

Cost Effective 6.5% Silicon Steel Laminate for Electric Machines

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Project
ID: elt091

IOWA STATE
UNIVERSITY

UNIVERSITY OF
DELAWARE

 **United Technologies
Research Center**

Overview

Timeline

- Start: October 1, 2016
- Finish: September 30, 2019
- Percent complete: 80%

Budget

- Total project funding
 - \$3,835K (Federal)
 - \$433K (Cost share)
- Funding for FY 2017: \$1,489K
- Funding for FY 2018: \$1,428K
- Funding for FY 2019: \$1,351K

Barriers and targets

- Magnet cost and rare-earth element price volatility
- Non-rare-earth electric motor performance
- 2020 DOE EDT cost target of \$4.7/kW and power density target of 5.7 kW/L.

Partners

- Iowa State University (Lead)
- Ames Laboratory
- United Tech. Research Center
- University of Delaware

Relevance

- MnBi based non-rare earth magnet:
 - Objective: Scale up and enable MnBi magnet for motor application
 - Impact: The price of MnBi bulk magnet is estimated at \$26/kg (NdFeB-Dy Grade N42HS, was \$69/kg in March 2016).
- Electrical steel with 6.5%Si:
 - Objective: Solve the brittleness problem and enable 6.5%Si steel for motor application
 - Impact: Reduces iron loss at higher frequency, improve motor power density and efficiency
- Non-rare earth motor
 - Objective: Demonstrate motor with MnBi as permanent magnet and 6.5%Si steel as the soft magnetics
 - Impact: Improve non-rare earth motor power density

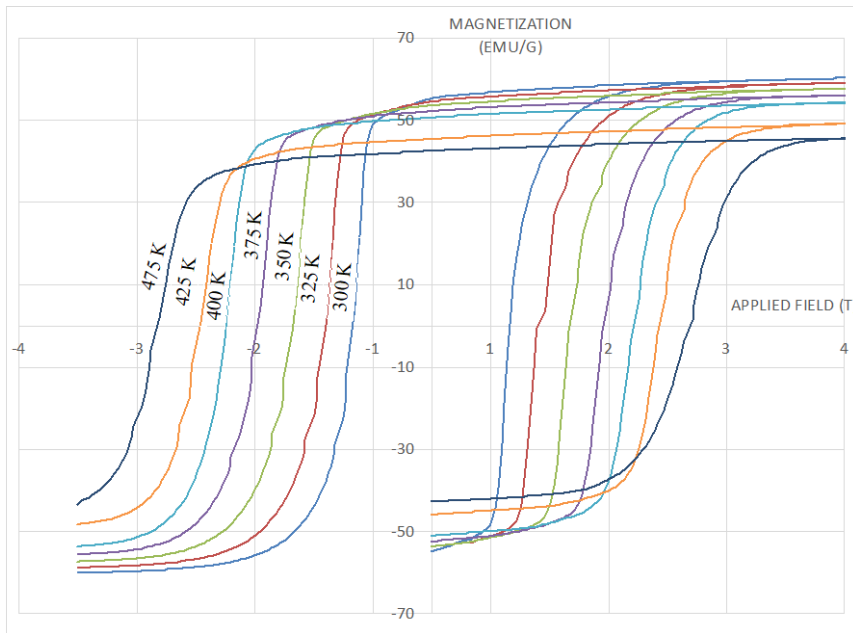
Milestones

[illegible]

Challenges (MnBi)

Advantages of MnBi

- Large coercivity that is increasing with temperature.
- Theoretical energy product $(BH)_{\max}$ 20 MGOe



Experimental M-H-T data showing increasing coercivity with increasing temperature

Challenges of MnBi

- Mn precipitation is inevitable, difficult to maintain high purity and high magnetization, which is limited at ~ 90 kG, any impurity will reduce the energy product
- At 340°C LTP-MnBi decomposes to HTP-Mn_{1.08}Bi and liquid Bi, making it difficult to fabricate bulk magnet using the conventional sintering or warm compaction method
- Need to magnetically separate each grain in order to maintain magnetic coercivity

Approach (MnBi)

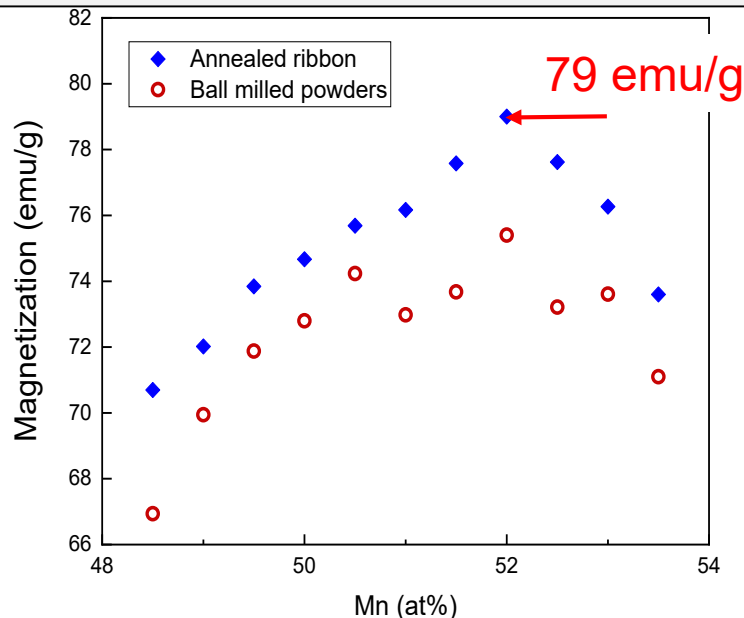
- Refine existing powder synthesis and magnet fabrication process, eliminate MnO formation
- Consistently produce bulk magnet with 8 MGOe
- Use amorphous feedstock to reduce Mn precipitation and improve energy product from 8.5 to 10 MGOe

	End results and annual go/no-goes
Yr 1	1. Produced 8 MGOe MnBi magnet (5 gram) 2. Produced 5 gram MnBi with 90% amorphous
Yr 2	1. Fabricated one 100 gram/pcs 8 MGOe MnBi magnet 2. Fabricate one small 10 MGOe MnBi (>2 gram)
Yr 3	1. Deliver 300 pieces of 8 MGOe MnBi magnet (10 gram each) machined to the desired dimension and coated

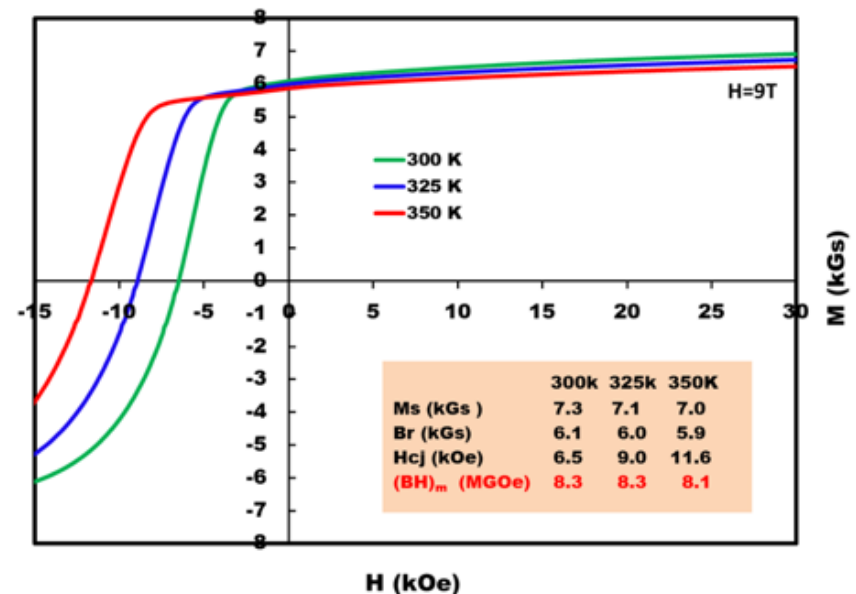
Table of year end results and go/no-goes

