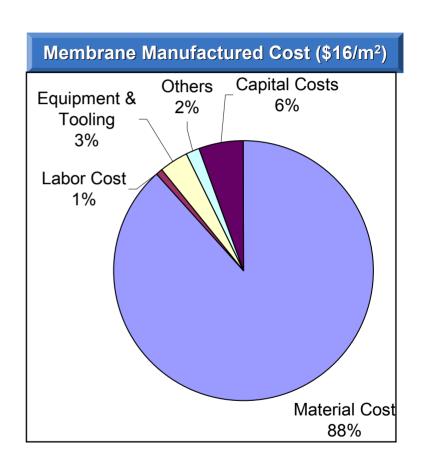


² Other costs include utilities, maintenance, and building

The estimated membrane cost on an active area basis is \$16/m², with material cost representing about 88% of the total cost.

| Membrane Manufactured Cost ¹ | | | | | | | |
|---|-------------------|---------|---------|---------|--|--|--|
| Component | Material | | Process | | | | |
| | (\$/m²) | (\$/kg) | (\$/m²) | (\$/kg) | | | |
| Film Handling | 0.31 | 6.71 | 0.23 | 5.01 | | | |
| Coating | 11.70 | 254.38 | 0.39 | 8.54 | | | |
| Drying & Cooling | 0.00 | 0.00 | 1.02 | 22.25 | | | |
| Quality Control | 0.00 | 0.00 | 0.07 | 1.47 | | | |
| Laminating | 0.00 | 0.00 | 0.06 | 1.28 | | | |
| Packaging | 1.82 | 39.61 | 0.07 | 1.61 | | | |
| Subtotal | 13.83 301.85 1.85 | | | 40.15 | | | |
| Total | 15.68 (\$/m²) | | | | | | |
| | 340.85 (\$/kg) | | | | | | |

¹ Manufactured cost on an active area basis or per kg of finished membrane basis (accounts for scrap and yield)



In 2005, the membrane cost was \$23/m² due to higher material costs (2 mil) and higher process costs (double pass required for coating).



The total capital investment on membrane equipment is about \$20 million to meet the requirement of 500,000 vehicles annual production.

- 500,000 vehicles would require 6 million square meter of membrane annually
 - Stack gross power = 86.9 kW
 - Stack power density = 716 mW/cm²
 - ➤ Downtime ~ 20%
 - ➤ Yield assumption ~ 95%
- Operating 3 shifts (20 hours)/day, 240 days/year
 - ➤ Required production rate is ~ 4,167 stacks/day
- A single coating line (1.2 mil membrane) is estimated to cost about \$6 million and a total of 3 lines would be required to meet this annual production.

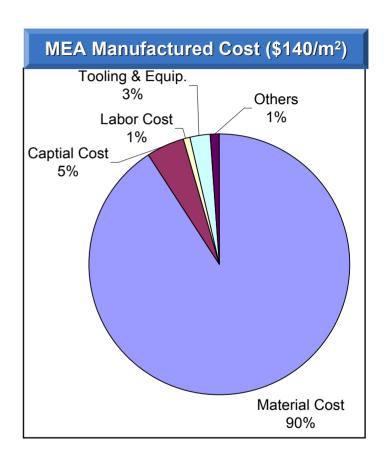
The 1.2 mil membrane needs only a single pass to complete the coating process; this may lead to a lower failure rate and higher yield assumption.

Backup Slides 2008 Membrane Electrode Assembly Cost

On an active area basis, the MEA and seal together cost \$140/m².

| Manufactured Cost ¹ | MEA (\$/m²) | Frame Seal (\$/m²) | | |
|---------------------------------------|---|--------------------|--|--|
| Material - Membrane - Electrode - GDL | 117.71 - 13.89 - 91.90 - 11.98 | 5.03 | | |
| Capital Cost | 6.57 | 1.27 | | |
| Labor | 1.02 | 0.93 | | |
| Tooling & Equipment | 3.73 | 1.10 | | |
| Other ² | 1.71 | 0.50 | | |
| Subtotal | 130.74 | 8.83 | | |
| Total | 139.57 | | | |

¹ Manufactured cost on an active area basis



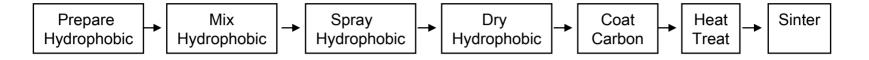
In 2005, the MEA and seal cost was \$325/m² due to higher material costs for the membrane (2 mil), electrodes (Pt loading = 0.75 mg/cm²) and GDL (woven carbon fiber = \$30/kg).



² Other costs include utilities, maintenance, and building

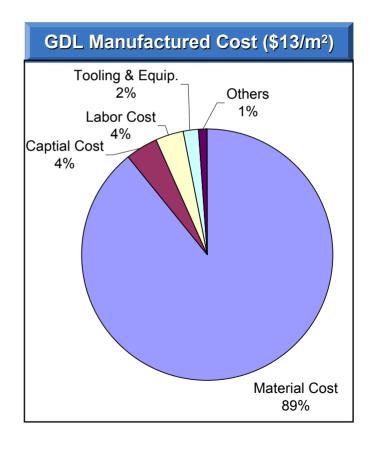
Backup Slides 2008 Gas Diffusion Layer Cost

The anode GDL has the same cost as the cathode GDL, of \sim \$13/m².



| Manufactured Cost¹ | GDL (\$/m²) |
|-----------------------|----------------|
| Material | 11.98 |
| Capital Cost | 0.57 |
| Labor | 0.52 |
| Tooling | 0.24 |
| Other ² | 0.16 |
| Total | 13.47 |

¹ Manufactured cost on an active area basis

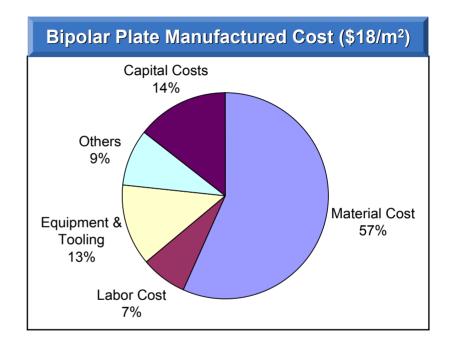




² Other costs include utilities, maintenance, and building

We estimate the expanded graphite foil bipolar plate cost is \$18/m² at high volume.

| Bipolar Plate Manufactured Cost¹ (\$/m²) | | | | | | | |
|--|----------|---------|--|--|--|--|--|
| Component | Material | Process | | | | | |
| Roll Form | 10.24 | 0.97 | | | | | |
| Impregnation | | 1.09 | | | | | |
| Calendar | | 0.70 | | | | | |
| Compression Molding | | 2.25 | | | | | |
| Die Cut | | 0.60 | | | | | |
| Curing | | 2.11 | | | | | |
| Subtotal | 10.24 | 7.70 | | | | | |
| Total | 17.94 | | | | | | |



We assumed a raw graphite flake cost of \$1.2/lb and expanded graphite flake cost of \$2/lb.



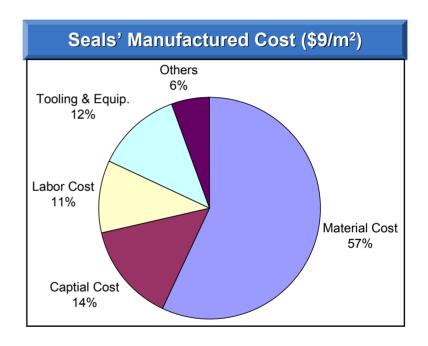
¹ Manufactured cost on an active area basis

Transfer molding is used to fabricate the seals between the MEA and bipolar plate (cooling plate).

Transfer Molding Bipolar Plate Gasket

| Manufactured Cost ¹ | Seals (\$/m²) |
|-----------------------------------|------------------|
| Material | 5.03 |
| Capital Cost | 1.27 |
| Labor | 0.93 |
| Tooling | 1.10 |
| Other ² | 0.50 |
| Total | 8.83 |

¹ Manufactured cost on an active area basis



The seal material is Viton® which costs about \$20/lb.



² Other costs include utilities, maintenance, and building

Detailed results of 2008 fuel cell stack cost breakdown.

| | Active Area Basis ¹ | | | | | | | | | |
|--------------------------|----------------------------------|---------------------|-------------------------|------------------------------------|-------------------------------------|--|---------|--|--|--|
| Stack Costs ² | | MtI Cost (\$/m²) | Process Cost (\$/m²) | Total Cost (\$/m ²) | Unit Cell Weight/Area (g/cm²) | Total Fuel Cell Module Weight | Cell | Total Fuel Cell Module Process Cost (\$) | Total Fuel Cell Module Cost (\$) | Total Fuel Cell Module Cost ² (\$/kW) |
| | Anode GDL | \$6.0 | \$0.7 | \$6.7 | 0.02 | 3 | \$73 | \$9 | \$82 | \$1 |
| | Anode Active Layer | \$31.2 | \$3.7 | \$34.8 | 0.00 | 0 | \$379 | \$44 | \$423 | \$5 |
| MEA | Electrolyte | \$13.8 | \$1.8 | \$15.7 | 0.00 | 1 | \$168 | \$22 | \$190 | \$2 |
| | Cathode Active Layer | \$60.7 | \$6.1 | \$66.8 | 0.00 | 0 | \$737 | \$74 | \$811 | \$10 |
| | Cathode GDL | \$6.0 | \$0.7 | \$6.7 | 0.02 | 3 | \$73 | \$9 | \$82 | \$1 |
| MEA Total | | \$117.7 | \$13.1 | \$130.8 | 0.05 | 7 | \$1,429 | \$159 | \$1,588 | \$20 |
| Bi | ipolar Coolant Plate | \$10.2 | \$7.7 | \$17.9 | 0.10 | 24 | \$124 | \$93 | \$218 | \$3 |
| Bi | ipolar Interconnect ² | \$0.0 | \$0.0 | \$0.0 | 0.24 | 0 | \$0 | \$0 | \$0 | \$0 |
| | Gaskets | | | | | 1 | \$78 | \$80 | \$158 | \$2 |
| | End Plates | | | | | 2 | \$4 | \$6 | \$10 | \$0.1 |
| | Current Collector | | | | | 1 | \$1 | \$2 | \$4 | \$0 |
| | Insulator | | | | | 1 | \$8 | \$9 | \$18 | \$0 |
| Outer Wrap | | | | | | 3 | \$8.9 | \$13.7 | \$22.6 | \$0.28 |
| Tie Bolts | | | | | | 3 | \$22 | \$2 | \$24 | \$0 |
| Final Assy | | | | | | | | \$273 | \$273 | \$3 |
| | Total Unit Cell | \$127.9 | \$20.8 | \$148.7 | 0.22 | 40 | \$1,676 | \$638 | \$2,314 | \$29 |

¹ Manufactured cost on an active area basis



² High-volume manufactured cost based on a 80 kW net power PEMFC system. Does not represent how costs would scale with power (kW).

We analyzed the manufactured cost of the PEM fuel cell Balance of Plant (BOP) at different production volumes based on the 2007 BOP configuration and sizing/specifications.

- At low production volumes, material and processing costs will not benefit from Economies of Scale (EOS), making the overall system more expensive than at high volumes.
- Stack components, because of their large number and compatibility with continuous processes, will realize EOS sooner than BOP components. (We completed the EOS analysis on the 2005/2006 stack in FY2006).
- BOP represents ~46% of the 2007 PEMFC system cost, thus bringing the relative importance of EOS analysis of BOP cost on par with that of the stack cost.
- Understanding the major cost contributors at low volume can highlight nearer term approaches and processes that might be necessary during the early stages of FCV commercialization.