Technical Accomplishments (MnBi)

- Achieved a new record of saturation magnetization of 79 emu/g (theoretical limit is 82 emu/g)
- Milestone 8.5 MGOe is closely met (8.3 MGOe demonstrated)
- Cost-effective Cold-Iso-Press (CIP)-sintering process was developed
- The CIP bulk magnet exhibited excellent temperature stability: $(BH)_{\max}$ drops 2% at 350K (15% for NdFeB)



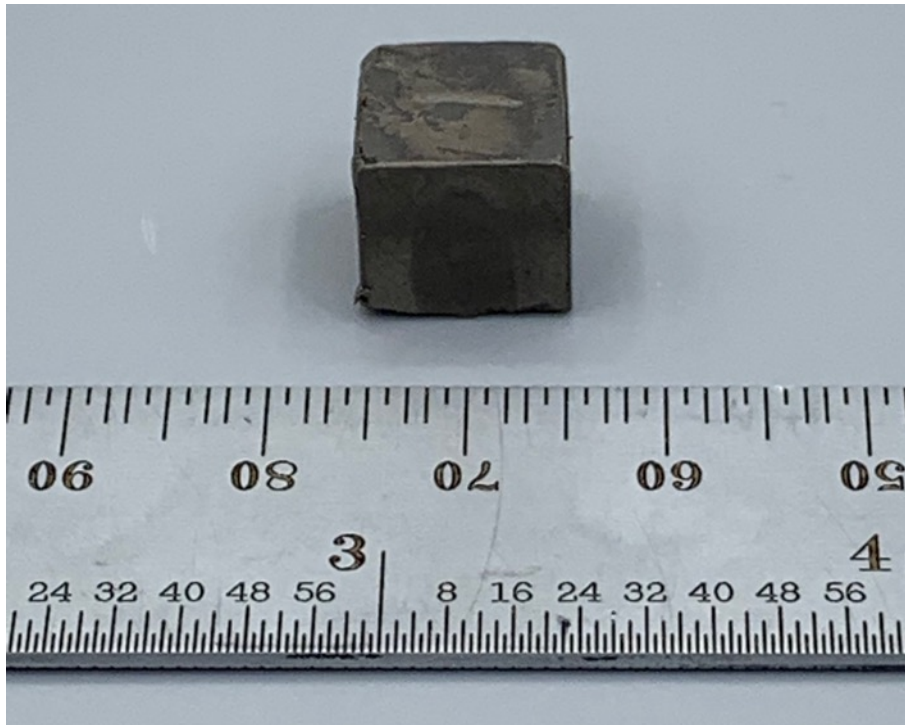
Measured magnetization of alloys with different amount of manganese



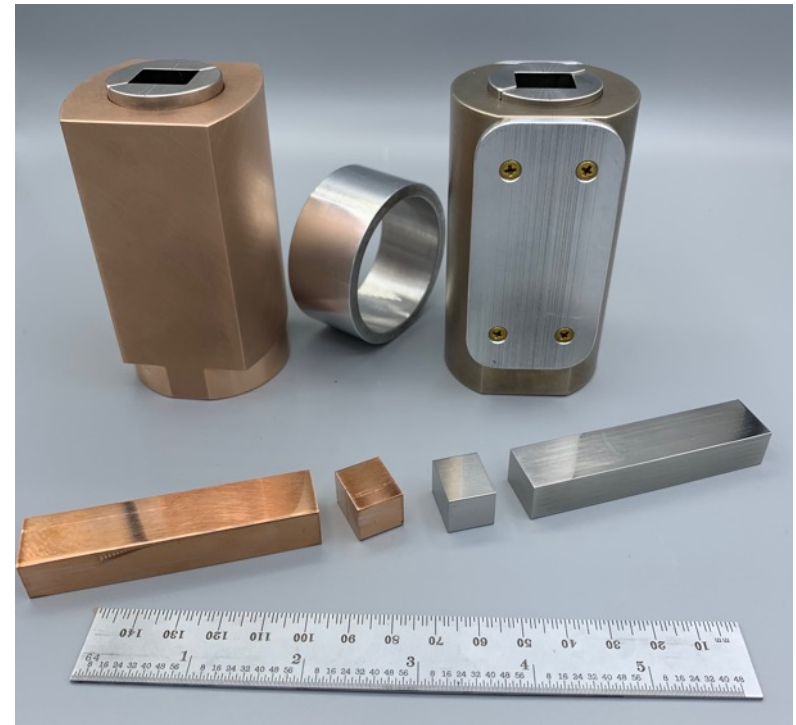
M-H curves of the MnBi bulk magnet at 300, 325 and 350 K

Technical Accomplishments (MnBi)

- Processes and facility for producing 300 magnets are setup.



Picture of a bulk MnBi magnet. It is the first of the 300 bulk MnBi magnets needed by the prototype motor



Picture of fabrication die set used to fabricate bulk magnet

Challenge (6.5% Si Steel)

Table of physical properties of various soft magnetic materials

Advantages
of 6.5% Si
Steel

Type	Materials	B _s (T)	H _c (A/m)	10 ³ μ _r 1 kHz	R (μΩ-cm)	λ (ppm)	W _{5/50} (V/kg)	W _{10/400} (V/kg)	Ref
Crystalline	Electrical Steel, 0.2mm N30 3.2% Si	2	26	15	57	8	0.7-1.2	11	[1,5]
	Electrical Steel, 0.2mm N30 6.5% Si	1.6	45	19	82	0.01	0.6	8.1	[1,2]
	Molypermalloy, 0.5mm N78Fe17Mo5	0.65- 0.82	0.25- 0.64	100- 800	60	2-3	0.07	0.3	[3,4]
	Hiperco 50, Fe49Co49V2	2.4	16-400	5-50	27	60	4	10	[4]
Nano-crystalline	FINEMET, Fe _{73.5} Si _{13.5} Nb ₃ B ₆ Co ₁	1.2	0.5-1.4	80	110	0-2	—	1.1	[4-6]
	NANOFERM, Fe ₈₈ B ₄ Zr ₇ Co ₁	1.5-1.6	2.4-4.5	48	56	~0	—	3	[4-6]
	HITFERM, (FeCo) ₄₄ Zr ₇ B ₄ Co ₁	1.6-2.0	80-200	1-10	120	36	—	20	[4-6]
Amorphous	Metglas, Fe78Si9B13	1.54	3	2.1	135	27	0.7	2-5	[7]
	Metglas 2650CO, Fe ₆₇ Co ₁₈ B ₁₄ Si ₁	1.8	3.5	50	123	35	0.3	3	[4,8]
Ferrite	Ferrite, MnZnFeO	0.36- 0.5	10-100	0.5-10	10 ⁷ -10 ⁸	5	—	—	[4]
	Ferrite, NiZnFeO	0.25- 0.42	14- 1600	0.01-1	10 ¹¹	-20	—	—	[4]