The DOE has requested costs for production volumes of 100 units/year for 4 consecutive years, 30K/yr, 80K/yr, 130K/yr, and then 500K/yr.



We estimated the raw material price at different production volumes for key materials used in the BOP components.

Variation of Price with Production Volume

1.4X

Raw Material & Purchased Component Price

> 100 - 30,000

> 30,000 - 80,000 1.2X

> 80,000 - 500,000 1.0X

| Major Materials Cost | Annual Production Volume (Units/Year) | | | | | | | | |
|---------------------------|---------------------------------------|----------|----------|----------|----------|----------|----------|----------|--|
| (\$/kg) | 100 | 1,000 | 5,000 | 10,000 | 30,000 | 80,000 | 130,000 | 500,000 | |
| Stainless Steel 316 | \$9.80 | \$9.80 | \$9.80 | \$8.40 | \$8.40 | \$7.00 | \$7.00 | \$7.00 | |
| Cordierite | \$6.16 | \$6.16 | \$6.16 | \$5.28 | \$5.28 | \$4.40 | \$4.40 | \$4.40 | |
| Nafion | \$246.40 | \$246.40 | \$246.40 | \$211.20 | \$211.20 | \$176.00 | \$176.00 | \$176.00 | |
| Cast Aluminum | \$4.90 | \$4.90 | \$4.90 | \$4.20 | \$4.20 | \$3.50 | \$3.50 | \$3.50 | |
| Clad Aluminum 3003 | \$5.49 | \$5.49 | \$5.49 | \$4.70 | \$4.70 | \$3.92 | \$3.92 | \$3.92 | |
| Polyphenyl sulphone (PPS) | \$6.16 | \$6.16 | \$6.16 | \$5.28 | \$5.28 | \$4.40 | \$4.40 | \$4.40 | |
| NdFeB Magnet | \$123.20 | \$123.20 | \$123.20 | \$105.60 | \$105.60 | \$88.00 | \$88.00 | \$88.00 | |

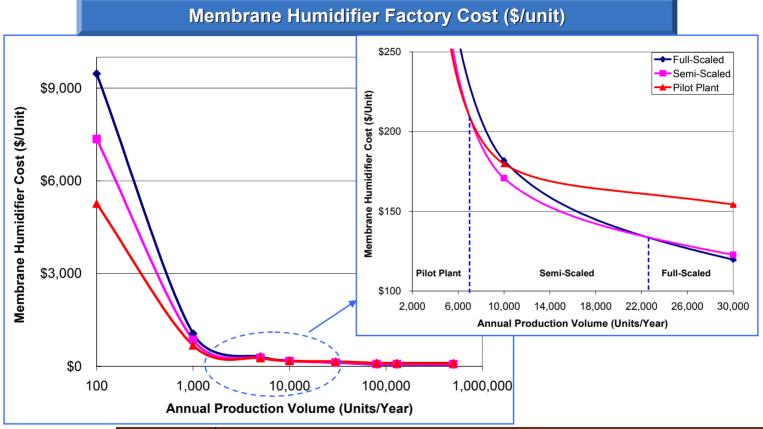


The cycle time, automation level (i.e. equipment capital cost) and material price are the major scaling parameters between the production scenarios.

| Parameters | | Pilot Plant | Semi-Scaled | Full-Scaled |
|---------------------|-------------------------------|----------------|-----------------|-----------------|
| | Automation Level | Semi-Automated | Fully Automated | Fully Automated |
| Extrude Nafion Tube | | 4.8 | 2.4 | 1.6 |
| | Hydrogen Peroxide Bath | 12.0 | 6.0 | 4.0 |
| | Sulfuric Acid Bath | 12.0 | 6.0 | 4.0 |
| Process Cycle | Tap Water Bath | 12.0 | 6.0 | 4.0 |
| Time | De-ionized Water Bath | 12.0 | 6.0 | 4.0 |
| (min/unit) | Injection Molding End Housing | 1.5 | 0.8 | 0.5 |
| | Wind Tube | 2.6 | 1.3 | 0.9 |
| | Cast in Place | 3.0 | 1.5 | 1.0 |
| | Assembly | 3.0 | 1.5 | 1.0 |
| | Extrude Nafion Tube | \$50,000 | \$75,000 | \$100,000 |
| | Hydrogen Peroxide Bath | \$100,000 | \$150,000 | \$200,000 |
| | Sulfuric Acid Bath | \$100,000 | \$150,000 | \$200,000 |
| Process | Tap Water Bath | \$100,000 | \$150,000 | \$200,000 |
| Equipment Cost | De-ionized Water Bath | \$100,000 | \$150,000 | \$200,000 |
| (\$/station) | Injection Molding End Housing | \$100,000 | \$150,000 | \$200,000 |
| | Wind Tube | \$50,000 | \$75,000 | \$100,000 |
| | Cast in Place | \$50,000 | \$75,000 | \$100,000 |
| | Assembly | \$5,000 | \$7,500 | \$10,000 |



The transition between production scenarios occur at volumes of approximately 7,000 and 23,000 units per year.



| MH Cost | Annual Production Volume (Units/Year) | | | | | | | |
|-------------|---------------------------------------|------------|----------|----------|----------|----------|----------|----------|
| (\$/Unit) | 100 | 1,000 | 5,000 | 10,000 | 30,000 | 80,000 | 130,000 | 500,000 |
| Full-Scaled | \$9,530.12 | \$1,066.52 | \$314.31 | \$182.08 | \$119.78 | \$64.17 | \$60.75 | \$57.71 |
| Semi-Scaled | \$7,428.83 | \$874.49 | \$291.99 | \$180.98 | \$143.77 | \$86.20 | \$85.21 | \$83.34 |
| Pilot Plant | \$5,327.55 | \$682.47 | \$269.67 | \$179.88 | \$154.35 | \$108.02 | \$104.57 | \$104.21 |



We developed process flow charts for the major CEM fabricated parts; the key manufacturing processes are tabulated below.

| # | Selected Components | Material | Major Manufacturing Processes |
|---|------------------------|----------|--|
| 1 | Turbine Housing | Al | Casting; Turning; Drilling |
| 2 | Motor Housing | Al | Casting; Turning; Drilling |
| 3 | Compressor Housing | Al | Casting; Turning; Drilling |
| 4 | Motor connecting shaft | Steel | Turning; Heat treatment; Grinding |
| 5 | NdFeB Magnet | NdFeB | Mixing; Molding; Sintering (purchased) |
| 6 | Turbine Wheel | Al | Investment casting; Hot Isostatic Pressing (HIP) |
| 7 | Compressor Impeller | Al | Investment casting; Hot Isostatic Pressing (HIP) |
| 8 | Thrust Bearing Runner | Steel | Turning; Heat treatment; Grinding |

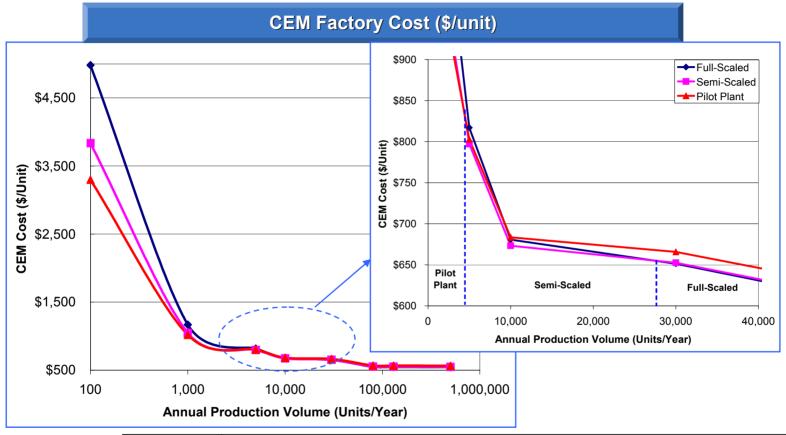


The casting processes are varied between the three production scenarios.

| P | arameters | Pilot Plant | Semi-Scaled | Full-Scaled |
|------------------------------------|---------------------------|---|--|--|
| Turbine Housing | | •Manual Sand Casting •Turning •Drilling | •Investment Casting •Turning •Drilling | •Cold Chamber Die Casting •Turning •Drilling |
| | Motor Housing | •Manual Sand Casting •Turning •Drilling | •Investment Casting •Turning •Drilling | •Cold Chamber Die Casting •Turning •Drilling |
| Selected Component Processes | Compressor Housing | •Manual Sand Casting•Turning•Drilling | •Investment Casting •Turning •Drilling | •Cold Chamber Die Casting •Turning •Drilling |
| | Motor Connecting Shaft | •Turning •Heat Treatment •Grinding | •Turning •Heat Treatment •Grinding | •Turning •Heat Treatment •Grinding |
| Thrust Bearing Runner | | •Turning •Heat Treatment •Grinding | •Turning •Heat Treatment •Grinding | •Turning •Heat Treatment •Grinding |



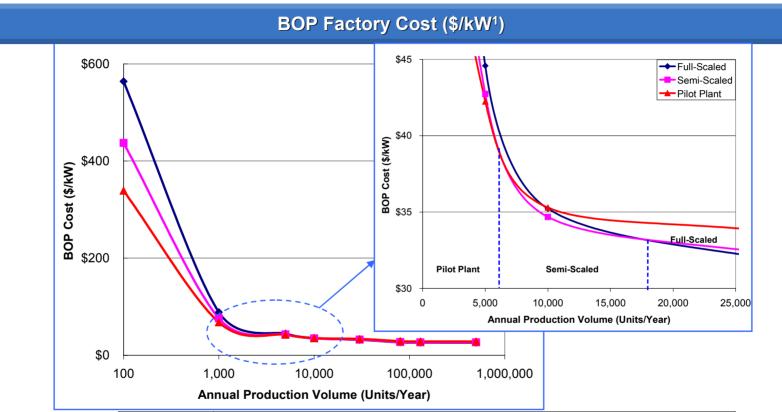
The transitions between production scenarios occur at volumes of approximately 5,000 and 28,000 units per year.



| CEM Cost | Annual Production Volume (Units/Year) | | | | | | | |
|-------------|---------------------------------------|------------|----------|----------|----------|----------|----------|----------|
| (\$/Unit) | 100 | 1,000 | 5,000 | 10,000 | 30,000 | 80,000 | 130,000 | 500,000 |
| Full-Scaled | \$4,982.40 | \$1,168.82 | \$816.91 | \$680.61 | \$651.28 | \$549.83 | \$548.06 | \$546.39 |
| Semi-Scaled | \$3,835.44 | \$1,046.44 | \$797.02 | \$673.26 | \$652.49 | \$553.25 | \$551.69 | \$549.62 |
| Pilot Plant | \$3,298.66 | \$1,018.78 | \$802.75 | \$683.43 | \$665.74 | \$568.52 | \$567.33 | \$565.92 |



On an overall BOP basis, the transitions between production scenarios occur at volumes of approximately 6,000 and 18,000 units per year.