Challenges
of 6.5% Si
Steel

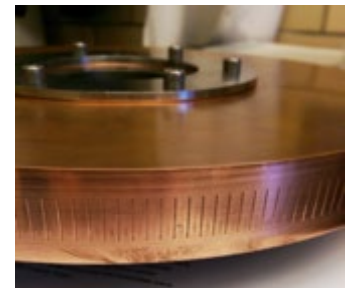
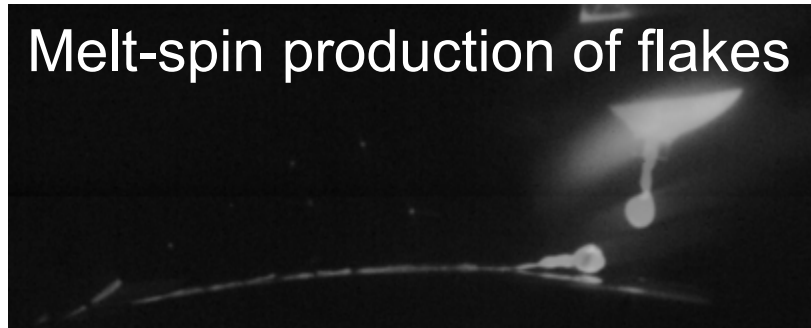
Too brittle to be manufactured using the cost effective cast/hot-roll/cold-roll process

Approach (6.5%Si Steel)

- Use rapid solidification to suppress the deleterious ordering phase and produce ductile thin flakes.
- Dip-coat flakes with thin CaF_2 layer for insulation.
- Consolidate ductile flakes into near-net-shape part with laminated internal structure.

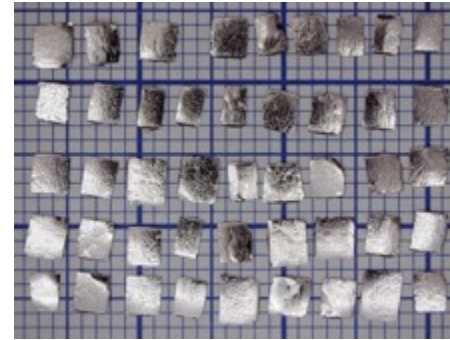
	End results and annual go/no-goes
Yr 1	1. Delivered 10 gram of ductile Fe-6.5%Si flakes (30 mm thick, 1x1 mm ² , 180° bending no crack)
Yr 2	1. Delivered Fe-6.5%Si rings with 0.1, 0.4, 1, and 4 mm thickness (OD: 1.5", ID: 1.25", 98% dense, various levels of oxidization) 2. Validated power loss $W_{10/400} < 6$ W/kg for the ring with 0.4 mm thickness.
Yr 3	1. Deliver 8" OD stator laminate with $W_{10/400} < 6$ W/kg 2. Project manufacturing cost for small scale mass production

Technical Accomplishments (6.5%Si Steel)

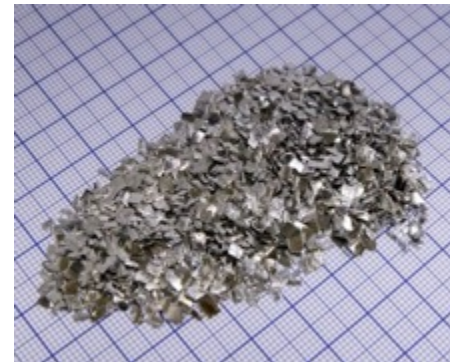


Grooved wheel
breaking continuous
ribbon to flakes

- Developed the process for producing flakes ($2 \times 2 \times 0.1 \text{ mm}^3$)
- Approximately 75% yield of the flakes with the desired size
- System capable of 500 gram per batch was installed



2017 (1st year)
Flakes with
desired size
produced in 5
gram quantity



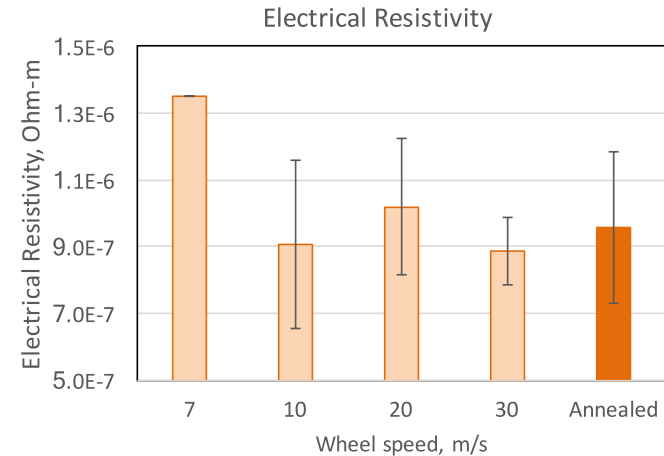
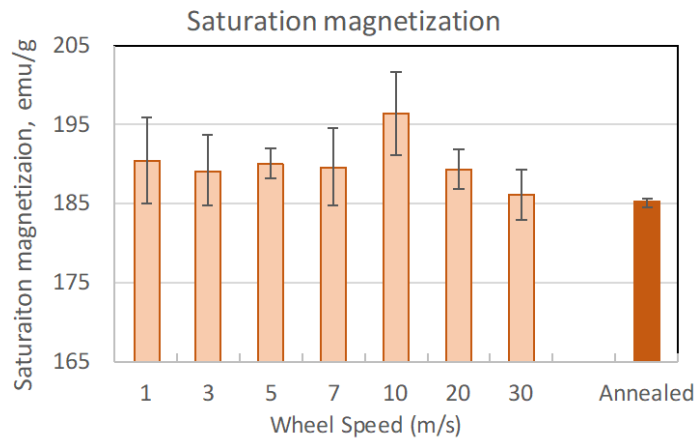
2018 (2rd year)
Flakes with
desired size
produced in 150
gram quantity



2019 (3rd year)
Flakes coating
process was
developed

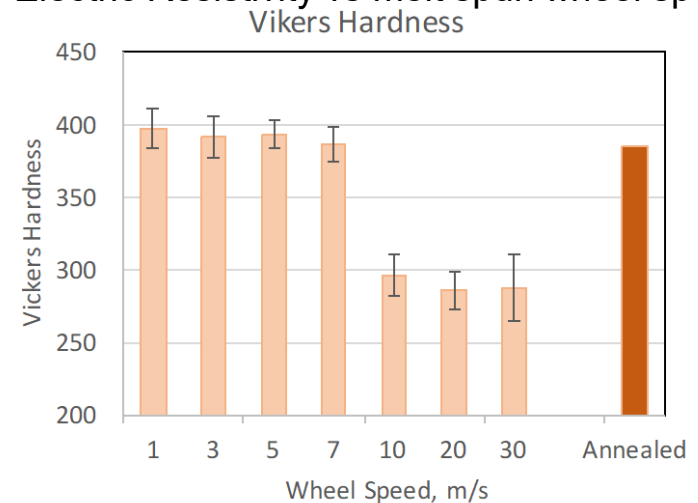
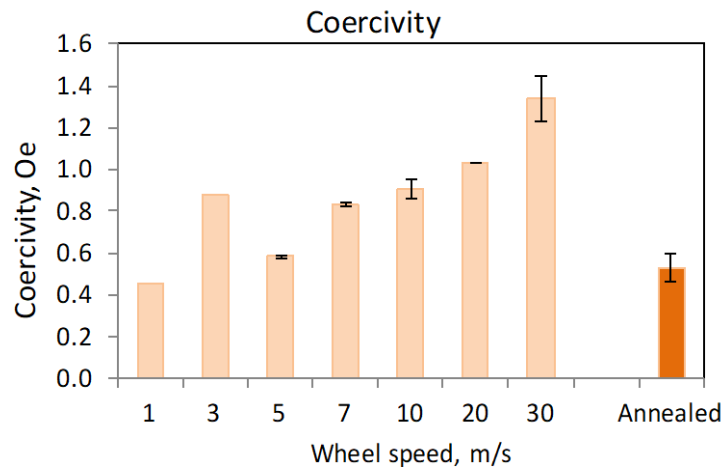
Technical Accomplishments (6.5%Si Steel)