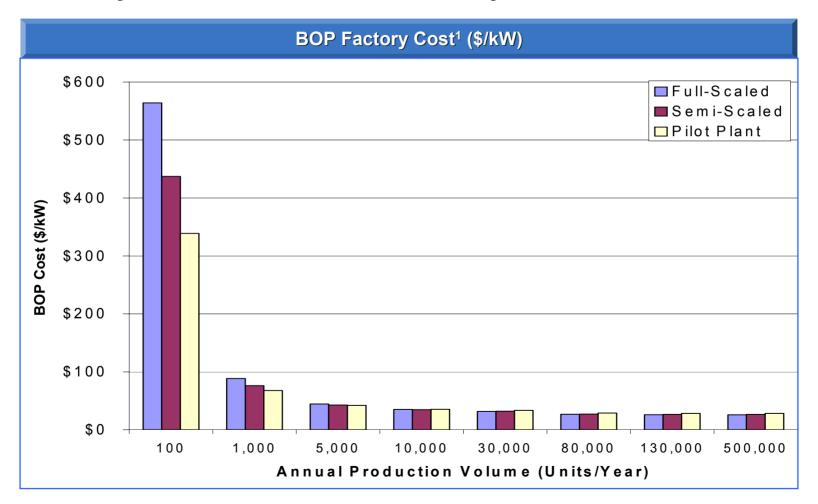


| BOP Cost | Annual Production Volume (Units/Year) | | | | | | | |
|-----------------------|---------------------------------------|---------|---------|---------|---------|---------|---------|---------|
| (\$/kW ¹) | 100 | 1,000 | 5,000 | 10,000 | 30,000 | 80,000 | 130,000 | 500,000 |
| Full-Scaled | \$564.09 | \$88.52 | \$44.58 | \$35.22 | \$31.69 | \$26.65 | \$26.01 | \$25.83 |
| Semi-Scaled | \$437.26 | \$76.19 | \$42.73 | \$34.68 | \$32.09 | \$27.22 | \$26.63 | \$26.49 |
| Pilot Plant | \$338.92 | \$67.80 | \$42.24 | \$35.29 | \$33.57 | \$28.98 | \$28.40 | \$28.30 |



¹ PEMFC net power (80 kW) basis

As expected, at low production volumes (100 units/year), the pilot plant scenario yields the lowest BOP cost, while at volumes greater than 80,000 units/year, the full-scaled scenario yields the lowest cost.





High-volume manufactured cost based on a 80 kW net power PEMFC system. Does not represent how costs would scale with power (kW).

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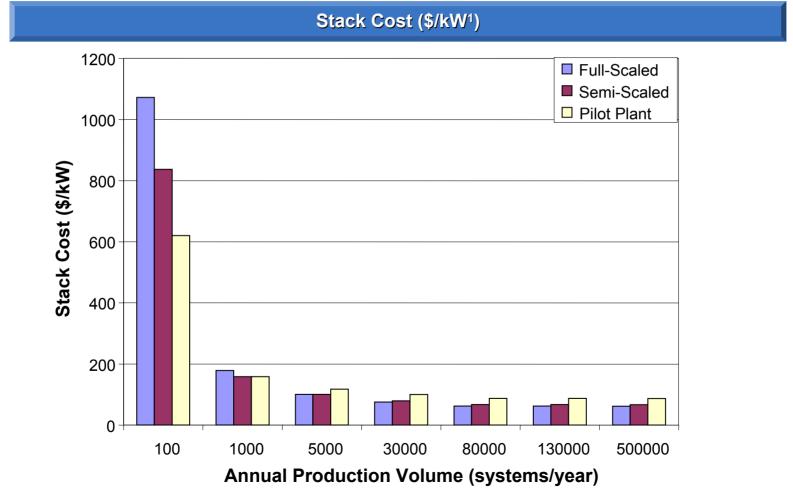
The 2006 EOS analysis is based on the 2005 stack specifications, with minor changes to the component material assumptions and processes.

| Parameters | Units | 2005 stack / 2006 EOS |
|-------------------------------|---------------------|--------------------------|
| Cell voltage @ rated power | V | 0.65 |
| Power density @ 0.65V | mW/cm ² | 600 |
| Total Pt Loading | mg/cm ² | 0.75 |
| Pt cost | \$/g (\$/tr.oz.) | 29 (900) |
| Fuel cell net power | kW _e | 80 |
| Fuel cell gross power | kW _e | 90 |
| Stack voltage @ rated power | V | 300 V @ 266 A |
| Number of stacks per system | | 2 |
| Number of cells per stack | | 231 |
| System pressure @ rated power | atm | 2.5 |
| Operating temperature | °C | 80 |

| Component | Parameter | 2006 EOS Assumptions |
|--------------------------|-----------|-----------------------------------|
| | Material | Sulfonated fluoro-polymer |
| Membrane | Supported | No |
| Membrane | Process | Cast dispersion |
| | Thickness | 50 μm |
| | Catalyst | Pt |
| Electrodes (Cathode & | Support | Carbon black |
| Anode) | Process | Screen printing / gravure coating |
| Gas Diffusion | Material | Non-woven carbon paper |
| Layer (GDL) | Process | Hydrophobic treatment |
| Pinolar Diata | Material | Molded graphite |
| Bipolar Plate | Process | Compression molding |

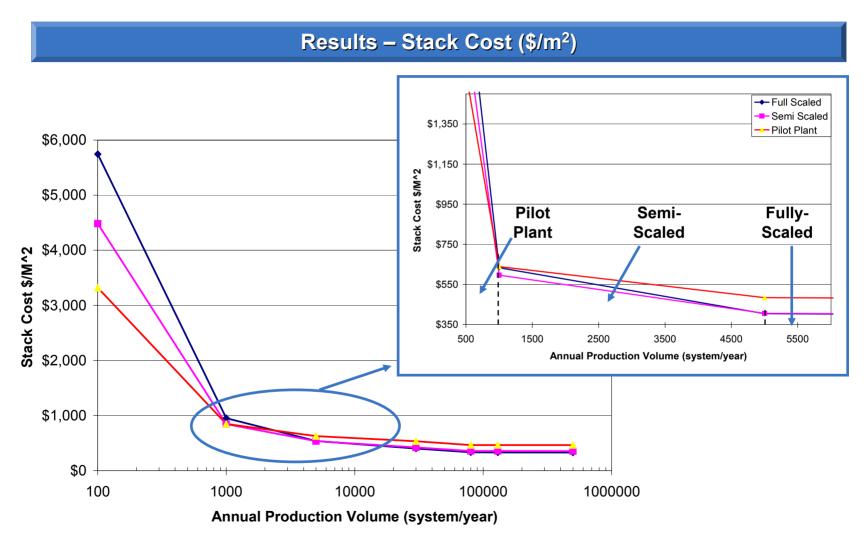
The 2008 stack is different from the 2005 stack in that it assumes an NSTFC¹-based MEA, a 30 µm 3M-like membrane, Pt loading=0.25 mg/cm² and power density=716 mW/cm² @ 0.685 V/cell.

At low volumes (~100 systems/year), the pilot plant yields the lowest stack cost of ~\$610/kW¹, while at high volumes (≥ 80,000 systems/year), the full-scaled scenario yields the lowest stack cost of ~\$61/kW¹.



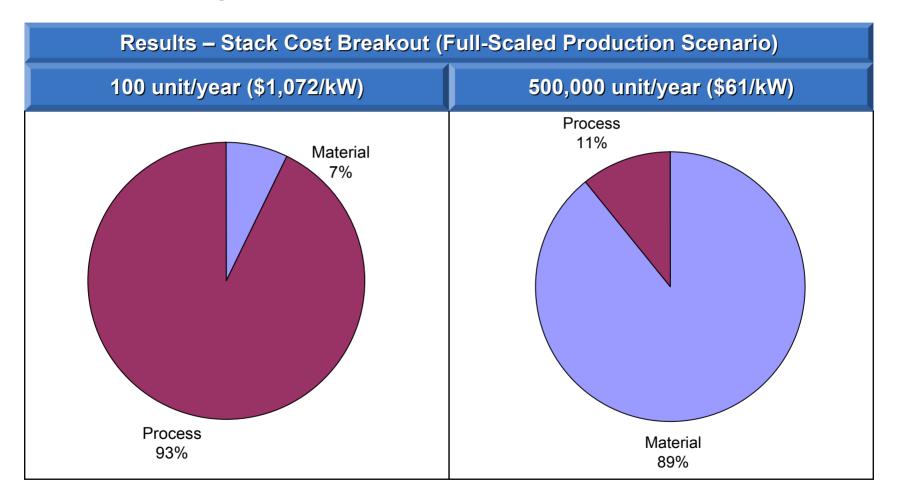


In 2006, we used a bottom-up approach to determine the impact of production volume on stack manufacturing cost.





CAPEX controls the stack cost at low volume, while material cost dominates as the production volume increases.





Backup Slides Review Meetings

We coordinated with DOE, ANL, developers, and stakeholders so far this year, with additional meetings to follow.

| Audience/ Reviewer | Date | Location |
|---|--------------|---------------|
| System Specifications Review Meeting with DOE and ANL | Feb 07 | Telecon |
| Manufacturing Process Review Mtg. with 3M | Mar 07 | Telecon |
| Fuel Cell Tech Team Mtg. | Apr 07 | Detroit MI |
| National Academy of Science Review | Apr 07 | Washington DC |
| DOE Merit Review | May 07 | Washington DC |
| Several Work-in-Progress Mtgs. with DOE and ANL | Jun – Sep 07 | Telecon |
| Final Presentation to HFCIT Team at DOE HQ | Nov 07 | Washington DC |
| Fuel Cell Tech Team Mtg. | May 08 | Detroit MI |
| DOE Annual Merit Review | June 08 | Arlington VA |
| DOE HFCIT Review | Sep 08 | Washington DC |
| Fuel Cell Tech Team Review | Sep 08 | Telecon |



We contacted developers of key stack and BOP components for their feedback on design, performance and cost assumptions.

Contacted in 2005-2006

- MEA
 - > 3M, DuPont, Gore
- GDL
 - ➤ E-Tek
 - > SpectraCorp, Toray, SGL Carbon
- Bipolar Plates
 - Porvair, GrafTech, SGL Carbon
 - Raw Materials Superior Graphite, Asbury Carbons
- Seals
 - > Freudenberg, SGL Carbon
- Stack and System Integrators
 - > Ballard
 - ➤ Tech Team (GM, Ford, Chrysler)

Contacted in 2007

- MEA
 - > 3M
- Water Management
 - PermaPure (Nafion membranebased)
 - Emprise (enthalpy wheel)
- Thermal Management
 - > Modine
- Air Management
 - Honeywell (compressorexpander-motor)
- Fuel management
 - > Parker Hannifin
 - > H₂ Systems



Backup Slides Cost Definition

We estimate an automotive OEM cost, applying no markup on stack components, and assuming a 15% markup on BOP components.

Markup applied to BOP components

Corporate Expenses

- · Research and Development
- · Sales and Marketing
- General & Administration
- Warranty
- Taxes

Factory Cost for Stack and BOP Components

Fixed Costs

- Operating
 - Tooling & Fixtures Amortization
 - Equipment Maintenance
 - Indirect Labor
 - Cost of operating capital (working period 3 months)
- Non-Operating
 - Equipment & Building Depreciation
 - Cost of non-operating capital

Variable Costs

- Manufactured Materials
- · Purchased Materials
- Direct Labor (Fabrication & Assembly)
- Indirect Materials
- Utilities

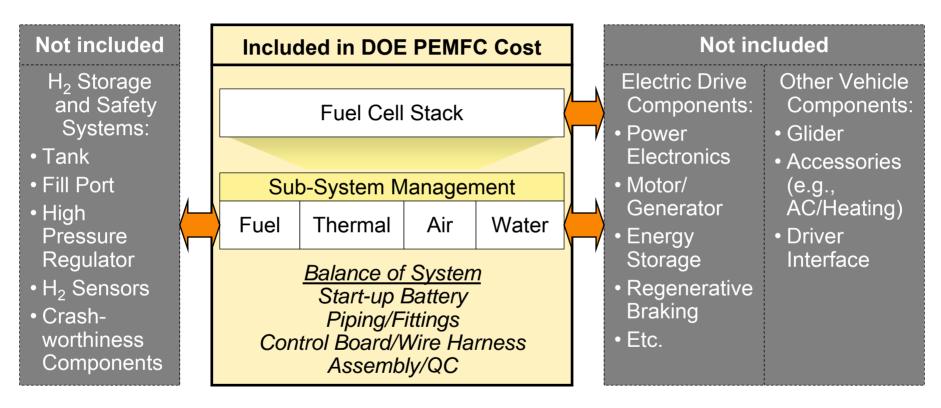
Automotive OEM Cost

- We assume a vertically integrated process for the manufacture of the stack by the automotive OEM, so no mark-up is included on the major stack components
- Raw materials are assumed to be purchased, and therefore implicitly include supplier markup
- We assume 100% debt financed with an annual interest rate of 15%, 10-year equipment life, and 25-year building life.



Backup Slides Scope

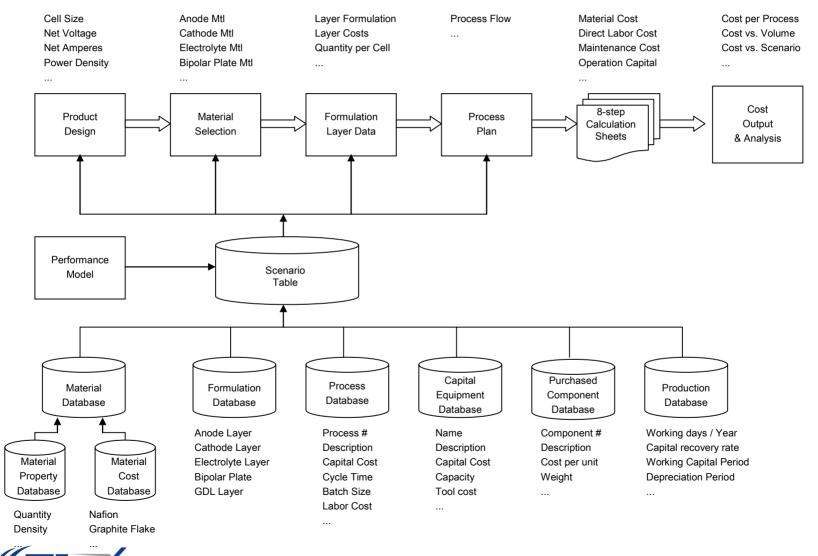
Our cost assessment includes the fuel cell stack and related BOP subsystems, but does not include electric drive or other necessary powertrain components.



Quality Control (QC) includes leak and voltage tests, but does not include stack conditioning.



Our PEM stack cost model integrates expertise in materials, design, and manufacturing operations.



We performed single and multi- variable sensitivity analyses to examine the impact of major stack and BOP parameters on PEMFC system cost.

- Single variable stack sensitivity analysis
 - Varied one parameter at a time, holding all others constant
 - Varied overall manufacturing assumptions, economic assumptions, key stack performance parameters, and direct material cost, capital expenses and process cycle time for individual stack components
 - Assumed stack rated power, operating pressure, temperature, humidity requirements and cell voltage remained invariant
- Single variable BOP sensitivity analysis
 - Varied one parameter at a time, holding all others constant
 - Varied overall manufacturing assumptions, economic assumptions, and direct material cost, capital expenses and process cycle time for individual BOP components
 - Assumed stack rated power, operating pressure, temperature, humidity requirements and cell voltage remained invariant
- Multi-variable (Monte Carlo) system sensitivity analysis
 - Varied all stack and BOP parameters simultaneously, using triangular PDF
 - Performed Monte Carlo analysis on individual stack and BOP components, the results of which were then fed into a system-wide Monte Carlo analysis



Raw materials for stack and BOP components are assumed to be purchased, and therefore implicitly include supplier markup.

| PEMFC Sub-system | Raw Materials / Purchased Components |
|--|--|
| Stack | |
| Membrane | PFSA ionomer, isopropanol, silicone-treated PET film, polypropylene film, water |
| Electrodes | Pt, Co, Mn, perylene red (PR-149) dye, aluminum-coated film substrate, Teflon sheet |
| GDL | Woven carbon fiber, PTFE, carbon powder, water |
| Seal | Viton |
| Bipolar Plates | Expanded graphite flake, vinyl ester, carbon fiber, poly dimethylsiloxane (SAG), methyl ethyl ketone peroxide, cobalt naphthenate |
| BOS | Stack manifold, bolts, end plates, current collector |
| Balance of Plant | |
| Water management (enthalpy wheel, membrane humidifier) | Cordierite, γ-alumina, Teflon seals, enthalpy wheel motor, Nafion, Noryl®, PPS, polyurethane, O-rings |
| Thermal management (radiator, fan, pump) | Aluminum coil, aluminum tube, radiator fan, coolant pump |
| Air management (CEM, motor controller) | NdFeB magnet, steel bar stock, Teflon insulation, copper coils, steel laminations, bearings, seals, motor controller, wire harness |
| Fuel management (H ₂ blower, H ₂ ejectors) | SS316 bar, SS316 sheet, seals, H ₂ blower motor, H ₂ ejectors |



Backup Slides BOP Overview

With the exception of heat exchangers, the BOP components have not been manufactured at high volumes.

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Technology advances such as high temperature, low R.H. membranes could simplify and reduce the size/cost of some of the BOP components.



Backup Slides CEM Overview

We estimated the cost of the CEM based on published presentations, reports. and patents from Honevwell.

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The references used to determine the overall design and major manufacturing processes for the CEM are tabulated below.

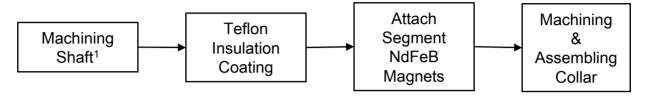
| Component | References |
|-------------------|--|
| Overall System | Honeywell, DOE program review, progress report & annual report, 2005, 2004, 2003, 2000 |
| Electrical Motor | Honeywell, DOE program review, progress report & annual report 2004; US patent 5,605,045; |
| Power Electronics | Honeywell, DOE program review, progress report & annual report, 2005; Caterpillar, DOE Contract DE-SC05-00OR-99OR22734 |
| Unison Ring | US patent 6,269,642; Garrett/Honeywell, DE-FC05- 00OR22809; |
| Journal Bearings | US patent, 2006/0153704; Honeywell 2005 fuel cell seminar; |

| # | Selected Components | Material | Major Manufacturing Processes |
|---|--------------------------|----------|--|
| 1 | Turbine Housing | Al | Cold chamber die casting; Turning; Drilling |
| 2 | Motor Housing | Al | Cold chamber die casting; Turning; Drilling |
| 3 | Compressor Housing | Al | Cold chamber die casting; Turning; Drilling |
| 4 | Motor connecting shaft | Steel | Turning; Heat treatment; Grinding |
| 5 | NdFeB Magnet | NdFeB | Mixing; Molding; Sintering (purchased) |
| 6 | Turbine Wheel | Al | Investment casing; HIP |
| 7 | Compressor Impeller | Al | Investment casting; HIP |
| 8 | Thrust Bearing Runner | Steel | Turning; Heat treatment; Grinding |



Backup Slides CEM Process Flow

The motor rotor manufacturing process represents the level of detail we captured in the costing of the CEM.



- Cut the material from bar stock
- Thermal heat treatment (annealing)
- -Machining in Lathe
 - Load Part to 3 jaw chuck
 - Face finish
 - chamber
 - Central drill & drill
 - Re-clamp the part
 - Contour turning rough
 - Reverse the part
 - face finish
 - chamber
 - Central drill and drill
 - Re- clamp the part using central holes
 - Contour turning finish
- -Thermal heat treatment (hardening)
- -Grinding rough
- -Grinding finish

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CEM Motor Rotor Manufacturing Process



The estimated CEM (including motor and motor controller) cost is \$535

per unit.