Relationship between wheel speed and physical properties established



Saturation magnetization vs melt spun wheel speed

Electric Resistivity vs melt spun wheel speed



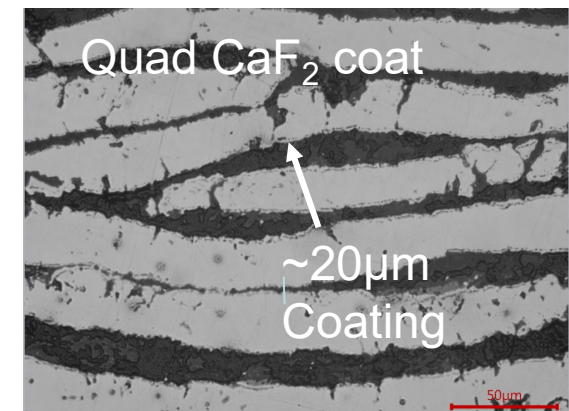
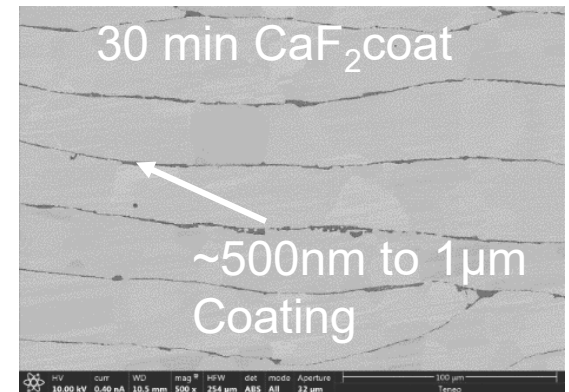
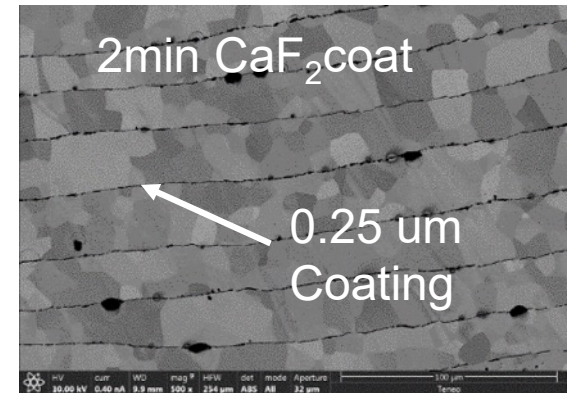
Coercivity vs melt spun wheel speed

Hardness vs melt spun wheel speed

Technical Accomplishments (6.5%Si Steel)

- Coating thicknesses (0.25-20 μm) has been investigated.
- Mg_2SiO_4 effectively increased the resistivity up to 800 times.

Coating	Density g/cc	Densification	Resistivity $\mu\Omega\text{-cm}$
None	7.48	100%	81.36; 84.29
CaF_2 , 2min	7.35	98.3%	108.2, 93.5
CaF_2 , 30min	7.32	97.8%	139.1; 115.4
CaF_2 , 2h	6.85	91.6%	322.5; 294.5
CaF_2 , quad coat	5.99	80.1%	339.5; 228.8
10% MgO , 30s dip	6.86	91.7%	510.1; 259.2
50% MgO , 30s dip	4.70	62.8%	66k; 22k
50% MgO anneal	6.34	84.8%	1111.5; 688.9

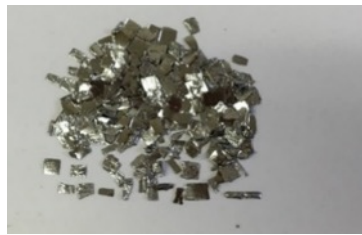


Figures on the right show consolidated Fe-Si flakes coated with different amount of CaF_2

Technical Accomplishments (6.5%Si Steel)

Coreloss performance met/exceeded the expectation

- 0.2mm sample achieved record low iron loss at 400 and 1000Hz.
- 0.1mm sample has W10/400 of 6.1W/kg



Melt-spun flakes

Hot press
→



Consolidated flakes

→ 1100°C x 2h
annealing
+ Slice →



A ring sliced from the consolidated flakes

		Ameslab GO2P23	NO Si steel	Ameslab GO2P23	JNHF	Ameslab GO2P23	JNEX
		Fe-6.5Si	Fe-3.2Si	Fe-6.5Si	Gradient Fe-6.5Si	Fe-6.5Si	Fe-6.5Si
thickness	(mm)	0.33	0.35	0.2	0.2	0.1	0.1
W10/400	(W/kg)	10.8	14.4	7.2	14.5	6.1	5.7
W10/1k	(W/kg)	45.7	62.0	27.3	29.1	20.2	18.7
DC, μ Max		28.7k	18.0k	28.4k	3.9K	25.8k	23.0k

UTRC Project Deliverables

Task 1: Preliminary Design:

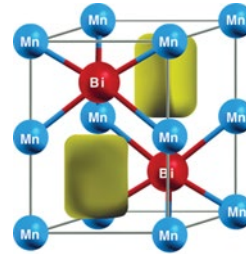
– End of Sept 2017 - **Completed**

Task 2: Detailed Design & Motor Build:

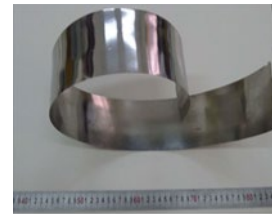
– End of Sept 2018 – **Design Completed** –
Motor Build Delayed. In-progress

Task 3: Experimental Validation, Re-build & Re-test:

– End of Sept 2019 – **Delayed start due to delay in materials**



Non Rare Earth Magnets
Manganese Bismuth (8-10 MGOe)



Low Loss Density Steel
6.5% Si Steel with improved ductility

High Frequency
Motor



Electric machine at
low cost & improved
performance (power
density & efficiency)

		Year-1				Year-2				Year-3			
Task Description		Q1	Q2	Q3	Q4	Q1	Q2	Q3	Q4	Q1	Q2	Q3	Q4
Task 1	Preliminary Design												
Task 2	Detailed Design and Motor Build												
Task 3	Experimental Validation, rebuild & retest												
Task 4	Project Management												

Today

Performance Metrics & Materials Considered

Machine Performance Specifications for 10 kW Peak, 6 kW Rated Power

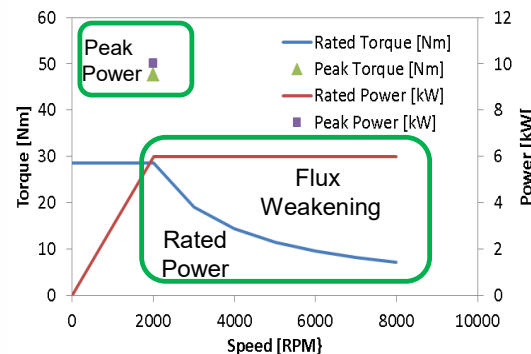
Performance Metric Targets

Cost	Specific Power	Power Density
≤\$4.7/kW	≥1.3 kW/kg	≥5.7 kW/Liter

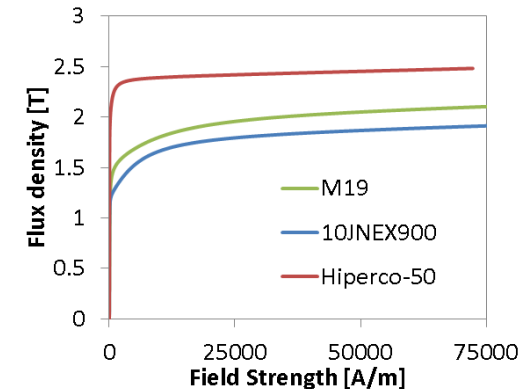
Target Motor Specifications

Specifications	Units	Values
Peak Power	kW	10
Continuous Power	kW	6
Max Speed	RPM	8000
Min Frequency	Hz	300
Voltage	V	325
Max per Phase Current	A rms	35
Characteristics Current	A rms	< 35
Weight	kg	7.69
Volume	l	2.2
Unit Material Cost	\$	47
Max Efficiency @ 1/2 Speed & 1/2 Torque	%	95%
Based Speed	RPM	2000
Peak Torque @ Rated Speed	Nm	47.75
Rated Torque @ Rated Speed	Nm	28.65
Max Speed	RPM	8000
Torque @ Max Speed	Nm	7.16

Torque/Power vs. Speed



Soft Magnetic Properties



Hard Magnet Properties

Material	Remnant Flux Density [T]	Coercive Force [kA/m]	Energy Product [MGOe]	Cost [\$ /kg]
NdFeB48	1.39	1060	46.2	80
MnBi	0.6	405.8	8.4	10
Ferrite	0.45	33.5	4.9	5

Modeling App

Suitable modeling method

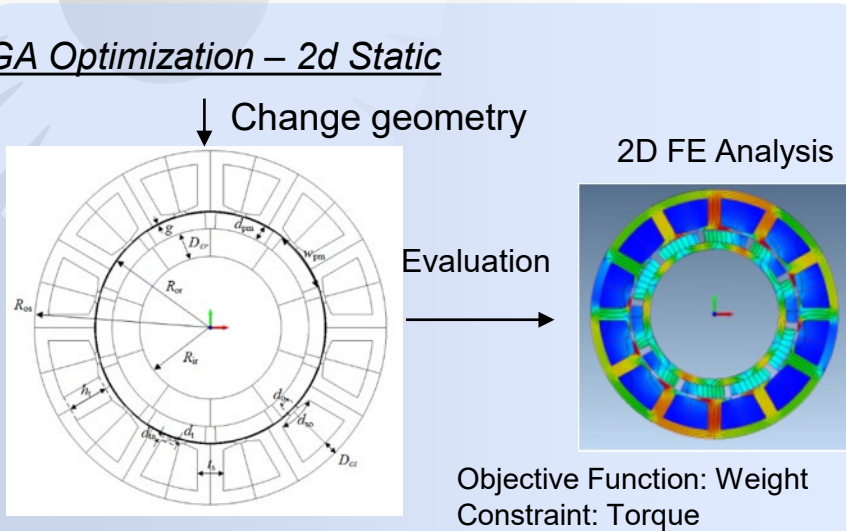
GA Optimization – 2d State

Suitable modeling methods to capture physics appropriately

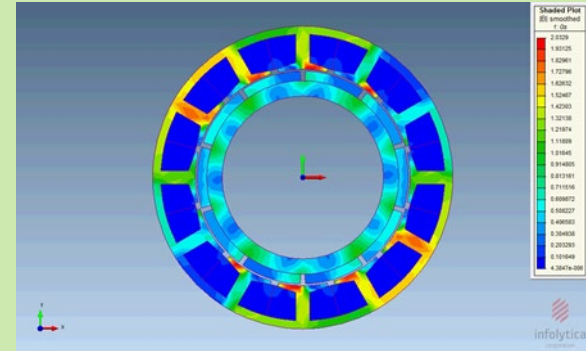
GA Optimization – 2d Static

Core Losses - Transient

GA Optimization – 2d Static



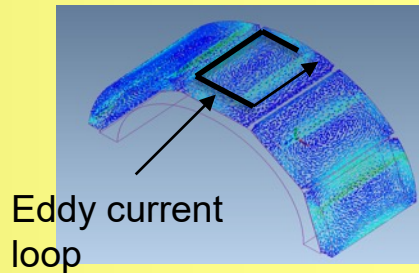
Core Losses - Transient 2D w Motion



Steinmetz's equations: $P = K_b f^\alpha B^\beta + K_e (fB)^2$

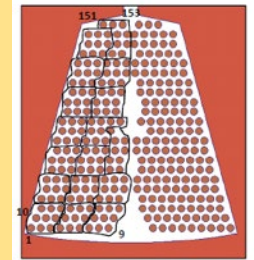
Magnet Losses - 3D Transient w Motion

Capture the Eddy current loops in the magnet



Analytical Formulation – AC Winding Losses

Compute skin depth and then use the wave equations to capture the AC copper losses in the conductors

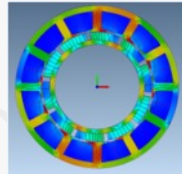
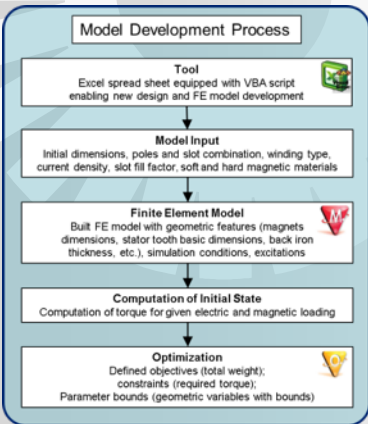


Stator slot view

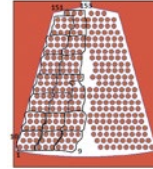
$$R_{ac} = \frac{d}{h} \left[\frac{\sinh(\frac{2d}{h}) + \sin(\frac{2d}{h})}{\cosh(\frac{2d}{h}) - \cos(\frac{2d}{h})} \right] R_{dc}[1]$$

Modeling Approach: Multi-Physics

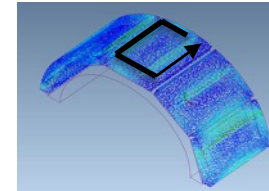
Multi-physics modeling to address some of the key risks identified