| # | Part Name | Quantity | Reference | Ref. Part # | | OD (cm) | L (cm) | W (cm) | H (cm) | Wall Thickness (cm) | Total Vol. (Cm^3) | Total Wt. (kg) | Final Total Cost (\$) |
|----------|------------------------------------|----------|----------------------------|-------------|---------------|---------|--------|--------|--------|---------------------------|----------------------|-------------------|--------------------------|
| | Turbine Housing | 1 | US6269642 | 24 | Al | 20.32 | | | 7.62 | 0.16 | 127.19 | 0.34 | \$ 5.46 |
| 2 | | 6 | | | Misc | 0.60 | 1.20 | | | | 2.03 | 0.02 | \$ 0.72 |
| 3 | | 6 | | | Misc | 0.60 | 0.10 | | | | | 0.01 | \$ 0.72 |
| | Tie Rod | 1 | US6269642 | 30 | Steel | 1.00 | 4.00 | | | | 3.14 | 0.02 | \$ 3.70 |
| | Turbine Wheel | 1 | | | Al | 5.00 | 5.00 | | | | | 0.20 | \$ 20.07 |
| | Variable Vane Assembly | | | | | | | | | | | | \$ - |
| 7 | Nozzle Wall | 1 | US6269642 | 38 | Steel | 17.78 | | | | 0.30 | 36.46 | 0.28 | \$ 2.61 |
| 8 | | 9 | US6269642 | 36 | Steel | 3.00 | 0.50 | 0.50 | | | 6.75 | 0.47 | \$ 2.34 |
| 9 | | 9 | US6269642 | 40 | Steel | 0.20 | 1.00 | | | | 0.28 | 0.02 | \$ 2.54 |
| 10 | | 9 | US6269642 | 44 | Steel | 15.01 | 1.00 | 0.30 | 0.30 | | 0.81 | 0.06 | \$ 2.63 |
| 11 | Unison Ring | 1 | US6269642 | 48 | Steel | 15.24 | 0.50 | 4.00 | 4.00 | | 84.88 | 0.66 | \$ 19.99 |
| 12 | Actuator Crank | 1 | US6269642 | 50 | Steel | 4.00 | 2.00 | 1.00 | 1.00 | 0.40 | 2.00 | 0.02 | \$ 1.18 |
| 13 | | 1 1 | US6269642 | 60 | Steel | 1.20 | 1.00 | | | 0.10 | 0.00 | 0.00 | \$ 0.07 |
| 14 | Crank Gear | 1 1 | US6269642 | 62 | Steel | 2.00 | 1.00 | | | 0.50 | 2.36 | 0.02 | \$ 4.28 |
| 15 | Crank Gear Pin | 1 | US6269642 | 64 | Steel | 0.20 | 2.00 | | | - | 0.06 | 0.00 | \$ 0.17 |
| 16 | Crank End Bearing | 1 | US6269642 | 66 | Misc | 20.22 | 4.50 | | | 254 | 3.00 | 0.02 | \$ 2.22 |
| 17 | Actuator Housing | 1 1 | LIDCOCCC 40 | 05 | Al | 20.32 | 1.50 | | | 2.54 | 212.71 | 0.57 | \$ 6.10 |
| 18 19 | | 1 1 | US6269642 US6269642 | 85 108 | Misc Steel | | 3.00 | 1.20 | | 0.20 | 0.72 | 0.20 | \$ 5.07 \$ 0.18 |
| | | 1 | US6269642 US6269642 | | Steel | 0.40 | 1.00 | 1.20 | | 0.20 | | 0.00 | \$ 0.18 |
| 20 21 | Solenoid Valve Bracket Bolt Washer | 1 | US6269642 US6269642 | 110 | | 0.40 | 1.00 | | | 0.10 | 0.13 | 0.00 | \$ 0.12 |
| 22 | | 1 | US6269642 US6269642 | 88 | | 0.60 | 6.00 | | | 0.10 | 1.70 | 0.00 | \$ 0.12 |
| | Motor Rotor Assembly | ' | 036269642 | - 00 | | 0.60 | 6.00 | | | | 1.70 | 0.01 | |
| 24 | | 1 | US5605045 | 16 | Steel | 3.61 | 20.32 | | | 0.00 | 207.88 | 1.62 | \$ - \$ 10.71 |
| 25 | | 1 | US5605045 | 60 | Teflon | 3.81 | 12.70 | | | 0.00 | 14.79 | 0.03 | \$ 10.71 |
| 26 | | 4 | US5605045 | 62 | NdFeB | 4.68 | 12.70 | | | 0.10 | 73.64 | 0.55 | \$ 48.88 |
| 27 | Collar | 1 | US5605045 | 70 | Steel | 5.08 | 12.70 | | | 0.20 | 38.92 | 0.30 | \$ 7.65 |
| | Labyrith Seal | 1 | US2006/0153704 | 130 | Misc | 3.61 | 12.70 | | | 1.00 | 30.32 | 0.02 | \$ 2.07 |
| | Journal Foil Bearing | 1 | US2006/0153705 | 130 | Steel | 3.61 | 5.08 | | | 1.00 | | 0.10 | \$ 10.42 |
| | Motor Housing | 1 | DE-FC36-02AL67624 | | Al | 20.32 | 20.32 | | | 0.20 | 432.55 | 1.17 | \$ 10.58 |
| 31 | Bolt | 8 | DE 1 000 027 (EST 024 | | Misc | 0.60 | 1.20 | | | 0.20 | 2.03 | 0.02 | \$ 0.96 |
| 32 | | 8 | | | Misc | 0.60 | 0.10 | | | | 0.00 | 0.02 | \$ 0.96 |
| | Motor Stator Assembly | 1 | FY2000 Progress Report | | Misc | 9.20 | 12.70 | | | 2.00 | 574.24 | 4.59 | \$ 26.30 |
| | Motor Sator Position Ring | 1 | FY2000 Progress Report | | | 0.20 | | | | | | | \$ 0.07 |
| 35 | Bolt | 8 | FY2000 Progress Report | | Misc | 0.60 | 1.20 | 0.00 | 0.00 | 0.00 | 2.03 | 0.02 | \$ 0.96 |
| 36 | | - 8 | FY2000 Progress Report | | Misc | 0.60 | 0.10 | 0.00 | 0.00 | 0.00 | 0.00 | 0.02 | \$ 0.96 |
| 37 | Motor Connect | 1 | | | Misc | | | | | | | | \$ 0.57 |
| | Labyrith Seal | 1 | FY2000 Progress Report | | Misc | 3.61 | | | | | | 0.02 | \$ 2.07 |
| 39 | Thrust Bearing Runner | 1 | FY2000 Progress Report | | Steel | 5.00 | 5.08 | | | | 40.52 | 0.32 | \$ 7.66 |
| 40 | Thrust Bearing | 2 | FY2000 Progress Report | | Misc | 5.00 | | | | | | 0.20 | \$ 20.83 |
| | Thrust Bearing Holder | 1 | FY2000 Progress Report | | Steel | 17.78 | 5.08 | | | | 124.08 | 0.97 | \$ 8.66 |
| | Labyrith Seal | 1 | | | Misc | | | | | | | 0.02 | \$ 2.07 |
| | Jounal Foil Bearing | 1 | US2006/0153705 | | Misc | 3.61 | 5.08 | | | | | 0.10 | \$ 10.42 |
| | Compressor Housing | 1 | FY2000 Progress Report | | Al | 25.40 | | | 7.62 | 0.16 | 134.69 | 0.36 | \$ 5.46 |
| 45 | | 8 | FY2000 Progress Report | | Misc | 0.60 | 1.20 | 0.00 | 0.00 | 0.00 | 2.03 | 0.02 | \$ 0.96 |
| 46 | | 8 | FY2000 Progress Report | | Misc | 0.60 | 0.10 | 0.00 | 0.00 | 0.00 | 0.00 | 0.01 | \$ 0.96 |
| | Compressor Impeller | 1 | FY2000 Progress Report | | Al | | | | | | | 0.20 | \$ 20.07 |
| | Compressor Impeller Tie Rod | 1 | FY2000 Progress Report | | Misc | 1.00 | 10.00 | | | | 7.85 | 0.06 | \$ 0.53 |
| | CEM Mounting Bracket Left | 1 | | | Steel | | 25.40 | 7.62 | | 0.10 | 19.35 | 0.15 | \$ 0.90 |
| | CEM Mounting Bracket Right | 1 | | L | Steel | | 25.40 | 7.62 | 0.00 | 0.10 | 19.35 | 0.15 | \$ 0.90 |
| | Control Box Assembly | 1 | DOE target \$40/kW / 5.5kW | / input | | | | | | | | 6.50 | \$ 250.83 |
| 52 | Box | 1 | | | | | | | | | | | + |
| 53 | Integrated Motor Cable | 1 | | | | | | | | | | | |
| 54 | Inverter | 1 | | | | | | | | | | | + |
| 55 56 | EMI Section | 1 | | | | | | | | - | | | + |
| 56 I | Wire Harness & Cooling pipes | 1 1 | | 1 | 1 | 1 | | 1 | I | 1 | | 1 | 1 |



The motor assembly and motor controller are projected to cost \$412, representing 77% of the CEM cost.

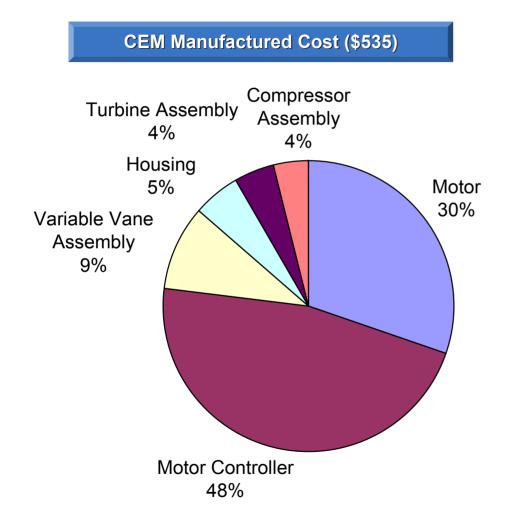
| Motor Subsystems | Components | Manufactured Cost (\$) | Comments |
|------------------------|--|---------------------------|--|
| | Copper Coils | | Assumed purchased part. The price is direct |
| Stator Assembly | Steel Laminations | 26 | materials with a markup of 1.15. 1 kg copper coil (\$7/kg) and 3.6 kg laminated steel (\$4.4/kg) with a markup of 1.15. |
| | Shaft | 11 | DFMA machining package |
| | Magnets | 49 | 0.55 kg NdFeB magnet with a cost of \$88/kg |
| | Journal Foil Bearing | 21 | Assumed purchased part at \$10 each |
| Rotor Assembly | Thrust Journal Bearings | 21 | Assumed purchased part at \$10 each |
| | Thrust Bearing Runner | 8 | DFMA machining package |
| | Thrust Bearing Holder | 9 | DFMA machining package |
| | Seals, collar, etc. | 17 | Assumed purchased parts |
| Motor Controller | 5.5 kW Inverter with DSP controller | 220 | \$40/kW from "A Novel Bidirectional Power Controller for Regenerative Fuel Cells", Final Report for DE-FG36-04GO14329, J. Hartvigsen and S.K. Mazumder, Oct. 10, 2005 |
| | Packaging, Wire harness, thermal management, etc | 31 | |
| Total Motor Cost (\$/u | ınit) | 412 | |

The 5.5 kW inverter is projected to dominate the motor controller cost.



Backup Slides CEM Cost

The CEM factory cost (without supplier markup) of \$535, is the largest contributor to the overall BOP cost.



| CEM Manufactured Cost (\$) | | | | | | | |
|-------------------------------|-----------------------|-----|--|--|--|--|--|
| Component | OEM Cost ¹ | | | | | | |
| Motor | 162 | | | | | | |
| Motor Controller ² | 251 | | | | | | |
| Variable Vane Assembly | 50 | | | | | | |
| Housing | 28 | 615 | | | | | |
| Turbine Assembly | 24 | | | | | | |
| Compressor Assembly | 21 | | | | | | |
| Total: | 535 | | | | | | |

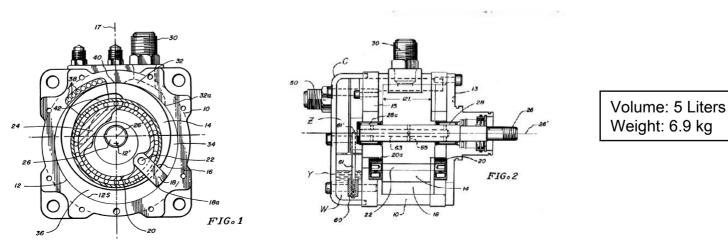
¹ Assumes 15% markup to the automotive OEM



² \$40/kW from "A Novel Bidirectional Power Controller for Regenerative Fuel Cells", Final Report for DE-FG36-04GO14329, J. Hartvigsen and S.K. Mazumder, Oct. 10, 2005

We costed the H₂ recirculating blower based on published information and patents on the Parker Hannifin Model 55 Univane™ rotary compressor.

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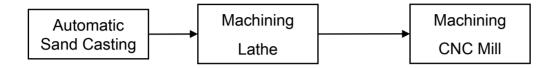
US Patent: 5,374,172

The major manufacturing processes for selected components of the H₂ blower are tabulated below.

| # | Selected Components | Material | Major Manufacturing Processes |
|---|----------------------|----------|--|
| 1 | Motor Side End Plate | SS316 | Automatic sand casting; turning; drilling |
| 2 | Blower Housing | SS316 | Automatic sand casting; turning; drilling |
| 3 | Inlet Manifold | SS316 | Powder metallurgy |
| 4 | Outlet Manifold | SS316 | Powder metallurgy |
| 5 | End Plate | SS316 | Automatic sand casting; turning; drilling |
| 6 | Blower Shaft | SS316 | Turning; Milling; Heat treatment; Grinding |
| 7 | Rotor | Al | Casting; Turing; Milling; Broaching |
| 8 | Vane | SS316 | Hot forging; Drilling; Reaming |



The blower housing manufacturing process represents the level of detail we captured in the costing¹ of the H₂ blower.



- Load part to 3 jaw chuck
- Face rough
- Face finish
- chamber
- Central hole boring rough
- Central hole boring finish
- Chamber
- Reverse the part
- Face rough
- Face finish
- Chamber (inner & outer)

- Load part to fixture
- Milling the manifold connect surface rough
- Milling the manifold connect surface finish
- Drilling & tapping
- Rotate the fixture
- Milling the manifold connect surface rough
- Milling the manifold connect surface finish
- Drilling & tapping
- -Load the part to vise
- -Drilling & tapping
- -Reverse the part (vise)
- -Drilling & tapping

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H₂ Blower Housing Manufacturing Process



The projected H₂ blower cost is \$193 per unit.