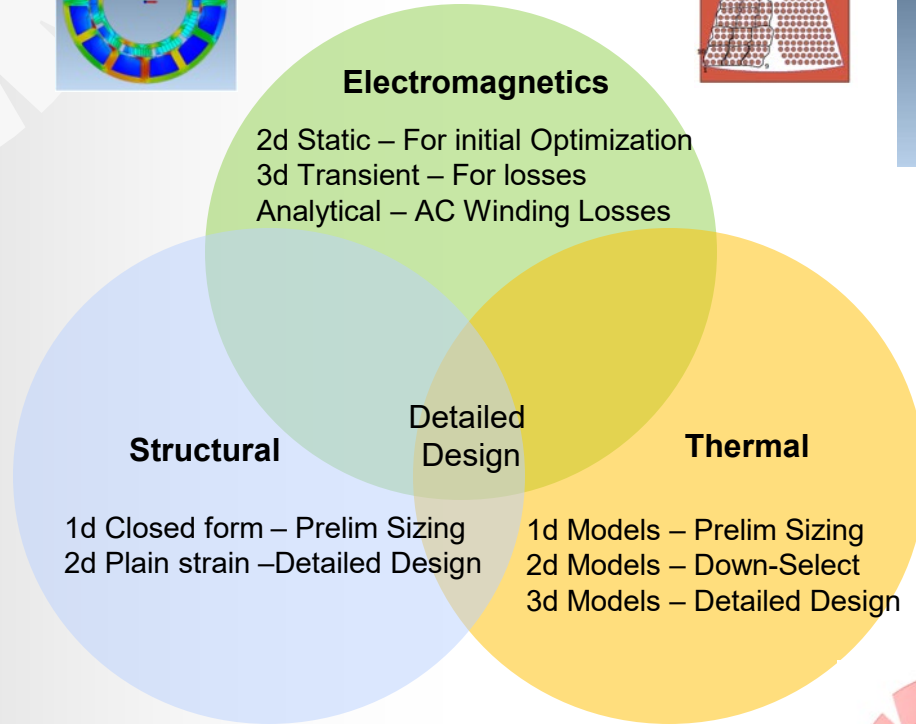
2D FE Analysis



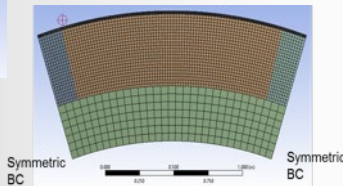
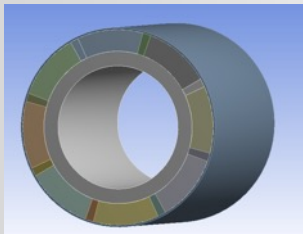
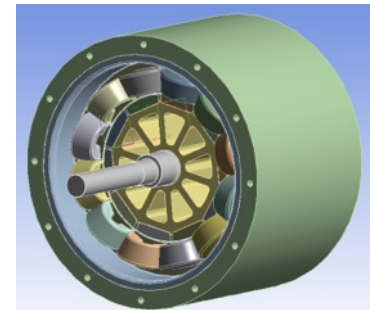
Stator slot view



Capture the Eddy current loops in the magnet



3d Model with End Winding



2d Model cross section

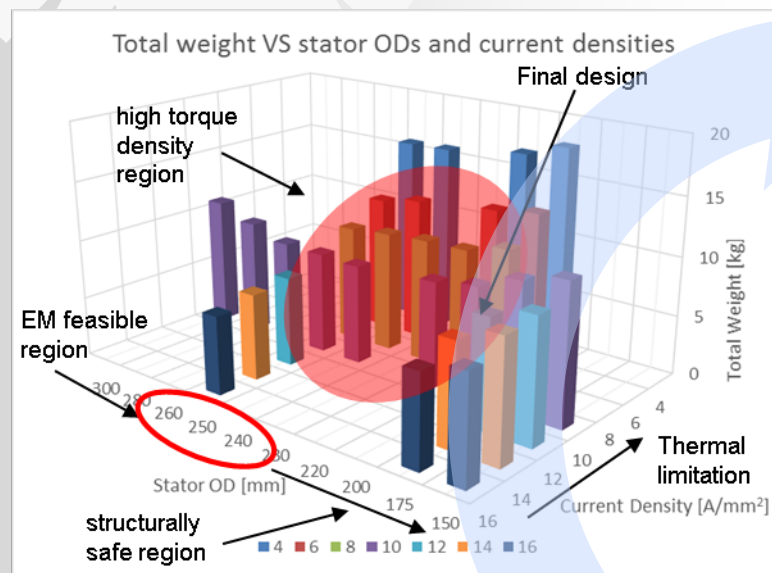


End fan

Design Iteration & Down Select

Design down select with multi-physics modeling and constraints

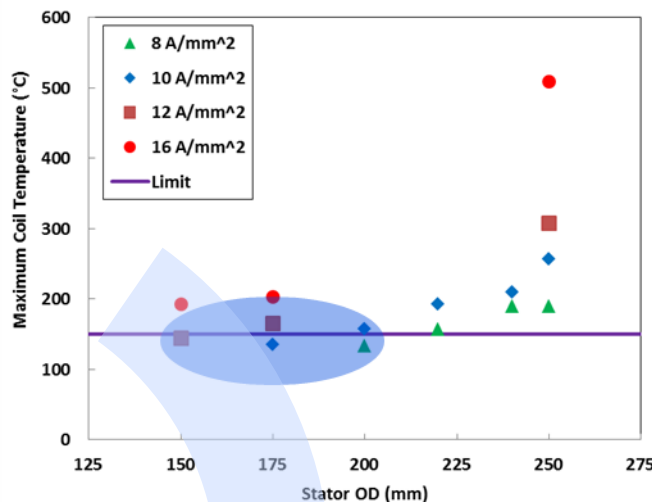
Electromagnetics



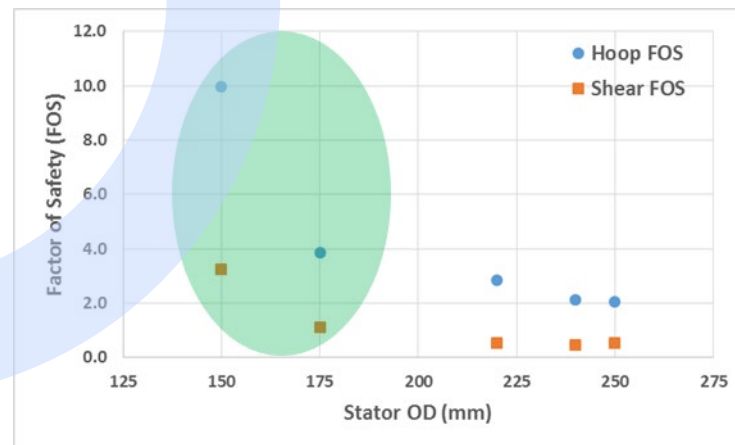
Down Selected Designs

Stator OD	Rotor OD	Stack length	Total weight	Current density	Max Temperature	FOS Hoop	FOS Shear
[mm]	[mm]	[mm]	[kg]	[A/mm ²]	[°C]		
150	96	126.4	10.32	12	145	3.29	1.19
175	101.5	89.3	11.24	10	135	9.93	2.04
175	122.5	83.4	9.2	12	148	4.5	1.3
200	128	59.8	9.44	10	158	3.51	0.99

Thermal: max coil temp vs stator OD



Structural: safety factor vs stator OD



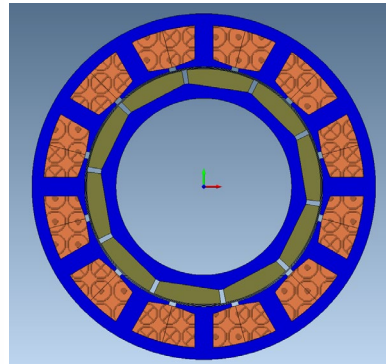
Design Parameters

Final prototype design key parameters

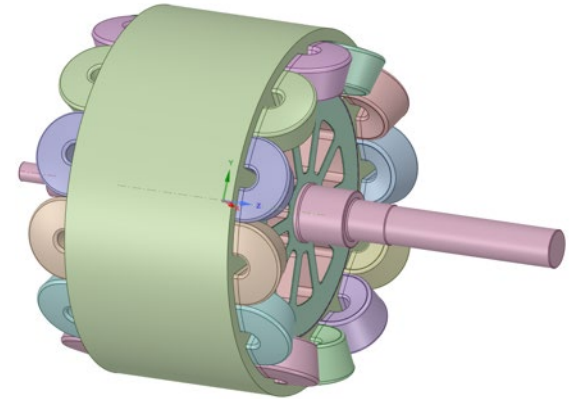
Key Dimensions

Number of slots	12
Number of poles	10
Number of phases	3
Slot per pole per phase	2/5
Stator outer diameter [mm]	180
Magnet thickness [mm]	7.0
Rotor OD [mm]	108.5
Air gap [mm]	1.135
Turns per coil	26
Turns per phase in series	104
Copper mass [kg]	3.4
Lamination mass [kg]	4.9
Magnet mass [kg]	1.8
Total mass [kg]	10.1
Power density [kW/kg]	0.99

2d Cross Section



3d Model with End Winding



Design Parameters

Parameter	Units	Values	
D-Axis Inductance	mH	2.15 Unsaturated	2.11 Saturated
Q-Axis Inductance	mH	2.29 Saturated	1.55 Saturated
Resistance:	Ohms	0.114	
Back EMF Constant	Vrms/kRPM	43.92	
Torque Constant	Nm/Arms	1.2	

Conclusions & Next Steps

Teams Recommendation: Go with First Motor Prototype Build

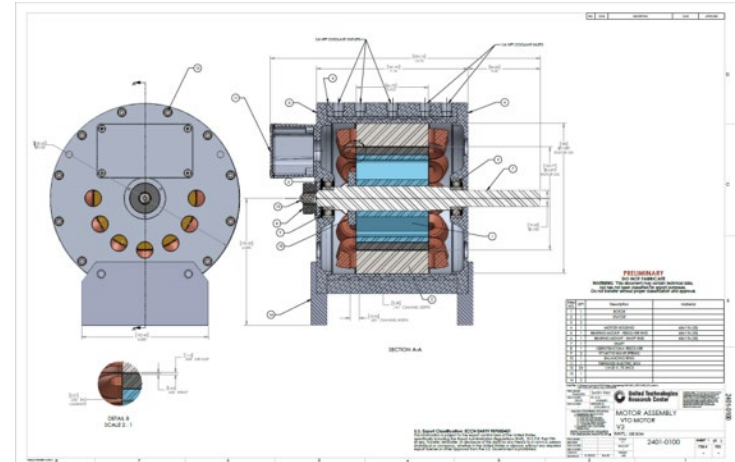
Phase-II

- Detailed Design – Due End of Sept 2018
- Tasks completed till date
 - Completed design down-select and detailed design
 - Motor build in progress. Delayed by 6 months due to material arrival from Japan and custom magnets to match with MnBi properties
 - Current status: Final stage of assembly and testing in progress

Next Steps – Phase-III – Delayed start due to Materials

- Experimental validation
- Refine design for MnBi and ISU steel
- Build second prototype and experimental validation

Prototype Drawings



Rotor & Stator Laminations



Stator with Winding



Rotor with Magnets

Responses to Previous Year Reviewers' Comments

Q1-Reviewer 2

It was not clear to the reviewer that MnBi magnets can provide a realistic path to replace RE NdFeB magnets while achieving the required performance metrics. Even though the PI mentioned that one of the key enablers is to go to high frequency/speed, the 400 Hertz (Hz) targeted frequency is fairly low compared to current traction motors.

The 6.5% silicon steel can lead to higher efficiency, but it was not clear to the reviewer how this can enable non-RE designs. Also, this material can be used with RE designs as well. In general, the reviewer stated that the project seems to be pursuing two or three technical areas that do not seem to be tied together and it was not clear how they can end up providing a comprehensive solution for the RE challenge.

Q1-Review 3

Reviewer expected a description of specific challenges and potential roadblock as expected as key outputs.

Q1-Reviewer 4

The increase in relative permeability of 6.5% SiFe with respect to 3.2% SiFe alone does not seem enough to make up the gap in remanence for the MnBi to RE materials.

Responses to Previous Year Reviewers' Comments

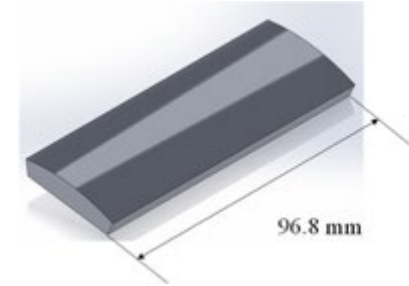
Reviewer comments	Reply
It was not clear MnBi magnets can provide a realistic path to replace NdFeB magnets while achieving the required performance. The 6.5%Si steel can lead to higher efficiency, but it was not clear how this can enable non-RE designs.	Non-RE motor will always have less power density than RE motor. MnBi will not replace RE magnet. But, it is possible for MnBi based motor to achieve 5.7 kW/L power density.
Progress made on addressing the brittleness of the 6.5% silicon steel is good but scalability needs to be proven.	Agree, mass production of thin sheet ductile 6.5%Si steel needs to be demonstrated
A disconnect between the team at Iowa State and UTRC, who are almost independently working on this project.	Separate objectives for each sub-team allow the project to proceed without inter-dependency. But at the end, only ISU team can deliver the MnBi bulk magnets for the final prototype
The research team re-visit the approach and confirm that the developed materials will really enable a feasible RE free design	Motor is designed to use a permanent magnet with 6 kG remanent magnetization and 6 kOe coercivity, a property unique to MnBi magnet

Collaboration and Coordination

Ames Laboratory	Melt-spin flakes production; Bulk magnet production
United Technology Research Center	Motor design and testing
University of Delaware	Amorphous MnBi flakes production
Electron Energy Corp.	Dummy magnet simulating the performance of MnBi magnet
JFE Steel Corp.	Commercial 6.5 Si% steel sheet (0.1 mm)
Leppert-Nutmeg Inc.	Motor construction

Remaining Challenges and Barriers

- MnBi:
 - Scale up
 - Increase energy product to 10 MGOe
- 6.5% Si steel:
 - Scale up
- Motor
 - Improve power density from 4.5 kW/L to 5.7 kW/L



Proposed Future Research

- MnBi

Milestone: 300 bulk MnBi magnet with 8 MGOe

 - Improve energy product to 10 MGOe
 - Quality control of mass production of bulk magnet (300+ magnets)
- 6.5% Si steel

Milestone: sectional stator fabrication

 - Optimize flake coating thickness and laminate architecture
 - Fabricate 8' OD stator with sectional approach
- Non-Re motor

Milestone: Construct 400 Hz non-Re PM motor.

 - Execute the motor design and coordinate with vendors

Any proposed future work is subject to change based on funding levels.