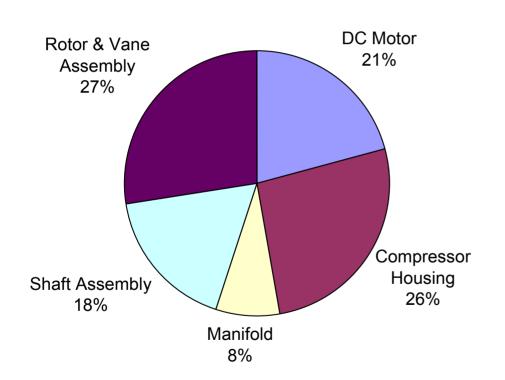
| | | | | | | | | Wall Thickness | Total Vol. | Total Wt. | Ein | al Total |
|----|------|----------------------|----------|----------|---------|--------|-----------|-------------------|------------|-----------|-----|----------|
| # | | Part Name | Quantity | Material | OD (cm) | L (cm) | W (cm) | (cm) | (Cm^3) | (kg) | | ost (\$) |
| 1 | 100 | We DC Motor | 1 | Misc | 16.51 | 8.89 | VV (CIII) | (CIII) | (CIII 3) | 1.00 | \$ | 40.21 |
| 2 | | Plate (motor side) | 1 | SS316 | 16.51 | 2.54 | | 0.32 | 96.48 | 0.75 | \$ | 13.33 |
| 3 | | Screw | 4 | Misc | 10.51 | 2.07 | | 0.02 | 30.40 | 0.02 | \$ | 0.48 |
| 4 | | O-Ring | 1 | Misc | 13.97 | | | | | 0.01 | \$ | 0.57 |
| 5 | | Labyrith Seal (main) | 1 | Misc | 5.08 | 1.27 | | | | 0.02 | \$ | 2.07 |
| 6 | | O-Ring | · | Misc | 5.08 | | | | | 0.01 | \$ | 0.20 |
| 7 | | C-Clip | 1 | SS316 | 5.08 | | | | | 0.01 | \$ | 0.17 |
| 8 | | Labyrith Seal | 1 | Misc | 4.45 | | | | | 0.02 | \$ | 2.07 |
| 9 | Blo | wer Housing | 1 | SS316 | 15.24 | 8.89 | | 0.32 | 106.65 | 0.83 | \$ | 16.88 |
| 10 | | Screw | 8 | Misc | | | | | | 0.04 | \$ | 0.96 |
| 11 | | O-Ring | 1 | Misc | 13.97 | | | | | 0.01 | \$ | 0.57 |
| 12 | | Compressor Shaft | 1 | SS316 | 1.59 | 12.70 | | | 25.12 | 0.20 | \$ | 9.71 |
| 13 | | Bearing | 2 | SS316 | 3.81 | 2.54 | | | 28.94 | 0.23 | \$ | 19.11 |
| 14 | | Seal | 2 | Misc | 3.81 | | | | | 0.01 | \$ | 0.54 |
| 15 | | Rotor | 1 | Al | 10.16 | 7.62 | | | 308.73 | 0.83 | \$ | 6.29 |
| 16 | | Vane Guide | 2 | SS316 | 7.62 | 1.27 | | 1.27 | 32.06 | 0.50 | \$ | 10.48 |
| 17 | | Vane Guide Bearing | 2 | Misc | 7.62 | | | | | | \$ | 30.42 |
| 18 | | Vane | 1 | SS316 | | 7.62 | 2.54 | 1.27 | 24.58 | 0.19 | \$ | 2.95 |
| 19 | | Vane Shaft | 1 | SS316 | 0.95 | 9.62 | | | 6.85 | 0.05 | \$ | 3.06 |
| 20 | | C-Clip | 2 | SS316 | 1.35 | | | | | 0.01 | \$ | 0.24 |
| 21 | Inle | t Manifold | 1 | SS316 | 4.45 | 8.89 | | 0.64 | 35.17 | 0.27 | \$ | 5.11 |
| 22 | | Seal | 1 | Misc | | 5.08 | 3.81 | | | 0.01 | \$ | 0.57 |
| 23 | | Screw | 4 | Misc | | | | | | 0.02 | \$ | 0.48 |
| 24 | | Fitting | 1 | SS316 | 4.45 | 5.08 | | | | 0.10 | \$ | 1.07 |
| 25 | | O-Ring | 1 | Misc | 2.54 | | | | | 0.01 | \$ | 0.27 |
| | Out | let Manifold | 1 | SS316 | 4.45 | 8.89 | | 0.64 | 35.17 | 0.27 | \$ | 5.11 |
| 27 | | Seal | 1 | Misc | | 5.08 | 3.81 | | | 0.01 | \$ | 0.57 |
| 28 | | Screw | 4 | Misc | | | | | | 0.02 | \$ | 0.48 |
| 29 | | Fitting | 1 | SS316 | 4.45 | 5.08 | | | | 0.10 | \$ | 1.07 |
| 30 | | O-Ring | 1 | Misc | 2.54 | | | | | 0.01 | \$ | 0.27 |
| | | l Plate | 1 | SS316 | 15.24 | 3.81 | | 0.64 | 72.36 | 0.56 | \$ | 11.69 |
| 32 | | Screw | 8 | Misc | | | | | | 0.04 | \$ | 0.96 |
| 33 | | O-Ring | 1 | Misc | 8.89 | | | | | 0.01 | \$ | 0.57 |
| 34 | | End Cover | 1 | SS316 | 7.62 | 0.64 | | | 28.94 | 0.23 | \$ | 2.00 |
| 35 | | Screw | 4 | Misc | | | | | | 0.02 | \$ | 0.48 |
| 36 | | O-Ring | 1 | Misc | 6.35 | | | | | 0.01 | \$ | 0.27 |
| 37 | Sup | port | 1 | Steel | | 15.24 | 15.24 | 0.25 | 58.99 | 0.46 | \$ | 2.21 |
| | | 7 | | | | | | | Total: | 6.88 | \$ | 193.44 |



Total: 6.88 \$ 193.44

The rotor & vane assembly, blower housing, and DC motor are the top three cost drivers for the H_2 blower.





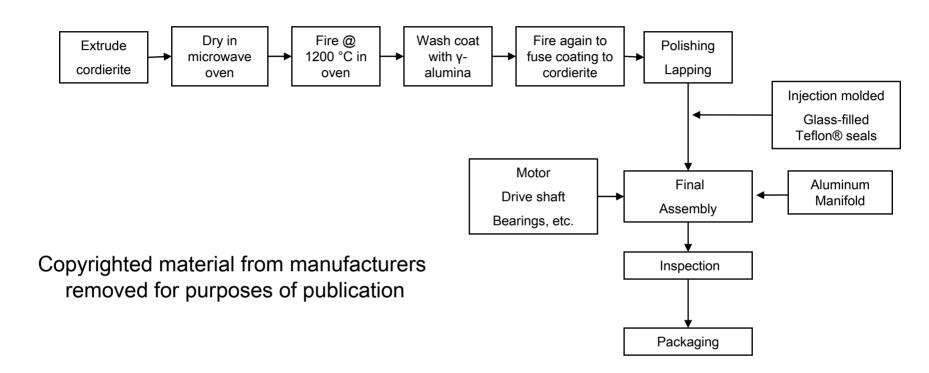
| H ₂ Blower Manufactured Cost (\$) | | | | | | | |
|--|-----------------------|-----|--|--|--|--|--|
| Component | OEM Cost ¹ | | | | | | |
| DC Motor | 40 | | | | | | |
| Blower Housing | 51 | | | | | | |
| Manifold | 15 | | | | | | |
| Shaft Assembly | 34 | 222 | | | | | |
| Rotor & Vane Assembly | 53 | | | | | | |
| Total: | 193 | | | | | | |

¹ Assumes 15% markup to the automotive OEM

We assumed that the material for the blower housing is stainless steel 316.



The enthalpy wheel manufacturing process was based on discussions with Emprise on their Humidicore™ humidifier.



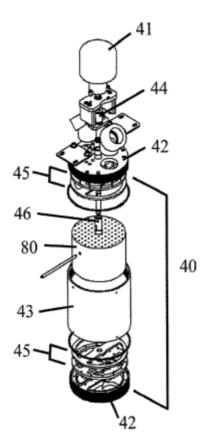
The ceramic honeycomb material, Cordierite, is in mass production and is commonly used in automotive catalytic converters.



The enthalpy wheel bill-of-materials was deduced from Emprise patents, white papers and personal communications.

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Volume: 12 liters Weight: 8 kg



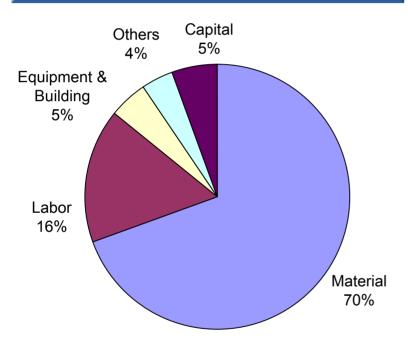
US Patent 2002/0071979

| Enthalpy Wheel Humidifier | | | | | | | | |
|------------------------------|----|----------------|--------------------------|--|--|--|--|--|
| Component | # | Material | Size | | | | | |
| 30 We DC motor with gear box | 1 | Misc. | Ф3" х 3 ¾" | | | | | |
| Shaft | 2 | Steel | Ф 3/8" х 3" | | | | | |
| Wheel shaft | 2 | Steel | OD:Ф1/2", ID:Ф 3/8", L1" | | | | | |
| Screw | 1 | Misc. | Ф3/8" х 1⁄4" | | | | | |
| Bearing | 2 | Misc. | ID Φ3/8" | | | | | |
| End plate | 2 | Teflon | Ф6" х ¼" | | | | | |
| Spring plate | 2 | Steel | Ф6" х 1/8" | | | | | |
| Springs | 26 | Misc. | Ф1/8" х ¼" | | | | | |
| End seal plate | 2 | Teflon | Ф6" х ¼" | | | | | |
| Core | 1 | Cordierit e | Ф6" х 7" | | | | | |
| Core pin | 1 | Steel | Φ¼" x 6" | | | | | |
| Manifold (motor side) | 1 | Al | Ф8" х 2" | | | | | |
| Bolts | 24 | Misc. | Ф¼" х З ½" | | | | | |
| Main housing | 1 | Al | Ф8" х 9" | | | | | |
| Bolts | 4 | Misc. | Ф3/8" х 10 ½" | | | | | |
| Base manifold | 1 | Al | Ф8" х 2 " | | | | | |



The motor is the largest contributor to the enthalpy wheel cost, followed by the cordierite core.

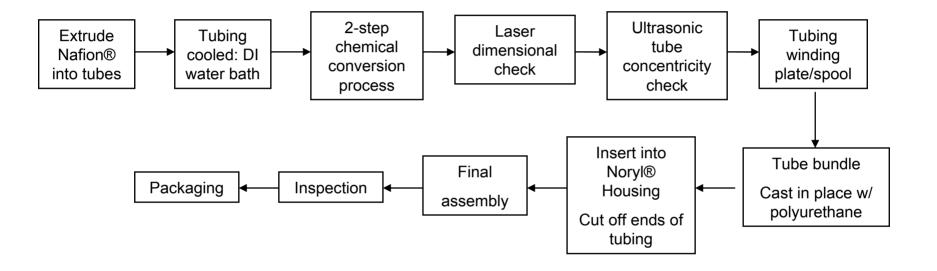




| Enthalpy Wheel Humidifier Manufactured Cost (\$) | | | | | | | | |
|--|----|----------|---------|--|--|--|--|--|
| Component | # | Material | Process | | | | | |
| DC motor with gear box | 1 | 50.00 | 0.00 | | | | | |
| Shaft | 2 | 0.10 | 2.86 | | | | | |
| Wheel shaft | 2 | 0.12 | 3.56 | | | | | |
| Screw | 1 | 0.05 | 0.00 | | | | | |
| Bearing | 2 | 4.30 | 0.00 | | | | | |
| End plate | 2 | 10.79 | 1.80 | | | | | |
| Spring plate | 2 | 1.04 | 1.68 | | | | | |
| Springs | 26 | 1.30 | 0.00 | | | | | |
| End seal plate | 2 | 10.79 | 1.80 | | | | | |
| Core | 1 | 8.48 | 20.39 | | | | | |
| Core pin | 2 | 2.00 | 0.00 | | | | | |
| Manifold (motor side) | 1 | 2.24 | 6.20 | | | | | |
| Bolts | 12 | 0.60 | 0.00 | | | | | |
| Main housing | 1 | 6.73 | 1.46 | | | | | |
| Bolts | 4 | 0.80 | 0.00 | | | | | |
| Base manifold | 1 | 2.24 | 6.20 | | | | | |
| Bolts | 12 | 0.60 | 0.00 | | | | | |
| Packaging | 1 | 2.00 | 0.00 | | | | | |
| Assembly & QC | - | - | 9.95 | | | | | |
| Total 1 160 | | | 60 | | | | | |



The Nafion tube bundle is the key component of the membrane humidifier and its manufacturing process is described below.



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The membrane humidifier manufacturing process was based on discussions with PermaPure on their FC200-780-7PP Series™ of humidifiers.

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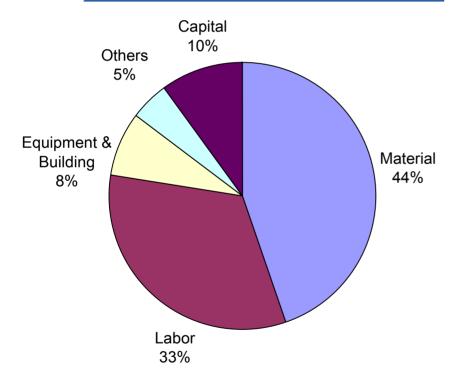
Volume: 2 liters Weight: 2 kg

| Membrane Humidifier | | | | | | | |
|---------------------|-----|--|---|--|--|--|--|
| Component | # | Material | Size | | | | |
| Right side housing | 1 | Polyphenylsulf one (PPS) | OD 3 3/4", Length 4" | | | | |
| Small O-ring | 2 | Viton | OD 3" | | | | |
| Big O-ring | 2 | Viton | OD 3 1/2" | | | | |
| C-clip | 2 | Steel | OD 3 1/2" | | | | |
| Nafion tubes | 960 | Nafion | ID 1mm, OD 1.12 mm, Length 178 mm | | | | |
| Nafion tube housing | 1 | Noryl® (Modified Polyphenylene Oxide) | OD 3 1/2", Length 7" | | | | |
| Nafion tube header | 2 | Polyurethane | OD 3 1/2", Length 1" | | | | |
| Mesh filter | 2 | Nylon | Width 2", length 2" | | | | |
| Left side housing | 1 | Polyphenylsulf one (PPS) | OD 3 3/4" Length 4" | | | | |



Material costs represent approximately 44% of the membrane humidifier cost projection.

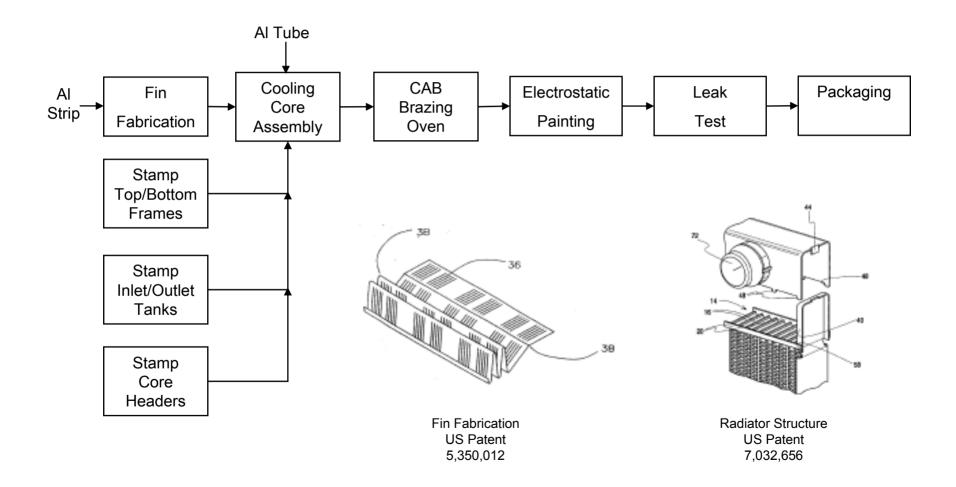




| Membrane Humidifier Manufactured Cost (\$) | | | | | | |
|--|-----|----------|---------|--|--|--|
| Component | # | Material | Process | | | |
| Right side housing | 1 | 2.62 | 0.84 | | | |
| Small O-ring | 2 | 1.00 | 0.00 | | | |
| Big O-ring | 2 | 1.00 | 0.00 | | | |
| C-clip | 2 | 0.20 | 0.00 | | | |
| Nafion tubes | 960 | 14.19 | 22.42 | | | |
| Nafion tube housing | 1 | 1.30 | 0.88 | | | |
| Nafion tube header | 2 | 0.20 | 0.00 | | | |
| Mesh filter | 2 | 0.20 | 0.00 | | | |
| Left side housing | 1 | 2.85 | 0.85 | | | |
| Assembly & packaging | - | 2.05 | 6.93 | | | |
| Subtotal | - | 25.85 | 31.93 | | | |
| Total | - | 58 | | | | |



We developed a manufacturing process flow chart for the radiator based on Modine patents and in-house experience.





We used a Modine all-aluminum automobile radiator structure as our baseline design.

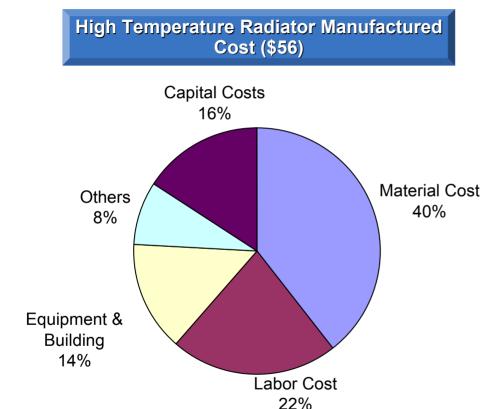
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| # | Components | # | Mtl. | Size (L x W x H) (mm) |
|----|------------------------------------|-------|--------|---------------------------|
| # | Components | *** | 14101. | Size (L X W X H) (IIIIII) |
| 1 | Serpentine Louvered Fin | 38381 | A3003 | 28.00 x 7.94 x 0.08 |
| 2 | Core Tube | 64 | A3003 | 600.00 x 28.00 x 2.76 |
| 3 | Inlet Header, Solder Well Type | 1 | A3003 | 500.00 x 68.00 x 1.80 |
| 5 | Outlet Header, Solder Well Type | 1 | A3003 | 500.00 x 68.00 x 1.80 |
| 8 | Top Side Piece | 1 | A3003 | 600.00 x 68.00 x 1.80 |
| 9 | Bottom Side Piece | 1 | A3003 | 600.00 x 68.00 x 1.80 |
| 10 | Inlet Tank | 1 | A3003 | 500.00 x 140.00 x 1.80 |
| 11 | Inlet Hose Connection | 1 | A3003 | 50.40 |
| 12 | Outlet Tank | 1 | A3003 | 500.00 x 140.00 x 1.80 |
| 13 | Outlet Hose Connection | 1 | A3003 | 50.40 |
| 14 | Filler neck/Overflow Tub | 1 | A3003 | 25.40 |
| 15 | Drain Fitting | 1 | A3003 | 25.40 |
| 16 | Heater Return Line Connection | 1 | A3003 | 25.40 |
| 17 | Coolant Level Indicator Fitting | 1 | A3003 | 25.40 |

Volume: 25 Liters Weight: 5 kg



The radiator manufactured cost is projected to be \$56, with an overall OEM cost for the thermal management system of \$220 assuming a 15% markup.



| Thermal Management System Cost (\$) | | | | | |
|-------------------------------------|--------------|-----------------------|--|--|--|
| Component | Factory Cost | OEM Cost ¹ | | | |
| Radiator | 56 | 65 | | | |
| Radiator Fan | - | 35 | | | |
| Coolant Pump | - | 120 | | | |
| Total | - | 220 | | | |

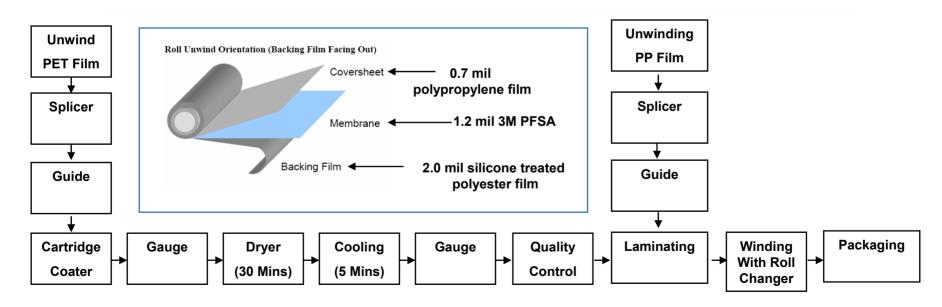
¹ Assumes 15% markup to the automotive OEM

The radiator fan and coolant pump are assumed to be purchased components, hence their price includes a markup.



We estimated the membrane manufacturing cost assuming a coaterlaminator line, with line rate of 20 ft/min.

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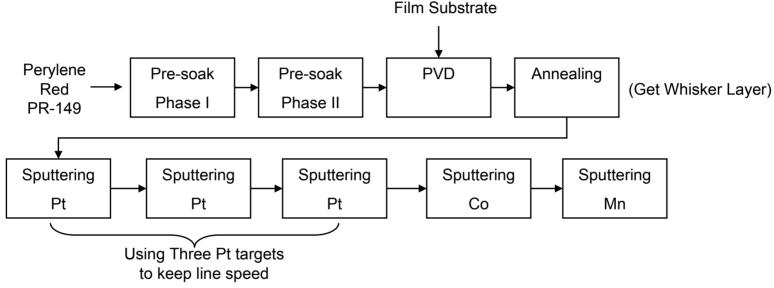
We assumed the use of a "cast dispersion" process to prepare the membrane.

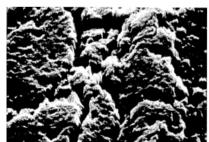
- The coating solution is a dispersion of 40 wt.% 3M PFSA in 30% water and 30% isopropanol
- The roll coating process deposits a 3 mil wet film thickness to produce a 1.2 mil dry film thickness
- The coating is applied to 2.0 mil silicone-treated PET (6 ft wide) backing film
- The preferred coating arrangement is "knife over roll"
 - An alternative coating arrangement is "reverse roll coating"
- The drying process is a "two-stage oven"
 - ➤ First Stage dry for 30 minutes at 50°C
 - > Full dry for 15 min. at 110°C
 - Forced air cooling for 5 minutes at 20°C
 - Catalytic combustor used to burn solvent
- The membrane is laminated with a 0.7 mil polypropylene coversheet
- A "Class 10,000" clean room environment was assumed in this estimate

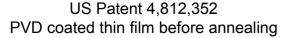


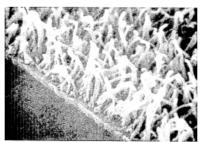
Organic whisker layer was fabricated by physical vapor deposition (PVD) with vacuum annealing process. Catalysts were coated to this layer via sputtering process¹.