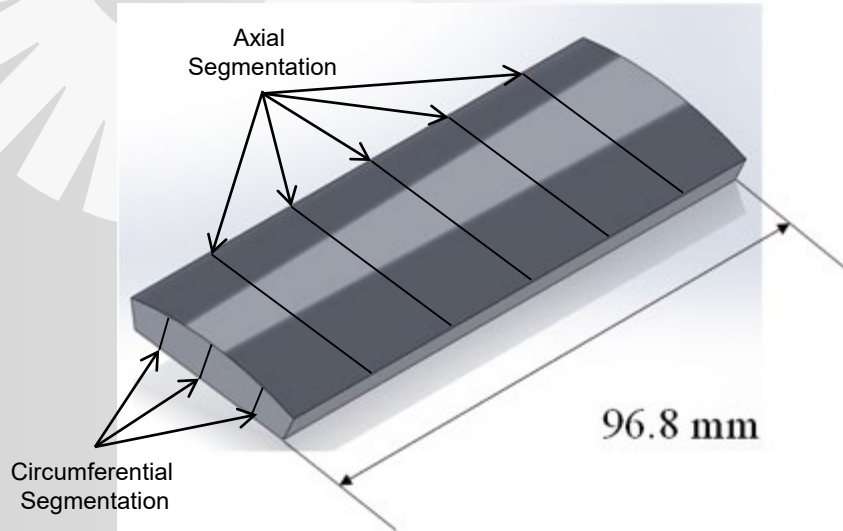
Summary

- MnBi
 - Powder quality was improved from 70 emu/g to 79 emu/g
 - Cost effective bulk magnet fabrication method was developed
 - Process of mass production bulk magnet has been initiated.
- 6.5% Si steel
 - Relationship between physical properties and cooling rate was established
 - Flake production method and capacity were established
 - Laminate inner structure was optimized and fabrication method was established
- Motor
 - 10 kW 400 Hz motor was designed.
 - Construction of the 1st prototype will be finished by May 2019

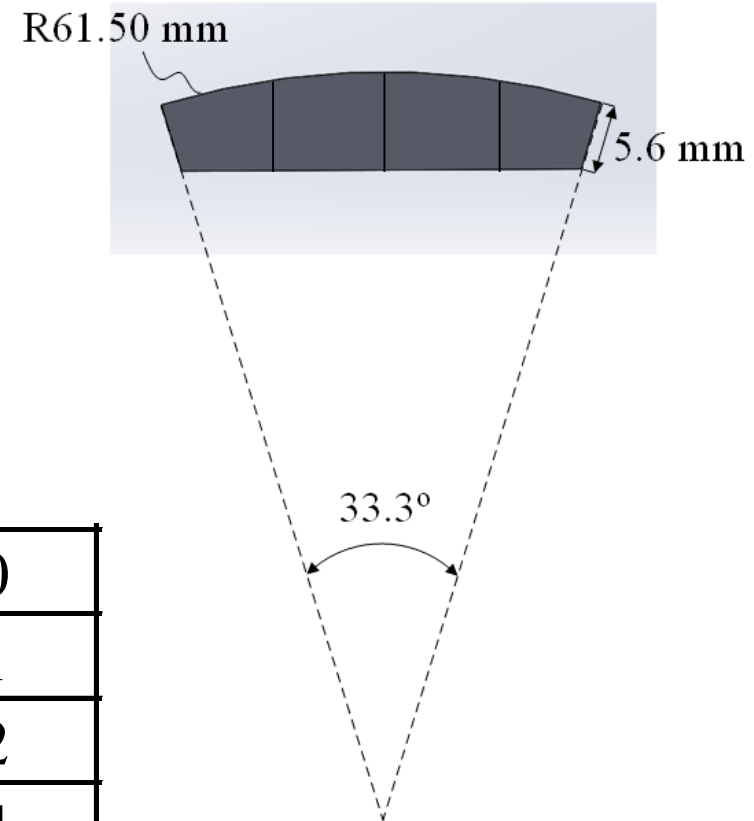
Technical Backup Slides

Magnets used in this project

Mn-Bi magnet geometry

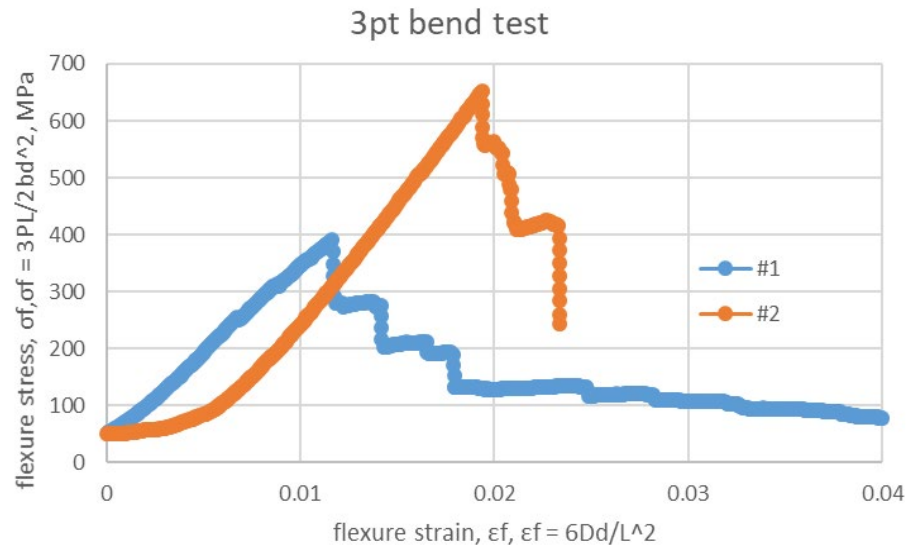


	Axial	Circumferential
Number of segments	4	5-10

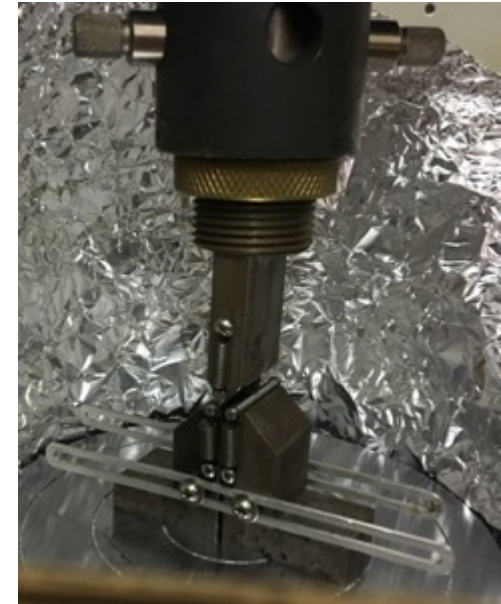
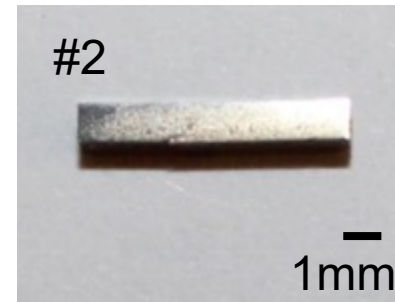
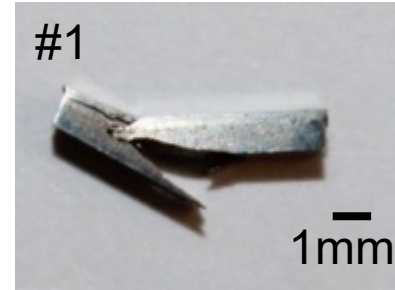


Br [kG]	6.0
Hc [kOe]	5.1
Hci [kOe]	6.2
Bhmax [MGoe]	8.4

Mechanical Properties



3pt bending test of flake-consolidated FeSi sample



Sample #1 has pre-existing crack

The mechanical properties of the CaF_2 coated is remarkable

- High bending strength (650MPa)
- CaF_2 interlayer bonding prevented the sample from catastrophic failure on breakage.