Aluminum Coated









US Patent 4,812,352 PVD coated thin film after annealing

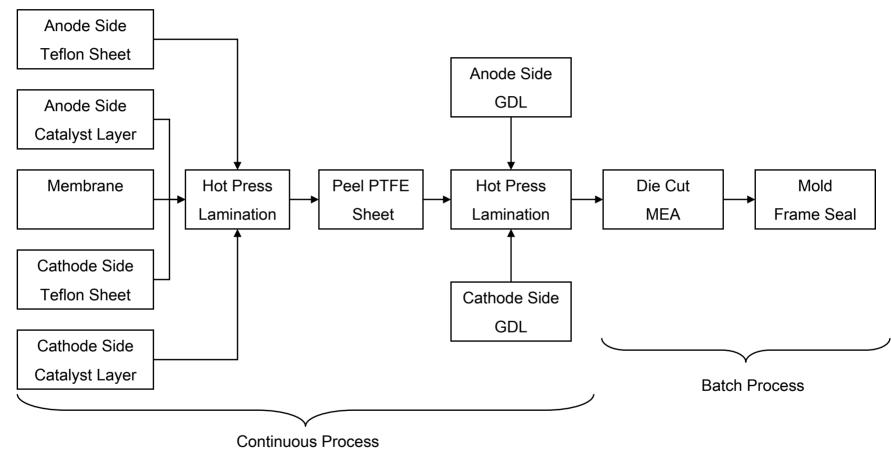
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¹M. K. Debe, Nano-Structured Thin Film Catalysts (NSTFC) for Next Generation PEM Fuel Cells, Northern Nano Workshop, November 2006



Backup Slides MEA Assembly

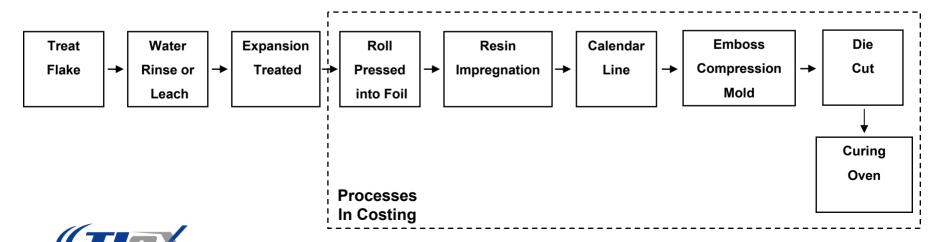
The anode and cathode organic whisker layers were hot pressed to the membrane with Teflon backing sheets.



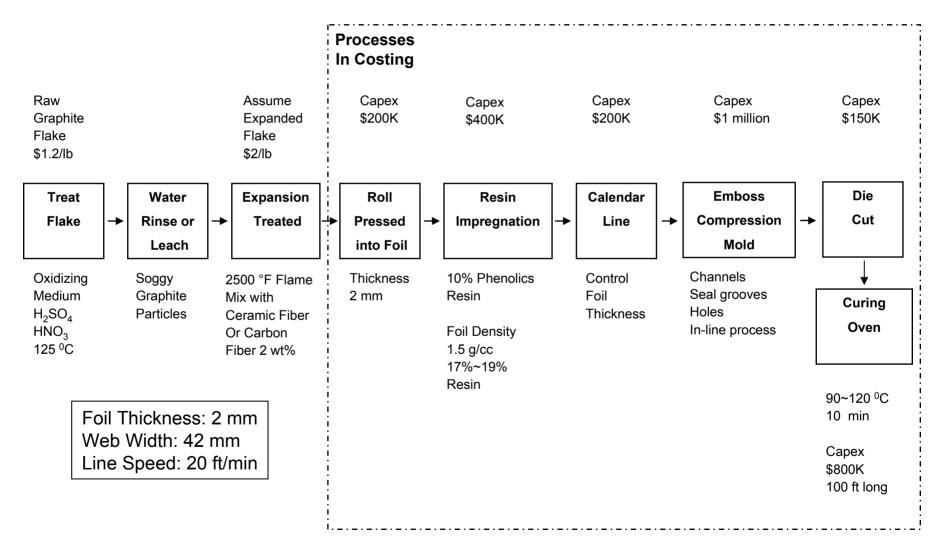
The catalyst coated membrane and GDL layers were laminated to form an MEA in roll good form; the MEA was cut into sheets and molded with a frame seal.

Our process flow for the expanded graphite bipolar plate is based on a GrafTech® process chart and related patents.

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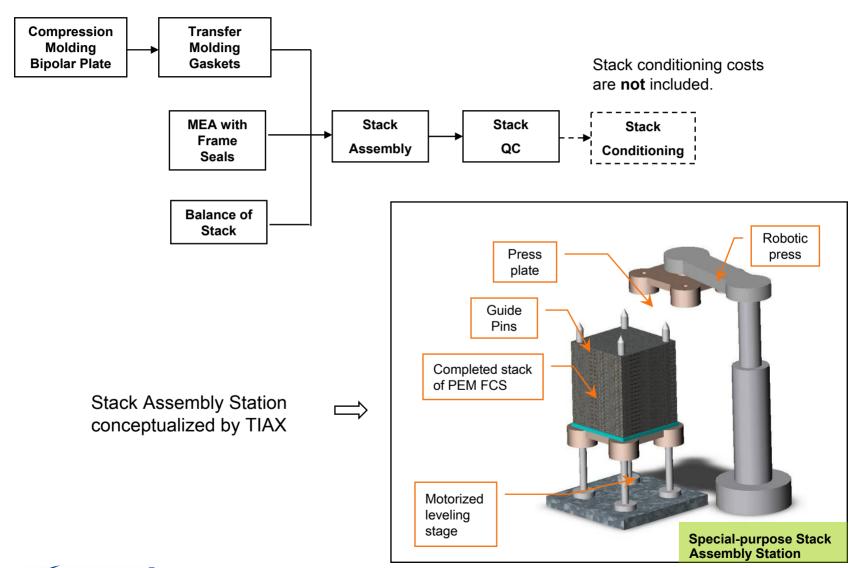
Our process flow for the expanded graphite bipolar plate is based on a GrafTech® process chart and related patents.





Backup Slides Stack Assembly Process Flow

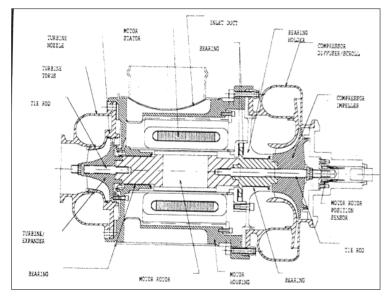
Top-level process flow diagram for the stack assembly.



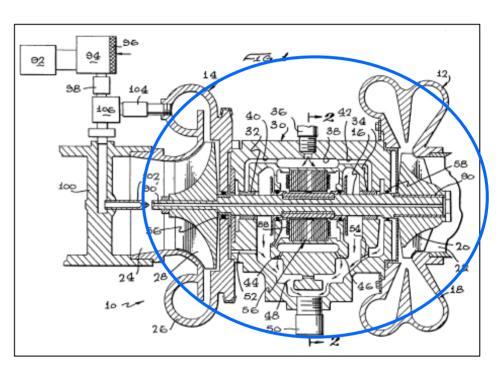


Backup Slides CEM Patents

The overall compressor/expander design is referenced from Honeywell DOE project presentations¹ and US patent 5,605,045.



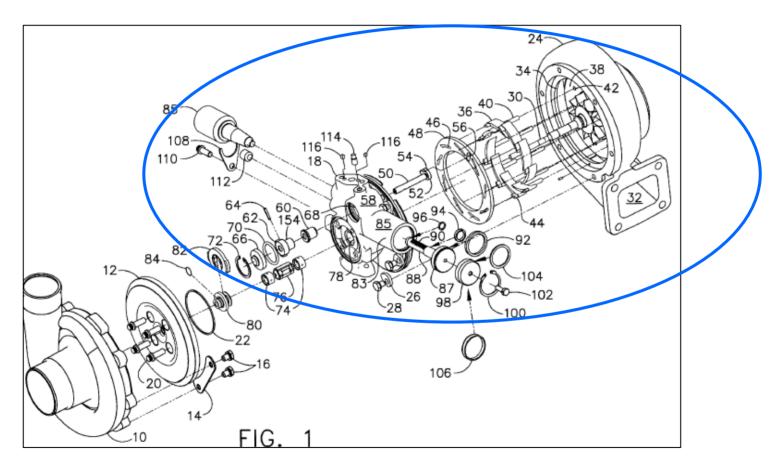
¹ Mark Gee, "Turbocompressor for PEM Fuel Cells," Progress Report, DOE Hydrogen, Fuel Cells, and Infrastructure Technologies Program, 2000.



The major sub-assemblies (e.g., variable nozzle vanes, motor, air bearing) are referenced from US patents, other public materials, and TIAX experience.



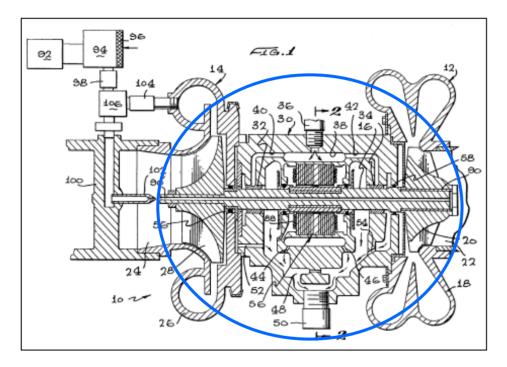
The turbine variable nozzle vanes and control assembly are referenced from US patent 6,269,642.

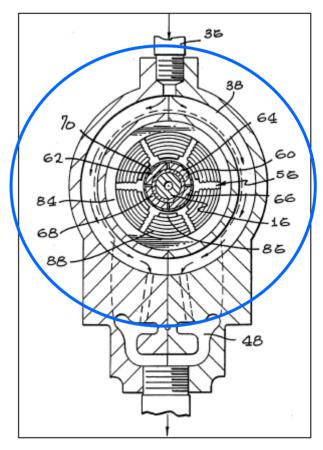




Backup Slides CEM Patents

The CEM motor stator and rotor assembly are referenced from US patent 5,605,045.

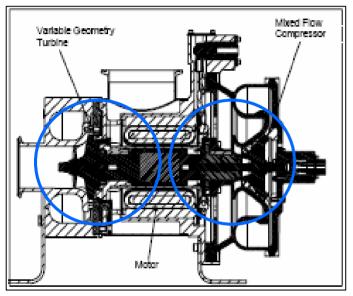




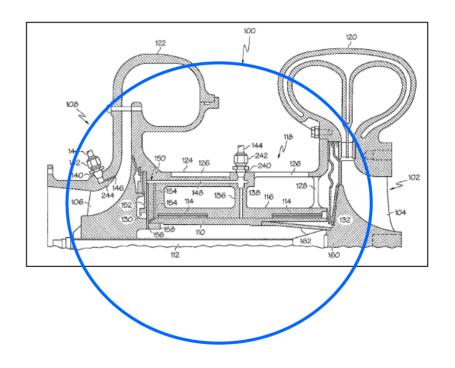


Backup Slides CEM Patents

The journal air bearing assemblies are referenced from Honeywell DOE project presentations¹ and US patent 2006/0153704.



¹ Mark Gee, "Turbocompressor for PEM Fuel Cells," Progress Report, DOE Hydrogen, Fuel Cells, and Infrastructure Technologies Program, 2002.





The rotor and single vane structure in the Parker Hannifin Model 55 Univane H₂ blower are referenced from US patent 5,374,172.

